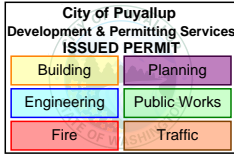
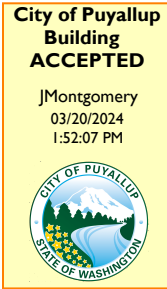


# BSE

Brien Structural Engineers, P.S.

FULL SIZED LEDGIBLE COLOR REPORTS  
IS REQUIRED TO BE PROVIDED BY THE  
PERMITTEE ON SITE FOR ALL  
INSPECTIONS



CENTERIS VOLTAGE PARK  
1023 39th Avenue South East  
Puyallup, WA 98374

UPS and Battery Room Build-Out  
Structural Calculations



Project Number 24201  
March 01, 2024

# **BSE**

**B**rienen **S**tructural **E**ngineers, P.S.

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**BSE**

**B**rienen **S**tructural **E**ngineers, P.S.

**INFILL STUD WALLS**  
**Design Criteria**

# BSE

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## Design Codes

Design Codes: International Building Code, 2018

ASCE 7-16

AISI Standards

AISI S100-16

AISI S200-12

AISI S210-12

AISI S211-12

AISI S212-12

AISI S240-12

## Vertical Loads on Ceiling Framing

Dead Load = 20 psf total

(includes weight of (4) layers of Gyp for 2-hour fire rating,

CFS joist weight, plywood wearing surface, and 5psf for MEP)

Live Load = 40 psf

(Access similar to Catwalks or Maintenance spaces)

<u>CEILING CONSTRUCTION: 2-HOUR RATING</u>	
2 psf/2ft =	2.5 psf PLYWOOD (3/4" ATTACHED w/ #10 SCREWS @ 12" o.c.)
	1.0 psf 8" STUFS, 13-MIL MIN 24" o.c. w/ SCREWS @ 12" o.c.
	2.5 psf 5/8" Gyp (1 <sup>st</sup> Layer)
	2.5 psf 5/8" Gyp (2 <sup>nd</sup> Layer)
	2.5 psf 5/8" Gyp (3 <sup>rd</sup> Layer)
1/2 psf/2ft =	1/4 psf HAT-SHAPED FLOORING PERP. TO JOISTS
	2.5 psf 5/8" Gyp (4 <sup>th</sup> Layer)
	5 psf MEP
	8/4 psf GIRDERS
	<u>19.5 psf</u>
	<u>w/ 20 psf DEAD LOAD</u>
	CEILING HEIGHT, Z = 12 FT
	STRUCTURE HEIGHT h =
	<u>ROOF LIVE LOAD = 40 psf</u>

# BSE

Brien Structural Engineers, P.S.

## Seismic Parameters

Site Class = D (Assumed)

$$S_{DS} = 1.006$$

Values per ASCE Hazards Report (See following pages)

### Seismic Coefficients from Table 13.5-1 (ASCE 7-16)

Table 13.5-1 Coefficients for Architectural Components

Architectural Component	$a_p^a$	$R_p$	$\Omega_0^b$
Interior nonstructural walls and partitions <sup>c</sup>			
Plain (unreinforced) masonry walls	1	1½	1½
All other walls and partitions	1	2½	2
Cantilever elements (unbraced or braced to structural frame below its center of mass)			
Parapets and cantilever interior nonstructural walls	2½	2½	2
Chimneys where laterally braced or supported by the structural frame	2½	2½	2
Cantilever elements (braced to structural frame above its center of mass)			
Parapets	1	2½	2
Chimneys	1	2½	2
Exterior nonstructural walls <sup>c</sup>	1 <sup>b</sup>	2½	2
Exterior nonstructural wall elements and connections <sup>b</sup>			
Wall element	1	2½	NA
Body of wall panel connections	1	2½	NA
Fasteners of the connecting system	1¼	1	1
Veneer			
Limited deformability elements and attachments	1	2½	2
Low-deformability elements and attachments	1	1½	2
Penthouses (except where framed by an extension of the building frame)	2½	3½	2
Ceilings			
All	1	2½	2
Cabinets			

<sup>a</sup>A lower value for  $a_p$  shall not be used unless justified by detailed dynamic analysis. The value for  $a_p$  shall not be less than 1. The value of  $a_p = 1$  is for rigid components and rigidly attached components. The value of  $a_p = 2½$  is for flexible components and flexibly attached components.

<sup>b</sup>Overstrength where required for nonductile anchorage to concrete and masonry. See Section 12.4.3 for seismic load effects including overstrength.

<sup>c</sup>Where flexible diaphragms provide lateral support for concrete or masonry walls and partitions, the design forces for anchorage to the diaphragm shall be as specified in Section 12.11.2.

# **BSE**

**B**rienen **S**tructural **E**ngineers, P.S.

## **Wall Design Criteria**

Ceiling height  $\leq 12'-0"$

Internal Pressure = 5 psf (ASD)

Maximum Deflection =  $L/240$  (Flexible Finishes)

Bearing Walls have Flexural and Axial Bracing  
at 72" oc (mid-ht) max

## **Joist and Girder Design Criteria**

See earlier page of Design Criteria for Loading

Maximum Live Load Deflection =  $L/360$

Maximum Total Deflection =  $L/240$

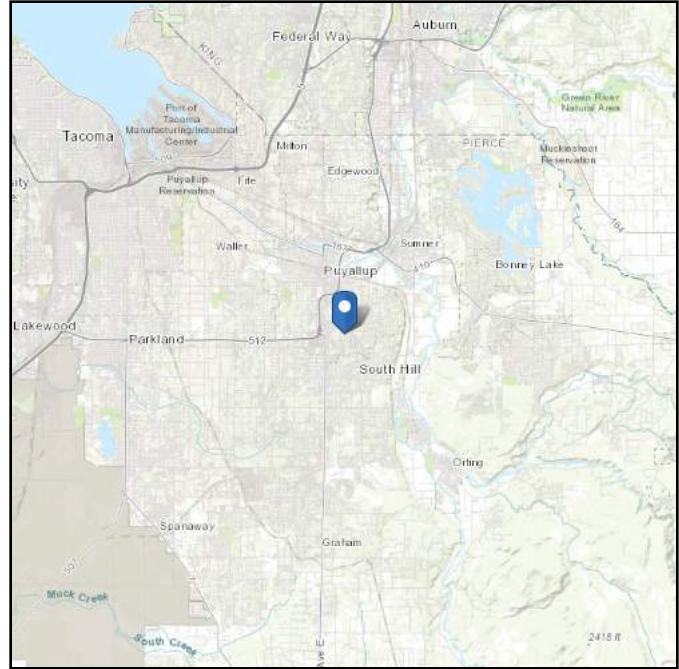


# ASCE Hazards Report

**Address:**  
1023 39th Ave SE  
Puyallup, Washington  
98374

**Standard:** ASCE/SEI 7-16  
**Risk Category:** II  
**Soil Class:** D - Default (see  
Section 11.4.3)

**Latitude:** 47.160853  
**Longitude:** -122.279318  
**Elevation:** 482.88472036372787 ft  
(NAVD 88)



## Wind

### Results:

Wind Speed	98 Vmph
10-year MRI	67 Vmph
25-year MRI	73 Vmph
50-year MRI	78 Vmph
100-year MRI	83 Vmph

Data Source: ASCE/SEI 7-16, Fig. 26.5-1B and Figs. CC.2-1–CC.2-4, and Section 26.5.2

Date Accessed: Mon Feb 05 2024

Value provided is 3-second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-16 Standard. Wind speeds correspond to approximately a 7% probability of exceedance in 50 years (annual exceedance probability = 0.00143, MRI = 700 years).

Site is not in a hurricane-prone region as defined in ASCE/SEI 7-16 Section 26.2.



**Site Soil Class:** D - Default (see Section 11.4.3)

**Results:**

$S_s$ :	1.257	$S_{D1}$ :	N/A
$S_1$ :	0.434	$T_L$ :	6
$F_a$ :	1.2	PGA :	0.5
$F_v$ :	N/A	PGA <sub>M</sub> :	0.6
$S_{MS}$ :	1.509	$F_{PGA}$ :	1.2
$S_{M1}$ :	N/A	$I_e$ :	1
$S_{DS}$ :	1.006	$C_v$ :	1.351

Ground motion hazard analysis may be required. See ASCE/SEI 7-16 Section 11.4.8.

**Data Accessed:** Mon Feb 05 2024

**Date Source:** [USGS Seismic Design Maps](#)



The ASCE Hazard Tool is provided for your convenience, for informational purposes only, and is provided “as is” and without warranties of any kind. The location data included herein has been obtained from information developed, produced, and maintained by third party providers; or has been extrapolated from maps incorporated in the ASCE standard. While ASCE has made every effort to use data obtained from reliable sources or methodologies, ASCE does not make any representations or warranties as to the accuracy, completeness, reliability, currency, or quality of any data provided herein. Any third-party links provided by this Tool should not be construed as an endorsement, affiliation, relationship, or sponsorship of such third-party content by or from ASCE.

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# BSE

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## Seismic Forces

## Wall Type Infill Walls

### Wall Seismic Weight, W

### PSF

- Metal Stud Framing
- (4) Layers 5/8" Gypsum Wall Board  
(Multiply weight by actual layers of GWB.)
- Acoustic Insulation
- 

1.5

10

2

Total = 14 PSF

### Wall & Fastener Seismic Force

$$a_p = \frac{1}{1.006} \quad R_p = \frac{2.5}{1} \quad z/h = \frac{1}{1}$$

$$F_d = \frac{0.4a_p S_{DS} W I_p}{R_p} \left(1 + 2 \frac{z}{h}\right)$$

$$F_d = 0.483W \quad (\text{LRFD})$$

$$E_{ASD} = 0.7F_d = 0.338W \quad (\text{ASD})$$

ASD  
Force = 4.6 PSF

### Fastener - Anchorage to Concrete

$$a_p = \frac{1}{1.006} \quad R_p = \frac{2.5}{1} \quad \Omega_o = \frac{2.5}{1}$$

$$F_d = \Omega_o \frac{0.4a_p S_{DS} W I_p}{R_p} \left(1 + 2 \frac{z}{h}\right)$$

$$F_d = 1.207W \quad (\text{LRFD})$$

$$E_{ASD} = 0.7F_d/1.2^* = 0.845W \quad (\text{ASD})$$

ASD  
Force = 11.4 PSF

# **BSE**

**B**rienen **S**tructural **E**ngineers, P.S.

**ANCHOR AND CONNECTOR**  
**DESIGN INFORMATION**

**Track Connection Distances - Based on Connector Capacities**

PRESSURE    MAX HEIGHT

For 5.0 psf (GWB finishes)

Max Considered Height

13.50	Track Demand =	$(Ht)/2 * 5\text{psf} =$	33.8 plf		
	Connection to Concrete**	MIN SHOTPIN CAPACITY $v =$	120lbs/anchor	spacing $\leq$	18.7 in @ (11.4psf)
	Connection to Steel	MIN SCREW CAPACITY $v =$	230lbs/anchor	spacing $\leq$	30.0 in

\*\* Where seismic forces control anchorage, Fastener spacing calculated includes Overstrength Reduction

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CHECK TRACK FOR MAX FASTENER SPACING

 $S_{max}$  must meet  $M_{A400T125-33} = 3.97 \text{ k}\cdot\text{in}$  $V_{A400T125-33} = 940^\#$ 

$$\text{UNIFORM LOAD (DEMAND)} = 5 \text{ psf} * (12'-0") / 2 \\ = 30 \text{ plf}$$

$$\text{for } 36" \text{ o.c. SPACING, } M_{\text{DEMAND}} = \frac{wL^2}{8} = \frac{(30 \text{ plf})(36")^2}{8} = 4.86 \text{ k}\cdot\text{in}$$

THIS IS TOO LARGE!

→ if SPACING IS 30" o.c. →  $M_{\text{DEMAND}} = 3.375 \text{ k}\cdot\text{in}$

$$\text{Check Shear} = V_{\text{DEMAND}} = 30 \text{ plf} * \frac{30' \text{ o.c.} * 1 \text{ ft}}{2 * 12'} = 37.5^\#$$

✓  
≤ 940#  
OK

PRCTI20240333

TABLE 2—ALLOWABLE LOADS FOR FASTENERS DRIVEN INTO STEEL<sup>1,2,3,4</sup>

FASTENER	SHANK DIAMETER (INCH)	ALLOWABLE LOADS (lbf)											
		1/8		3/16		1/4		3/8		1/2		3/4	
Steel Thickness (inch):		Tension	Shear	Tension	Shear	Tension	Shear	Tension	Shear	Tension	Shear	Tension	Shear
X-S13 THP	0.145	140 <sup>10</sup>	300	300 <sup>10</sup>	450	300 <sup>10</sup>	450	300 <sup>10</sup>	450	--	--	--	--
X-S16P8TH	0.145	--	--	225 <sup>10</sup>	420	225 <sup>10</sup>	430	225 <sup>10</sup>	430	225 <sup>10</sup>	430	--	--
X-EGN14 X-S 14 B3 X-S 14 G3	0.118	140	230	220	245	225	290	280 <sup>6</sup>	330 <sup>6</sup>	280 <sup>6</sup>	330 <sup>6</sup>	280 <sup>6</sup>	330 <sup>6</sup>
X-EGN14 <sup>5</sup> X-S 14 B3 <sup>5</sup> X-S 14 G3 <sup>5</sup>	0.118	--	--	220	295	260	355	280 <sup>6</sup>	385 <sup>6</sup>	280 <sup>6</sup>	385 <sup>6</sup>	280 <sup>6</sup>	385 <sup>6</sup>
X-GHP## X-P ## G3 X-P ## B3	0.118	125 <sup>10</sup>	230	170 <sup>10</sup>	245	200 <sup>10</sup>	230	250 <sup>10</sup>	255	--	--	--	--
X-P 17 G2 <sup>7</sup> X-P 20 G2 <sup>7</sup>	0.118	--	--	140 <sup>10</sup>	220	180 <sup>8</sup>	200 <sup>8</sup>	225 <sup>6</sup>	220 <sup>6</sup>	--	--	--	--
X-P 14 G2 <sup>7</sup>	0.118	--	--	--	--	215 <sup>8</sup>	290 <sup>8</sup>	150 <sup>9</sup>	195 <sup>9</sup>	130 <sup>9</sup>	150 <sup>9</sup>	130 <sup>9</sup>	150 <sup>9</sup>

For SI: 1 inch = 25.4 mm, 1 ksi = 6.89 MPa, 1 lbf = 4.4 N.

X-GHP/X-P B3 EMBED CAPACITY TO STEEL

- <sup>1</sup>Unless otherwise noted, fasteners must be driven to where the full length of the point of the fastener penetrates through the steel base material.
- <sup>2</sup>Unless otherwise noted, steel base material must have minimum yield and tensile strengths ( $F_y$  and  $F_u$ ) equal to 36 ksi and 58 ksi, respectively.
- <sup>3</sup>Unless otherwise noted, allowable loads are applicable to static loads and seismic loads in accordance with Section 4.1.
- <sup>4</sup>Fastener spacing must be a minimum of 1.0 inch and edge distance must be a minimum of 0.50 inch.
- <sup>5</sup>Steel base material must have minimum yield and tensile strengths ( $F_y$  and  $F_u$ ) equal to 50 ksi and 65 ksi, respectively.
- <sup>6</sup>Fastener point penetration through the steel is not necessary, provided a minimum embedment of 0.320 inch is achieved.
- <sup>7</sup>Tabulated loads for this fastener apply to static load conditions only. For seismic loading, allowable loads must be limited in accordance with Section 4.1.5, Item 3.
- <sup>8</sup>Full fastener point penetration through the steel is not necessary, provided a minimum point penetration of 0.08 inch is achieved.
- <sup>9</sup>Fastener point penetration through the steel is not necessary, provided a minimum embedment of 0.25 inch is achieved.
- <sup>10</sup>For steel-to-steel connections designed in accordance with Section 4.1.4, the tabulated allowable load may be increased by a factor of 1.25, and the design strength may be taken as the tabulated allowable load multiplied by a factor of 2.0.

PRCTI20240333

TABLE 3—ALLOWABLE LOADS FOR FASTENERS DRIVEN INTO NORMALWEIGHT CONCRETE<sup>1,2,3</sup>

FASTENER	SHANK DIAMETER (inch)	MINIMUM EMBEDMENT DEPTH (inches)	ALLOWABLE LOADS (lbf)					
			2,000 psi		4,000 psi		6,000 psi	
Concrete Compressive Strength:			Tension	Shear	Tension	Shear	Tension	Shear
Load Direction:			Tension	Shear	Tension	Shear	Tension	Shear
X-C ## (Black Collated Strip or Guidance Washer)	0.138	3/4	45	75	65	105	95	195
		1	85	150	160	200	105	270
		1 1/4	130	210	270	290	165	325
		1 1/2	175	260	270	360	--	--
X-C ## (White Collated Strip or Guidance Washer)	0.138	3/4	45	75	60	105	--	--
		1	85	150	90	200	--	--
		1 1/4	130	210	130	290	--	--
X-C22 P8TH (Black Collated Strip or Guidance Washer)	0.138	3/4	55	130	90	170	100	200
X-C22 P8TH (White Collated Strip or Guidance Washer)	0.138	3/4	55	130	90	170	--	--
X-GN (except for X-GN 39)	0.118	3/4	95	120	95	120	--	--
		1	115	220	115	220	--	--
X-GN39 X-C 39 G2 X-C 39 G3	0.101	5/8	50	80	50	80	--	--
		1	60	100	60	100	--	--
X-GHP## X-P 17 G2, X-P 20 G2 X-P ## G3 X-P ## B3	0.118	5/8	--	--	50	120	50	90
		3/4	80	120	--	--	--	--
X-C ## G2 (except for X-C 39 G2) X-C 36 B3	0.108	3/4	110	190	110	190	110	190
X-C ## G3 (except for X-C 39 G3) X-C ## B3 (except for X-C 36 B3)	0.118	3/4	110	190	110	190	110	190

For SI: 1 inch = 25.4 mm, 1 psi = 6.89 kPa, 1 lbf = 4.4 N.

<sup>1</sup>Fasteners must not be driven until the concrete has reached the designated minimum compressive strength, or the minimum compressive strength specified in the applicable code, whichever is greater.

<sup>2</sup>Concrete thickness must be a minimum of 3 times the embedment depth of the fastener. Fastener spacing must be a minimum of 4 inches and edge distance must be a minimum of 3 inches.

<sup>3</sup>The fasteners listed in the table above may be used for static load conditions and for the seismic load conditions described in Section 4.1.5, as applicable. The tabulated allowable loads apply to static load conditions. For seismic load conditions, the allowable loads must be limited in accordance with Section 4.1.5, Items 2 and 4, as applicable.

3(5/8") = 1 7/8" < 2 1/2" OK

X-GHP/X-P B3 EMBED  
CAPACITY TO CONCRETE

PRCTI20240333

TABLE 1—FASTENER DESCRIPTION AND APPLICATIONS

FASTENER <sup>1</sup>	FASTENER DESCRIPTION	SHANK TYPE	SHANK DIAMETER [inch (mm)]	HEAD DIAMETER [inch (mm)]	MAXIMUM POINT LENGTH [inch (mm)]	MINIMUM EFFECTIVE SHANK LENGTH [inch (mm)]	FASTENER COATING	APPLICABLE BASE MATERIAL	APPLICABLE LOAD TABLES
X-U ##	Universal Powder Actuated Fastener	Knurled, straight	0.157 (4.0)	0.323 (8.2)	0.433 (11.0)	See Footnote 2	ASTM B633, SC1, Type III	Steel	2, 7
								Concrete	3, 4
								Conc.-filled deck	5
								CMU	6
X-U 15	Powder Actuated Fastener	Knurled, stepped	0.145 (3.7)	0.323 (8.2)	0.413 (10.5)	0.61 (15.5)	ASTM B633, SC1, Type III	Steel	2
X-P ##	Powder Actuated Fastener	Smooth straight	0.157 (4.0)	0.323 (8.2)	0.524 (13.3)	See Footnote 3	ASTM B633, SC1, Type III	Concrete	3
								Conc.-filled deck	5
								CMU	6

For SI: 1 inch = 25.4 mm.

<sup>1</sup>## denotes numbers used in fastener designation to represent nominal fastener length in mm, e.g. X-U 27 has a nominal shank length of 27 mm.

<sup>2</sup>For fastener length of 16 mm, the minimum effective shank length is 14.8 mm (0.58 inch). For longer fasteners, the minimum effective shank length can be calculated in terms of the designated length as (##-0.5) in mm and (##-0.5)/25.4 in inches.

<sup>3</sup>The minimum effective shank length can be calculated in terms of the designated length as (##-1) in mm and (##-1)/25.4 in inches.

TABLE 2—ALLOWABLE LOADS FOR FASTENERS DRIVEN INTO STEEL<sup>1,2,6</sup>

FASTENER DESCRIPTION	FASTENER	SHANK DIAMETER (inch)	ALLOWABLE LOADS (lbf)									
			<sup>3</sup> / <sub>16</sub>		<sup>1</sup> / <sub>4</sub>		<sup>3</sup> / <sub>8</sub>		<sup>1</sup> / <sub>2</sub>		≥ <sup>3</sup> / <sub>4</sub>	
Steel Thickness (inch):			Tension	Shear	Tension	Shear	Tension	Shear	Tension	Shear	Tension	Shear
Load Direction:			Tension	Shear	Tension	Shear	Tension	Shear	Tension	Shear	Tension	Shear
Universal Knurled Shank	X-U	0.157	500 <sup>7</sup>	720	775 <sup>7</sup>	720	935	720	900	720	350 <sup>4</sup>	375 <sup>4</sup>
											275 <sup>3</sup>	350 <sup>3</sup>
Universal Knurled Shank	X-U 15	0.145	155	400	230	395	420	450	365 <sup>5</sup>	500 <sup>5</sup>	365 <sup>5</sup>	400 <sup>5</sup>

For SI: 1 inch = 25.4 mm, 1 lbf = 4.4 N; 1 ksi = 6.9 MPa.

