



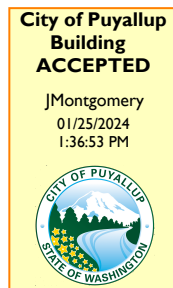
Seattle	1011 Western Avenue, Suite 810 Seattle, WA 98104 206.292.5076
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www.pcs-structural.com	

STRUCTURAL CALCULATIONS

FOR

ARCO PUYALLUP CAR WASH
EQUIPMENT ANCHORAGE
1402 S MERIDIAN
PUYALLUP, WA 98371

PREPARED BY
PCS STRUCTURAL SOLUTIONS



OCTOBER 25, 2023
23-703

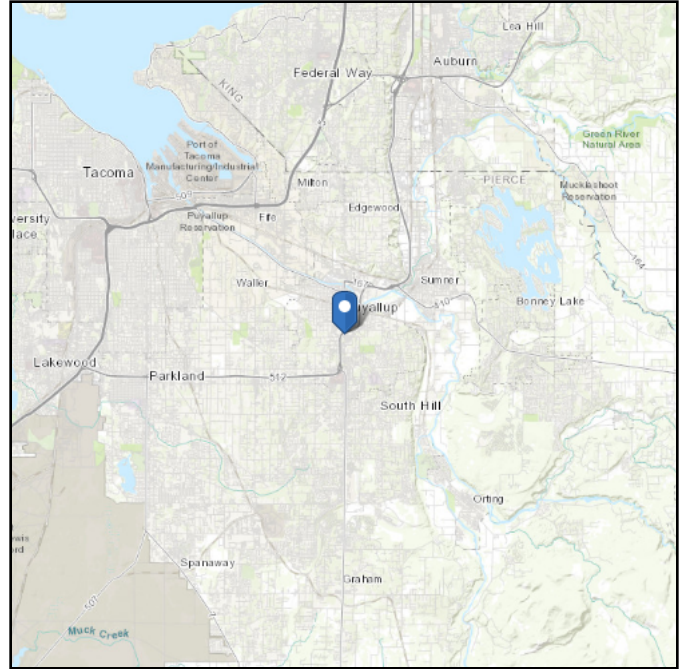
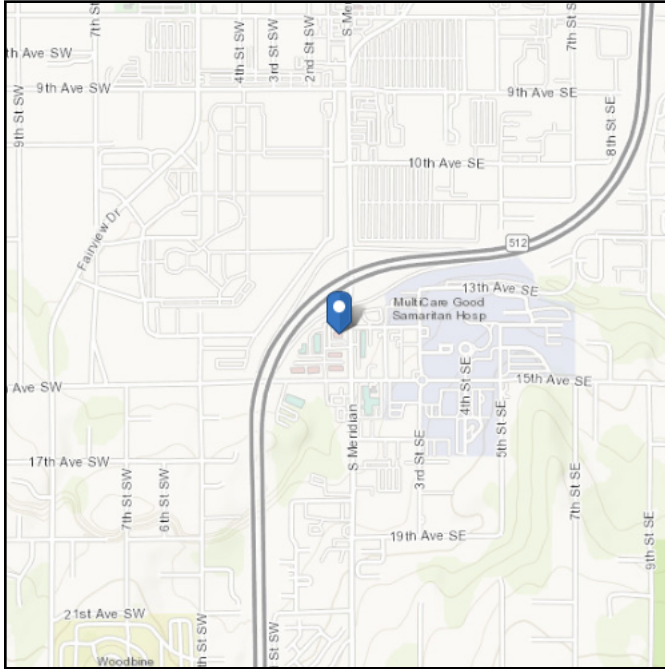


ASCE 7 Hazards Report

Address:
1402 S Meridian
Puyallup, Washington
98371

Standard: ASCE/SEI 7-16
Risk Category: II
Soil Class: D - Stiff Soil

Latitude: 47.178514
Longitude: -122.293971
Elevation: 47.922924404268436 ft (NAVD 88)





Seismic

Site Soil Class: D - Stiff Soil

Results:

S_s :	1.268	S_{D1} :	N/A
S_1 :	0.437	T_L :	6
F_a :	1	PGA :	0.5
F_v :	N/A	PGA _M :	0.55
S_{MS} :	1.268	F_{PGA} :	1.1
S_{M1} :	N/A	I_e :	1
S_{DS} :	0.845	C_v :	1.354

Ground motion hazard analysis may be required. See ASCE/SEI 7-16 Section 11.4.8.

