FULL SIZED LEDGIBLE REPORT ARE REQUIRED TO BE PROVIDED BY THE PERMITTEE ON SITE FOR ALL INSPECTIONS





Structural Calculations

FOR

JD SPORTS #1315 South Hill Mall, Puyallup, WA 98373

> Citv Submittal January 10th, 2024



Project No: 17016.8

EUGENE

FRAMING KEY PLAN





Ceiling/Soffit Spans (S-Sections)

JOISTS

PRCTI20240063

Page 2

					Inte	rior All	owabl	e Ceili	ng/Sof	fit Spa	ns (S-S	Sectior	າs) - L/2	240					
				4 p	osf					6 p	osf					13 p	sf*		
	-		Lateral Su	pport of	Compressi	ion Flange	•		Lateral S	upport of (Compress	ion Flange	e		Lateral S	upport of (Compress	ion Flange	e
Section	ry (ksi)	U	nsupporte	ed		Midspan		ι	Insupport	ed		Midspan		ι	Insuppor	ted		Midspan	
	x - 7	Joist Spa	acing (in) o	on center	Joist Spa	acing (in) o	on center	Joist Sp	acing (in)	on center	Joist Spa	acing (in) o	on center	Joist Sp	acing (in)	on center	Joist Spa	acing (in) o	on center
		12	16	24	12	16	24	12	16	24	12	16	24	12	16	24	12	16	24
162S125-18	33	7'3"	6'7" 7'11"	5' 10"	8'6"	7'8"	6'7" 7'9"	6'5"	5' 10"	5'1"	7'4"	6'7"	5'9"	5'0"	4'5"	3'9"	5'7"	4' 10"	3' 11"
162S125-27	33	9'0"	8'3"	7'4"	10'0"	9'1"	7 0	8'0"	7'4"	6'7"	8'9"	7 0	6' 11"	6'5"	5' 10"	4 9 5'0"	6'9"	6' 1"	5 Z 5' 4"
162S125-33	33	9' 6"	8' 8"	7' 8"	10' 4"	9' 5"	8' 2"	8' 4"	7' 8"	6' 10"	9' 0"	8' 2"	7' 2"	6' 8"	6' 1"	5' 4"	7'0"	6' 4"	5' 6"
162S137-27 162S137-30	33 33	9' 11" 10' 4"	9'2" 9'6"	8' 0" 8' 3"	10' 1" 10' 5"	9'2" 9'6"	8'0" 8'3"	8' 10" 9' 1"	8' 0" 8' 3"	7'0" 7'3"	8' 10" 9' 1"	8' 0" 8' 3"	7'0" 7'3"	6' 10" 7' 0"	6' 2" 6' 5"	5' 5" 5' 7"	6' 10" 7' 0"	6' 2" 6' 5"	5' 5" 5' 7"
162S137-33	33	10'9"	9'9"	8'7"	10'9"	9' 9"	8'7"	9' 5"	8' 7"	7'6"	9' 5"	8' 7"	7'6"	7'3"	6' 7"	5' 9"	7'3"	6' 7"	5' 9"
250S125-18	33	8' 5"	7'9"	6' 11"	11' 7"	10'6"	9'1"	7'6"	6' 11"	6'2"	10' 1"	9' 1"	7'8"	6'0"	5'6"	4' 10"e	7' 5"	6'3"e	5' 2"e
250S125-27 250S125-30	33 33	9' 8" 10' 1"	8' 11" 9' 3"	8' 0" 8' 3"	13' 5"	12' 2"	10' 7"	8'8" 9'0"	8' 0" 8' 3"	7' 2" 7' 5"	11'8"	10' 7"	9' 3" 9' 7"	7'0"	6' 6" 6' 8"	5' 9" 6' 0"	9' 0" 9' 4"	8'2" 8'5"	6' 10" 7' 3"
250S125-33	33	10' 6"	9' 8"	8' 7"	14' 3"	13' 0"	11' 4"	9' 4"	8'7"	7'8"	12' 6"	11' 4"	9' 11"	7'6"	6' 11"	6'2"	9' 7"	8' 9"	7'7"
250S125-43	33	11' 9"	10' 10"	9'7"	15' 6"	14' 1"	12' 4"	10' 5"	9'7"	8'6" 8'2"	13' 7"	12' 4"	10' 9"	8' 4" 8' 0"	7'8"	6' 10"	10' 6"	9'6" 9'7"	8'4"
250S137-27 250S137-30	33	11'5"	10'2	9 Z 9' 5"	14 0	12 9	11'6"	10'2"	9 2 9' 5"	8' 5"	12' 8"	11' 6"	10' 0"	8'3"	7'8"	6' 10"	9'9"	8' 10"	7'9"
250S137-33	33	11' 10"	10' 11"	9' 9"	14' 11"	13' 7"	11' 10"	10' 7"	9' 9"	8' 9"	13' 1"	11' 10"	10' 4"	8' 7"	7' 11"	7' 1"	10' 1"	9' 2"	8' 0"
