

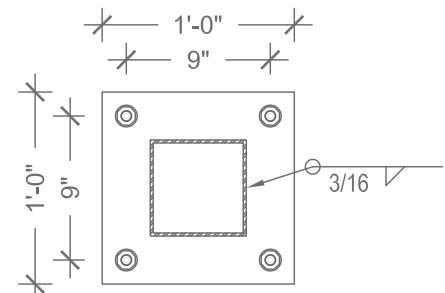
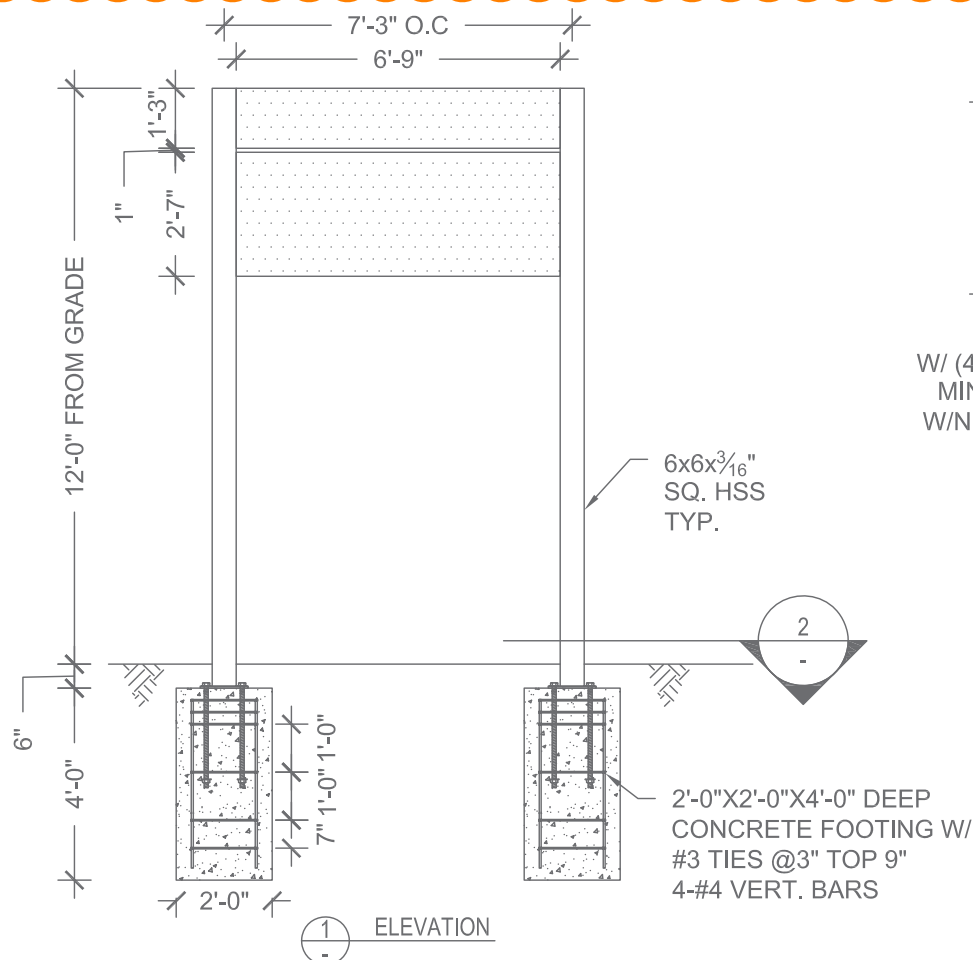


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PROJECT: FERRUCCI JHS, 3213 WILDWOOD PARK DR., PUYALLUP, WA  
PROJECT #: 38928-1  
CLIENT: EVERGREEN SIGN CO

DATE: 2/13/2023  
ENGINEER: TH  
LAST REVISED:

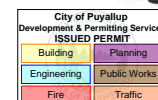
**THE APPROVED CONSTRUCTION PLANS AND ALL ENGINEERING DOCUMENTS MUST BE POSTED ON THE JOB AT ALL INSPECTIONS IN A VISIBLE AND READILY ACCESSIBLE LOCATION.**