<sup>1</sup>Allowable load capacities are based on base steel with a minimum yield strength ( $F_y$ ) of 36 ksi and a minimum tensile strength ( $F_u$ ) of 58 ksi.

<sup>2</sup>The fasteners must be driven to where the point of the fastener penetrates through the steel base material, unless otherwise noted.

<sup>3</sup>Based upon a minimum point penetration of <sup>3</sup>/<sub>8</sub> inch.

<sup>4</sup>Based upon a minimum point penetration of <sup>1</sup>/<sub>2</sub> inch.

<sup>5</sup>Based upon a minimum point penetration of <sup>15</sup>/<sub>32</sub> inch.

<sup>6</sup>Allowable loads are applicable to static and seismic loads in accordance with Section 4.1.

<sup>7</sup>For steel-to-steel connections designed in accordance with Section 4.1.6 for static loads only, the tabulated allowable load may be increased by a factor of 1.25, and the design strength maybe taken as the tabulated allowable load multiplied by a factor of 2.0.

X-U EMBED CAPACITY TO STEEL

PRCTI20240333

TABLE 3—ALLOWABLE LOADS FOR FASTENERS DRIVEN INTO NORMAL-WEIGHT CONCRETE<sup>1,2,4</sup>

FASTENER DESCRIPTION	FASTENER	SHANK DIAMETER (inch)	MINIMUM EMBEDMENT DEPTH (inches)	ALLOWABLE LOADS (lbf)							
				Concrete Compressive Strength:				2500 psi		4000 psi	
Load Direction:				Tension	Shear	Tension	Shear	Tension	Shear	Tension	Shear
Universal Knurled Shank	X-U	0.157	3/4	100	125	100	125	105	205	—	—
			1	165	190	170	225	110 <sup>3</sup>	280 <sup>3</sup>	—	—
			1 1/4	240	310	280	310	180	425	—	—
			1 1/2	275	420	325	420	—	—	—	—
Smooth Shank	X-P	0.157	3/4 <sup>5</sup>	100	155	100	175	105	205	135	205
			1 <sup>5</sup>	165	220	180	225	150	300	150	215
			1 1/4 <sup>5</sup>	240	310	280	310	180	425	—	—
			1 1/2 <sup>5</sup>	310	420	—	—	—	—	—	—

For SI: 1 inch = 25.4 mm, 1 lbf = 4.4 N, 1 psi = 6895 Pa.

<sup>1</sup>Unless otherwise noted, values apply to normal weight cast-in-place concrete. Fasteners must not be driven until the concrete has reached the designated minimum compressive strength.

<sup>2</sup>Unless otherwise noted, concrete thickness must be a minimum of 3 times the embedment depth of the fastener.

<sup>3</sup>This allowable load value for the X-U fastener also applies to normal weight hollow core concrete slabs with  $f_c$  of 6600 psi and minimum dimensions shown in Figure 7, when installed in accordance with Section 4.2.4.

<sup>4</sup>The fasteners listed in the table above may be used for static load conditions and for the seismic load conditions described in Section 4.1.6, as applicable. The tabulated allowable loads apply to static load conditions. For seismic load conditions, the allowable loads must be limited in accordance with Section 4.1.6, Items 2 and 3, as applicable.

<sup>5</sup>Applies to fastening of cold-formed steel up to 54 mil thick using the X-P 22, X-P 27, X-P 34 and X-P 40 fasteners, respectively, for the 3/4, 1, 1 1/4 and 1 1/2 inch embedment depths.

$3(3/4") = 2 1/4" < 2 1/2" \text{ OK}$

X-U/X-P EMBED CAPACITY TO CONCRETE

TABLE 4—ALLOWABLE LOADS FOR FASTENERS DRIVEN INTO NORMAL-WEIGHT CONCRETE USING DX-KWIK<sup>1,2,3,4</sup>

FASTENER DESCRIPTION	FASTENER	SHANK DIAMETER (inch)	MINIMUM EMBEDMENT (inches)	ALLOWABLE LOADS (lbf)			
				4,000 psi		6,000 psi	
Concrete Compressive Strength:				Tension	Shear	Tension	Shear
Universal Knurled Shank	X-U 47 P8 w/ DX-KWIK	0.157	1 1/2	395	405	360	570

For SI: 1 inch = 25.4 mm, 1 lbf = 4.4 N, 1 psi = 6895 Pa.

<sup>1</sup>X-U Fastener is installed using the DX-KWIK drilled pilot hole installation procedure described in Section 4.2.5.

<sup>2</sup>Pilot holes must not be drilled until the concrete has reached the designated minimum compressive strength.

<sup>3</sup>Concrete thickness must be a minimum of 3 times the embedment depth of the fastener.

<sup>4</sup>The fasteners listed in the table above may be used for static load conditions and for the seismic load conditions described in Section 4.1.6, as applicable. The tabulated allowable loads apply to static load conditions. For seismic load conditions, the allowable loads must be limited in accordance with Section 4.1.6, Items 2 and 3, as applicable.





# Screw Capacities

## Table Notes

- Capacities based on AISI S100 Section E4.
- When connecting materials of different steel thicknesses or tensile strengths, use the lowest values. Tabulated values assume two sheets of equal thickness are connected.
- Capacities are based on Allowable Strength Design (ASD) and include safety factor of 3.0.
- Where multiple fasteners are used, screws are assumed to have a center-to-center spacing of at least 3 times the nominal diameter (d).
- Screws are assumed to have a center-of-screw to edge-of-steel dimension of at least 1.5 times the nominal diameter (d) of the screw.
- Pull-out capacity is based on the lesser of pull-out capacity in sheet closest to screw tip or tension strength of screw.
- Pull-over capacity is based on the lesser of pull-over capacity for sheet closest to screw header or tension strength of screw.
- Values are for pure shear or tension loads. See AISI Section E4.5 for combined shear and pull-over.
- Screw Shear (Pss), tension (Pts), diameter, and head diameter are from CFSEI Tech Note (F701-12).
- Screw shear strength is the average value, and tension strength is the lowest value listed in CFSEI Tech Note (F701-12).
- Higher values for screw strength (Pss, Pts), may be obtained by specifying screws from a specific manufacturer.

Allowable Screw Connection Capacity (lbs)

Thickness (Mils)	Design Thickness	Fy Yield (ksi)	Fu Tensile (ksi)	#6 Screw (Pss = 643 lbs, Pts = 419 lbs)			#8 Screw (Pss = 1278 lbs, Pts = 586 lbs)			#10 Screw (Pss = 1644 lbs, Pts = 1158 lbs)			#12 Screw (Pss = 2330 lbs, Pts = 2325 lbs)			¼" Screw (Pss = 3048 lbs, Pts = 3201 lbs)		
				0.138" dia, 0.272" Head			0.164" dia, 0.272" Head			0.190" dia, 0.340" Head			0.216" dia, 0.340" Head			0.250" dia, 0.409" Head		
				Shear	Pull-Out	Pull-Over	Shear	Pull-Out	Pull-Over	Shear	Pull-Out	Pull-Over	Shear	Pull-Out	Pull-Over	Shear	Pull-Out	Pull-Over
18	0.0188	33	33	44	24	84	48	29	84	52	33	105	55	38	105	60	44	127
27	0.0283	33	33	82	37	127	89	43	127	96	50	159	102	57	159	110	66	191
30	0.0312	33	33	95	40	140	103	48	140	111	55	175	118	63	175	127	73	211
33	0.0346	33	45	151	61	140	164	72	195	177	84	265	188	95	265	203	110	318
43	0.0451	33	45	214	79	140	244	94	195	263	109	345	280	124	345	302	144	415
54	0.0566	33	45	214	100	140	344	118	195	370	137	386	394	156	433	424	180	521
68	0.0713	33	45	214	125	140	426	149	195	523	173	386	557	196	545	600	227	656
97	0.1017	33	45	214	140	140	426	195	195	548	246	386	777	280	775	1,016	324	936
118	0.1242	33	45	214	140	140	426	195	195	548	301	386	777	342	775	1,016	396	1,067
54	0.0566	50	65	214	140	140	426	171	195	534	198	386	569	225	625	613	261	752
68	0.0713	50	65	214	140	140	426	195	195	548	249	386	777	284	775	866	328	948
97	0.1017	50	65	214	140	140	426	195	195	548	356	386	777	405	775	1,016	468	1,067
118	0.1242	50	65	214	140	140	426	195	195	548	386	386	777	494	775	1,016	572	1,067



## SCREW ALLOWABLE LOADS & UL ASSEMBLIES

### SCREW ALLOWABLE LOADS (LBS.)

MODEL NO.	DESIGN THICKNESS (in)	MIN. THICKNESS (in)	FY YIELD (ksi)	FU TENSILE (ksi)	#6 SCREW (0.138" dia; 0.25" head)		#8 SCREW (0.164" Dia; 0.3125" Head)		#10 SCREW (0.190" Dia; 0.340" Head)		#12 SCREW (0.216" Dia; 0.340" Head)	
					SHEAR	TENSION	SHEAR	TENSION	SHEAR	TENSION	SHEAR	TENSION
VIPER-X-18	0.0188	0.0179	57	65	142 <sup>1</sup>	48	150 <sup>1</sup>	57	164 <sup>1</sup>	66	109	75
VIPER-X-22	0.0235	0.0223	57	65	174 <sup>1</sup>	60	184 <sup>1</sup>	71	236 <sup>1</sup>	82	152	93

#### Notes:

1. Shear values are tested per AISI S100-12 and S905 procedure.
2. Capacities are based on section E4 of the AISI S100-12 Specification.
3. Capacities are based on Allowable Strength Design (ASD).
4. Screw pull-out capacities are based on listed head diameter.
5. Two sheets of equal thickness and tensile strength are assumed in tabulated values.
6. When materials of different steel thickness and tensile strength are connected, use the lowest value for shear capacity (tilting and bearing), for pull-out capacity use sheet closest to screw tip and for pull-over capacity use sheet closest to screw head.
7. Where multiple fasteners are used, screws are assumed to have a center-to-center spacing of at least 3 times the nominal diameter.
8. Screws are assumed to have a center-of-screw to edge-of-steel dimension of at least 1.5 times the nominal diameter of the screw.
9. When screws are subjected to combination of shear and tension forces, interaction equation of AISI S100-12 Specification section E4.5 shall be used.

### UL ASSEMBLIES – VIPER-X FIRE TESTING DATA (ASTM E119)

UL DESIGN NO.	VIPER-X (DESIGN THICKNESS)	WALL RATING
U411	18 MIL	2 HR
U412	18 MIL	2 HR
U419	18 MIL	1, 2, 3 or 4 HR
U435	18 MIL	3 or 4 HR
U465	18 MIL	1 HR Chase
V417	18 MIL	1 HR
V435	18 MIL	1 HR
V448	18 MIL	1 HR
V469	18 MIL	1 or 2 HR Chase
V486	18 MIL	1, 2, or 2-1/2 HR
V489	18 MIL	1, 2, 3 or 4 HR
V496	18 MIL	1 or 2 HR Chase
V498	18 MIL	1, 2, 3 or 4 HR
W411	18 MIL	1/2 or 1 HR
W424	18 MIL	1/2 or 1 HR
W433	18 MIL	1/2 HR
W440	18 MIL	1, 2, 3 or 4 HR

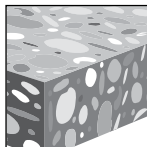


### 3.3.20 KWIK-CON+ CONCRETE AND MASONRY SCREW

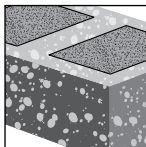
#### PRODUCT DESCRIPTION

##### KWIK-CON+ concrete and masonry screw anchors

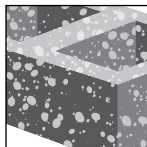
Anchor System	Features and Benefits
<div style="display: flex; flex-direction: column; align-items: center;">  <p data-bbox="563 730 775 751">KWIK-CON+ fastener</p>  <p data-bbox="563 1266 858 1323">KWIK-CON+ drive tool and installation accessories</p> </div>	<ul style="list-style-type: none"> <li>• Zinc coating with proprietary finish that exceeds 1000 hours of protection from red rust per ASTM B117</li> <li>• Salt spray testing per ASTM G85</li> <li>• Coating is more durable than zinc plating alone</li> <li>• Base material specific carbide tipped bits optimize performance in concrete or masonry</li> <li>• Torx Hex washer head for fast secure installations into base material</li> <li>• Torx or Phillips flat head for countersunk applications</li> <li>• Load data available for installations in concrete, grout-filled and hollow concrete masonry units (CMU) and brick</li> <li>• Available in AISI Type 410 Stainless Steel</li> </ul>



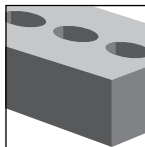
Uncracked concrete



Grout-filled concrete masonry



Ungrouted concrete masonry



Brick

Approvals/Listings	
Metro-Dade County	NOA 19-1113.04

**Table 1 – Material Properties**

Property	Carbon Steel		Stainless Steel	
	Fastener Diameter (inches)		Fastener Diameter (inches)	
	3/16	1/4	3/16	1/4
Minimum Tensile Strength (ksi)	150		130	
Minimum Yield Strength (ksi)	120		105	
Coating	Zinc with organic top coat		N/A	

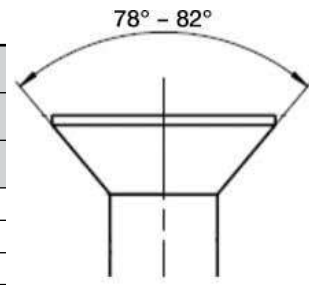


Figure 1 – Flathead KWIK CON+ Head Angle

**Table 2 – Physical Dimensions**

Characteristic	Nominal anchor diameter (inches)					
	3/16			1/4		
Head Style	Tapered Flat Head	Tapered Flat Head	5/16-in. Hex Washer	Tapered Flat Head	Tapered Flat Head	5/16-in. Hex Washer
Internal recess	#3 Phillips	T-25 TORX	T-25 TORX	#3 Phillips	T-27 TORX	T-25 TORX
Maximum Head Diameter (inches)	0.507	0.385	0.433	0.507	0.507	0.433
Major Thread Diameter (inches)	0.217			0.283		
Minor Diameter (inches)	0.145			0.190		
Shank Diameter (inches)	0.170			0.224		

## INSTALLATION

**Table 3 – KWIK CON+ Installation Specifications**

Setting information	Symbol	Nominal anchor diameter (inches)			
		3/16		1/4	
Embedment (inches)	$h_{nom}$	1	1-3/4	1	1-3/4
Nominal drill bit diameter (inches) <sup>1</sup>	$d_{bit}$	3/16		1/4	
Minimum fixture hole diameter (inches)	$d_h$	1/4		5/16	
Minimum hole depth (inches)	$h_o$	1-1/4	2	1-1/4	2
Minimum member thickness (inches)	$h_{min}$	2-1/2	3-1/4	2-1/2	3-1/4
Minimum anchor spacing (inches)	$s_{min}$	2-1/4		2-1/2	
Critical anchor spacing (inches)	$s_{cr}$	3	4	3	4
Minimum edge distance (inches)	$c_{min}$	1-1/8		1-1/2	
Critical edge distance (inches)	$c_{cr}$	2-1/2	3-1/2	2-1/2	3-1/2

<sup>1</sup> Requires matched tolerance drill bit from Hilti, TKC drill bits for concrete, TKB drill bits for other materials.

**Table 4 – Load adjustment factors for Hilti KWIK CON+ screw anchors in concrete**

Load adjustment factors for anchor spacing $f_A$						Load adjustment factors for edge distance $f_R$									
Tension/Shear loads						Tension				Shear					
Embedment (inches)		1	1-3/4	1	1-3/4	Embedment (inches)		1	1-3/4	1	1-3/4	1	1-3/4	1	1-3/4
Spacing (s)		Anchor diameter				Edge Distance		Anchor Diameter				Anchor Diameter			
in.	(mm)	3/16		1/4		in.	(mm)	3/16		1/4		3/16		1/4	
2-1/4	(57)	0.80	0.80			1-1/8	(29)	0.80	0.80			0.30	0.30		
2-1/2	(64)	0.87	0.83	0.80	0.80	1-1/4	(32)	0.82	0.81			0.36	0.34		
2-3/4	(70)	0.93	0.86	0.90	0.86	1-1/2	(38)	0.85	0.83	0.80	0.80	0.49	0.41	0.30	0.30
3	(76)	1.00	0.89	1.00	0.89	1-3/4	(44)	0.89	0.85	0.85	0.83	0.62	0.48	0.48	0.39
3-1/4	(83)		0.91		0.91	2	(51)	0.93	0.87	0.90	0.85	0.75	0.56	0.65	0.48
3-1/2	(89)		0.94		0.94	2-1/4	(57)	0.96	0.89	0.95	0.88	0.87	0.63	0.83	0.56
3-3/4	(95)		0.97		0.97	2-1/2	(64)	1.00	0.92	1.00	0.90	1.00	0.71	1.00	0.65
4	(102)		1.00		1.00	3	(76)		0.96		0.95		0.85		0.83
						3-1/2	(89)		1.00		1.00		1.00		1.00

<sup>1</sup> Reduction factors are multiplicative and linear interpolation between  $s_{cr}$  and  $s_{min}$ ,  $c_{cr}$  and  $c_{min}$  is permitted.

## DESIGN INFORMATION IN CONCRETE PER ALLOWABLE STRESS DESIGN

**Table 5 — Tension and shear allowable loads in concrete** <sup>1,2,3</sup>

Nominal anchor diameter (in.)	Nominal embedment in. (mm)	$f'_c = 2,000$ psi		$f'_c = 4,000$ psi		$f'_c = 6,000$ psi	
		Tension lb (kN)	Shear lb (kN)	Tension lb (kN)	Shear lb (kN)	Tension lb (kN)	Shear lb (kN)
3/16	1 (25)	100 (0.4)	260 (1.2)	125 (0.6)	260 (1.2)	185 (0.8)	280 (1.3)
3/16	1-3/4 (44)	275 (1.2)	260 (1.2)	295 (1.3)	265 (1.2)	325 (1.5)	300 (1.3)
1/4	1 (25)	190 (0.9)	325 (1.4)	240 (1.1)	390 (1.7)	275 (1.2)	540 (2.4)
1/4	1-3/4 (44)	425 (1.9)	560 (2.5)	475 (2.1)	600 (2.8)	525 (2.3)	600 (2.7)

- Screws installed in holes drilled with Hilti TKC carbide bits.
- Allowable loads are based on a factor of safety of 4.
- Apply spacing and edge distance reduction factors in Table 4 as needed.

**Table 6 — Tension and shear ultimate loads in concrete**<sup>1</sup>

Nominal anchor diameter (in.)	Nominal embedment in. (mm)	$f'_c = 2,000$ psi		$f'_c = 4,000$ psi		$f'_c = 6,000$ psi	
		Tension lb (kN)	Shear lb (kN)	Tension lb (kN)	Shear lb (kN)	Tension lb (kN)	Shear lb (kN)
3/16	1 (25)	400 (1.8)	1,050 (4.7)	500 (2.2)	1,050 (4.7)	750 (3.3)	1,150 (5.1)
3/16	1-3/4 (44)	1,100 (4.9)	1,050 (4.7)	1,180 (5.3)	1,070 (4.8)	1,300 (5.8)	1,200 (5.3)
1/4	1 (25)	760 (3.4)	1,300 (5.8)	970 (4.3)	1,575 (7.0)	1,100 (4.9)	2,175 (9.7)
1/4	1-3/4 (44)	1,700 (7.6)	2,250 (10.0)	1,900 (8.5)	2,400 (11.3)	2,100 (9.34)	2,400 (10.7)

- Screws installed in holes drilled with TKC bits.

**Table 7 — Tension and shear allowable loads in grout-filled and hollow concrete masonry units (CMU)** <sup>1,2,3,4,5</sup>

Nominal anchor diameter (in.)	Nominal embedment in. (mm)	Tension lb (kN)	Shear lb (kN)
3/16	1 (25)	150 (0.7)	225 (1.0)
3/16	1-3/4 (44)	290 (1.3)	300 (1.3)
1/4	1 (25)	165 (0.7)	275 (1.2)
1/4	1-3/4 (44)	310 (1.4)	400 (1.8)

- All values for anchors installed in grout-filled or hollow concrete masonry (CMU) with a minimum prism strength of 1,500 psi. CMU may be lightweight, medium-weight or normal-weight conforming to ASTM C90.
- Screws installed in holes drilled with TKB bits.
- Allowable loads calculated using a factor of safety of 4.
- Installation in the mortar joints is outside the scope of the published data.
- $C_{min}$ ,  $S_{min}$  equals 4 inches

**Table 8 — Tension and shear allowable loads in brick** <sup>1,2,3,4,5</sup>

Nominal anchor diameter (in.)	Nominal embedment in. (mm)	Tension lb (kN)	Shear lb (kN)
3/16	1 (25)	125 (0.6)	235 (1.0)
3/16	1-3/4 (44)	350 (1.6)	300 (1.3)
1/4	1 (25)	205 (0.9)	415 (1.8)
1/4	1-3/4 (44)	350 (1.6)	500 (2.2)

- This test was performed on individual specimens of ASTM C62 common brick. Due to the wide variations encountered in the compressive strength of brick, these values should be considered guide values.
- Allowable loads are based on a factor of safety of 4.
- Installation in the mortar joints is outside the scope of the published data.
- KWIK CON+ installed with TKB bits.
- $C_{min}$ ,  $S_{min}$  equals 4 inches

Load values are for anchors installed a minimum of sixteen diameters on center and a minimum edge distance of sixteen diameters. Anchor spacing may be reduced to twelve diameters provided loads are reduced by 20 percent. Edge distance may be reduced to six diameters provided loads are reduced by 20 percent in tension and 70 percent in shear.