Data Accessed: Mon Oct 23 2023

Date Source: [USGS Seismic Design Maps](#)



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WASH MACHINE

$Wp = 4000\#$

HORIZONTAL: $Fp = [(0.4 \cdot ap \cdot Sds \cdot Wp) / (Rp / lp)] (1 + (2z/h))$

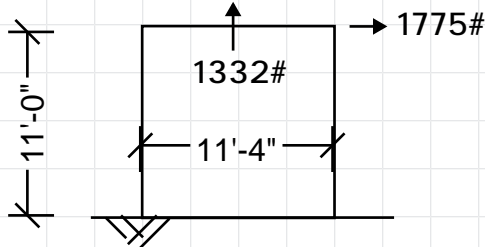
$ap = 1.0$
 $Rp = 1.5$
 $l = 1.0$
 $Sds = 1.664$ ←
 $Wp = 4000\#$
 $z/h = 0$

Sds = 0.85,
THEREFORE, THESE
CALCS ARE
CONSERVATIVE

$Fp = [(0.4 \cdot 1.0 \cdot 1.664 \cdot 4000) / (1.5)] (1 + (2 \cdot 0)) = 1775\#$

VERTICAL: $Fp = +/- (0.2)(Sds)(Wp) = (0.2)(1.664)(4000\#) = +/- 1332\#$

ANCHORAGE:



$Mot = 0.7(1775\#)(11') = 13668ft \cdot \#$
 $Mr = [0.6(4000) - 0.7(1332)] (11.33'/2)$
 $Mr = 8313lb$
 $T = (13668 - 8313) / 11.33 = 473\#$

$Tu = 473\# / 0.7 = 676\#$

$\omega \cdot Tu = 676\# \cdot 2.5 = 1688\# = \underline{844\# / rail}$

$\omega \cdot Vu = 1775\# \cdot 2.5 / (4 \text{ locations} \cdot 0.7) = \underline{1585 \# / rail}$

USE 1/2" DIA. EXP. ANCHOR (EMBED 3-1/4")

SEE HILTI PROFIS OUTPUT FOR ANCHORAGE DESIGN



Hilti PROFIS Engineering 3.0.88

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Company:		Page:	1
Address:		Specifier:	
Phone Fax:		E-Mail:	
Design:	ARCO Puyallup - Wash Machine Anchorage	Date:	10/23/2023
Fastening point:			

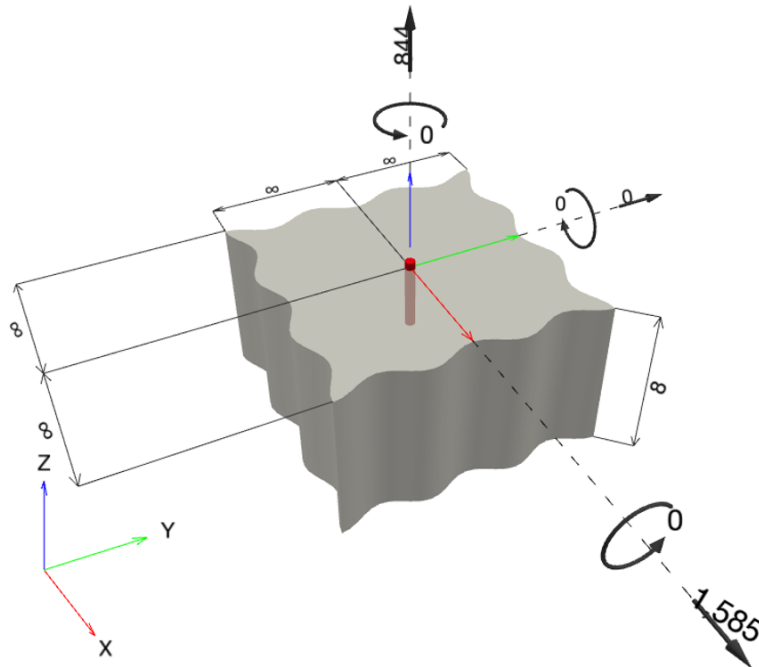
Specifier's comments:

1 Input data

Anchor type and diameter:	Kwik Bolt TZ2 - CS 1/2 (3 1/4)
Item number:	2210255 KB-TZ2 1/2x4 1/2
Effective embedment depth:	$h_{ef,act} = 3.250$ in., $h_{nom} = 3.750$ in.
Material:	Carbon Steel
Evaluation Service Report:	ESR-4266
Issued Valid:	12/17/2021 12/1/2023
Proof:	Design Method ACI 318-14 / Mech
Stand-off installation:	
Profile:	
Base material:	cracked concrete, 2500, $f'_c = 2,500$ psi; $h = 8.000$ in.
Installation:	hammer drilled hole, Installation condition: Dry
Reinforcement:	tension: condition B, shear: condition B; no supplemental splitting reinforcement present
	edge reinforcement: none or < No. 4 bar
Seismic loads (cat. C, D, E, or F)	Tension load: yes (17.2.3.4.3 (d))
	Shear load: yes (17.2.3.5.3 (c))



Geometry [in.] & Loading [lb, in.lb]





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Fastening point:			

1.1 Design results

Case	Description	Forces [lb] / Moments [in.lb]	Seismic	Max. Util. Anchor [%]
1	Combination 1	N = 844; V _x = 1,585; V _y = 0; M _x = 0; M _y = 0; M _z = 0;	yes	36


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Design:	ARCO Puyallup - Wash Machine Anchorage	Date:	10/23/2023
Fastening point:			

2 Proof I Utilization (Governing Cases)

Loading	Proof	Design values [lb]		Utilization	
		Load	Capacity	β_N / β_V [%]	Status
Tension	Concrete Breakout Failure	844	2,428	35 / -	OK
Shear	Steel Strength	1,585	4,471	- / 36	OK

Loading	β_N	β_V	ζ	Utilization $\beta_{N,V}$ [%]	Status
Combined tension and shear loads	0.348	0.355	5/3	35	OK

3 Warnings

- Please consider all details and hints/warnings given in the detailed report!

Fastening meets the design criteria!

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Design:	ARCO Puyallup - Wash Machine Anchorage	Date:	10/23/2023
Fastening point:			

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DRYER SYSTEM $W_p = 1500\#$ (3 FAN DRYER)HORIZONTAL: $F_p = [(0.4 \cdot a_p \cdot S_{ds} \cdot W_p) / (R_p / I_p)] (1 + (2z/h))$

$a_p = 1.0$

$R_p = 1.5$

$I = 1.0$

$S_{ds} = 1.664$

$W_p = 1500\#$

$z/h = 7.92/11.17 = 0.71$

$S_{ds} = 0.85,$
 THEREFORE, THESE
 CALCS ARE
 CONSERVATIVE

$F_p = [(0.4 \cdot 1.0 \cdot 1.664 \cdot 1500) / (1.5)] (1 + (2 \cdot 0.71)) = 1611\#$

VERTICAL: $F_p = +/- (0.2)(S_{ds})(W_p) = (0.2)(1.664)(1500\#) = +/- 500\#$ ANCHORAGE TO STUD WALL:

$V_x = 1611\#/2 = 806\# \quad V_y = 500\#/2 = 205\#$

1/2" DIA LAG INTO HEM-FIR --> $Z_{perp} = 260\#, Z_{para} = 430\#$

$\phi = \text{ARCTAN}(205/806) = 14.3 \text{ DEG}$

$Z_{\phi} = (430 \cdot 205) / (430 \cdot \sin^2(14.3) + 260 \cdot \cos^2(14.3)) = 312\#$

$Z'_{\phi} = 312 \cdot 1.6 = 500\# \text{ PER ANCHOR}$

$V_u = 0.7 \cdot [(806^2) + (205^2)] / 2 = 292\# < 500\# \quad \text{OK}$

GROUND-MOUNTED EQUIP.