2 BASE PLATE, TYP.

#### GENERAL NOTES

1. DESIGN CODE: IBC 2018 & WASHINGTON SBCC 2018
2. DESIGN LOADS: ASCE 7-16
3. WIND VELOCITY 100 MPH EXPOSURE C
4. CONCRETE 2500 PSI MINIMUM
5. SQ. HSS STEEL ASTM A500 GR. B,  $F_y = 46$  KSI MIN.
6. PLATE STEEL ASTM A36
7. WELDING STRENGTH,  $F_{exx} = 70$  KSI
8. THREADED ANCHOR ROD STEEL ASTM F1554 GR. 36
9. STEEL REINFORCEMENT IN CONCRETE ASTM A615 GR 60
10. PROVIDE MIN. 3" CLEAR COVER ON ALL STEEL EMBEDDED IN CONCRETE WHEN CAST AGAINST SOIL AND ALL STEEL EXPOSED TO SOIL
11. LATERAL SOIL BEARING PER IBC CLASS 4 (150 PSF/FT)
12. PROVIDE PROTECTION AGAINST DISSIMILAR METALS
13. ALL DIMENSIONS TO BE VERIFIED PRIOR TO FABRICATION
14. ALL EXISTING ELEMENTS AND DIMENSIONS TO BE VERIFIED IN FIELD.



2/13/2023

**PRSG20230064**



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V5.5

units; pounds, feet unless noted otherwise

### Applied Wind Loads; from ASCE 7-16

$F = q_z * G * C_f * A_f$  with  $q_z = 0.00256 K_z K_{zt} K_d V^2$  (29.3.2 & 29.4)  
 $C_f = 1.604$  (Fig. 29.3-1) 2 pole  $C_f$  factor = 0.87 7.25 max. height = 12.50  
 $K_{zt} = 1.0$  (26.8.2) (=1.0 unless unusual landscape)  
 $K_z =$  from table 28.3-1 Exposure = c  
 $K_d = 0.85$  for signs (table 26.6-1)  
 $V = 100$  mph  
 $G = 0.85$  (26.9) weight = 0.379 kips  
 $s/h = 0.100$   $M_{DL} = 0.00$  k-ft  
 $B/s = 5.40$

Pole Loads	structure component	height at section c.g.	$K_z$	$q_z$	pressure $q_z * G * C_f$	$A_f$	shear	Wind Moment $M_W$
	1	0.25	0.85	18.50	25.22	0.00	0	0
	2	4.54	0.85	18.50	25.22	8.08	204	926
	3	9.88	0.85	18.50	25.22	20.02	505	4985
	4	11.21	0.85	18.50	25.22	0.08	2	24
	5	11.88	0.85	18.50	25.22	9.69	244	2901
					sums:	37.88	955	8.84 ( $M_W$ ) k-ft arm = 9.3
two pole distribution factor *b*s (asce fig. 29.4-1):					x 0.53		508	4.70
					$P_u = 0.45$ kip		$M = 4.70$ k-ft	$M = \sqrt{M_{DL}^2 + M_W^2}$
$M_u = \sqrt{(1.2 M_{DL}^2 + 1.0 M_W^2)} =$					4.70 k-ft			

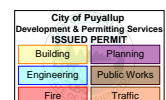
### Pole Design section; tube

$M_u \leq \phi M_n$ with $M_n = f_y Z$		$f_y =$	46	ksi	$\phi = 0.9$		
H	$M_u$ (k-ft)	Z req'd. (in)	Size(in)	t (in)	Z	Use	
at 6" below grade	4.70	1.36	3	0.174	2.0	6x6x3/16" SQ.HSS, $\phi M_n = 27.8$ k-ft	