### Combined shear and tension loading

$$\left( \frac{N_d}{N_{rec}} \right) + \left( \frac{V_d}{V_{rec}} \right) \leq 1.0$$

## INSTALLATION INSTRUCTIONS

Installation Instructions For Use (IFU) / Operating Instructions (OI) throughout the document are included with each product package. They can also be viewed or downloaded online at [www.hilti.com](http://www.hilti.com). Because of the possibility of changes, always verify that downloaded IFU are current when used. Proper installation is critical to achieve full performance. Training is available on request. Contact Hilti Technical Services for applications and conditions not addressed in the (IFU)/Operating Instructions (OI).

c) The metal-critical joint may fail in one of two ways. Failure occurs when the resistance of the screw head to embedment is greater than the resistance of the metal to lateral and/or withdrawal load, and the screw tears away from the metal framing. Failure also occurs when thin metal in a metal-to-plywood joint crushes or tears away from the screw.

Tables 1 and 2 present ultimate lateral loads for wood- and sheet-metal-screw connections in plywood-and-metal joints. Loaded end distance in these tests was one inch. Plywood face grain was parallel to the load since this direction yields the lowest lateral loads when the joint is plywood-critical. All wood-screw specimens were tested with a 3/16-in.-thick steel side plate, and values should be modified if thinner steel is used.

DIVIDE BY 5 SAFETY FACTOR FOR ALLOWABLE LOADS

TABLE 1

SCREWS: METAL-TO-PLYWOOD CONNECTIONS<sup>(a)</sup>

Depth of Threaded Penetration (in.)	Ultimate Lateral Load (lbf) <sup>(b)</sup>					
	Wood Screws			Sheet Metal Screws		
	#8	#10	#12	#8	#10	#12
1/2	415	(500)	590	465	(565)	670
5/8	-	-	-	500	(600)	705
3/4	-	-	-	590	(655)	715

(a) Plywood was C-D grade with exterior glue (all plies Group 1), face grain parallel to load. Side plate was 3/16"-thick steel.

(b) Values in parentheses are estimates based on other tests.

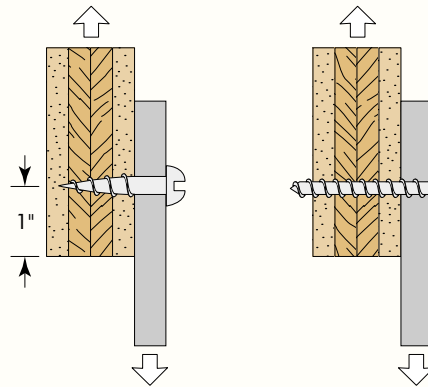


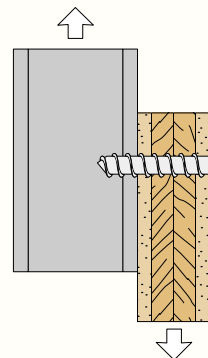
TABLE 2

SHEET METAL SCREWS: PLYWOOD-TO-METAL CONNECTIONS<sup>(a)</sup>

Framing	Plywood Thickness (in.)	Ultimate Lateral Load (lbf) <sup>(b)</sup>				
		Screw Size				1/4"-20 Self Tapping Screw
		#8	#10	#12	#14	
0.080-in. Aluminum	1/4	330	360	390	410	590
	1/2	630	850*	860	920	970
	3/4	910*	930*	1250	1330	1440
0.078-in. Galvanized Steel (14 gage)	1/4	360	380	400	410	650
	1/2	700*	890*	900	920	970
	3/4	700*	950*	1300*	1390*	1500

(a) Plywood was A-C EXT (all plies Group 1), face grain parallel to load.

(b) Loads denoted by an asterisk(\*) were limited by screw-to-framing strength; others were limited by plywood strength.



IF ALLOWABLE IS A FOS = 5, THEN  
 #8 #10 #12  
 140 190 260 LBS

# SCW Head-of-Wall Slide-Clip Connector

PRCTI20240333

The SCW connectors offer 1" of upward and 1" of downward movement. They are primarily used in head-of-wall applications that require vertical movement relative to the structure. SCW connectors are often used to strengthen window and door jambs for projects that utilize slip or slotted track.

**Material:** 54 mil (16 ga.)

**Finish:** Galvanized (G90)

**Installation:**

- Use the specified type and number of anchors.
- Use the specified number of #14 shouldered screws (included). Install shouldered screws in the slots adjacent to the No-Equal® stamp.
- Use a maximum of one screw per slot.
- For installations to wood framing, see Simpson Strong-Tie® engineering letter L-CF-DEFCLIPW at [strongtie.com](http://strongtie.com).

**Codes:** See p. 13 for Code Reference Key Chart

**Ordering Information:**

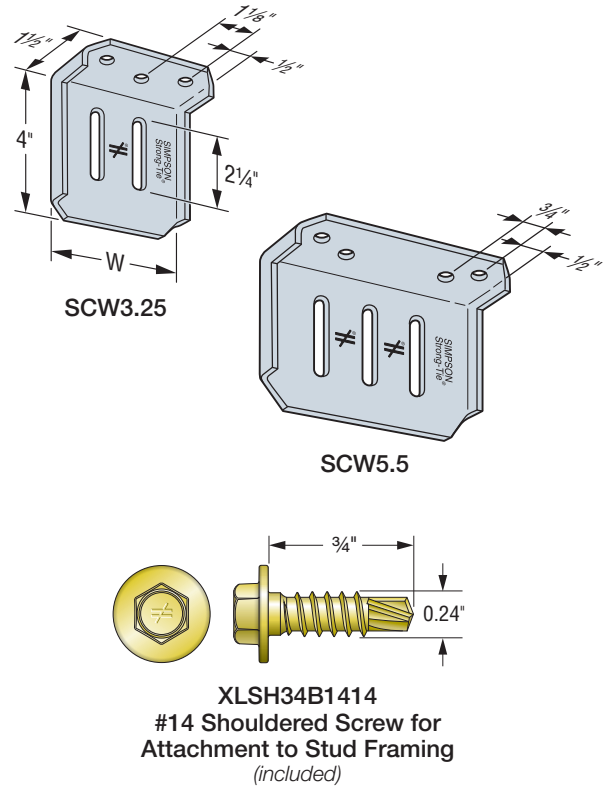
SCW3.25-KT contains:

- Box of 25 connectors
- 55 XLSH34B1414 #14 shouldered screws

SCW5.5-KT contains:

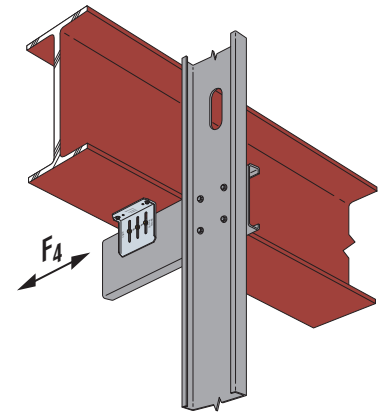
- Box of 25 connectors
- 83 XLSH34B1414 #14 shouldered screws

**Note:** Replacement #14 shouldered screws for SCW connectors are XLSH34B1414-RP83.



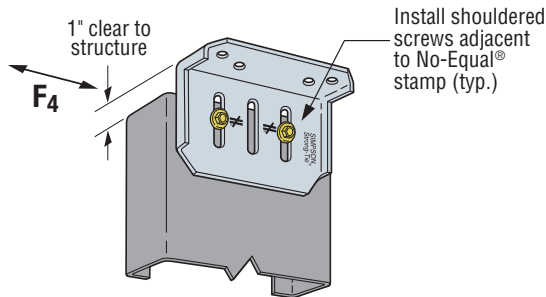
## SCW Allowable Connector Loads (lb.)

Model No.	Connector Material Thickness mil (ga.)	W (in.)	No. of #14 Shouldered Screws	Stud Thickness			Code Ref.
				33 mil (20 ga.)	43 mil (18 ga.)	54 mil (16 ga.)	
				F <sub>4</sub>	F <sub>4</sub>	F <sub>4</sub>	
SCW3.25	54 (16)	3 3/4	2	455	630	755	IBC, FL, LA
SCW5.5	54 (16)	5 1/2	2 <sup>1</sup>	455	630	995	
			3	455	630	1,220 <sup>3</sup>	

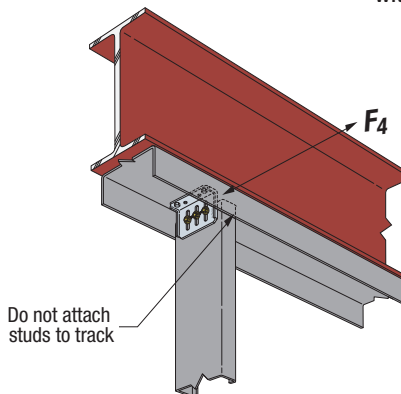


Typical SCW Installation with Stud Strut

1. When the SCW5.5 connector is used with two shouldered screws, install screws in the outermost slots.
2. Allowable loads are based on clips installed with all holes in the anchor leg filled with #12–14 screws. For other anchorage installations, the capacity of the connection system will be the minimum of the tabulated value and the allowable load from the SCW Allowable Anchorage Loads table on p. 49.
3. Tabulated loads are applicable for the following framing widths:  
 SCW3.25 — 3 1/2", 3 3/4", 4" and 5 1/2"  
 SCW5.5 — 6", 8" (18 ga. min.), 10" and 12" (16 ga. min.)



SCW5.5 Installation with Two Shouldered Screws (three shouldered screws and SCW3.25 similar)

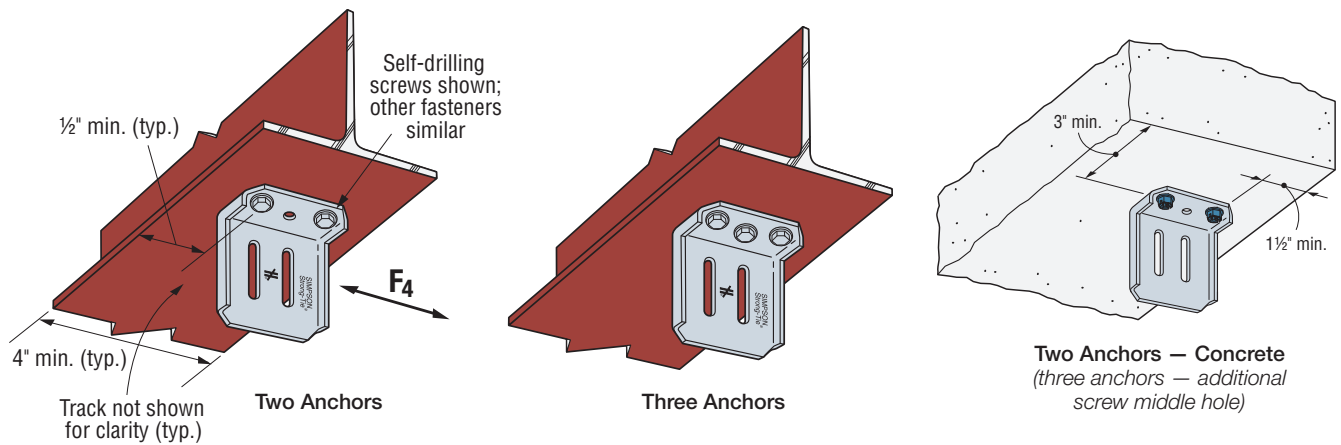


Typical SCW Installation at Stud

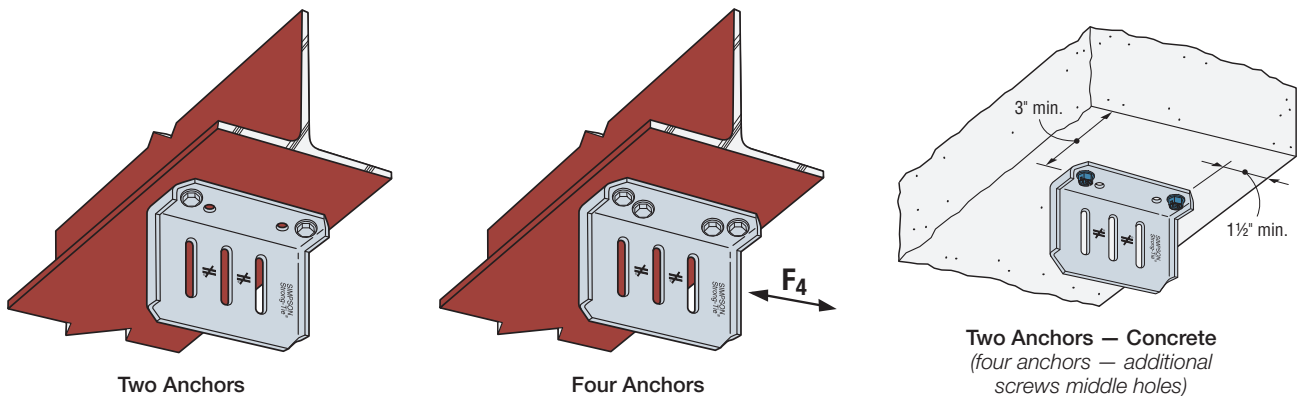
## SCW Allowable Anchorage Loads (lb.)

Model No.	Anchorage Type	Minimum Base Material	No. of Anchors	Allowable Load F <sub>4</sub>
SCW3.25	#12-24 self-drilling screws	A36 steel 3/16" thick	2	715
	#12-24 self-drilling screws	A36 steel 3/16" thick	3	1,075
	Simpson Strong-Tie® 0.157" x 3/16" powder-actuated fasteners PDPAT-62KP	A36 steel 3/16" thick	2	715
	Simpson Strong-Tie 0.157" x 3/16" powder-actuated fasteners PDPAT-62KP	A36 steel 3/16" thick	3	1,075
SCW5.5	Simpson Strong-Tie 1/4" x 1 1/4" Titen Turbo™ <sup>3</sup>	Concrete f' <sub>c</sub> = 2,500 psi	2	285
	Simpson Strong-Tie 1/4" x 1 1/4" Titen Turbo™ <sup>3</sup>	Concrete f' <sub>c</sub> = 2,500 psi	3	350
	#12-24 self-drilling screws	A36 steel 3/16" thick	2	775
	#12-24 self-drilling screws	A36 steel 3/16" thick	4	1,550
SCW5.5	Simpson Strong-Tie 0.157" x 3/16" powder-actuated fasteners PDPAT-62KP	A36 steel 3/16" thick	2	745
	Simpson Strong-Tie 0.157" x 3/16" powder-actuated fasteners PDPAT-62KP	A36 steel 3/16" thick	4	1,490
	Simpson Strong-Tie 1/4" x 1 1/4" Titen Turbo™ <sup>3</sup>	Concrete f' <sub>c</sub> = 2,500 psi	2	285
	Simpson Strong-Tie 1/4" x 1 1/4" Titen Turbo™ <sup>3</sup>	Concrete f' <sub>c</sub> = 2,500 psi	4	775

- For additional important information, see General Information and Notes on p. 26.
- Allowable loads are for clip anchorage only. The capacity of the connection system will be the minimum of the tabulated value and the allowable load from the SCW Allowable Connector Loads table on p. 48.
- Tabulated values require a minimum 1 1/2" edge distance for masonry screws in concrete.
- See the current *Fastening Systems* catalog at [strongtie.com](http://strongtie.com) for more information on Simpson Strong-Tie fasteners.



SCW3.25 Anchor Layout



SCW5.5 Anchor Layout

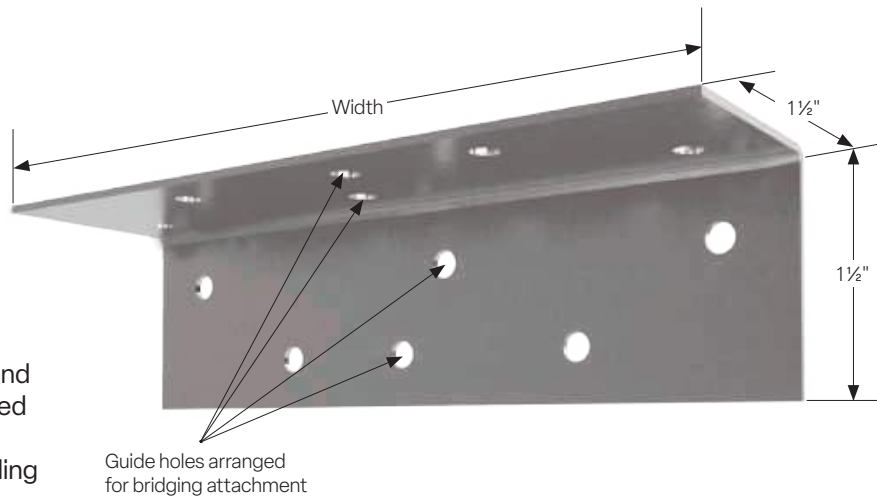


# MA Multi-Use Secure Clip

## Product Application

The MA multi-use secure clip is used in a variety of different applications, including head-of-wall, joist connections, rafter and truss connections, reinforcing header connections, and bridging.

The MA secure clip is designed to resist vertical and lateral loads. Pre-punched guide holes are provided in each leg to allow for efficient installation. Clips come packaged in durable buckets for easy handling on the jobsite.



Guide holes arranged for bridging attachment

## Features and Benefits

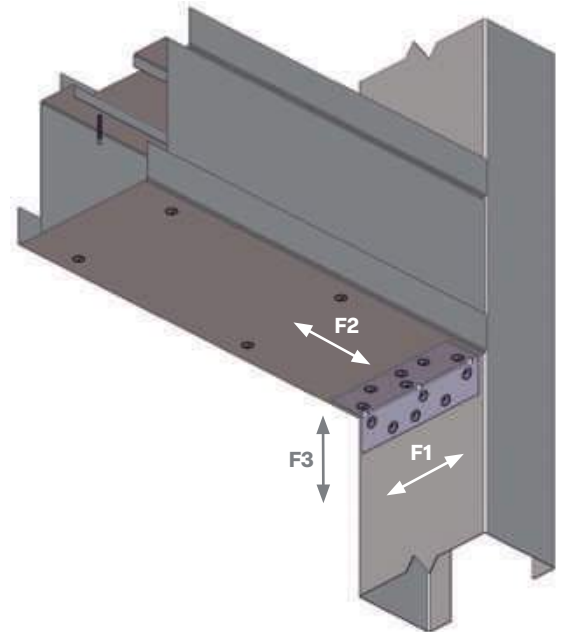
- Variety of lengths available
- Loads based on #10 screws
- Pre-punched guide holes
- No labor used cutting scrap or angle

## Material Composition

- Mill certified steel
- ASTM A653/A653M
- 54 mil
  - 57 ksi yield strength
  - 65 ksi tensile strength
  - G60/G90 galvanized coating
- 68 mil
  - 57 ksi yield strength
  - 65 ksi tensile strength
  - G60/G90 galvanized coating

## Quantity / Order Information

Part No.	Length	Qty / Bucket	Lbs / Bucket
MA350-54	3 1/2"	200	34
MA350-68	3 1/2"	200	42
MA550-54	5 1/2"	100	26
MA550-68	5 1/2"	100	32
MA750-54	7 1/2"	100	35
MA750-68	7 1/2"	100	44
MA950-54	9 1/2"	100	44
MA950-68	9 1/2"	100	55





# Multi-Use Secure Clip Allowable Loads



Part No.	Stud Properties			F1 Allowable Loads (lbs)		F2 Allowable Loads (lbs)		F3 Allowable Loads (lbs)	
	Mil	Gauge	Fy (ksi)	2 #10 Screws	3 #10 Screws	2 #10 Screws	3 #10 Screws	2 #10 Screws	3 #10 Screws
MA350	33EQS	20	57	402	603	206	310	206	310
	33	20	33	353	530	168	251	168	251
	43EQS	18	57	635	952	280	420	280	420
	43	18	33	526	789	219	328	219	328
	54	16	50	1068	1602	396	594	396	594
	68	14	50	1510	2266	499	749	499	749
	97	12	50	2261	2420	712	965	712	965
	<b>Maximum Allowable Clip Capacity</b>				<b>Max F1 = 2420 lbs</b>		<b>Max F2 = 965 lbs</b>		<b>Max F3 = 965 lbs</b>

Part No.	Stud Properties			F1 Allowable Loads (lbs)			F2 Allowable Loads (lbs)			F3 Allowable Loads (lbs)		
	Mil	Gauge	Fy (ksi)	2 #10 Screws	4 #10 Screws	5 #10 Screws	2 #10 Screws	4 #10 Screws	5 #10 Screws	2 #10 Screws	4 #10 Screws	5 #10 Screws
MA550	33EQS	20	57	402	804	1005	206	413	516	206	413	516
	33	20	33	353	707	884	168	335	419	168	335	419
	43EQS	18	57	635	1269	1587	280	560	700	280	560	700
	43	18	33	526	1052	1315	219	437	547	219	437	547
	54	16	50	1068	2136	2671	396	792	855	396	792	855
	68	14	50	1510	2980	2980	499	855	855	499	855	855
	97	12	50	2261	2980	2980	712	855	855	712	855	855
	<b>Maximum Allowable Clip Capacity</b>				<b>Max F1 = 2980 lbs</b>			<b>Max F2 = 855 lbs</b>			<b>Max F3 = 855 lbs</b>	

Part No.	Stud Properties			F1 Allowable Loads (lbs)			F2 Allowable Loads (lbs)			F3 Allowable Loads (lbs)		
	Mil	Gauge	Fy (ksi)	2 #10 Screws	4 #10 Screws	7 #10 Screws	2 #10 Screws	4 #10 Screws	7 #10 Screws	2 #10 Screws	4 #10 Screws	7 #10 Screws
MA750	33EQS	20	57	402	804	1407	206	413	722	206	413	722
	33	20	33	353	707	1237	168	335	597	168	335	597
	43EQS	18	57	635	1269	2221	280	560	980	280	560	980
	43	18	33	526	1052	1841	219	437	765	219	437	765
	54	16	50	1068	2136	3739	396	792	1387	396	792	1387
	68	14	50	1510	3021	5286	499	998	1740	499	998	1740
	97	12	50	2261	4521	6100	712	1424	1740	712	1424	1740
	<b>Maximum Allowable Clip Capacity</b>				<b>Max F1 = 6100 lbs</b>			<b>Max F2 = 1740 lbs</b>			<b>Max F3 = 1740 lbs</b>	

Part No.	Stud Properties			F1 Allowable Loads (lbs)			F2 Allowable Loads (lbs)			F3 Allowable Loads (lbs)		
	Mil	Gauge	Fy (ksi)	2 #10 Screws	5 #10 Screws	9 #10 Screws	2 #10 Screws	5 #10 Screws	9 #10 Screws	2 #10 Screws	5 #10 Screws	9 #10 Screws
MA950	33EQS	20	57	402	1005	1809	206	516	929	206	516	929
	33	20	33	353	884	1590	168	419	754	168	419	754
	43EQS	18	57	635	1587	2856	280	700	1260	280	700	1260
	43	18	33	526	1315	2367	219	547	984	219	547	984
	54	16	50	1068	2671	4807	396	991	1740	396	991	1740
	68	14	50	1510	3776	6100	499	1248	1740	499	1248	1740
	97	12	50	2261	5652	6100	712	1740	1740	712	1740	1740
	<b>Maximum Allowable Clip Capacity</b>				<b>Max F1 = 6100 lbs</b>			<b>Max F2 = 1740 lbs</b>			<b>Max F3 = 1740 lbs</b>	

**Table Notes**

- Allowable loads have not been increased for wind, seismic activity, or other factors.
- The allowable loads are based on the steel properties of the members being connected, per AISI S100.
- The nominal strength of the screw must be at least 3.75 times the allowable load.
- Screw shear capacities are based on allowable strength design (ASD) and include a safety factor of 3.0.
- Penetration of screws through joined materials should not be less than three exposed threads. Install and tighten screws in accordance with the screw manufacturer's recommendations.
- Allowable loads indicated on the table(s) are for force in single direction only. The designer shall use the combined forces check as required by AISI S100 if more than one force is applied to the connection.