250S137-43	33	13' 3"	12' 2"	10' 10"	16' 3"	14' 9"	12' 11"	11' 9"	10' 10"	9'7" 10'0"	14' 2"	12' 11"	11' 3"	9' 5" 0' 10"	8' 8" 0' 1"	7'9" 8'1"	10' 11"	9' 11"	8' 8"
250S162-33	33	15'0"	13' 9"	12' 3"	17' 1"	15' 6"	13' 6"	13' 4"	12' 3"	10' 0	14' 11"	13' 6"	11' 10"	10' 9"	9' 11"	8' 10"	11' 6"	10' 5"	9' 2"
350S125-18	33	9'2"	8'6"	7'6"	12' 6"	11' 5"	9' 11"	8' 3"	7'6"	6' 8"	11'0"	9' 11"	8' 5"e	6' 6"	5' 11"e	5' 3"e	8' 2"e	7' 2"e	6'0"e
350S125-27 350S125-30	33 33	10' 7"	9' 9" 10' 1"	8' 9" 9' 0"	14' 11" 15' 5"	13' 9"	12' 3" 12' 9"	9' 5" 9' 9"	8'9" 9'0"	7' 9" 8' 1"	13' 4"	12' 3"	10' 7"	7' /"	7' 1"	6' 4" 6' 6"	10' 4"	9' 3" 9' 9"	7'9" 8'3"
350S125-33	33	11' 4"	10' 5"	9' 4"	16' 0"	14' 9"	13' 2"	10' 1"	9' 4"	8' 4"	14' 3"	13' 2"	11'9"	8' 2"	7'7"	6'9"	11' 5"	10' 4"	8' 10"
350S125-43	33	12' 7"	11'7"	10' 4"	17'7"	16' 3"	14' 6"	11' 2"	10' 4"	9'2"	15' 8"	14' 6"	12' 11"	9'0"	8' 3"	7'5"	12'7"	11'6"	10' 1"
350S137-27 350S137-30	33	12' 4"	11'5"	9 11 10' 3"	17 0	15 9	14 1	10 8	9 11 10' 3"	9'2"	15 3	14 1	12 4	0 0 9'0"	8'4"	7 3	12'6"	10 7	9'6"
350S137-33	33	12' 9"	11' 10"	10' 7"	18' 2"	16' 9"	15' 1"	11' 5"	10' 7"	9' 6"	16' 3"	15' 1"	13' 4"	9' 3"	8'7"	7'8"	13' 0"	11' 9"	10' 0"
350S137-43	33	14' 2" 14' 6"	13' 0"	11' 7" 12' 1"	19' 10" 20' 3"	18' 4"	16' 5" 16' 1"	12' 7" 13' 0"	11' 7" 12' 1"	10' 4" 10' 10"	17' 9" 17' 9"	16' 5" 16' 1"	14' 7" 14' 1"	10' 2"	9'4" 9'10"	8' 5" 8' 10"	14' 2" 13' 8"	12' 11"	11' 3"
350S162-33	33	16' 0"	14' 9"	13' 2"	20 3	20'0"	17' 6"	14' 3"	13' 2"	11' 9"	19' 3"	17' 6"	15' 3"	11'6"	10' 8"	9'7"	14' 11"	13' 6"	11' 10"
362S125-18	33	9' 3"	8'7"	7'7"	12' 8"	11' 7"	10' 0"	8'4"	7'7"	6'9"	11' 1"	10' 0"	8'6"e	6'7"	6'0"e	5' 4"e	8' 3"e	7' 4"e	6' 1"e
3625125-27	33	10'8"	9"10" 10'2"	9'10"	15'0"	13'11''	12' 4"	9'6" 9'10"	8''10'' 9' 1"	7' 10" 8' 2"	13'5"	12'4"	10'9''	7'8' 8'0"	7'1"	6'7"	10'5"	9'4" 9'11"	8'5"
362S125-33	33	11' 5"	10' 7"	9' 5"	16' 2"	14' 10"	13' 3"	10' 3"	9' 5"	8' 5"	14' 5"	13' 3"	11' 10"	8' 3"	7' 8"	6' 10"	11'7"	10' 6"	9' 0"
362S125-43	33	12' 8"	11' 8"	10' 5"	17' 9"	16' 5"	14' 8"	11' 3"	10' 5"	9' 3" 9' 0"	15' 10"	14' 8"	> M/	AX JC	DIST	SPAN	= 6'-	0". O	K. 1"0
362S137-27	33	12' 5"	11'6"	10'0"	17' 8"	16' 5"	14' 8"	11' 2"	10' 4"	9'3"	15' 10"	14' 8"	13.0.	9.1	8.2	/ ⁻ 0	12.8	11.5	9 8"
362S137-33	33	12' 11"	11' 11"	10' 8"	18' 4"	16' 11"	15' 2"	11' 6"	10' 8"	9'7"	16' 5"	15' 2"	13' 6"	9' 4"	8' 8"	7'9"	13' 2"	11' 11"	10' 2"
362S137-43	33	14' 3" 14' 8"	13' 2" 13' 7"	11' 8" 12' 2"	20' 0" 20' 10"	18' 6" 18' 11"	16' 7" 16' 6"	12' 8" 13' 2"	11' 8" 12' 2"	10' 5" 10' 11"	17' 11"	16' 7" 16' 6"	14' 9" 14' 5"	10' 3" 10' 8"	9'5" 9'11"	8' 6" 8' 11"	14' 5" 14' 1"	13' 2"	11' 5" 11' 2"