Wp = 500#

HORIZONTAL: $F_p = [(0.4 \cdot a_p \cdot S_{ds} \cdot W_p) / (R_p / I_p)] (1 + (2z/h))$

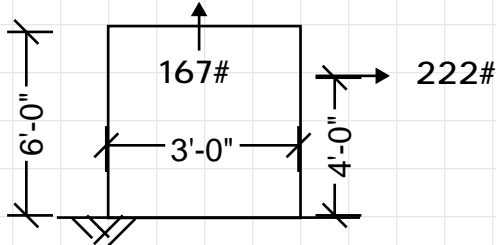
ap = 1.0
 Rp = 1.5
 I = 1.0
 Sds = 1.664 ←
 Wp = 500#
 z/h = 0

Sds = 0.85,
 THEREFORE, THESE
 CALCS ARE
 CONSERVATIVE

$F_p = [(0.4 \cdot 1.0 \cdot 1.664 \cdot 500) / (1.5)] (1 + (2 \cdot 0)) = 222\#$

VERTICAL: $F_p = +/- (0.2)(S_{ds})(W_p) = (0.2)(1.664)(500\#) = +/- 167\#$

ANCHORAGE:



$M_{ot} = 0.7(222\#)(4') = 622\text{ft}\cdot\#$

$M_r = [0.6(500) - 0.7(167)] (1.5'/2)$
 $M_r = 138\text{lb}$

$T = (622 - 138) / 3 = 162\#$

$T_u = 473\# / 0.7 = 676\#$

$\omega \cdot T_u = 162\# \cdot 2.5 = 404\# = \underline{202\# / \text{anchor}}$

$\omega \cdot V_u = 222\# \cdot 2.5 / (4 \text{ locations}) = \underline{139\# / \text{rail}}$

USE 1/2" DIA. EXP. ANCHOR (EMBED 2-1/2")

SEE HILTI PROFIS OUTPUT FOR ANCHORAGE DESIGN



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Company:
 Address:
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 Design: ARCO Puyallup - Floor Mount Anchorage
 Fastening point:

Page: 1
 Specifier:
 E-Mail:
 Date: 10/23/2023

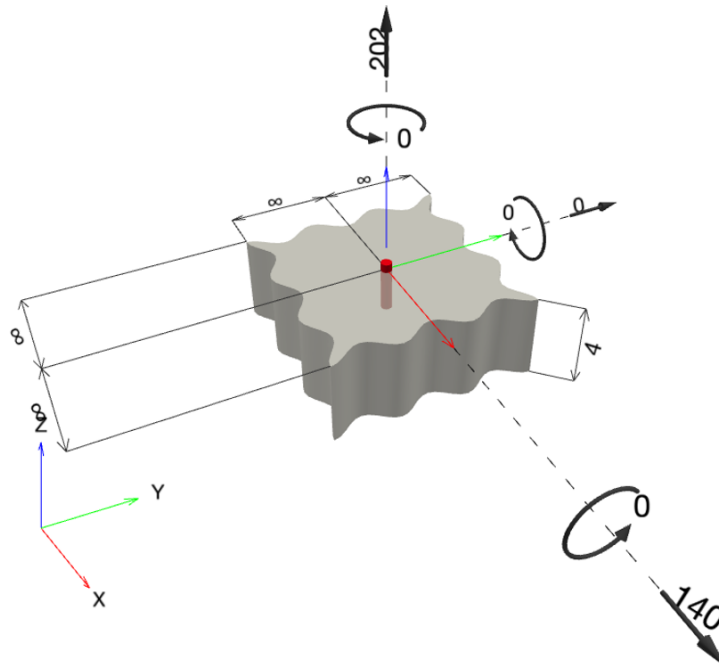
Specifier's comments:

1 Input data

Anchor type and diameter: Kwik Bolt TZ2 - CS 1/2 (2) hnom2
 Item number: 2210254 KB-TZ2 1/2x3 3/4
 Effective embedment depth: $h_{ef,act} = 2.000$ in., $h_{nom} = 2.500$ in.
 Material: Carbon Steel
 Evaluation Service Report: ESR-4266
 Issued | Valid: 12/17/2021 | 12/1/2023
 Proof: Design Method ACI 318-14 / Mech
 Stand-off installation:
 Profile:
 Base material: cracked concrete, 2500, $f'_c = 2,500$ psi; $h = 4.000$ in.
Installation: hammer drilled hole, **Installation condition: Dry**
 Reinforcement: tension: condition B, shear: condition B; no supplemental splitting reinforcement present
 edge reinforcement: none or < No. 4 bar
 Seismic loads (cat. C, D, E, or F) Tension load: yes (17.2.3.4.3 (d))
 Shear load: yes (17.2.3.5.3 (c))