# S/JCT and S/HJCT Steel-Joist Connectors



This product is preferable to similar connectors because of a) easier installation, b) higher loads, c) lower installed cost, or a combination of these features.

The S/JCT and S/HJCT are unique, skewable steel-joist framing connectors that combine strength, versatility and low installed cost. The connectors can be used with CFS headers, wood headers, steel I-beams (with welds or PAF fasteners) and masonry walls. **Installed cost is minimized since these products are shear rather than bearing connectors, eliminating the need for web stiffeners.** The connectors also feature horizontal tabs that facilitate top flange alignment and joist support during screw installation.

**Material:** S/JCT — 68 mil (14 ga.); S/HJCT — 97 mil (12 ga.)

**Finish:** Galvanized

**Features:**

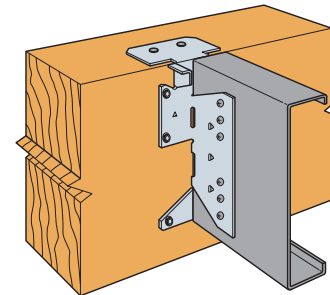
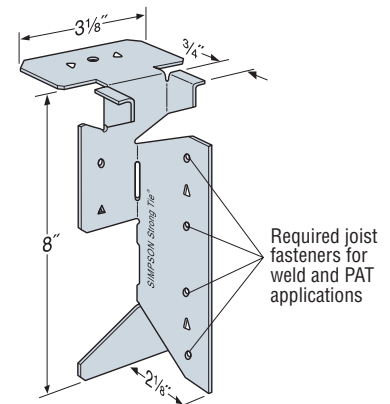
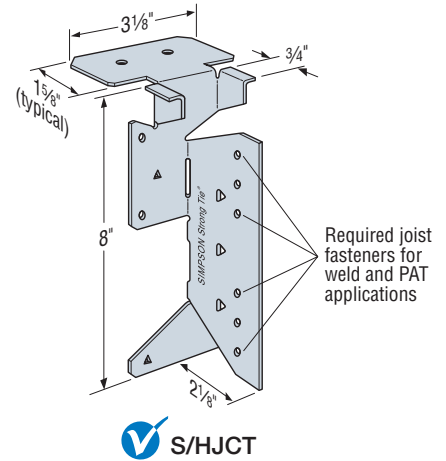
- Uni-directional: Joist can be attached from left or right
- One size fits joists 8" through 14" deep
- Optional holes for additional load capacity
- Simplicity of design
- Quick and easy installation
- Field skewable up to 45° left or right

**Installation:**

- Attach hanger with specified fasteners. Use round holes for minimum load, use round and triangle holes for maximum load.
- May be used for weld-on applications. The minimum required weld to the top flange is 1/8" x 2 1/2" fillet weld to each side of top flange. Consult the code for special considerations when welding galvanized steel.
- May be installed using PDPAT-62KP (0.157" x 5/8") powder-actuated fasteners. Steel headers with thicknesses between 1/4" and 3/4" having a minimum F<sub>y</sub> = 36 ksi. A Red (level 5) or Purple (level 6) powder load may be required to achieve specified penetration (p). See illustration on p. 203.

**Codes:** See p. 13 for Code Reference Key Chart

**Ordering Information:** The S/JCT is sold in cartons of 50. The S/HJCT is sold in kits as the S/HJCT-KT and contains five (5) connectors and (95) #14 screws.



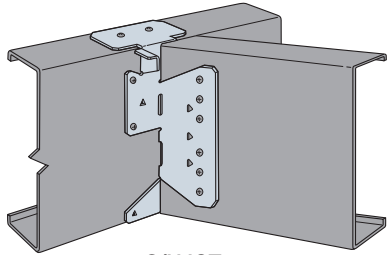
**S/HJCT Installation with a 4x10 Wood Header**

1. Allowable loads are based on a minimum of single 54 mil (16 ga.) CFS joist member. CFS joist shall be laterally braced per designer specification.
2. Allowable loads for wood header are based on 4x DF/SP minimum, for SPF/HF wood species use an adjustment factor of 0.72.
3. CFS header must be braced to prevent web buckling per designer specification and header must have full bearing of 1 1/2" flange-depth.
4. Backing in the steel beam cavity is not required behind the hanger for load listed.
5. Screws shall be installed using joist hanger holes screwing through the hanger into the joist.
6. CFS joists with up to a 0.50" gap (short cut), use an adjustment factor of 0.87 and joists with a 0.50" to 0.90" gap (short cut), use an adjustment factor of 0.75.
7. See the current *Fastening Systems* catalog at [strongtie.com](http://strongtie.com) for more information on Simpson Strong-Tie fasteners.
8. See p. 203 for more information.

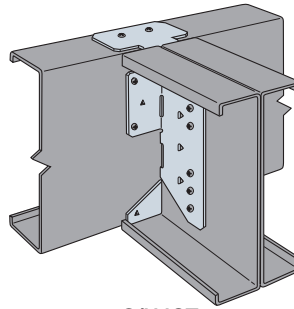
Model No.	Fasteners <sup>7</sup>			Allowable Load <sup>1</sup> (lb.)		Code Ref.
	Top	Face	Joist	Uplift	Down	
<b>Attached to CFS Header: 54 mil (16 ga.)<sup>3</sup> — Straight Hanger</b>						
S/JCT (min.)	(1) #10	(2) #10	(4) #10	940	1,195	IBC, FL, LA
S/JCT (max.)	(1) #10	(4) #10	(6) #10	1,435	2,105	
S/HJCT (min.)	(2) #10	(4) #14	(6) #14	1,510	2,920	
S/HJCT (max.)	(2) #10	(8) #14	(9) #14	1,670	3,855	
<b>Attached to CFS Header: 54 mil (16 ga.)<sup>3</sup> — Skewed Hanger</b>						
S/JCT (min.)	(1) #10	(2) #10	(4) #10	940	1,135	IBC, FL, LA
S/JCT (max.)	(1) #10	(4) #10	(6) #10	940	1,185	
S/HJCT (min.)	(2) #10	(4) #14	(6) #14	1,510	2,305	
Attached to Steel Header <sup>4</sup> — Straight and Skewed Hanger						
S/JCT (min.)	1/8" x 2 1/2" fillet weld to each side of top flange		(4) #10	145	940	—
S/HJCT (min.)			(4) #14	195	1,450	
S/HJCT (min.) Skew	(2) 0.157" x 5/8" powder-actuated fastener <sup>8</sup>		(4) #14	195	1,235	
S/JCT (min.)			(4) #10	145	750	
S/HJCT (min.)			(4) #14	195	1,185	
<b>Attached to Masonry — Straight and Skewed Hanger</b>						
S/HJCT (min.)	(2) 1/4" x 2 1/4" Titen Turbo™	(4) 1/4" x 2 1/4" Titen Turbo	(6) #14	710	1,785	—
S/HJCT (min.) Skew				710	1,410	

Model No.	Fasteners <sup>7</sup>			Allowable Load <sup>1,2</sup> (lb.)		Code Ref.
	Top	Face	Joist	Uplift (160)	Down (100)	
<b>Attached to 4x DF/SP Wood Header — Straight Hanger</b>						
S/JCT (min.)	(1) 10d	(2) 10d	(4) #10	555	945	IBC, FL, LA
S/JCT (max.)	(1) 10d	(4) 10d	(6) #10	945	1,465	
S/HJCT (min.)	(2) 10d	(4) 1/4"x3" SDS	(6) #14	1,210	2,625	
S/HJCT (max.)	(2) 10d	(8) 1/4"x3" SDS	(9) #14	1,475	2,980	
<b>Attached to 4x DF/SP Wood Header — Skewed Hanger</b>						
S/JCT (min.)	(1) 10d	(2) 10d	(4) #10	390	845	IBC, FL, LA
S/JCT (max.)	(1) 10d	(4) 10d	(6) #10	775	1,300	
S/HJCT (min.)	(2) 10d	(4) 1/4" x 3" SDS	(6) #14	1,210	1,935	

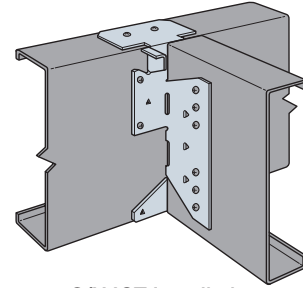
# S/JCT and S/HJCT Steel-Joist Connectors



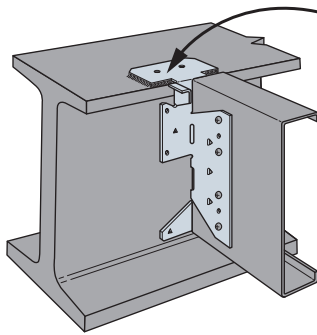
**S/HJCT**  
Skewed 45° Installation



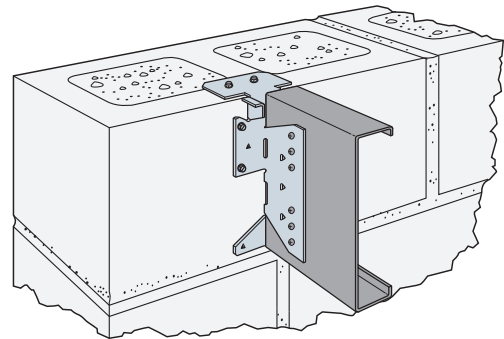
**S/HJCT**  
Double-Joist Installation



**S/HJCT Installation**  
with a CFS Steel Header

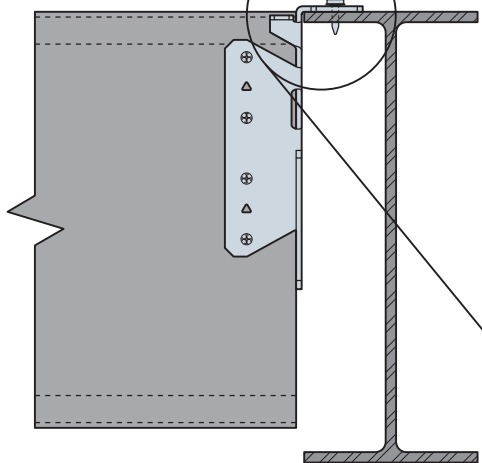


**S/HJCT Weld-On**  
Installation with  
an I-Beam.  
Apply 5" of total  
weld at left and right  
edges, as shown.

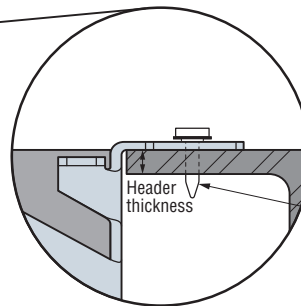


**S/HJCT Installation**  
on Masonry Header

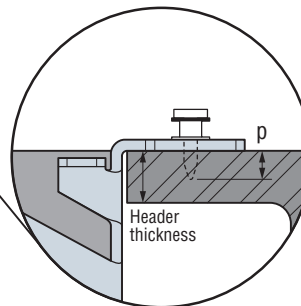
PDPAT-62KP fasteners  
installed into existing  
top-flange nail holes



**S/JCT Installed on a Steel Header**  
with Powder-Actuated Fasteners



**Steel header**  
**thickness:**  
1/4" to 1/2"  
Point of PDPAT-62KP  
must penetrate through  
the steel header



**Steel header**  
**thickness:**  
>1/2" to 3/4"  
p = 0.46" min.  
for A36 steel  
p = 0.36" min.  
for A572 or  
A992 steel

# **BSE**

**B**rienen **S**tructural **E**ngineers, P.S.

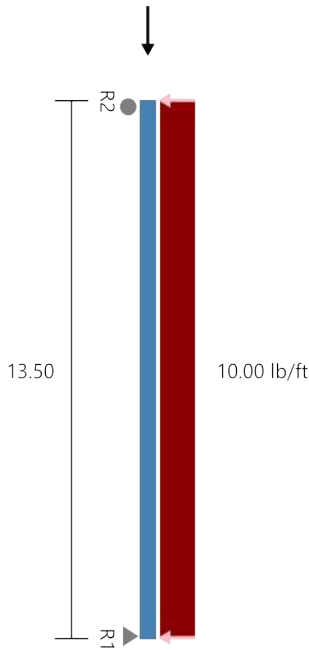
## INFILL CFS WALL DESIGNS

# TYPICAL INFILL WALL 6" STUDS

Project Name: Centeris

Model: 6" STUD 13'-6"

Code: 2012 NASPEC [AISI S100-2012]



**Section : 600S125-33 (33 ksi) @ 24" o.c. Single C Stud (punched)**

Maxo = 608.4 ft-lb      Va = 638.1 lb      I = 1.36 in<sup>4</sup>

Loads have not been modified for strength checks  
Loads have not been modified for deflection calculations

**Bridging Connectors - Design Method =AISI S100**

Span	Axial KyLy, KtLt	Flexural, Distortional	Connector	Stress Ratio
Span	48.0", 48.0"	48.0", 162.0"	N/A	-

**Web Crippling**

Support	Load (lb)	Bearing (in)	Pa (lb)	M (ft-lbs)	Max Int.	Stiffener?
R2	67.5	--Slip Track Design, Ref Connectors--				NO
R1	67.5	--Stud/Track Design, Ref Connectors--				NO

**Gravity Load**

Type	Load (lb)
Uniform	24.00plf

	Code Check	Required	Allowed	Interaction	Notes
Span	Max. Axial, lbs	324.0(c)	1282.2(c)	25%	KΦ=0.00 lb-in/in Max KL/r = 128 Shear (Punched) Ma-dist (control), KΦ=0.00 lb-in/in Shear 0.0, Moment 227.8 Axial 192.5(c), Moment 219.8
	Max. Shear, lbs	67.5	638.1	11%	
	Max. Moment (MaFy, Ma-dist), ft-lbs	227.8	526.3	43%	
	Moment Stability, ft-lbs	227.8	518.4	44%	
	Shear/Moment	0.37	1.00	37%	
	Axial/Moment	0.58	1.00	58%	
	Deflection Span, in	0.186	--meets L/870--		

Support	Rx(lb)	Ry(lb)	Connector	Connector Interaction	Anchor Interaction
R2	67.5	0.0	Simpson Strong-Tie Connector 600SLT250-33 (33) & (1) .157" SST PDPA/PDPAT-62KP to steel (3/16" to 1/2" thickness)	45.00 %	41.25 %
R1	67.5	324.0		600T125-33 (33) & (1) .157", 3/4" embed SST PDPA/PDPAT to 4000 nw concrete	27.78 %

\* Reference catalog for connector and anchor requirement notes as well as screw placement requirements



## PHYSICAL PROPERTIES

### Viper-X Stud®

MODEL NO.	DESIGN THICKNESS (in)	MINIMUM THICKNESS (in)	YIELD (ksi)	WEB SIZES (in)	COATING <sup>1,2</sup>	FLANGE (in)	RETURN LIP (in)
VIPER-X-18	0.0188	0.0179	57	1-5/8, 2-1/2, 3-1/2, 3-5/8, 4, 6	G40	1-7/16	3/8
VIPER-X-22	0.0235	0.0223	57	1-5/8, 2-1/2, 3-1/2, 3-5/8, 4, 6	G40	1-7/16	3/8

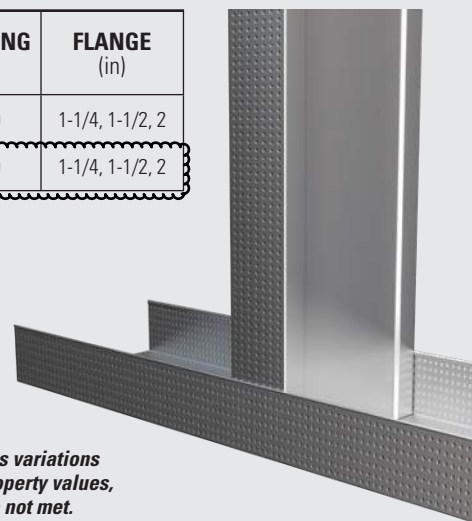
### Viper-X Track®

MODEL NO.	DESIGN THICKNESS (in)	MINIMUM THICKNESS (in)	YIELD (ksi)	WEB SIZES (in)	COATING <sup>1,2</sup>	FLANGE (in)
VIPER-X-18 TRACK	0.0188	0.0179	57	1-5/8, 2-1/2, 3-1/2, 3-5/8, 4, 6	G40	1-1/4, 1-1/2, 2
VIPER-X-22 TRACK	0.0235	0.0223	57	1-5/8, 2-1/2, 3-1/2, 3-5/8, 4, 6	G40	1-1/4, 1-1/2, 2

#### Notes:

1. Web height to thickness ratio ( $h/t$ ) exceeds 200. Web stiffeners required at all support points and concentrated loads.
2. Members having a web height to thickness ratio ( $h/t$ ) value exceeding 260 will not have effective properties listed, only gross properties will be listed.
3. Web height value ( $h$ ) used for  $h/t$  calculation is the flat width of the web. For (S) members, this is the out to out member size, minus twice the thickness, minus twice the inside bend radius.
4. Members having a flange width to thickness ratio ( $b/t$ ) value exceeding 60 must be considered for use with the limitations described in AISI S100-12 section B1.
5. Flange width value ( $b$ ) used for  $b/t$  calculation is the flat width of the flange. For (S) members, this is the out to out member size, minus twice the thickness, minus twice the inside bend radius.
6. Per ASTM C645 & ASTM A1003 Table 1.
7. G60 and G90 available upon request.

**Viper-X High Performance Studs and Tracks are in compliance with ASTM C645. ASTM C645 Section 5.1 allows for permissible dimensional thickness variations, Section 8.2 allows for thickness variations and exemptions from minimum section property values, if specified performance requirements are not met. The Viper-X Framing product meets and exceeds these requirements.**



## GENERAL TABLE NOTES

1. The yield strength for all Viper-X Products is 57 ksi.
2. Tabulated gross properties are based on full, unreduced section away from punchouts.
3. Punch-out sizes are 0.75" x 2.00" for stud depths 1.625" and 2.50", and 1.50" x 2.75" for stud depths 3.50" and deeper.
4. Factory punchouts are in accordance with section C5 of AISI S201-12. The distance from the center of the last punchout to the end of the stud is 12 inches.
5. For Allowable Stress Design (ASD) method, factors of safety of 1.67 and 1.6 respectively, are used for moment and shear capacities as per AISI S100-12.
6. Design stiffening lip is 3/8" for all studs.