362S162-43	33	16' 2"	14' 11"	13' 4"	22' 8"	20'7"	18'0"	14' 5"	13' 4"	11' 11"	19' 10"	18' 0"	15' 9"	11' 8"	10' 9"	9' 8"	15' 4"	13' 11"	12' 2"
400S125-18	33	9'6"e	8'9"e	7' 10"e	13' 0"e	11' 11"e	10' 5"e	8'6"e	7' 10"e	6' 11"e	11'6"e	10' 5"e	8' 11"e	6'9"e	6'2"e	5'6"e	8'7"e	7' 8"e	6' 5"e
400S125-27 400S125-30	33	10 11	10 1	9 1 9' 4"	15 5	14 3	12 9	9 9 10' 1"	9 1 9'4"	o 1 8' 4"	13 10	12 9	11 Z	8'2"	7 4 7 7	6'9"	10 10	9 9 10' 4"	03 8'9"
400S125-33	33	11' 9"	10' 10"	9' 8"	16' 7"	15' 3"	13' 8"	10' 6"	9' 8"	8' 8"	14' 9"	13' 8"	12' 2"	8' 6"	7' 10"	7'0"	11' 11"	10' 11"	9' 4"
400S125-43	33	13'0"	12'0"	10' 8"	18' 3"	16' 10"	15'0"	11' 7"	10' 8"	9'6"	16' 3"	15' 0"	13' 5"	9' 4" 0' 0"	8'7"	7'8"	13' 1"	12' 0"	10' 7"
400S137-27 400S137-30	33	12 4	11' 10"	10'5"	18' 2"	16' 4	14 0	11' 5"	10'5"	9 2 9' 6"	16' 4"	14 8	13'5"	9'0"	8'7"	7'9"	13' 1"	11' 10"	10' 1"
400S137-33	33	13' 3"	12' 3"	10' 11"	18' 9"	17' 4"	15' 7"	11' 10"	10' 11"	9' 10"	16' 10"	15' 7"	13' 11"	9' 7"	8' 11"	8' 0"	13' 7"	12' 4"	10' 8"
400S137-43	33	14' 7" 15' 0"	13' 6"	12' 0" 12' 6"	20' 7"	19' 0" 19' 10"	17' 0" 17' 9"	13' 0" 13' 6"	12'0"	10' 9" 11' 2"	18' 4" 10' 3"	17'0" 17'9"	15' 2" 15' 7"	10' 6"	9'8" 10'2"	8' 8" Q' 1"	14' 10"	13' 7" 13' 9"	11' 10" 11' Q"
400S162-33	33	16'7"	15' 3"	13' 8"	21 3	21'7"	19' 4"	14' 9"	13' 8"	12' 2"	20' 11"	19' 4"	16' 11"	11' 11"	11'0"	9' 11"	16' 6"	15' 0"	13' 1"
600S125-27	33	12' 5"e	11' 6"e	10' 4"e	17' 11"e	16' 6"e	14'9"e	11' 2"e	10' 4"e	9'4"e	16' 0"e	14' 9"e	13' 2"e	9'2"e	8'6"e	7' 7"e	12' 11"e	11' 10"e	10' 4"e
600S125-30	33 33	12' 9"	12' 3"	10' 8"	18' 5"	17' 1"	15' 3" 15' 10"	11' 10"	11' 0"	9'7" 9'10"	17'0"	15' 3"	13' 8"	9'5" 9'8"	8' 9" 8' 11"	7°10" 8'1"	13' 4"	12' 4" 12' 9"	10°11°e
600S125-43	33	14' 6"	13' 4"	11' 11"	20'6"	19' 0"	17' 0"	12' 11"	11' 11"	10' 8"	18' 4"	17' 0"	15' 3"	10' 5"	9' 8"	8' 8"	15' 0"	13' 11"	12' 6"
600S137-27	33	14' 0"e 14' 5"	13' 0"e	11' 9"e 12' 0"	20' 2"e	18' 8"e	16' 9"e 17' 3"	12' 7"e	11' 9"e	10' 6"e 10' 10"	18' 1"e	16' 9"e 17' 3"	15' 0"e	10' 4"e	9'7"e	8' 7"e 8' 10"	14' 8"e	13' 7"e 14' 0"	11' 10"e
600S137-30	33	14' 11"	13' 9"	12' 5"	21'5"	19' 10"	17' 10"	13' 4"	12' 5"	11' 2"	19' 3"	17' 10"	16' 0"	10' 11"	10'2"	9' 2"	15' 8"	14' 6"	12' 11"e
600S137-43	33	16' 3"	15' 0"	13' 5"	23' 1"	21' 5"	19' 3"	14' 6"	13' 5"	12' 0"	20' 9"	19' 3"	17' 4"	11' 9"	10' 11"	9' 10"	16' 11"	15' 9"	14' 2"
600S162-33 600S162-43	33 33	16' 11" 18' 5"	15' 8" 17' 0"	14' 1" 15' 3"	24' 5" 26' 4"	22' 8" 24' 4"	20'5" 21'11"	16' 6"	14' 1" 15' 3"	12' 8"	22'0"	20'5"	18' 5" 19' 9"	12' 5"	12' 5"	10' 5" 11' 2"	18'0"	16'8" 17' 11"	14' 9"e 16' 0"