### Footing Design footprint: rectangle

$\omega = 1.3$	IBC 1605.3.2	IBC Table 1806.2, sections 1806.3.4, 1807.3.2	$S = (1.3 \times 2 \times 150 \text{ psf/ft})$
$P = 0.40$ kip		$S1 = S \times d / 3$	$A = 2.34 \times P / (S1 \times b)$ $S = 400$
$S1 = 426$		$d = 0.5 \times A (1 + (1 + 4.36 \times h/A)^{.5})$	IBC 1807.3.2.1
$A = 0.77$			

footing: 2' - 0" by 2' - 0" 3' - 2" deep  
 4' - 0" deep OK



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### Check 0.625" dia. Threaded Anchor Rods, F1554 Gr.36

$$\begin{aligned}
 \mu &= \text{at 6" below grade} &= 4.70 \text{ k-ft (See Page\#2)} \\
 \nu &= \text{at 6" below grade} &= 0.508 \text{ kips (See Page\#2)} \\
 n &= \text{\#bolts per row} &= 2 \\
 s &= &= 9 \text{ in} \\
 T_u \text{ per bolt} &= &= \mu/s/n = 3.133 \text{ kips} \\
 V_u \text{ per bolt} &= &= \nu/n = 0.254 \text{ kips}
 \end{aligned}$$

Per AISC J3:

$$\begin{aligned}
 d(\text{bolt}) &= 0.625 \text{ in} & F_u &= 58 \text{ ksi} & \phi &= 0.75 \\
 A(\text{bolt}) &= & & & &= 0.307 \text{ in}^2 \\
 F_{nt} &= & 0.75 \cdot F_u &= 43.50 \text{ ksi} \\
 F_{nv} &= & 0.45 \cdot F_u &= 26.10 \text{ ksi} \\
 \phi R_{nt} &= & \phi \cdot F_{nt} \cdot A(\text{bolt}) &= 10.01 \text{ kips} & \text{OK} \\
 \phi R_{nv} &= & \phi \cdot F_{nv} \cdot A(\text{bolt}) &= 6.01 \text{ kips} & \text{OK}
 \end{aligned}$$

### Combined Tension & Shear Check:

$$\begin{aligned}
 f_{rv} &= & V \text{ per bolt} / A(\text{bolt}) &= 0.83 \text{ ksi} \\
 F'_{nt} &= & 1.3F_{nt} - F_{nt}/\phi F_{nv} \cdot f_{rv} \leq F_{nt} &= 43.50 \text{ ksi} \\
 \phi R_{nt} &= & \phi F'_{nt} \cdot A(\text{bolt}) &= 10.01 \text{ kips} & \text{OK}
 \end{aligned}$$

### Embedment Length Calculation:

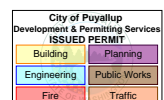
$$\begin{aligned}
 D &= (\text{Dia. of smaller anchor or rebar}) = 0.500 \text{ in} \\
 \text{lap length} &= 40 \cdot D = 20 \text{ in} \\
 \text{min. embed} &= 3" + \text{lap length} = 23 \text{ in}
 \end{aligned}$$

### Check 12x12x0.5" Steel Base Plate, A36

$$\begin{aligned}
 \text{arm} &= 1.650 \text{ in} & b &= 12.00 \text{ in} & t &= 0.5 \text{ in} \\
 M_{\text{plate}} &= & T \text{ per bolt} \cdot n \cdot \text{arm} &= 10.339 \text{ k-in (T= See above, n=2)} \\
 Z &= & b t^2/4 &= 0.750 \text{ in}^3 \\
 \phi M_n &= & \phi \cdot F_y \cdot Z = 0.9 \cdot 36 \text{ ksi} \cdot Z &= 24.300 \text{ k-in} & \text{OK}
 \end{aligned}$$

### Check Vertical Rebar

$$\begin{aligned}
 2 \cdot T_u \text{ per bolt} / \# \text{bars} &= 1.57 \text{ k} & f_y &= 60 \text{ ksi} \\
 \# \text{ of bars (within embed. length):} &= 4 & d_b &= 0.500 \text{ in} \\
 \text{bar \#} &= 4 & A_b &= 0.1963 \text{ in}^2 \\
 T_c = \phi f_y A_b &= 8.84 \text{ k} & \phi &= 0.75 & \text{OK}
 \end{aligned}$$



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