### Notations

I <sub>x</sub>	Moment of Inertia about the X axis of Gross Section
I <sub>y</sub>	Moment of Inertia about the Y axis of Gross Section
R <sub>x</sub> , R <sub>y</sub>	Radius of Gyration about the X and Y axes, respectively of Gross Section
J	St. Venant Torsion Constant
C <sub>w</sub>	Torsional Warping Constant
X <sub>o</sub>	Distance from Shear Center to Centroid Along the X axis
R <sub>o</sub>	Polar Radius of Gyration about the Shear Center
β	Torsional-Flexural Constant
I <sub>xe</sub>	Effective Moment of Inertia at Punch-out about the X axis (for deflection calculation)
S <sub>xe</sub>	Effective Section Modulus about the X axis at Punch-out
M <sub>a-l</sub>	Allowable Moment based on Local Buckling
M <sub>a-d</sub>	Allowable Moment based on Distortional Buckling
V <sub>ag</sub>	Allowable Shear at Gross Section





# NON-COMPOSITE LIMITING WALL HEIGHTS – FULLY BRACED

VIPER-X MEMBER	YIELD (ksi)	DESIGN THICKNESS (in)	SPACING O.C. (in)	5 PSF			7.5 PSF			10 PSF		
				L/120	L/240	L/360	L/120	L/240	L/360	L/120	L/240	L/360
162VXS144-18	57	0.0188	12	10' 3"	8' 2"	7' 2"	9' 0"	7' 2"	6' 3"	8' 2"	6' 6"	5' 8"
	57	0.0188	16	9' 5"	7' 6"	6' 6"	8' 3"	6' 6"	5' 9"	7' 6"	5' 11"	5' 2"
	57	0.0188	24	8' 2"	6' 6"	5' 8"	7' 2"	5' 8"	4' 11"	6' 3" f	5' 2"	4' 6"
250VXS144-18	57	0.0188	12	14' 2"	11' 4"	9' 10"	12' 5"	9' 10"	8' 8"	11' 4"	9' 0"	7' 10"
	57	0.0188	16	13' 1"	10' 4"	9' 1"	11' 5"	9' 1"	7' 11"	10' 1" f	8' 3"	7' 2"
	57	0.0188	24	11' 4"	9' 0"	7' 10"	9' 6" f	7' 10"	6' 10"	8' 3" f	7' 1"	6' 3"
350VXS144-18	57	0.0188	12	18' 6"	14' 8"	12' 10"	16' 0" f	12' 10"	11' 2"	13' 11"	11' 8"	10' 2"
	57	0.0188	16	16' 11"	13' 5"	11' 9"	13' 11" f	11' 9"	10' 3"	12' 0" f	10' 8"	9' 4"
	57	0.0188	24	13' 11" f	11' 8"	10' 2"	11' 4" f	10' 2"	8' 11"	9' 10" f	9' 3"	8' 1"
362VXS144-18	57	0.0188	12	19' 0"	15' 2"	13' 2"	16' 4" f	13' 2"	11' 6"	14' 2" f	12' 0"	10' 6"
	57	0.0188	16	17' 4" f	13' 10"	12' 1"	14' 2" f	12' 1"	10' 7"	12' 3" f	11' 0"	9' 7"
	57	0.0188	24	14' 2" f	12' 0"	10' 6"	11' 7" f	10' 6"	9' 2"	10' 0"	9' 6"	8' 4"
400VXS144-18 <sup>1</sup>	57	0.0188	12	20' 6"	16' 3"	14' 3"	17' 3" f	14' 3"	12' 5"	14' 11" f	13' 0"	11' 4"
	57	0.0188	16	18' 4" f	14' 11"	13' 0"	14' 11" f	13' 0"	11' 5"	12' 11" f	11' 10"	10' 4"
	57	0.0188	24	14' 11" f	12' 11"	11' 4"	12' 2" f	11' 4"	9' 10"	10' 6" f	10' 3"	9' 0"
600VXS144-18 <sup>1</sup>	57	0.0188	12	25' 9" f	22' 4"	19' 6"	21' 0" f	19' 6"	17' 0"	17' 7" w	17' 7" w	15' 6"
	57	0.0188	16	22' 3" f	20' 6"	17' 11"	17' 8" w	17' 8" w	15' 7"	13' 3" w	13' 3" w	13' 3" w
	57	0.0188	24	17' 7" w	17' 7" w	15' 6"	11' 9" w	11' 9" w	11' 9" w	8' 10" w	8' 10" w	8' 10" w
162VXS144-22	57	0.0235	12	10' 7"	8' 5"	7' 4"	9' 3"	7' 4"	6' 5"	8' 5"	6' 8"	5' 10"
	57	0.0235	16	9' 8"	7' 8"	6' 9"	8' 6"	6' 9"	5' 10"	7' 8"	6' 1"	5' 4"
	57	0.0235	24	8' 5"	6' 8"	5' 10"	7' 4"	5' 10"	5' 1"	6' 8"	5' 3"	4' 7"
250VXS144-22	57	0.0235	12	15' 6"	12' 4"	10' 9"	13' 6"	10' 9"	9' 5"	12' 4"	9' 9"	8' 6"
	57	0.0235	16	14' 2"	11' 3"	9' 10"	12' 5"	9' 10"	8' 7"	11' 3"	8' 11"	7' 10"
	57	0.0235	24	12' 4"	9' 9"	8' 6"	10' 9"	8' 6"	7' 5"	9' 8" f	7' 9"	6' 9"
350VXS144-22	57	0.0235	12	20' 1"	15' 11"	13' 11"	17' 7"	13' 11"	12' 2"	15' 11"	12' 8"	11' 1"
	57	0.0235	16	18' 5"	14' 7"	12' 9"	16' 1"	12' 9"	11' 2"	14' 1" f	11' 7"	10' 2"
	57	0.0235	24	15' 11"	12' 8"	11' 1"	13' 3" f	11' 1"	9' 8"	11' 6" f	10' 1"	8' 9"
362VXS144-22	57	0.0235	12	20' 8"	16' 5"	14' 4"	18' 0"	14' 4"	12' 6"	16' 5"	13' 0"	11' 4"
	57	0.0235	16	18' 11"	15' 0"	13' 1"	16' 6"	13' 1"	11' 6"	14' 4" f	11' 11"	10' 5"
	57	0.0235	24	16' 5"	13' 0"	11' 4"	13' 6" f	11' 4"	9' 11"	11' 8" f	10' 4"	9' 0"
400VXS144-22 <sup>1</sup>	57	0.0235	12	22' 4"	17' 8"	15' 6"	19' 6"	15' 6"	13' 6"	17' 6" f	14' 1"	12' 3"
	57	0.0235	16	20' 5"	16' 3"	14' 2"	17' 6" f	14' 2"	12' 5"	15' 2" f	12' 11"	11' 3"
	57	0.0235	24	17' 6" f	14' 1"	12' 3"	14' 3" f	12' 3"	10' 9"	12' 4" f	11' 2"	9' 9"
600VXS144-22 <sup>1</sup>	57	0.0235	12	30' 3" f	24' 4"	21' 3"	24' 8" f	21' 3"	18' 7"	21' 5" f	19' 4"	16' 10"
	57	0.0235	16	26' 3" f	22' 4"	19' 6"	21' 3" f	19' 6"	17' 1"	19' 4" f	17' 1"	15' 5"
	57	0.0235	24	21' 5" f	19' 4"	16' 10"	17' 1" f	16' 10"	14' 11"	16' 10" f	14' 11"	13' 5"

UP TO 14'-2" MAX WITHOUT WEB STIFFENERS BASED ON #8 SMS TENSION LOAD = 71 LBS

**Notes:**

1. Web height to thickness ratio ( $h/t$ ) exceeds 200. Web stiffeners required at all support points and concentrated loads.
2. Lateral loads of 5 psf, 7.5 psf, and 10 psf have NOT been reduced for strength or deflection checks. Full lateral load is applied.
3. Limiting heights are in accordance with AISI S100-12 using all steel non-composite design.
4. Limiting heights are established by considering flexure ( $f$ ), web crippling ( $w$ ) and deflection.
5. Allowable moment is the lesser of  $M_{al}$  and  $M_{ad}$ . Stud distortional buckling based on an assumed  $K\phi = 0$ .
6. For bending, studs are assumed to be adequately braced to develop full allowable moment.
7. Studs are fully braced when unbraced length is less than  $L_u$ . See section properties table for  $L_u$  values.
8. Web crippling check is based on AISI S100-12 section C3.4.2 Condition 1: End One-Flange Loading with 1" end bearing.
9. See page 4 for additional table notes.





# ALLOWABLE COMPOSITE HEIGHTS – NON-LOAD BEARING WALLS

VIPER-X MEMBER	YIELD (ksi)	DESIGN THICKNESS (in)	SPACING O.C. (in)	5 PSF			7.5 PSF			10 PSF		
				L/120	L/240	L/360	L/120	L/240	L/360	L/120	L/240	L/360
162VXS144-18	57	0.0188	12	14'-6"	11'-6"	10'-0"	12'-8"	10'-0"	8'-6"	11'-6"	8'-11"	7'-7"
	57	0.0188	16	13'-2"	10'-5"	8'-10"	11'-6"	8'-11"	7'-7"	10'-5"	7'-11"	-
	57	0.0188	24	11'-6"	8'-11"	7'-7"	10'-0"	7'-7"	-	8'-11"	-	-
250VXS144-18	57	0.0188	12	18'-5"	14'-7"	12'-9"	16'-1"	12'-9"	11'-2"	14'-7"	11'-7"	10'-2"
	57	0.0188	16	16'-9"	13'-4"	11'-7"	14'-8"	11'-7"	10'-2"	13'-4"	10'-7"	8'-10"
	57	0.0188	24	14'-7"	11'-7"	10'-2"	12'-9"	10'-2"	8'-6"	11'-6"	8'-11"	7'-6"
350VXS144-18	57	0.0188	12	22'-3"	17'-8"	15'-4"	19'-5"	15'-5"	13'-6"	17'-8"	14'-0"	12'-3"
	57	0.0188	16	20'-3"	16'-1"	14'-0"	17'-8"	14'-0"	12'-3"	15'-10"	12'-9"	11'-2"
	57	0.0188	24	17'-8"	13'-12"	12'-3"	14'-11"	12'-3"	10'-9"	12'-11"	11'-2"	9'-8"
362VXS144-18	57	0.0188	12	22'-6"	17'-11"	15'-8"	19'-8"	15'-8"	13'-8"	17'-11"	14'-3"	12'-5"
	57	0.0188	16	20'-5"	16'-3"	14'-3"	17'-11"	14'-3"	12'-5"	16'-0"	12'-11"	11'-4"
	57	0.0188	24	17'-10"	14'-3"	12'-5"	15'-2"	12'-5"	10'-9"	13'-1"	11'-3"	9'-10"
400VXS144-18	57	0.0188	12	23'-7"	18'-8"	16'-4"	20'-7"	12'-11"	14'-3"	18'-8"	14'-10"	13'-0"
	57	0.0188	16	21'-5"	17'-0"	14'-10"	18'-9"	14'-10"	13'-0"	16'-9"	13'-6"	11'-10"
	57	0.0188	24	18'-8"	14'-10"	13'-0"	15'-10"	13'-0"	11'-4"	13'-9"	11'-10"	10'-0"
600VXS144-18	57	0.0188	12	31'-5"	24'-11"	21'-9"	27'-0"	21'-9"	19'-0"	23'-5"	19'-10"	17'-4"
	57	0.0188	16	28'-7"	22'-8"	19'-10"	22'-6"	19'-10"	17'-4"	20'-3"	18'-0"	15'-9"
	57	0.0188	24	23'-5"	19'-10"	17'-4"	19'-1"	17'-4"	15'-1"	16'-7"	15'-9"	13'-7"
162VXS144-22	57	0.0235	12	14'-8"	11'-8"	10'-2"	12'-10"	10'-2"	8'-8"	11'-8"	9'-1"	7'-8"
	57	0.0235	16	13'-4"	10'-7"	10'-0"	11'-8"	9'-1"	7'-9"	10'-7"	8'-1"	-
	57	0.0235	24	11'-8"	9'-1"	-	10'-2"	-	-	9'-1"	-	-
250VXS144-22	57	0.0235	12	18'-11"	15'-0"	13'-1"	16'-6"	13'-1"	11'-5"	15'-0"	11'-11"	10'-5"
	57	0.0235	16	17'-2"	13'-8"	11'-11"	15'-0"	11'-11"	10'-6"	13'-8"	10'-10"	10'-0"
	57	0.0235	24	15'-0"	11'-11"	10'-5"	13'-1"	10'-5"	8'-10"	11'-10"	9'-3"	7'-9"
350VXS144-22	57	0.0235	12	23'-4"	18'-6"	16'-2"	20'-5"	16'-2"	14'-2"	18'-6"	14'-8"	12'-10"
	57	0.0235	16	21'-3"	16'-10"	14'-9"	18'-6"	14'-9"	12'-10"	16'-8"	13'-4"	11'-8"
	57	0.0235	24	18'-6"	14'-8"	12'-10"	15'-11"	12'-10"	11'-3"	14'-1"	11'-8"	10'-1"
362VXS144-22	57	0.0235	12	25'-0"	18'-9"	16'-5"	20'-8"	16'-5"	14'-4"	18'-9"	14'-11"	13'-0"
	57	0.0235	16	23'-8"	17'-1"	14'-11"	18'-10"	14'-11"	13'-1"	17'-0"	13'-7"	11'-10"
	57	0.0235	24	18'-9"	14'-11"	13'-0"	16'-2"	13'-0"	11'-5"	14'-4"	11'-10"	10'-3"
400VXS144-22	57	0.0235	12	24'-9"	19'-8"	17'-2"	21'-8"	19'-0"	15'-0"	19'-8"	15'-7"	13'-8"
	57	0.0235	16	22'-6"	17'-11"	15'-8"	19'-8"	15'-8"	13'-8"	17'-9"	14'-2"	12'-5"
	57	0.0235	24	19'-8"	15'-7"	13'-8"	16'-11"	13'-8"	11'-11"	15'-0"	12'-5"	10'-8"
600VXS144-22	57	0.0235	12	33'-1"	26'-3"	22'-11"	28'-8"	22'-11"	20'-1"	25'-5"	20'-10"	18'-3"
	57	0.0235	16	30'-1"	23'-11"	20'-10"	31'-0"	20'-10"	18'-3"	22'-6"	18'-12"	16'-7"
	57	0.0235	24	25'-5"	20'-10"	18'-3"	21'-5"	18'-3"	15'-11"	19'-0"	16'-7"	14'-5"

**Notes:**

- Viper composite limiting heights are based on testing in accordance with ICC-ES acceptance criteria AC86-2012.
- Limiting heights are established by considering flexure, shear, web crippling, and deflection.
- No screws are required between stud and track, except as required by ASTM C754. Composite heights are based on using standard top track. Mechanically fastening of gypsum panel to the stud and track is required.
- Viper-X composite limiting heights based on a single layer of 5/8" type X gypsum board applied vertically to both sides of the wall over full height. 5/8" Type X wallboard from the following manufacturers are acceptable: USG, National, Georgia-Pacific, Temple Inland, CertainTeed, American, & LaFarge.
- See page 4 for additional table notes.



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## Table Notes

1. 5 pounds per square foot (psf), 7.5 psf, and 10 psf loads have **not** been reduced for strength or deflection checks; full lateral load is applied.
2. Web crippling check is based on 1" end bearing.
3. Allowable moment is the lesser of  $M_{ai}$  and  $M_{ad}$ . Stud distortional buckling based on an assumed  $K_{\phi} = 0$ .
4. Limiting heights are based on steel properties only (non-composite) without the contribution of sheathing to strengthen and stiffen the assembly. Properly fastened sheathing is still required for members to be considered fully braced.
5. See page 5 for additional table notes.

SUPREME Interior Wall Heights - Non-Composite - Fully Braced												
Section	F <sub>y</sub> (ksi)	L <sub>u</sub>	Spacing (in) oc	5 psf			7.5 psf			10 psf		
				L/120	L/240	L/360	L/120	L/240	L/360	L/120	L/240	L/360
162SFS125-D25	57	24.4	12	9' 4"	-	-	-	-	-	-	-	-
			16	8' 1"	-	-	-	-	-	-	-	-
			24	-	-	-	-	-	-	-	-	-
162SFS-D20	57	29.1	12	10' 5"	8' 3"	-	9' 1"	-	-	-	-	-
			16	9' 5"	-	-	-	-	-	-	-	-
			24	-	-	-	-	-	-	-	-	-
162SFS-30EQD	57	29.0	12	11' 0"	8' 9"	-	9' 8"	-	-	8' 9"	-	-
			16	10' 0"	-	-	8' 9"	-	-	-	-	-
			24	8' 9"	-	-	-	-	-	-	-	-
162SFS-33EQD	57	29.0	12	11' 0"	8' 9"	-	9' 8"	-	-	8' 9"	-	-
			16	10' 0"	-	-	8' 9"	-	-	-	-	-
			24	8' 9"	-	-	-	-	-	-	-	-
250SFS125-D25	57	24.0	12	12' 10"	10' 2"	8' 11"	10' 6"	8' 11"	-	9' 1"	8' 1"	-
			16	11' 2"	9' 3"	8' 1"	9' 1"	8' 1"	-	-	-	-
			24	9' 1"	8' 1"	-	-	-	-	-	-	-
250SFS-D20	57	28.1	12	14' 4"	11' 4"	9' 11"	12' 4"	9' 11"	8' 8"	10' 8"	9' 0"	-
			16	13' 0"	10' 4"	9' 0"	10' 8"	9' 0"	-	9' 3"	8' 2"	-
			24	10' 8"	9' 0"	-	8' 9"	-	-	-	-	-
250SFS-30EQD	57	28.0	12	15' 4"	12' 2"	10' 7"	13' 5"	10' 7"	9' 3"	12' 2"	9' 8"	8' 5"
			16	13' 11"	11' 1"	9' 8"	12' 2"	9' 8"	8' 5"	11' 1"	8' 9"	-
			24	12' 2"	9' 8"	8' 5"	10' 7"	8' 5"	-	9' 5"	-	-
250SFS-33EQD	57	28.0	12	15' 4"	12' 2"	10' 7"	13' 5"	10' 7"	9' 3"	12' 2"	9' 8"	8' 5"
			16	13' 11"	11' 1"	9' 8"	12' 2"	9' 8"	8' 5"	11' 1"	8' 9"	-
			24	12' 2"	9' 8"	8' 5"	10' 7"	8' 5"	-	9' 5"	-	-
350SFS125-D25 <sup>1</sup>	57	23.6	12	14' 4"	12' 11"	11' 3"	11' 8"	11' 3"	9' 10"	10' 1"	10' 1"	8' 11"
			16	12' 5"	11' 9"	10' 3"	10' 1"	10' 1"	8' 11"	8' 9"	8' 9"	8' 1"
			24	10' 1"	10' 1"	8' 11"	8' 3"	8' 3"	-	-	-	-
350SFS-D20	57	27.6	12	17' 11"	14' 7"	12' 8"	14' 7"	12' 8"	11' 1"	12' 8"	11' 7"	10' 1"
			16	15' 6"	13' 3"	11' 7"	12' 8"	11' 7"	10' 1"	10' 11"	10' 6"	9' 2"
			24	12' 8"	11' 7"	10' 1"	10' 4"	10' 1"	8' 10"	8' 11"e	8' 11"e	8' 0"
350SFS-30EQD	57	27.6	12	19' 11"	15' 10"	13' 10"	17' 5"	13' 10"	12' 1"	15' 10"	12' 7"	10' 11"
			16	18' 1"	14' 4"	12' 7"	15' 10"	12' 7"	10' 11"	13' 9"	11' 5"	9' 11"
			24	15' 10"	12' 7"	10' 11"	13' 0"	10' 11"	9' 7"	11' 3"	9' 11"	8' 8"
350SFS-33EQD	57	27.6	12	19' 11"	15' 10"	13' 10"	17' 5"	13' 10"	12' 1"	15' 10"	12' 7"	10' 11"
			16	18' 1"	14' 4"	12' 7"	15' 10"	12' 7"	10' 11"	13' 9"	11' 5"	9' 11"
			24	15' 10"	12' 7"	10' 11"	13' 0"	10' 11"	9' 7"	11' 3"	9' 11"	8' 8"
362SFS125-D25 <sup>1</sup>	57	23.6	12	14' 6"	13' 5"	11' 9"	11' 10"	11' 8"	10' 3"	10' 3"	10' 3"	9' 4"
			16	12' 7"	12' 2"	10' 8"	10' 3"	10' 3"	9' 4"	8' 11"	8' 11"	8' 5"
			24	10' 3"	10' 3"	9' 4"	8' 5"	8' 5"	8' 1"	-	-	-
362SFS-D20	57	27.6	12	18' 4"	15' 2"	13' 3"	14' 11"	13' 2"	11' 7"	12' 11"	11' 11"	10' 6"
			16	15' 10"	13' 9"	12' 0"	12' 11"	11' 11"	10' 6"	11' 3"	10' 9"	9' 7"
			24	12' 11"	11' 11"	10' 6"	10' 7"	10' 4"	9' 2"	9' 2"e	9' 2"e	8' 3"
362SFS-30EQD	57	27.5	12	20' 6"	16' 3"	14' 2"	17' 11"	14' 2"	12' 5"	16' 3"	12' 11"	11' 3"
			16	18' 7"	14' 9"	12' 11"	16' 3"	12' 11"	11' 3"	14' 1"	11' 9"	10' 3"
			24	16' 3"	12' 11"	11' 3"	13' 3"	11' 3"	9' 10"	11' 6"	10' 3"	8' 11"
362SFS-33EQD	57	27.5	12	20' 6"	16' 3"	14' 2"	17' 11"	14' 2"	12' 5"	16' 3"	12' 11"	11' 3"
			16	18' 7"	14' 9"	12' 11"	16' 3"	12' 11"	11' 3"	14' 1"	11' 9"	10' 3"
			24	16' 3"	12' 11"	11' 3"	13' 3"	11' 3"	9' 10"	11' 6"	10' 3"	8' 11"

<sup>1</sup>Web height-to-thickness ratio exceeds 200. Web stiffeners are required at all support points and concentrated loads.  
 "e" Web stiffeners required at ends.