*Loads that exceed 10 psf limit require an approved CP60 coating.

"e" web stiffeners required at ends.

See Table Notes and figures on page 61.



Project Name: 17016.8_Light Ga HDR Model: HEADER Code: 2012 NASPEC [AISI S100-2012]



Simpson Strong-Tie® CFS Designer™ 5.2.1.0

	30.00 lb/ft	
		B2

Span

Section:	(2) 800S162-4	3 (50 ksi) Boxed C Stu	d (punched)	
Maxo =	4321.3 ft-lb	Va = 2102.3 lb	I = 8.86 in^4	

Loads have not been modified for strength checks Loads have not been modified for deflection calculations

30.00 lb/ft	<u>Bri</u>	Bridging Connectors - Design Method =AISI S100							•	
	Sp	an	Axia KyLy, ∣	al KtLt	Fle Dis	xual, stortio	nal	Connector	Stress Ratio	
R2	Spa	an	NA		None, N/A		4	N/A	-	
20.25	We	eb Crip	pling	Beari	ng	Ра	м			
	Su	pport	Load (Ib)	(in)		(lb)	(ft-lbs)	Max Int.	Stiffener?	
	R1		303.75	1.00		748.3	0.0	0.21	NO	
	R2		303.75	1.00		748.3	0.0	0.21	NO	
Code Check	Required	AI	lowed	Inte	ract	ion I	lotes			
Max. Axial, lbs	0.0(t)		-		0%	ł	(Φ=0.00	lb-in/in Max	KL/r = N/A	
Max. Shear, lbs	303.8	2	102.3		14%	5	Shear (Pu	inched)		
Max. Moment (MaFy, Ma-dist), ft-lbs	1537.7	4	321.3	3	36%					
Moment Stability, ft-lbs	1537.7	4	321.3	3	36%					
Shear/Moment	0.36		1.00	3	36%	5	Shear 0.0	, Moment 1	537.7	
Axial/Moment	0.36		1.00	3	36%	A	Axial 0.0(c), Moment	1537.7	
Deflection Span, in	0.434	mee	ets L/559							