Geometry [in.] & Loading [lb, in.lb]





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Design:	ARCO Puyallup - Floor Mount Anchorage	Date:	10/23/2023
Fastening point:			

1.1 Design results

Case	Description	Forces [lb] / Moments [in.lb]	Seismic	Max. Util. Anchor [%]
1	Combination 1	N = 202; V _x = 140; V _y = 0; M _x = 0; M _y = 0; M _z = 0;	yes	14


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Phone Fax:		E-Mail:	
Design:	ARCO Puyallup - Floor Mount Anchorage	Date:	10/23/2023
Fastening point:			

2 Proof I Utilization (Governing Cases)

Loading	Proof	Design values [lb]		Utilization	
		Load	Capacity	β_N / β_V [%]	Status
Tension	Concrete Breakout Failure	202	1,448	14 / -	OK
Shear	Pryout Strength	140	2,079	- / 7	OK

Loading	β_N	β_V	ζ	Utilization $\beta_{N,V}$ [%]	Status
Combined tension and shear loads	0.140	0.067	5/3	5	OK

3 Warnings

- Please consider all details and hints/warnings given in the detailed report!

Fastening meets the design criteria!

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WALL-MOUNTED EQUIP.

Wp = 300#

HORIZONTAL: $F_p = [(0.4 \cdot a_p \cdot S_{ds} \cdot W_p) / (R_p / I_p)] (1 + (2z/h))$

ap = 1.0

Rp = 1.5

I = 1.0

Sds = 1.664

Wp = 300#

z/h = 6/11.17 = 0.54

Sds = 0.85, THEREFORE, THESE CALCS ARE CONSERVATIVE
--

controls screw shear demand

 $F_p = [(0.4 \cdot 1.0 \cdot 1.664 \cdot 300) / (1.5)] (1 + (2 \cdot 0.54)) = 277\#$ VERTICAL: $F_p = +/- (0.2)(S_{ds})(W_p) = (0.2)(1.664)(300\#) = +/- 100\#$ ANCHORAGE: $Z' = (102\#)(1.6) = 163\# / \text{ANCHOR} > 277\# / 4 = 70\#$ OK $w' = 121\# / \text{in}(1.59\text{in})(1.6) = 307\# / \text{ANCHOR} > 277\#$ OK

USE (4) 1/4" DIA. x 2-1/2" SCREWS

Project: ARCO PUYALLUPJob No: 23-703Subject: EQUIP. ANCHOR. Sheet _____Name: BRTOriginating Office: Seattle Tacoma PortlandDate: 10-23-23

**WALL-MOUNTED TANK
(165 GAL)**

Wp = 1500#

HORIZONTAL: $F_p = [(0.4 \cdot a_p \cdot S_{ds} \cdot W_p) / (R_p / I_p)] (1 + (2z/h))$

ap = 1.0

Rp = 1.5

I = 1.0

Sds = 0.85

Wp = 1500#

z/h = 4/11.17 = 0.36

$$F_p = [(0.4 \cdot 1.0 \cdot 0.85 \cdot 1500) / (1.5)] (1 + (2 \cdot 0.36)) = 584\#$$

VERTICAL: $F_p = +/- (0.2)(S_{ds})(W_p) = (0.2)(0.85)(1500\#) = +/- 255\#$

ANCHORAGE:

$$Z_{perp} = (120\#)(1.6) = 192\# / \text{ANCHOR} > 584\# / 4 = 146\# \quad \underline{\text{OK}}$$

$$Z_{para} = (180\#)(1.6) = 288\# / \text{ANCHOR} > 255\# / 4 = 64\# \quad \underline{\text{OK}}$$

$$w' = 235\# / \text{in}(3.93\text{in})(1.6) = 1477\# / \text{ANCHOR} > 584\# \quad \underline{\text{OK}}$$

USE (4) 3/8" DIA. x 4" LAG SCREWS