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## SUPREME Interior Wall Heights - Non-Composite - Fully Braced

Section	F <sub>y</sub> (ksi)	L <sub>w</sub>	Spacing (in) oc	5 psf			7.5 psf			10 psf		
				L/120	L/240	L/360	L/120	L/240	L/360	L/120	L/240	L/360
400SFS125-D25 <sup>1</sup>	57	23.4	12	15' 0"	14' 1"	12' 4"	12' 3"	12' 3"	10' 9"	10' 7"	10' 7"	9' 9"
			16	13' 0"	12' 10"	11' 2"	10' 7"	10' 7"	9' 9"	9' 2"	9' 2"	8' 10"
			24	10' 7"	10' 7"	9' 9"	8' 8"	8' 8"	8' 6"	-	-	-
400SFS-D20 <sup>1</sup>	57	27.5	12	19' 5"	16' 0"	14' 0"	15' 11"	14' 0"	12' 3"	13' 9"	12' 9"	11' 1"
			16	16' 10"	14' 7"	12' 9"	13' 9"	12' 9"	11' 1"	11' 11"	11' 7"	10' 1"
			24	13' 9"	12' 9"	11' 1"	11' 3"	11' 1"	9' 8"	9' 8"	9' 9"	8' 10"
400SFS-30EQD	57	27.4	12	22' 2"	17' 7"	15' 4"	19' 4"	15' 4"	13' 5"	17' 1"	13' 11"	12' 2"
			16	20' 2"	16' 0"	13' 11"	17' 1"	13' 11"	12' 2"	14' 10"	12' 8"	11' 1"
			24	17' 1"	13' 11"	12' 2"	13' 11"	12' 2"	10' 8"	12' 1"	11' 1"	9' 8"
400SFS-33EQD	57	27.4	12	22' 2"	17' 7"	15' 4"	19' 4"	15' 4"	13' 5"	17' 1"	13' 11"	12' 2"
			16	20' 2"	16' 0"	13' 11"	17' 1"	13' 11"	12' 2"	14' 10"	12' 8"	11' 1"
			24	17' 1"	13' 11"	12' 2"	13' 11"	12' 2"	10' 8"	12' 1"	11' 1"	9' 8"
550SFS-30EQD <sup>1</sup>	57	26.9	12	28' 5"	22' 8"	19' 10"	23' 3"	19' 10"	17' 4"	20' 1"	18' 0"	15' 9"
			16	24' 8"	20' 7"	18' 0"	20' 1"	18' 0"	15' 9"	17' 5"	16' 4"	14' 3"
			24	20' 1"	18' 0"	15' 9"	16' 5"	15' 9"	13' 9"	14' 2"	14' 2"	12' 6"
550SFS-33EQD <sup>1</sup>	57	26.9	12	28' 5"	22' 8"	19' 10"	23' 3"	19' 10"	17' 4"	20' 1"	18' 0"	15' 9"
			16	24' 8"	20' 7"	18' 0"	20' 1"	18' 0"	15' 9"	17' 5"	16' 4"	14' 3"
			24	20' 1"	18' 0"	15' 9"	16' 5"	15' 9"	13' 9"	14' 2"	14' 2"	12' 6"
600SFS-30EQD <sup>1</sup>	57	26.7	12	29' 8"	23' 7"	20' 8"	24' 2"	20' 8"	18' 0"	20' 11"	18' 9"	16' 4"
			16	25' 8"	21' 5"	18' 9"	20' 11"	18' 9"	16' 4"	18' 2"	17' 0"	14' 10"
			24	20' 11"	18' 9"	16' 4"	17' 1"	16' 4"	14' 3"	14' 10"	14' 10"	13' 0"
600SFS-33EQD <sup>1</sup>	57	26.7	12	29' 8"	23' 7"	20' 8"	24' 2"	20' 8"	18' 0"	20' 11"	18' 9"	16' 4"
			16	25' 8"	21' 5"	18' 9"	20' 11"	18' 9"	16' 4"	18' 2"	17' 0"	14' 10"
			24	20' 11"	18' 9"	16' 4"	17' 1"	16' 4"	14' 3"	14' 10"	14' 10"	13' 0"

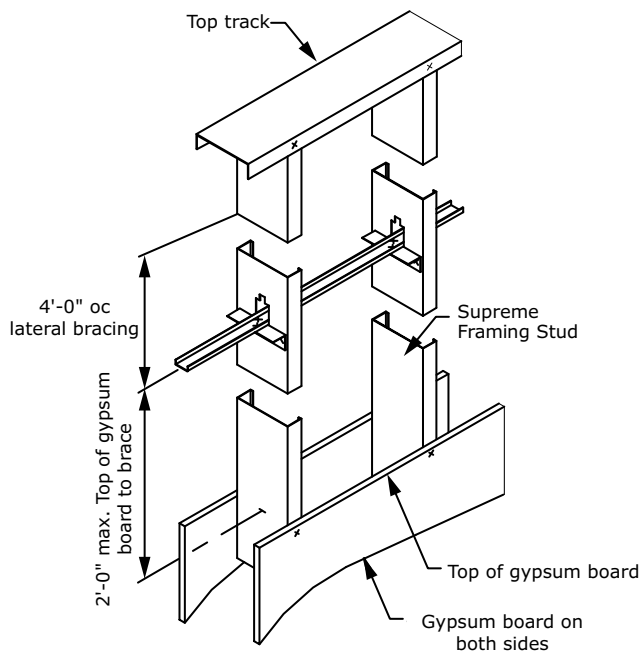
<sup>1</sup>Web height-to-thickness ratio exceeds 200. Web stiffeners are required at all support points and concentrated loads.

<sup>2</sup>"e" Web stiffeners required at ends.

See Table Notes on page 24.

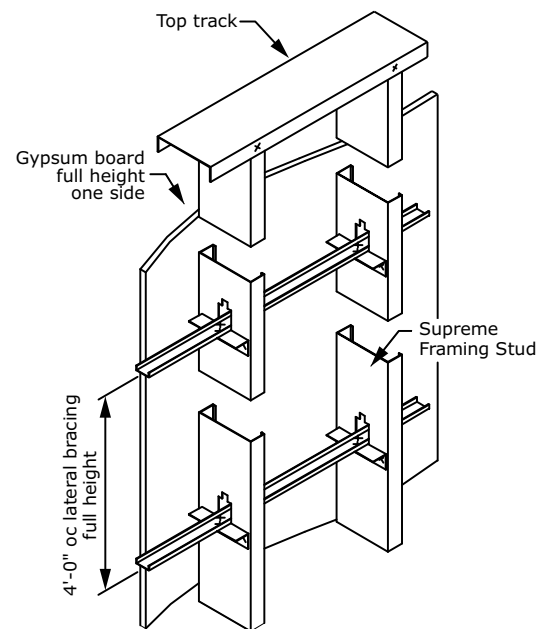
### Lateral Bracing

Example of lateral bracing at wall not sheathed at full height.



### Lateral Bracing

Example of lateral bracing at wall sheathed at full height on one side.



***BSE***

**B**rienen **S**tructural **E**ngineers, P.S.

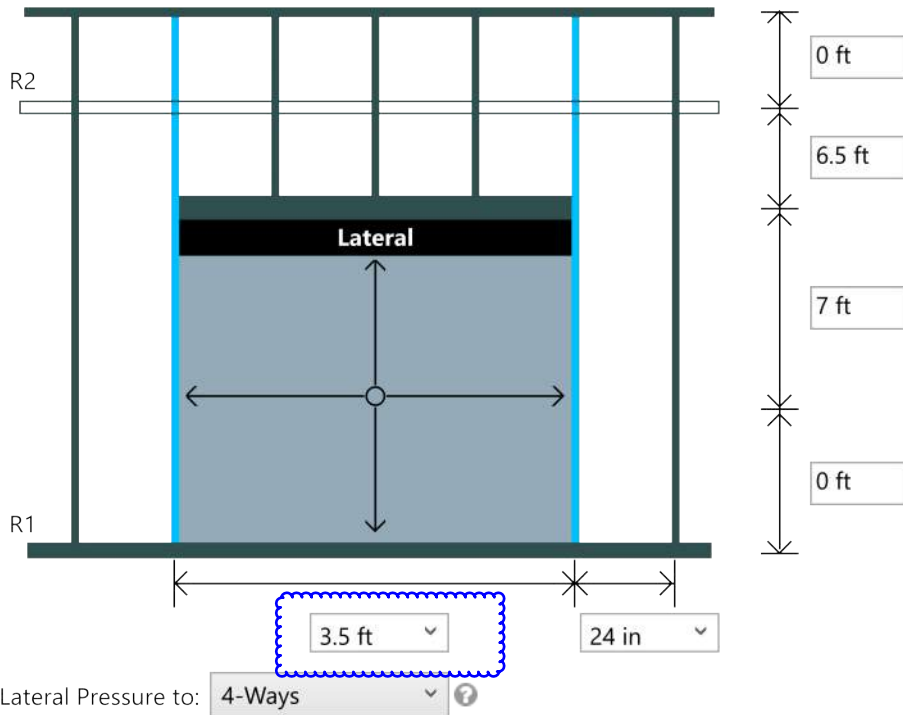
**INFILL CFS OPENING DESIGNS**

# SINGLE DOOR OPN'G INFILL WALL 6" STUDS

Project Name: Centeris - Copy  
 Model: FINAL - 6" INFILL HDR @ SGL DRWY  
 Code: 2012 NASPEC [AISI S100-2012]

Date: 02/29/2024

Simpson Strong-Tie® CFS Designer™ 5.0.1.0



**Design Loads**

Wall Lateral Pressure :	<b>5 psf</b>
Parapet Lateral Pressure :	
RO Lateral Pressure :	<b>4-Ways</b>
Lateral element force multiplier	
Strength :	<b>1.0</b>
Deflection :	<b>0.7</b>
Header:	<b>Strongback, Lateral Track</b>
Gravity Load at Header:	<b>14 psf</b>

**Brace Settings**

Component(s)	Members(s)	Flexural Bracing	Axial KyLy	Axial KtLt	Distortional K-Phi(lb-in/in)	Distortional Lm	Interconnection Spacing
Wall Studs	600S125-33(33), Single@24 in o/c	48 in	48 in	48 in	0	None	N/A
Jamb Studs	600S125-33(33), Single	48 in	48 in	48 in	0	None	N/A
Lateral Header	600T125-33(33), Single	Full	N/A	N/A	0	None	N/A

**Analysis Results**

Component(s)	Members(s)	Axial Load (lb)	Max KL/r	Max. Moment (ft-lb)	Max. Shear (lb)	Bottom Reaction (lb)	Top or End Reaction (lb)
Wall Studs	600S125-33(33), Single@24 in o/c	0.0	N/A	227.8	67.5	67.5	67.5
Jamb Studs	600S125-33(33), Single	159.3	128	312.8	85.2	92.8	64.4
Lateral Header	600T125-33(33), Single	N/A	N/A	33.8	36.1	N/A	36.1

**Design Results**

Component(s)	Members(s)	Deflection		A + M Interaction	V + M Interaction	Web Stiffeners	Design OK
		Span	Parapet				
Wall Studs	600S125-33(33), Single@24 in o/c	L/1243	L/0	0.439	0.11	NA	Yes
Jamb Studs	600S125-33(33), Single	L/964	L/0	0.724	0.52	NA	Yes
Lateral Header	600T125-33(33), Single	L/30173	NA	0.07	0.07	No	Yes

**Simpson Strong-Tie® Connectors @ Studs**

Support	Rx(lb)	Ry(lb)	Simpson Strong-Tie® Connector	Connector Interaction	Anchor Interaction
R2	67.50	0.00	SCB45.5(2) & (2) #12-24 SST X or XL to A36 Steel	13.78 %	6.05 %
R1	67.50	378.00	600T125-33 (33) & (1) .157" SST PDPA/PDPAT-62KP to steel (3/16" to 1/2" thickness)	27.78 %	30.65 %

\* Reference catalog for connector and anchor requirement notes as well as screw placements requirement

Project Name: Centeris - Copy

Model: FINAL - 6" INFILL HDR @ SGL DRWY

Date: 02/29/2024

Code: 2012 NASPEC [AISI S100-2012]

Simpson Strong-Tie® CFS Designer™ 5.0.1.0

**Simpson Strong-Tie® Connectors @ Jamb**

Support	Rx(lb)	Ry(lb)	Simpson Strong-Tie® Connector	Connector Interaction	Anchor Interaction
R2	64.38	0.00	600T250-33 (33) & (1) .157" SST PDPA/PDPAT-62KP to steel (3/16" to 1/2" thickness)	67.42 %	39.34 %
R1	92.81	446.25	600T125-33 (33) & (1) .157", 3/4" embed SST PDPA/PDPAT to 4000 nw concrete	76.40 %	68.75 %

\* Reference catalog for connector and anchor requirements, as well as screw placement requirements.

**Simpson Strong-Tie® Wall Stud Bridging Connectors @ Stud**

Span/Parapet	Bracing Length(in.)	Design Number of Braces	Pn(lb.)	LSUBH (Min) <sup>1</sup>	LSUBH (Max) <sup>1</sup>	SUBH (Min) <sup>1</sup>	SUBH (Max) <sup>1</sup>	MSUBH (Min) <sup>1</sup>	MSUBH (Max) <sup>1</sup>
Span	48	N/A	0.0	No Soln	No Soln	No Soln	No Soln	No Soln	No Soln

**Simpson Strong-Tie® Wall Stud Bridging Connectors @ Jamb**

Span/Parapet	Bracing Length(in.)	Design Number of Braces	Pn(lb.)	LSUBH (Min) <sup>1</sup>	LSUBH (Max) <sup>1</sup>	SUBH (Min) <sup>1</sup>	SUBH (Max) <sup>1</sup>	MSUBH (Min) <sup>1</sup>	MSUBH (Max) <sup>1</sup>
Span	48	4	0.0	No Soln	No Soln	No Soln	No Soln	No Soln	No Soln

**Notes:**

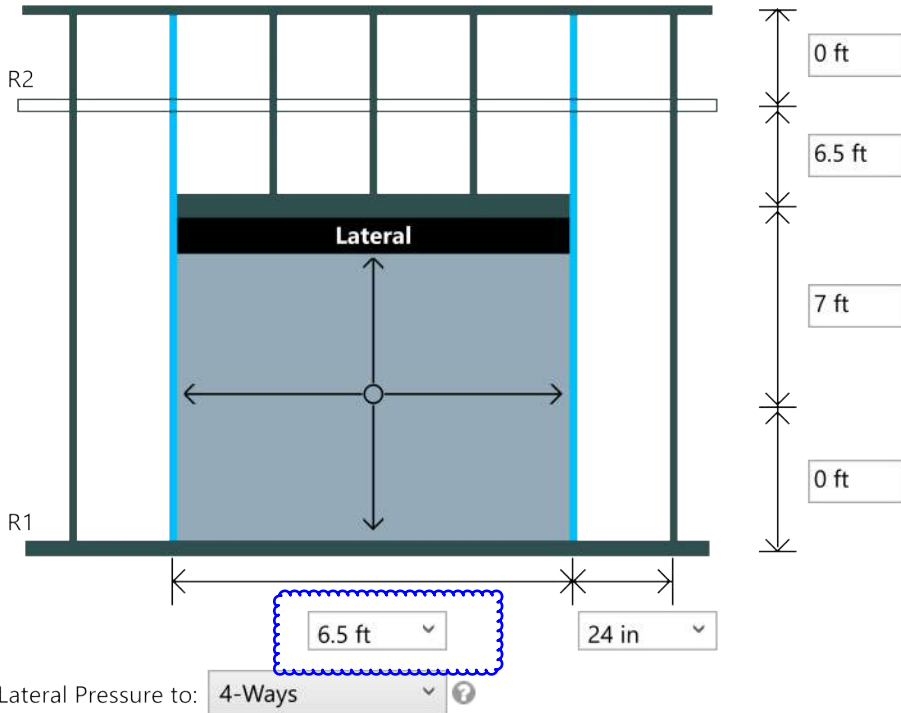
- 1) Values in parentheses are stress ratios.
- 2) Bridging connectors are not designed for back-back, box, or built-up sections.
- 3) Reference [www.strongtie.com](http://www.strongtie.com) for latest load data, important information, and general notes.
- 4) CFS Designer will not select bridging connectors unless all flexural and axial bracing settings are the same.
- 5) If the bracing length is larger than the span length, bridging connectors are not designed.

# DOUBLE DOOR OPN'G INFILL WALL 6" STUDS

Project Name: Centeris - Copy  
 Model: FINAL - 6" INFILL HDR @ DBL DRWY  
 Code: 2012 NASPEC [AISI S100-2012]

Date: 02/29/2024

Simpson Strong-Tie® CFS Designer™ 5.0.1.0



**Design Loads**

Wall Lateral Pressure :	5 psf
Parapet Lateral Pressure :	
RO Lateral Pressure :	4-Ways
Lateral element force multiplier	
Strength :	1.0
Deflection :	1
Header:	<b>Strongback, Lateral Track</b>
Gravity Load at Header:	14 psf

**Brace Settings**

Component(s)	Members(s)	Flexural Bracing	Axial KyLy	Axial KtLt	Distortional K-Phi(lb-in/in)	Distortional Lm	Interconnection Spacing
Wall Studs	600S125-33(33), Single@24 in o/c	48 in	48 in	48 in	0	None	N/A
Jamb Studs	600S125-43(33), Single	48 in	48 in	48 in	0	None	N/A
Lateral Header	600T125-33(33), Single	Full	N/A	N/A	0	None	N/A

**Analysis Results**

Component(s)	Members(s)	Axial Load (lb)	Max KL/r	Max. Moment (ft-lb)	Max. Shear (lb)	Bottom Reaction (lb)	Top or End Reaction (lb)
Wall Studs	600S125-33(33), Single@24 in o/c	0.0	N/A	227.8	67.5	67.5	67.5
Jamb Studs	600S125-43(33), Single	295.8	130	483.4	117.0	143.4	90.6
Lateral Header	600T125-33(33), Single	N/A	N/A	143.0	79.2	N/A	79.2

**Design Results**

Component(s)	Members(s)	Deflection		A + M Interaction	V + M Interaction	Web Stiffeners	Design OK
		Span	Parapet				
Wall Studs	600S125-33(33), Single@24 in o/c	L/870	L/0	0.439	0.11	NA	Yes
Jamb Studs	600S125-43(33), Single	L/601	L/0	0.829	0.53	NA	Yes
Lateral Header	600T125-33(33), Single	L/2704	NA	0.29	0.29	No	Yes

**Simpson Strong-Tie® Connectors @ Studs**

Support	Rx(lb)	Ry(lb)	Simpson Strong-Tie® Connector	Connector Interaction	Anchor Interaction
R2	67.50	0.00	SCB45.5(2) & (2) #12-24 SST X or XL to A36 Steel	13.78 %	6.05 %
R1	67.50	378.00	600T125-33 (33) & (1) .157" SST PDPA/PDPAT-62KP to steel (3/16" to 1/2" thickness)	27.78 %	30.65 %

\* Reference catalog for connector and anchor requirement notes as well as screw placements requirement

Project Name: Centeris - Copy

Model: FINAL - 6" INFILL HDR @ DBL DRWY

Date: 02/29/2024

Code: 2012 NASPEC [AISI S100-2012]

Simpson Strong-Tie® CFS Designer™ 5.0.1.0

**Simpson Strong-Tie® Connectors @ Jamb**

Support	Rx(lb)	Ry(lb)	Simpson Strong-Tie® Connector	Connector Interaction	Anchor Interaction
R2	90.63	0.00	600T250-33 (33) & (1) .157" SST PDPA/PDPAT-62KP to steel (3/16" to 1/2" thickness)	94.91 %	55.38 %
R1	143.44	582.75	600T125-33 (33) & (1) .157" SST PDPA/PDPAT-62KP to steel (3/16" to 1/2" thickness)	69.96 %	65.14 %

\* Reference catalog for connector and anchor requirements, as well as screw placement requirements.

**Simpson Strong-Tie® Wall Stud Bridging Connectors @ Stud**

Span/Parapet	Bracing Length(in.)	Design Number of Braces	Pn(lb.)	LSUBH (Min) <sup>1</sup>	LSUBH (Max) <sup>1</sup>	SUBH (Min) <sup>1</sup>	SUBH (Max) <sup>1</sup>	MSUBH (Min) <sup>1</sup>	MSUBH (Max) <sup>1</sup>
Span	48	N/A	0.0	No Soln	No Soln	No Soln	No Soln	No Soln	No Soln

**Simpson Strong-Tie® Wall Stud Bridging Connectors @ Jamb**

Span/Parapet	Bracing Length(in.)	Design Number of Braces	Pn(lb.)	LSUBH (Min) <sup>1</sup>	LSUBH (Max) <sup>1</sup>	SUBH (Min) <sup>1</sup>	SUBH (Max) <sup>1</sup>	MSUBH (Min) <sup>1</sup>	MSUBH (Max) <sup>1</sup>
Span	48	4	0.0	No Soln	No Soln	No Soln	No Soln	No Soln	No Soln

**Notes:**

- 1) Values in parentheses are stress ratios.
- 2) Bridging connectors are not designed for back-back, box, or built-up sections.
- 3) Reference [www.strongtie.com](http://www.strongtie.com) for latest load data, important information, and general notes.
- 4) CFS Designer will not select bridging connectors unless all flexural and axial bracing settings are the same.
- 5) If the bracing length is larger than the span length, bridging connectors are not designed.



PRCTI20240333

# **BSE**

**B**rienen **S**tructural **E**ngineers, P.S.

## CFS JOIST FRAMING DESIGN

# BSE

Brien Structural Engineers, P.S.

JOISTS : DEAD = 20PSF TOT  
LIVE = 40PSF

IF WE USE 8" STUDS → 800 S200-68 @ 24" o.c.  
800 S162-54 @ 16" o.c.

IF WE USE 10" STUDS → 1000 S200-54 @ 24" o.c.  
1000 S137-54 @ 16" o.c.

R<sub>XIL</sub> = @ 24" SPACING = 960#  
@ 16" SPACING = 640#

JOIST CONNECTOR TO GIRDER: USE S/HJC W/ (6) #14 SMS TO JOIST  
AND 0.157" PDPAT-62KP TO STEEL

FOR 54 mil JOISTS, V<sub>ALLOW</sub> = 1190#  
DEMAND (ASD) = 960#  
DCR = 0.81 ✓

(FOR MORE INFO, SEE SIMPSON CFS DESIGNER OUTPUT)

# BSE

Brien Structural Engineers, P.S.

## JOIST BRACING REQUIREMENTS, CONTINUED

### B2.6 Bracing Design

Bracing members shall be designed either on the basis of discretely braced design or on the basis of continuously braced design, in accordance with the following:

- (a) Discretely Braced Design. For discretely braced design, *bracing* members shall be designed in accordance with Section C2.2 of AISI S100 [CSA S136].
- (b) Continuously Braced Design. For continuously braced design, *bracing* members shall be designed in accordance with Section C2.2 of AISI S100 [CSA S136], unless the following requirements, as applicable, are met:
  - (1) Members are spaced no greater than 24 inches (610 mm) on center.
  - (2) The sheathing or deck shall consist of a minimum of 3/8 inch (9.5 mm) wood structural sheathing that complies with DOC PS 1, DOC PS 2, CSA O437 or CSA O325, or steel deck with a minimum profile depth of 9/16 in. (14.3 mm) and a minimum thickness of 0.0269 in. (0.683 mm). The sheathing or deck shall be attached with minimum No. 8 screws at a maximum 12 inches (305 mm) on center.
  - (3) Floor joists and ceiling joists with simple or continuous spans that exceed 8 feet (2.44 m) shall have the tension flanges laterally braced. Each intermediate brace shall be spaced at 8 feet (2.44 m) maximum and shall be designed to resist a required lateral force,  $P_L$ , determined in accordance with the following:

For uniform loads:

$$P_L = 1.5(m/d) F \quad (\text{Eq. B2.6-1})$$

where

$m$  = Distance from shear center to mid-plane of *web*

$d$  = Depth of *C-shape* section

$F$  =  $wa$

$w$  = Uniform design load [factored load]

$a$  = Distance between center line of braces

### FOR OUR 10" DEEP JOISTS

$$P_L = 1.5 * (1.14" / 10") * (1.2 * 20\text{psf} + 1.6 * 40\text{psf}) * (2\text{ft oc}) * (8\text{ft})$$

$$P_L = 240 \text{ lbs}$$

### YIELD STRENGTH OF 33MIL x 1 1/2" STRAP

$$\phi T_n = (0.9) * (1.5") * (0.035") * (33\text{ksi}) = 1560 \text{ lbs}$$

# BSE

Brien Structural Engineers, P.S.