Support	Rx(lb)	Ry(lb)	Simpson Strong-Tie Connector	Connector Interaction	Anchor Interaction
R1	0.0	303.8	LSSC4.25 Max (5#10) & (4) #10 to Carrying (18/33) (Side Attached)	69.03 %	69.03 %
R2	0.0	303.8	SSC4.25 Max (5#10) & (4) #10 to Carrying (20/33) (Side Attached)	50.63 %	83.22 %

* Reference catalog for connector and anchor requirement notes as well as screw placement requirements

Project Title: Engineer: Project ID: Project Descr:

velopment & Permitting Se ISSUED PERMIT

Page 4 City of Puyallup

Planning

Public Works

Traffic

Steel Beam

LIC# : KW-06014324, Build:20.23.08.30

HOHBACH-LEWIN

(c) ENERCALC INC 1983-2023

Building

Engineering

Fire

Project File: 17016.8F_JD Sports.ec6

46.0 ksi

29,000.0 ksi

DESCRIPTION: HDR

CODE REFERENCES

Calculations per AISC 360-16, IBC 2021, ASCE 7-16 Load Combination Set : IBC 2021

Material Properties

Analysis Method Load Resistance Factor Design Beam Bracing: Completely Unbraced Bending Axis : Major Axis Bending



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Fy : Steel Yield :

E: Modulus :

Beam self weight calculated and added to loading Uniform Load : D = 0.080 k/ft, Tributary Width = 1.0 ft, (SOFFIT WALL (H = 8'-0))

Uniform Load : D = 0.010, Lr = 0.020 ksf, Tributary Width = 2.110 ft, (JOISTS)

DESIGN SUMMARY

DESIGN SUMMARY					Design OK
Maximum Bending Stress Ratio =	0.138 :1	Ma	ximum S	hear Stress Ratio =	0.016 : 1
Section used for this span	HSS10x4x3/8		Sect	ion used for this span	HSS10x4x3/8
Mu : Applied	12.866 k-ft			Vu : Applied	2.422 k
Mn * Phi : Allowable	93.150 k-ft			Vn * Phi : Allowable	155.230 k
Load Combination	+1.20D+1.60Lr		Load Loca	Combination tion of maximum on span	+1.20D+1.60Lr 0.000 ft
Span # where maximum occurs	Span # 1		Spar	# where maximum occurs	Span # 1
Maximum Deflection Max Downward Transient Deflection Max Upward Transient Deflection Max Downward Total Deflection Max Upward Total Deflection	0.064 in Ratio = 0 in Ratio = 0.269 in Ratio = 0 in Ratio =	3,954 0 949 0	>=360 <360 >=240. <240.0	Span: 1 : Lr Only n/a Span: 1 : +D+Lr n/a	

Maximum Forces & Stresses for Load Combinations

Load Combination		Max Stres	s Ratios	Su	immary of Mc	oment Valu	les			Summa	ry of She	ar Values
Segment Length	Span #	Μ	V max l	Mu + max Mu -	Mu Max	Mnx I	Phi*Mnx	Cb	Rm	VuMax	Vnx	Phi*Vnx
+1.40D												
Dsgn. L = 21.25 ft	1	0.113	0.013	10.56	10.56	103.50	93.15	1.14	1.00	1.99	172.48	155.23
+1.20D+0.50Lr												
Dsgn. L = 21.25 ft	1	0.110	0.012	10.25	10.25	103.50	93.15	1.14	1.00	1.93	172.48	155.23
+1.20D												
Dsgn. L = 21.25 ft	1	0.097	0.011	9.05	9.05	103.50	93.15	1.14	1.00	1.70	172.48	155.23
+1.20D+1.60Lr												
Dsgn. L = 21.25 ft	1	0.138	0.016	12.87	12.87	103.50	93.15	1.14	1.00	2.42	172.48	155.23
+0.90D												
Dsgn. L = 21.25 ft	1	0.073	0.008	6.79	6.79	103.50	93.15	1.14	1.00	1.28	172.48	155.23
Overall Maximum	Deflectio	ons										
Load Combination		Span M	lax. "-" Defl L	ocation in Span	Load Con	nbination			Max	. "+" Defl I	_ocation i	in Span
+D+Lr		1	0.2688	10.686						0.0000		0.000
Vertical Reactions				Suppo	ort notation : F	ar left is #	ŧ		Values	in KIPS		
Load Combination			Support 1	Support 2								
Max Upward from all	Load Con	ditions	1.869	1.869								
Max Upward from Lo	ad Combir	nations	1.869	1.869								
Max Upward from Lo	ad Cases		1.420	1.420								



Project Title: Engineer: Project ID: Project Descr:

Page 5 City of Puyallup Development & Permiting services /ISSUED PERMIT Building Planning Engineering Public Works Fire Traffic

Steel Beam

LIC# : KW-06014324, Build:20.23.08.30

HOHBACH-LEWIN

Project File: 17016.8F_JD Sports.ec6 (c) ENERCALC INC 1983-2023

DESCRIPTION: HDR

Vertical Reactions		S	Support notation : Far left is #	Values in KIPS	
Load Combination	Support 1	Support 2			
D Only	1.420	1.420			
+D+Lr	1.869	1.869)		
+D+0.750Lr	1.757	1.757	,		
+0.60D	0.852	0.852	•		
Lr Only	0.448	0.448	5		

Project Title: Engineer: Project ID: Project Descr:

Page 6 City of Puyallup ment & Permitting Ser ISSUED PERMIT Building Planning Engineering Public Works Fire Traffic

Steel Column

LIC# : KW-06014324, Build:20.23.08.30

HOHBACH-LEWIN

Project File: 17016.8F_JD Sports.ec6

(c) ENERCALC INC 1983-2023

DESCRIPTION: COL

Code References

Calculations per AISC 360-16, IBC 2021, ASCE 7-16 Load Combinations Used : IBC 2021

General Information

Steel Section Name	e : HSS4x4x1/4	Overall Column Height	18.0 ft
Analysis Method : Steel Stress Grade	Load Resistance Factor	Top & Bottom Fixity Brace condition :	Top & Bottom Pinned
Fy : Steel Yield E : Elastic Bending Mo	46.0 ksi dulus 29,000.0 ksi	Unbraced Length for b Unbraced Length for b	uckling ABOUT X-X Axis = 18.0 ft, K = 1.0 uckling ABOUT Y-Y Axis = 18.0 ft, K = 1.0
Applied Loads		Service loads enter	ed. Load Factors will be applied for calculations.

Applied Loads

Column self weight included : 219.780 lbs * Dead Load Factor AXIAL LOADS ... HDR x2: Axial Load at 18.0 ft, D = 2.840, LR = 0.880 k

DESIGN SUMMARY

Bending & Shear Check Results						
PASS Max. Axial+Bending Stress Ratio =	0.1347 :1	Maximum Load	Reactions .			
Load Combination	+1.20D+1.60Lr	Top along X	-X		0.0 k	
Location of max.above base	0.0 ft	Bottom alon	g X-X		0.0 k	
At maximum location values are		Top along Y	-Y		0.0 k	
Pu	5.080 k	Bottom alon	g Y-Y		0.0 k	
0.9 * Pn	37.701 k					
Mu-x	0.0 k-ft	Maximum Load	Deflections	• • •		
0.9 * Mn-x :	16.181 k-ft	Along Y-Y for load combin	0.0 in ation [.]	at	0.0ft	above base
Mu-y	0.0 k-ft					
0.9 * Mn-y :	16.181 k-ft	Along X-X	0.0 in	at	0.0ft	above base
		for load combin	ation :			
PASS Maximum Shear Stress Ration	0.0 : 1					
Load Combination	0.0					
Location of max.above base At maximum location values are	0.0 ft					
Vu : Applied	0.0 k					
Vn * Phi : Allowable	0.0 k					

Load Combination Results

	Maximum Axia	+ Bending	Stress Ratio	<u>DS</u>					Maximum S	Shear R	atios
Load Combination	Stress Ra	tio Status	Location		Cbx	Cby	KxLx/Ry	KyLy/Rx	Stress Ratio S	Status	Location
+1.40D	0.11	4 PASS	0.00	ft	1.00	1.00	142.11	142.11	0.000	PASS	0.00 ft
+1.20D+0.50Lr	0.10	9 PASS	0.00	ft	1.00	1.00	142.11	142.11	0.000	PASS	0.00 ft
+1.20D	0.09	7 PASS	0.00	ft	1.00	1.00	142.11	142.11	0.000	PASS	0.00 ft
+1.20D+1.60Lr	0.13	5 PASS	0.00	ft	1.00	1.00	142.11	142.11	0.000	PASS	0.00 ft
+0.90D	0.07	3 PASS	0.00	ft	1.00	1.00	142.11	142.11	0.000	PASS	0.00 ft
Maximum Reactions	5							Note	: Only non-zero	reactio	ns are listed.
	Axi	al Reaction	X-X Axis F	Reaction	k	Y-Y Axis	Reaction	Mx - End	Moments k-ft	My - E	End Moments
Load Combination		@ Base	@ Base	@ Top		@ Base	@ Top	@ Base	е @ Тор	@ Ba	ise @ Top
D Only		3.060									
+D+Lr		3.940									
+D+0.750Lr		3.720									
+0.60D		1.836									
Lr Only		0.880									
Extreme Reactions											
	Axia	I Reaction	X-X Axis F	Reaction	n k	Y-Y Axis	Reaction	Mx - End	Moments k-ft	My - E	End Moments
Item	Extreme Value	@ Base	@ Base	@ Top)	@ Base	@ Top	@ Base	е @ Тор	@ Ba	ase @ Top
Axial @ Base	Maximum	3.940									
"	Minimum	0.880									
Reaction, X-X Axis Base	e Maximum	3.060									

Project Title: Engineer: Project ID: Project Descr:

> Fire Traffic Project File: 17016.8F_JD Sports.ec6

Steel Column

LIC# : KW-06014324, Build:20.23.08.30

HOHBACH-LEWIN

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DESCRIPTION: COL

		Axial Reaction	X-X Axis I	Reaction	k	Y-Y Axis Reaction	Mx - End M	oments k-ft	My - End	Moments
Item	Extreme Value	e @ Base	@ Base	@ Top		@ Base @ Top	@ Base	@ Top	@ Base	@ Top
"	Minimum	3.060								
Reaction, Y-Y Axis Bas	e Maximum	3.060								
"	Minimum	3.060								
Reaction, X-X Axis Top	Maximum	3.060								
	Minimum	3.060								
Reaction, Y-Y Axis Top	Maximum	3.060								
	Minimum	3.060								
Moment, X-X Axis Base	Maximum	3.060								
n	Minimum	3.060								
Moment, Y-Y Axis Base	e Maximum	3.060								
	Minimum	3.060								
Moment, X-X Axis Top	Maximum	3.060								
"	Minimum	3.060								
Moment, Y-Y Axis Top	Maximum	3.060								
"	Minimum	3.060								

Load Combination	า	Max. Defle	ection in X dir	Distance	Max. Deflection in Y dir	Distance		
D Only			0.0000 in	0.000 ft	0.000 in	0.000 ft		
+D+Lr			0.0000 in	0.000 ft	0.000 in	0.000 ft		
+D+0.750Lr			0.0000 in	0.000 ft	0.000 in	0.000 ft		
+0.60D			0.0000 in	0.000 ft	0.000 in	0.000 ft		
Lr Only			0.0000 in	0.000 ft	0.000 in	0.000 ft		
Steel Section P	roperties	S: HSS4x4	4x1/4					
Depth	=	4.000 in	l xx	=	7.80 in^4	J	=	12.800 in^4
Design Thick	=	0.233 in	S xx	=	3.90 in^3			
Width	=	4.000 in	R xx	=	1.520 in			
Wall Thick	=	0.250 in	Zx	=	4.690 in^3			
Area	=	3.370 in^2	l yy	=	7.800 in^4	С	=	6.560 in^3
Weight	=	12.210 plf	S yy	=	3.900 in^3			
			R yy	=	1.520 in			

Ycg = 0.000 in



Project Title: Engineer: Project ID: Project Descr:

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Steel Column

LIC# : KW-06014324, Build:20.23.08.30

HOHBACH-LEWIN

Project File: 17016.8F_JD Sports.ec6 (c) ENERCALC INC 1983-2023

DESCRIPTION: COL

Sketches





SIMPSON

Strong-I

Anchor Designer™ Software Version 3.0.7775.33

Company:	Date:		
Engineer:	Page:	1/5	
Project:	(Developn	City of P nent & Pe	uyallup rmitting Service:
Address:	Build	SSUED	PERMIT
Phone:	Engine	eering	Public Works
E-mail:	Fir	e OF V	Traffic

1.Project information

Customer company: Customer contact name: Customer e-mail: Comment:

2. Input Data & Anchor Parameters

General Design method:ACI 318-14 Units: Imperial units

Anchor Information:

Anchor type: Concrete screw Material: Carbon Steel Diameter (inch): 0.500 Nominal Embedment depth (inch): 3.250 Effective Embedment depth, hef (inch): 2.350 Code report: ICC-ES ESR-2713 Anchor category: 1 Anchor ductility: No hmin (inch): 5.00 c_{ac} (inch): 3.56 Cmin (inch): 1.75 Smin (inch): 3.00

Recommended Anchor

Anchor Name: Titen HD® - 1/2"Ø Titen HD, hnom:3.25" (83mm) Code Report: ICC-ES ESR-2713



Project description: Location: Fastening description:

Base Material

Concrete: Normal-weight Concrete thickness, h (inch): 5.00 State: Cracked Compressive strength, f'c (psi): 2500 $\Psi_{c,V}$: 1.0 Reinforcement condition: B tension, B shear Supplemental reinforcement: Not applicable Reinforcement provided at corners: No Ignore concrete breakout in tension: No Ignore concrete breakout in shear: No Ignore 6do requirement: Not applicable Build-up grout pad: No

Base Plate

Length x Width x Thickness (inch): 5.00 x 10.00 x 0.50 Yield stress: 36000 psi

Profile type/size: HSS4X4X3/8

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Company:	Date:	
Engineer:	Page:	2/5
Project:	Cit	y of Puyallup ht & Permitting Services
Address:	Buildin	g Planning
Phone:	Engineer	ing Public Works
E-mail:	Fire	Traffic

Load and Geometry Load factor source: ACI 318 Section 5.3 Load combination: not set Seismic design: No Anchors subjected to sustained tension: Not applicable Apply entire shear load at front row: No Anchors only resisting wind and/or seismic loads: No

Strength level loads:

N_{ua} [lb]: -3720 V_{uax} [lb]: 200 V_{uay} [lb]: 0 M_{ux} [ft-lb]: 0 M_{uy} [ft-lb]: 0 Muz [ft-lb]: 0





SIM	PSON
Stro	ng-Tie

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Company:	Date:
Engineer:	Page: 3/5
Project:	City of Puyallup
Address:	Bevelopment & Permitting Servic / ISSUED PERMIT
Phone:	Engineering Public Works
E-mail:	Fire

<Figure 2>



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i ago	14

	Company:	Date:
	Engineer:	Page: 4/5
trong-Tie Software	Project:	City of Puvaliup
Version 3.0.7775.33	Address:	Development & Permitting Services
	Phone:	Building Planning Engineering Public Works
	E-mail:	Fire

3. uiting Anchor Fo

Anchor	Tension load, N _{ua} (Ib)	Shear load x, V _{uax} (lb)	Shear load y, V _{uay} (Ib)	Shear load combined, $\sqrt{(V_{uax})^2 + (V_{uay})^2}$ (lb)
1	0.0	50.0	0.0	50.0
2	0.0	50.0	0.0	50.0
3	0.0	50.0	0.0	50.0
4	0.0	50.0	0.0	50.0
Sum	0.0	200.0	0.0	200.0

Maximum concrete compression strain (‰): 0.00

Maximum concrete compression stress (psi): 0

Resultant tension force (lb): 0

Resultant compression force (lb): 0

Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00 Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00 Eccentricity of resultant shear forces in x-axis, e'vx (inch): 0.00 Eccentricity of resultant shear forces in y-axis, e'vy (inch): 0.00

<Figure 3>



8. Steel Strength of Anchor in Shear (Sec. 17.5.1)

V _{sa} (lb)	$\phi_{ m grout}$	ϕ	$\phi_{grout} \phi V_{sa}$ (lb)
7455	1.0	0.60	4473

10. Concrete Pryout Strength of Anchor in Shear (Sec. 17.5.3)

 $\phi V_{cpg} = \phi k_{cp} N_{cbg} = \phi k_{cp} (A_{Nc} / A_{Nco}) \Psi_{ec,N} \Psi_{ed,N} \Psi_{c,N} \Psi_{cp,N} N_b$ (Sec. 17.3.1 & Eq. 17.5.3.1b)

Kcp	A_{Nc} (in ²)	A_{Nco} (in ²)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	Ψc,N	$\Psi_{cp,N}$	N _b (lb)	ϕ	ϕV_{cpg} (lb)
1.0	141.71	49.70	1.000	1.000	1.000	1.000	3062	0.70	6111

11. Results

11. Interaction of Tensile and Shear Forces (Sec. D.7)?

Shear	Factored Load, V _{ua} (lb)	Design Strength, øV _n (lb)	Ratio	Status
Steel	50	4473	0.01	Pass
Pryout	200	6111	0.03	Pass (Governs)

1/2"Ø Titen HD, hnom:3.25" (83mm) meets the selected design criteria.





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Company:	Date:	
Engineer:	Page:	5/5
Project:	C	ity of Puyallup
Address:	Developm / IS	ant & Permitting Services
Phone:	Engine	ering Public Works
E-mail:	Fire	Traffic

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12. Warnings

- Designer must exercise own judgement to determine if this design is suitable.

- Refer to manufacturer's product literature for hole cleaning and installation instructions.