## JOIST BRACING REQUIREMENTS

### B1.2 Design Basis

The proportioning, designing and detailing of *cold-formed steel light-frame lateral force-resisting systems, trusses, structural members, connections and connectors* shall be in accordance with AISI S100 [CSA S136], and the reference documents except as modified or supplemented by the requirements of this Standard.

#### B1.2.1 Floor Joists, Ceiling Joists and Roof Rafters

**B1.2.1.1** *Floor joists, ceiling joists and roof rafters* shall be designed either on the basis of discretely braced design or on the basis of continuously braced design, in accordance with the following:

- (a) Discretely Braced Design. Floor and roof assemblies using discretely braced design shall be designed neglecting the structural *bracing* and composite-action contribution of attached sheathing or deck. The discretely braced design requirements of the Standard shall be applied to assemblies where the

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APPLICABLE SECTION  
FOR DETAIL 14/MS1.2

sheathing or deck is not attached directly to *structural members*.

- (b) Continuously Braced Design. Unless noted otherwise in Section B2 or B4, the continuously braced design requirements of this Standard shall be limited to assemblies where *structural sheathing or steel deck* is attached directly to *floor joists, ceiling joists and roof rafters* that comply with all of the following conditions:

- (1) Maximum *web* depth = 14 inches (356 mm)
- (2) Maximum *design thickness* = 0.1242 inches (3.155 mm)
- (3) Minimum design *yield strength*,  $F_y = 33$  ksi (230 MPa)
- (4) Maximum design *yield strength*,  $F_y = 50$  ksi (345 MPa)

APPLICABLE SECTION  
FOR BRACING USING  
PW WEAR SURFACE  
TOP AND GYP BOT

# TYP CFS CEILING JOISTS

## 10" STUDS, 24" OC.

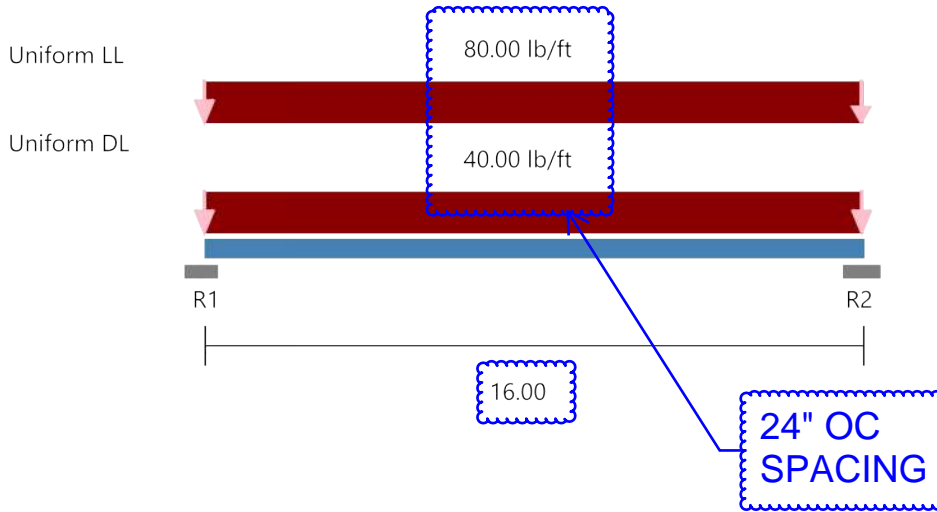
Project Name: Centeris

Model: 16ft Floor Joist @ 10" @ 24" OC

Code: 2012 NASPEC [AISI S100-2012]

Date: 02/08/2024

Simpson Strong-Tie® CFS Designer™ 5.0.1.0



**Section :** 1000S200-54 (50 ksi) @ 24 in" o.c. Single C Stud (punched)

**Maxo =** 4254.2 ft-lb      **Va =** 1660.8 lb      **I =** 10.769 in<sup>4</sup>

**Deflection Limits:** Total Load - 240      Live Load - 360

- Load Comb:**
- 1. DL + LL All spans
  - 2. DL + LL Even spans
  - 3. DL + LL Odd spans
  - 4. LL All spans
  - 5. LL Even spans
  - 6. LL Odd spans

HANGER CONNECTION STIFFENS JOIST

**Joist Flexural and Deflection**

Span	Mmax (ft-lb)	K-phi (lb-in/in)	Lm (in)	Ma-dist (ft-lb)	Mmax/Ma min	Load Comb.	TL Defl	Load Comb.	LL Defl	Load Comb.
Span	3840	0.0	192.0	3884.7	0.988	1	L/345	1	L/517	4

**Joist Bending and Web Crippling**

Support	Load (lb)	Load Comb.	Bearing (in)	Pa (lb)	Pn (lb)	Max Intr.	Load Comb.	Stiffeners Required
R1	960.0	1	1.00	553.2	968.1	0.90	1	YES
R2	960.0	1	1.00	553.2	968.1	0.90	1	YES

**Joist Bending and Shear**

Support	Vmax (lb)	Load Comb.	Va Factor	V/Va	M/Ma	Intr. Unstiffened	Load Comb.	Intr. Stiffened	Load Comb.
R1	960.0	1	1.000	0.58	0.00	0.58	1	N/A	N/A
R2	960.0	1	1.000	0.58	0.00	0.58	1	N/A	N/A

**Joist Reaction and Connections**

Support	Rx(lb)	Ry(lb)	Simpson Strong-Tie Connector	Connector Interaction	Anchor Interaction
R1	0.0	960.0	S/HJCT (min) (6)#14 joist & (2) SST 0.157" PDPAT-62KP to A36 Steel	32.88 %	81.01 %

Project Name: Centeris

Model: 16ft Floor Joist @ 10" @ 24" OC - 40 psf LL - Duplicate

Date: 02/08/2024

Code: 2012 NASPEC [AISI S100-2012]

Simpson Strong-Tie® CFS Designer™ 5.0.1.0

R2	0.0	960.0	S/HJCT (min) (6)#14 joist & (2) SST 0.157" PDPAT-62KP to A36 Steel	32.88 %	81.01 %
----	-----	-------	---	---------	---------

\* Reference catalog for connector and anchor requirement notes as well as screw placement requirements

PRCTI20240333

**BSE**

**B**rienen **S**tructural **E**ngineers, P.S.

**HSS GIRDER FRAMING DESIGN**

# BSE

Brien Structural Engineers, P.S.

GIRDERS : LENGTH = 16'-20" column  $\approx$  14'-6"  
 DEAD = 20 psf, LIVE = 40 psf

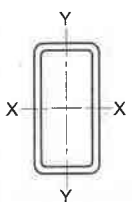
~~If we use 10" STUBS  $\rightarrow$  (2) 100S 550-97 BOX W/2 (mom = 92.89)~~

If we use HSS TUBE  $\rightarrow$   $M_A = 25.5 \text{ K}\cdot\text{ft}$   
 $I_{REQ'D} \geq \frac{5(960 \text{ lb/ft})(14.5')^4}{384(29,000 \text{ ksi})(0.7')} * \frac{1 \text{ K}(12 \text{ in})^3}{1440(1 \text{ ft})^3} = 47.0 \text{ in}^4$

USE HSS 8x4x5/16"

$R_{X-X} = 7.0 \text{ KIPS (ASD)} \text{ OR } (10.3 \text{ KIPS LRFD})$

## CHECK STIFFNESS OF HSS

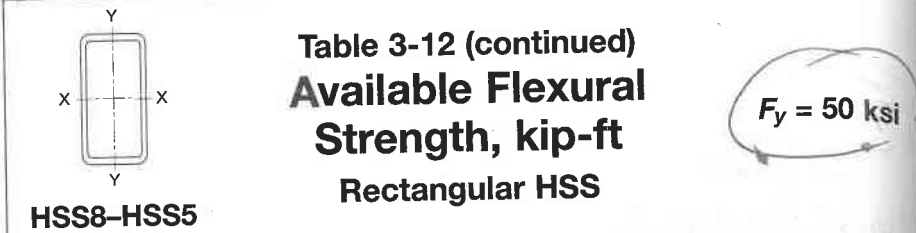


**Table 1-11 (continued)**  
**Rectangular HSS**  
**Dimensions and Properties**

Shape	Design Wall Thickness, t in.	Nominal Wt. lb/ft	Area, A in. <sup>2</sup>	b/t	h/t	Axis X-X			
						I	S	r	Z
						in. <sup>4</sup>	in. <sup>3</sup>	in.	in. <sup>3</sup>
HSS8x4x5/8	0.581	42.30	11.7	3.88	10.8	82.0	20.5	2.64	27.4
x1/2	0.465	35.24	9.74	5.60	14.2	71.8	17.9	2.71	23.5
x3/8	0.349	27.48	7.58	8.46	19.9	56.7	14.7	2.78	18.8
x5/16	0.291	23.34	6.43	10.7	24.5	51.0	12.8	2.82	16.1
x1/4	0.233	19.02	5.24	14.2	31.3	42.5	10.6	2.85	13.3
x3/16	0.174	14.53	3.98	20.0	43.0	33.1	8.27	2.88	10.2
x1/8	0.116	9.86	2.70	31.5	66.0	22.9	5.73	2.92	7.02



## CHECK STRENGTH OF HSS



**Table 3-12 (continued)**  
**Available Flexural Strength, kip-ft**  
**Rectangular HSS**

HSS8-HSS5

$F_y = 50 \text{ ksi}$

Shape		X-Axis		Y-Axis		Shape		X-Axis		Y-Axis	
		$M_n/\Omega_b$	$\phi_b M_n$	$M_n/\Omega_b$	$\phi_b M_n$			$M_n/\Omega_b$	$\phi_b M_n$	$M_n/\Omega_b$	$\phi_b M_n$
		ASD	LRFD	ASD	LRFD			ASD	LRFD	ASD	LRFD
HSS8x4x	5/8	68.4	103	41.4	62.3	HSS7x2x	1/4	19.1	28.7	7.53	11.3
	1/2	58.6	88.1	35.7	53.6		3/16	14.8	22.3	4.97	7.47
	3/8	46.9	70.5	28.7	43.1		1/8	10.3	15.5	2.79	4.19
	5/16	40.2	60.4	24.7	37.2	HSS6x5x	1/2	42.9	64.5	37.9	57.0
	1/4	33.2	49.9	18.9	28.4		3/8	34.4	51.8	30.4	45.8
	3/16	25.4	38.3	12.5	18.8	5/16	29.7	44.6	26.2	39.4	
	1/8	15.4	23.1	6.94	10.4	1/4	24.6	37.0	21.8	32.7	

## CHECK AVAILABILITY OF HSS

### AISC MEMBERS

HSS Rectangular	Grade	Atlas Tube Inc.	Nucor Tubular Products
8 x 4 x 5/16	A500	✓	✓

### NON-MEMBERS

HSS Rectangular	Grade	Bull Moose Tube Company	EXLTUBE	Hanna Steel Corp.	Longhorn Tube LP	Maruichi American Corp.	Maruichi Leavitt Pipe and Tube	Vest Inc.	Welded Tube Of Canada
8 x 4 x 5/16	A500	✓		✓	✓	✓	✓	✓	✓

# BSE

Brien Structural Engineers, P.S.

## CHECK CONNECTION OF HSS GIRDERS TO (E) CONC. COLUMNS

DEMANDS : VERTICAL RXNS = 7.0 KIPS (ASD) USE THIS IN HILTI PROFIS  
 OR 10.3 K (LRFD)

AXIAL DEMANDS =  $F_{P,ASD} = 0.7 F_p$  PER LATERAL SECTION

$$F_{P,ASD} = (0.7)(1.3K) = 910 \# (ASD)$$

$$\text{AMPLIFIED COMP LOAD} = (2.5)(910 \#)$$

$$F_p \Omega_c = 2275 \# (ASD)$$

$$F_{P,LRFD} = F_p = 1.3K$$

$$\text{AMPLIFIED COMP LOAD} = (2.5)(1.3K)$$

$$F_p \Omega_c = 3.25 K (LRFD)$$

USE THIS IN HILTI PROFIS

## BASEPLATE CHECKS OUT - PER HILTI PROFIS ANCHORAGE MAX PLATE STRESS USING FEM

$$\text{Overstresses} = 14.5 \text{ ksi} \rightarrow \text{DCR} = \frac{14.5 \text{ ksi}}{(36)(1.67)} = \underline{\underline{0.67}}$$

OK

## ANCHORAGE TO CONCRETE

COMBINED FORCES ON ANCHORS OK PER HILTI PROFIS  
 CALCULATIONS ON FOLLOWING PAGES

$$\text{Tension} \leq 62\% \text{ utilization (SEISMIC CASE)} \quad \frac{1.2D + 0.5L + E}{1.2D + 1.6L}$$

$$\text{Shear} \leq 90\% \text{ UTILIZATION (NON-SEISMIC CASE)}$$

$$\text{COMBINATION} \leq 90\% \text{ (NON-SEISMIC CASE)}$$

# BSE

Brien Structural Engineers, P.S.

## CHECK BOLTS in Side Plates

AMPLIFIED SEISMIC LOAD, TOTAL = 3.25 K

$$\phi T_n \text{ of A36 A.B.} = (0.9)(36 \text{ ksi})(0.442 \text{ in}^2) = 14.32 \text{ K}$$

## CHECK BOLT BRG @ HOLE - AISC SECTION J 3.10

$$\begin{aligned} R_{u \text{ max}} &= \sqrt{(\text{TENSION DEMAND})^2 + (\text{SHEAR DEMAND})^2} \\ &= \sqrt{(3.25 \text{ K}/4)^2 + (10.7 \text{ K}/4)^2} \\ &= 2.8 \text{ KIPS} \end{aligned}$$

$$\begin{aligned} \phi R_n &= (0.75) (1.2 * 2" * \frac{3}{8}" * 58 \text{ ksi}) = 39 \text{ K OK} \checkmark \\ &\text{OR} \\ &= (0.75) (2.4 * \frac{3}{4}" * \frac{3}{8}" * 58 \text{ ksi}) = 29 \text{ K OK} \checkmark \\ &\quad \text{CONTROLS} \end{aligned}$$

## Check Weld of SIDE CANN. PL to Face-Mounted PLATE

AMPLIFIED LOAD = 3.25 K (LREQ'D)

Length of 3/16" fillet weld Req'd

$$\phi R_n = 1.392 \text{ DL}$$

$$3.25 \text{ K} = 1.392 (3) (L)$$

L = 0.78" REQ'D, BUT 8" ON (2) WELDS  
EA. ARE PROVIDED.

OK



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**Specifier's comments:**

## 1 Input data

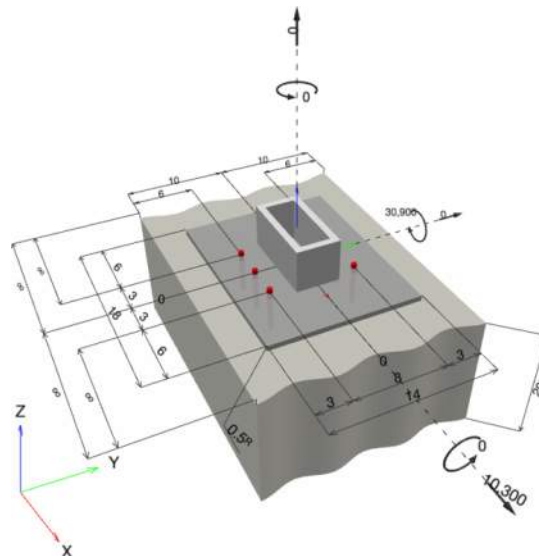
<b>Anchor type and diameter:</b>	<b>KWIK HUS-EZ (KH-EZ) 1/2 (4 1/4)</b>
Item number:	418076 KH-EZ 1/2"x5"
Effective embedment depth:	$h_{ef,act} = 3.220$ in., $h_{nom} = 4.250$ in.
Material:	Carbon Steel
Evaluation Service Report:	ESR-3027
Issued   Valid:	4/1/2022   12/1/2023
Proof:	Design Method ACI 318-19 / Mech
Stand-off installation:	$e_b = 0.000$ in. (no stand-off); $t = 0.500$ in.
Anchor plate <sup>R</sup> :	$l_x \times l_y \times t = 18.000$ in. x $14.000$ in. x $0.500$ in.; (Recommended plate thickness: not calculated)
Profile:	Rectangular HSS (AISC), HSS8X4X.625; (L x W x T) = $8.000$ in. x $4.000$ in. x $0.625$ in.
Base material:	cracked concrete, 4000, $f'_c = 4,000$ psi; $h = 20.000$ in.
<b>Installation:</b>	<b>hammer drilled hole, Installation condition: Dry</b>
Reinforcement:	tension: not present, shear: not present; no supplemental splitting reinforcement present edge reinforcement: none or < No. 4 bar



Application also possible with KWIK-X 1/2 (4 1/4)  $h_{nom2}$  under the selected boundary conditions.  
More information in section Alternative fastening data of this report.

<sup>R</sup> - The anchor calculation is based on a rigid anchor plate assumption.

### Geometry [in.] & Loading [lb, in.lb]





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1.1 Load combination and design results

Case	Description	Forces [lb] / Moments [in.lb]	Seismic	Max. Util. Anchor [%]
1	Combination 1	N = 3,250; V <sub>x</sub> = 5,800; V <sub>y</sub> = 0; M <sub>x</sub> = 0; M <sub>y</sub> = 17,400; M <sub>z</sub> = 0;	yes	75
<u>2</u>	<u>Combination 2</u>	<u>N = 0; V<sub>x</sub> = 10,300; V<sub>y</sub> = 0;</u> <u>M<sub>x</sub> = 0; M<sub>y</sub> = 30,900; M<sub>z</sub> = 0;</u>	<u>no</u>	<u>90</u>

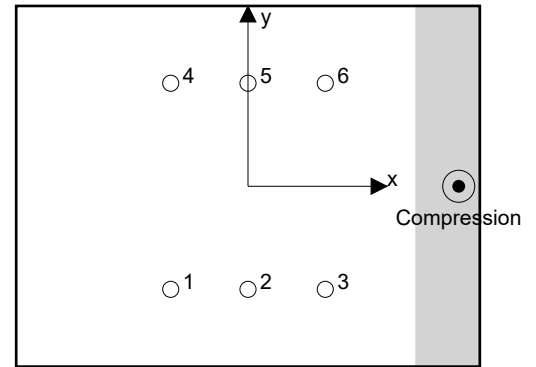
2 Load case/Resulting anchor forces

Controlling load case: 2 Combination 2

Anchor reactions [lb]

Tension force: (+Tension, -Compression)

Anchor	Tension force	Shear force	Shear force x	Shear force y
1	825	1,717	1,717	0
2	566	1,717	1,717	0
3	307	1,717	1,717	0
4	825	1,717	1,717	0
5	566	1,717	1,717	0
6	307	1,717	1,717	0



max. concrete compressive strain: 0.05 [%]  
 max. concrete compressive stress: 198 [psi]  
 resulting tension force in (x/y)=(0.000/0.000): 0 [lb]  
 resulting compression force in (x/y)=(17.182/7.000): 3,396 [lb]

Anchor forces are calculated based on the assumption of a rigid anchor plate.

3 Tension load

	Load N <sub>ua</sub> [lb]	Capacity $\phi N_n$ [lb]	Utilization $\beta_N = N_{ua}/\phi N_n$	Status
Steel Strength*	825	11,778	8	OK
Pullout Strength*	N/A	N/A	N/A	N/A
Concrete Breakout Failure**	3,396	10,059	34	OK

\* highest loaded anchor    \*\*anchor group (anchors in tension)


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**3.1 Steel Strength**

$N_{sa}$  = ESR value refer to ICC-ES ESR-3027  
 $\phi N_{sa} \geq N_{ua}$  ACI 318-19 Table 17.5.2

**Variables**

$A_{se,N}$ [in. <sup>2</sup> ]	$f_{uta}$ [psi]
0.16	112,540

**Calculations**

$N_{sa}$ [lb]
18,120

**Results**

$N_{sa}$ [lb]	$\phi_{steel}$	$\phi N_{sa}$ [lb]	$N_{ua}$ [lb]
18,120	0.650	11,778	825



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### 3.2 Concrete Breakout Failure

$$N_{cbg} = \left( \frac{A_{Nc}}{A_{Nc0}} \right) \psi_{ec,N} \psi_{ed,N} \psi_{c,N} \psi_{cp,N} N_b \quad \text{ACI 318-19 Eq. (17.6.2.1b)}$$

$$\phi N_{cbg} \geq N_{ua} \quad \text{ACI 318-19 Table 17.5.2}$$

$A_{Nc}$  see ACI 318-19, Section 17.6.2.1, Fig. R 17.6.2.1(b)

$$A_{Nc0} = 9 h_{ef}^2 \quad \text{ACI 318-19 Eq. (17.6.2.1.4)}$$

$$\psi_{ec,N} = \left( \frac{1}{1 + \frac{2 e_N}{3 h_{ef}}} \right) \leq 1.0 \quad \text{ACI 318-19 Eq. (17.6.2.3.1)}$$

$$\psi_{ed,N} = 0.7 + 0.3 \left( \frac{c_{a,min}}{1.5 h_{ef}} \right) \leq 1.0 \quad \text{ACI 318-19 Eq. (17.6.2.4.1b)}$$

$$\psi_{cp,N} = \text{MAX} \left( \frac{c_{a,min}}{c_{ac}}, \frac{1.5 h_{ef}}{c_{ac}} \right) \leq 1.0 \quad \text{ACI 318-19 Eq. (17.6.2.6.1b)}$$

$$N_b = k_c \lambda_a \sqrt{f_c} h_{ef}^{1.5} \quad \text{ACI 318-19 Eq. (17.6.2.2.1)}$$

#### Variables

$h_{ef}$ [in.]	$e_{c1,N}$ [in.]	$e_{c2,N}$ [in.]	$c_{a,min}$ [in.]	$\psi_{c,N}$
3.220	0.917	0.000	6.000	1.000
$c_{ac}$ [in.]	$k_c$	$\lambda_a$	$f_c$ [psij]	
5.250	17	1.000	4,000	

#### Calculations

$A_{Nc}$ [in. <sup>2</sup> ]	$A_{Nc0}$ [in. <sup>2</sup> ]	$\psi_{ec1,N}$	$\psi_{ec2,N}$	$\psi_{ed,N}$	$\psi_{cp,N}$	$N_b$ [lb]
276.56	93.32	0.840	1.000	1.000	1.000	6,212

#### Results

$N_{cbg}$ [lb]	$\phi_{concrete}$	$\phi N_{cbg}$ [lb]	$N_{ua}$ [lb]
15,475	0.650	10,059	3,396



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### 4 Shear load

	Load $V_{ua}$ [lb]	Capacity $\phi V_n$ [lb]	Utilization $\beta_v = V_{ua}/\phi V_n$	Status
Steel Strength*	1,717	5,547	31	OK
Steel failure (with lever arm)*	N/A	N/A	N/A	N/A
Pryout Strength**	10,300	25,776	40	OK
Concrete edge failure in direction y-**	10,300	12,465	83	OK

\* highest loaded anchor \*\*anchor group (relevant anchors)

#### 4.1 Steel Strength

$V_{sa}$  = ESR value refer to ICC-ES ESR-3027  
 $\phi V_{steel} \geq V_{ua}$  ACI 318-19 Table 17.5.2

#### Variables

$A_{se,V}$ [in. <sup>2</sup> ]	$f_{uta}$ [psi]
0.16	112,540

#### Calculations

$V_{sa}$ [lb]
9,245

#### Results

$V_{sa}$ [lb]	$\phi_{steel}$	$\phi V_{sa}$ [lb]	$V_{ua}$ [lb]
9,245	0.600	5,547	1,717





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#### 4.2 Pryout Strength

$$V_{cp,g} = k_{cp} \left[ \left( \frac{A_{Nc}}{A_{Nc0}} \right) \psi_{ec,N} \psi_{ed,N} \psi_{c,N} \psi_{cp,N} N_b \right] \quad \text{ACI 318-19 Eq. (17.7.3.1b)}$$

$$\phi V_{cp,g} \geq V_{ua} \quad \text{ACI 318-19 Table 17.5.2}$$

$A_{Nc}$  see ACI 318-19, Section 17.6.2.1, Fig. R 17.6.2.1(b)

$$A_{Nc0} = 9 h_{ef}^2 \quad \text{ACI 318-19 Eq. (17.6.2.1.4)}$$

$$\psi_{ec,N} = \left( \frac{1}{1 + \frac{2 e_N}{3 h_{ef}}} \right) \leq 1.0 \quad \text{ACI 318-19 Eq. (17.6.2.3.1)}$$

$$\psi_{ed,N} = 0.7 + 0.3 \left( \frac{c_{a,min}}{1.5 h_{ef}} \right) \leq 1.0 \quad \text{ACI 318-19 Eq. (17.6.2.4.1b)}$$

$$\psi_{cp,N} = \text{MAX} \left( \frac{c_{a,min}}{c_{ac}}, \frac{1.5 h_{ef}}{c_{ac}} \right) \leq 1.0 \quad \text{ACI 318-19 Eq. (17.6.2.6.1b)}$$

$$N_b = k_c \lambda_a \sqrt{f_c} h_{ef}^{1.5} \quad \text{ACI 318-19 Eq. (17.6.2.2.1)}$$

#### Variables

$k_{cp}$	$h_{ef}$ [in.]	$e_{c1,N}$ [in.]	$e_{c2,N}$ [in.]	$c_{a,min}$ [in.]
2	3.220	0.000	0.000	6.000
$\psi_{c,N}$	$c_{ac}$ [in.]	$k_c$	$\lambda_a$	$f_c$ [psi]
1.000	5.250	17	1.000	4,000

#### Calculations

$A_{Nc}$ [in. <sup>2</sup> ]	$A_{Nc0}$ [in. <sup>2</sup> ]	$\psi_{ec1,N}$	$\psi_{ec2,N}$	$\psi_{ed,N}$	$\psi_{cp,N}$	$N_b$ [lb]
276.56	93.32	1.000	1.000	1.000	1.000	6,212

#### Results

$V_{cp,g}$ [lb]	$\phi_{concrete}$	$\phi V_{cp,g}$ [lb]	$V_{ua}$ [lb]
36,823	0.700	25,776	10,300



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## 4.3 Concrete edge failure in direction y-

$$V_{cbg} = \left( \frac{A_{Vc}}{A_{Vc0}} \right) \Psi_{ec,V} \Psi_{ed,V} \Psi_{c,V} \Psi_{h,V} \Psi_{parallel,V} V_b \quad \text{ACI 318-19 Eq. (17.7.2.1b)}$$

$$\phi V_{cbg} \geq V_{ua} \quad \text{ACI 318-19 Table 17.5.2}$$

$A_{Vc}$  see ACI 318-19, Section 17.7.2.1, Fig. R 17.7.2.1(b)

$$A_{Vc0} = 4.5 c_{a1}^2 \quad \text{ACI 318-19 Eq. (17.7.2.1.3)}$$

$$\Psi_{ec,V} = \left( \frac{1}{1 + \frac{e_v}{1.5c_{a1}}} \right) \leq 1.0 \quad \text{ACI 318-19 Eq. (17.7.2.3.1)}$$

$$\Psi_{ed,V} = 0.7 + 0.3 \left( \frac{c_{a2}}{1.5c_{a1}} \right) \leq 1.0 \quad \text{ACI 318-19 Eq. (17.7.2.4.1b)}$$

$$\Psi_{h,V} = \sqrt{\frac{1.5c_{a1}}{h_a}} \geq 1.0 \quad \text{ACI 318-19 Eq. (17.7.2.6.1)}$$

$$V_b = \left( 7 \left( \frac{l_e}{d_a} \right)^{0.2} \sqrt{d_a} \right) \lambda_a \sqrt{f'_c} c_{a1}^{1.5} \quad \text{ACI 318-19 Eq. (17.7.2.2.1a)}$$

## Variables

$c_{a1}$ [in.]	$c_{a2}$ [in.]	$e_{cV}$ [in.]	$\Psi_{c,V}$	$h_a$ [in.]
6.000	-	0.000	1.000	20.000
$l_e$ [in.]	$\lambda_a$	$d_a$ [in.]	$f'_c$ [psi]	$\Psi_{parallel,V}$
3.220	1.000	0.500	4,000	2.000

## Calculations

$A_{Vc}$ [in. <sup>2</sup> ]	$A_{Vc0}$ [in. <sup>2</sup> ]	$\Psi_{ec,V}$	$\Psi_{ed,V}$	$\Psi_{h,V}$	$V_b$ [lb]
216.00	162.00	1.000	1.000	1.000	6,678

## Results

$V_{cbg}$ [lb]	$\phi_{concrete}$	$\phi V_{cbg}$ [lb]	$V_{ua}$ [lb]
17,807	0.700	12,465	10,300

## 5 Combined tension and shear loads, per ACI 318-19 section 17.8

$\beta_N$	$\beta_V$	$\zeta$	Utilization $\beta_{N,V}$ [%]	Status
0.338	0.826	5/3	90	OK

$$\beta_{NV} = \beta_N^{\zeta} + \beta_V^{\zeta} \leq 1$$

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**6 Warnings**

- The anchor design methods in PROFIS Engineering require rigid anchor plates per current regulations (AS 5216:2021, ETAG 001/Annex C, EOTA TR029 etc.). This means load re-distribution on the anchors due to elastic deformations of the anchor plate are not considered - the anchor plate is assumed to be sufficiently stiff, in order not to be deformed when subjected to the design loading. PROFIS Engineering calculates the minimum required anchor plate thickness with CBFEM to limit the stress of the anchor plate based on the assumptions explained above. The proof if the rigid anchor plate assumption is valid is not carried out by PROFIS Engineering. Input data and results must be checked for agreement with the existing conditions and for plausibility!
- Condition A applies where the potential concrete failure surfaces are crossed by supplementary reinforcement proportioned to tie the potential concrete failure prism into the structural member. Condition B applies where such supplementary reinforcement is not provided, or where pullout or pryout strength governs.
- Refer to the manufacturer's product literature for cleaning and installation instructions.
- For additional information about ACI 318 strength design provisions, please go to <https://submittals.us.hilti.com/PROFISAnchorDesignGuide/>
- Hilti post-installed anchors shall be installed in accordance with the Hilti Manufacturer's Printed Installation Instructions (MPII). Reference ACI 318-19, Section 26.7.

**Fastening meets the design criteria!**



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### 7 Installation data

Profile: Rectangular HSS (AISC), HSS8X4X.625; (L x W x T) = 8.000 in. x 4.000 in. x 0.625 in.

Hole diameter in the fixture:  $d_f = 0.625$  in.

Plate thickness (input): 0.500 in.

Recommended plate thickness: not calculated

Drilling method: Hammer drilled

Cleaning: Manual cleaning of the drilled hole according to instructions for use is required.

Anchor type and diameter: KWIK HUS-EZ (KH-EZ) 1/2 (4 1/4)

Item number: 418076 KH-EZ 1/2"x5"

Maximum installation torque: 540 in.lb

Hole diameter in the base material: 0.500 in.

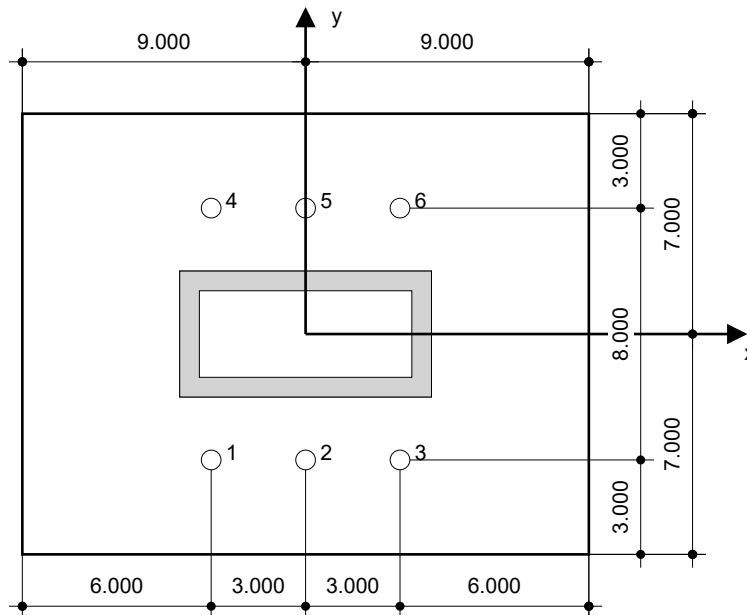
Hole depth in the base material: 4.625 in.

Minimum thickness of the base material: 6.750 in.

Hilti KH-EZ screw anchor with 4.25 in embedment, 1/2 (4 1/4), Carbon steel, installation per ESR-3027

#### 7.1 Recommended accessories

<b>Drilling</b>	<b>Cleaning</b>	<b>Setting</b>
<ul style="list-style-type: none"> <li>• Suitable Rotary Hammer</li> <li>• Properly sized drill bit</li> </ul>	<ul style="list-style-type: none"> <li>• Manual blow-out pump</li> </ul>	<ul style="list-style-type: none"> <li>• Torque wrench</li> </ul>



Coordinates Anchor [in.]

Anchor	x	y	c <sub>-x</sub>	c <sub>+x</sub>	c <sub>-y</sub>	c <sub>+y</sub>	Anchor	x	y	c <sub>-x</sub>	c <sub>+x</sub>	c <sub>-y</sub>	c <sub>+y</sub>
1	-3.000	-4.000	-	-	6.000	14.000	4	-3.000	4.000	-	-	14.000	6.000
2	0.000	-4.000	-	-	6.000	14.000	5	0.000	4.000	-	-	14.000	6.000
3	3.000	-4.000	-	-	6.000	14.000	6	3.000	4.000	-	-	14.000	6.000

Input data and results must be checked for conformity with the existing conditions and for plausibility!  
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## 8 Alternative fastening

### 8.1 Alternative fastening data

<b>Anchor type and diameter:</b>	<b>KWIK-X 1/2 (4 1/4) hnom2</b>	
Item number:	418076 KH-EZ 1/2"x5" (element) / 2362252 KHC 1/2" LARGE (capsule)	
Effective embedment depth:	$h_{ef, opti} = 4.250$ in. ( $h_{ef, limit} = 5.500$ in.), $h_{nom} = 4.250$ in.	
Material:	Carbon Steel	
Evaluation Service Report:	ESR-5065	
Issued   Valid:	1/1/2023   12/1/2023	
Proof:	Design Method ACI 318-19 / Chem	
Stand-off installation:	$e_b = 0.000$ in. (no stand-off); $t = 0.500$ in.	
Anchor plate <sup>R</sup> :	$l_x \times l_y \times t = 18.000$ in. x $14.000$ in. x $0.500$ in.; (Recommended plate thickness: not calculated)	
Profile:	Rectangular HSS (AISC), HSS8X4X.625; (L x W x T) = $8.000$ in. x $4.000$ in. x $0.625$ in.	
Base material:	cracked concrete, $4000$ , $f_c' = 4,000$ psi; $h = 20.000$ in., Temp. short/long: 32/32 °F	
<b>Installation:</b>	<b>hammer drilled hole, Installation condition: Dry</b>	
Reinforcement:	tension: not present, shear: not present; no supplemental splitting reinforcement present edge reinforcement: none or < No. 4 bar	

## Max. Utilization with KWIK-X 1/2 (4 1/4) hnom2: 80 % Fastening meets the design criteria!

### 8.2 Installation data

Profile: Rectangular HSS (AISC), HSS8X4X.625; (L x W x T) =  $8.000$  in. x  $4.000$  in. x  $0.625$  in.  
Hole diameter in the fixture:  $d_f = 0.625$  in.  
Plate thickness (input):  $0.500$  in.  
Recommended plate thickness: not calculated  
Drilling method: Hammer drilled  
Cleaning: No cleaning of the drilled hole is required

Anchor type and diameter: KWIK-X 1/2 (4 1/4) hnom2  
Item number: 418076 KH-EZ 1/2"x5" (element) / 2362252 KHC 1/2" LARGE (capsule)  
Maximum installation torque: -  
Hole diameter in the base material:  $0.500$  in.  
Hole depth in the base material:  $5.250$  in.  
Minimum thickness of the base material:  $6.500$  in.

1/2 (4 1/4) hnom2 Hilti KH-EZ Carbon steel screw anchor with Hilti KHC

#### 8.2.1 Recommended accessories

Drilling	Cleaning	Setting
<ul style="list-style-type: none"> <li>Suitable Rotary Hammer</li> <li>Properly sized drill bit</li> </ul>	<ul style="list-style-type: none"> <li>No accessory required</li> </ul>	<ul style="list-style-type: none"> <li>SIW 6-A22 Impact Screw Driver</li> </ul>

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Design:	REVISED ONBED PLATE DESIGN - 2024-02-22	Date:	2/23/2024
Fastening point:			

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## 9 Remarks; Your Cooperation Duties

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# **BSE**

**B**rienen **S**tructural **E**ngineers, P.S.

**LATERAL DESIGN**

Brienen Structural Engineers, P.S.

WALL CONSTRUCTION :

(4) layers Gyp	(4)(2.5psf)	= 10psf
MTL STUDS	1.5psf	= 1.5psf
ACOUSTIC INS.		= 2psf
		<u>13.5psf</u>
		USE 14psf

BATTERY ROOM + UPS COMBINED

$$\text{TOTAL CEILING SEISMIC WEIGHT} = (20\text{psf}) (1540 \text{ ft}^2) = 30.8 \text{ K}$$

$$\text{TOP HALF OF WALLS} = \left(\frac{1}{2}\right) (13 \text{ ft}) (160\text{ft}) (14\text{psf}) = 14.6 \text{ K}$$

$$\text{TOTAL WALL LENGTH} = (32 \text{ ft} \times 2) + (48 \text{ ft} \times 2) = 160 \text{ ft}$$

$$\text{TOTAL SEISMIC MASS} = 45.4 \text{ K}$$

FIND  $F_p$  PER ASCE 7-16, EQN 13.3-1

$$F_p = \frac{(0.4)(ap) S_{DS} W_p}{R_p / I_p} \left(1 + 2 \frac{Z}{h}\right) = \frac{(0.4)(1.0)(1.006)(45.4 \text{ K})}{2.5/1.0} \left(1 + 2 \left(\frac{12 \text{ ft}}{47 \text{ ft}}\right)\right)$$

$$F_p = 0.2432 W$$

$$= \underline{11.0 \text{ K}} \quad \text{TOTAL}$$

FIND SEISMIC LOAD TO EACH COLUMN  
# of COLUMNS = (12) Cols

$$\text{SEISMIC LOAD PER COLUMN} = \frac{11.0 \text{ K}}{(12) \text{ Cols}} = 0.92 \text{ K/Column}$$

$$\text{AT INTERIOR COLUMNS} = 16' \times 16' \times 20\text{psf} = 5.12 \text{ K MASS}$$

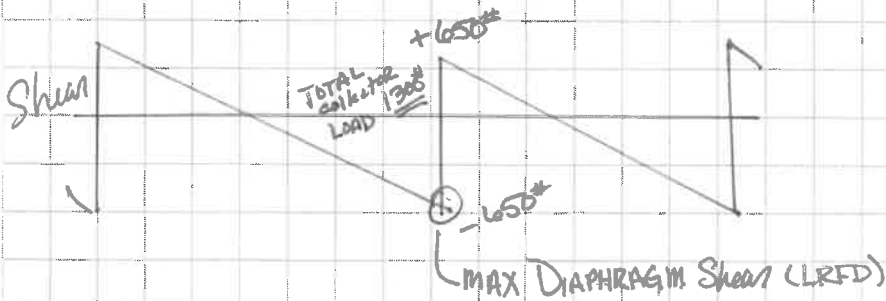
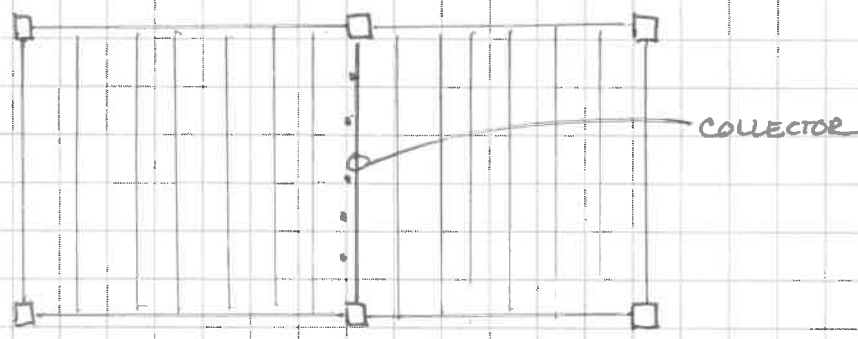
$$F_p = (0.2432)(5.12 \text{ K}) = 1.245 \text{ K/COL.}$$

Controls 



PLYWOOD - ON - MH Joist DIAPHRAGMS

SEISMIC DEMAND



COLLECTOR LOAD =  $1300 \times LRFD$   
 $= 910 \times (LRSD)$

SHEAR TRANSFER FROM DIAPHRAGM TO collector = (15) SCREWS  
 THRU PW into Collector

$V_{A, \text{SCREW } \#10} = 190 \times$

$\# \text{ of SCREWS Req'd} = \frac{910 \times_{TOT}}{190 \times / \text{SCREW}} = 4.8 \text{ SCREWS}$

(15) SCREWS PROVIDED

ALLOWABLE DIAPH. SHEAR PER AISI 5400-20, § F2.4

$\phi V_n = \phi v_n L$   
 $\phi V_n = (0.60)(555 \times / \text{ft})(16 \text{ft}) = 5,328 \times$

DCR = 0.24



Brien Structural Engineers, P.S.

# Diaphragm Shear Provisions from AISI 400-20, Section F2.4

## F2.4 Shear Strength

### F2.4.1 Nominal Strength

The nominal strength of diaphragms sheathed with wood structural panels is permitted to be determined in accordance with Eq. F2.4.1-1 subject to the requirements in Section F2.4.1.1.

$$V_n = v_n L \quad (\text{Eq. F2.4.1-1})$$

where

L = Diaphragm resistance length, in ft (m)

v<sub>n</sub> = Nominal shear strength per unit length as specified in Table F2.4-1, lb/ft (kN/m)

### F2.4.1.1 Requirements for Tabulated Systems

The following requirements shall apply to diaphragms sheathed with wood structural panels:

- (a) The aspect ratio (length:width) of the diaphragm does not exceed 4:1 for blocked diaphragms and 3:1 for unblocked diaphragms.
- (b) Joists and tracks are ASTM A1003 Structural Grade 33 (Grade 230) Type H steel for members with a designation thickness of 33 and 43 mils, and ASTM A1003 Structural Grade 50 (Grade 340) Type H steel for members with a designation thickness equal to or greater than 54 mils.
- (c) The minimum designation thickness of structural members is 33 mils.
- (d) Joists are C-shape members with a minimum flange width of 1-5/8 in. (41.3 mm), minimum web depth of 3-1/2 in. (89 mm) and minimum edge stiffener of 3/8 in. (9.5 mm).
- (e) Track has a minimum flange width of 1-1/4 in. (31.8 mm) and a minimum web depth of 3-1/2 in. (89 mm).
- (f) Screws for structural members are a minimum No. 8 and are in accordance with ASTM C1513.
- (g) Wood structural panel sheathing is manufactured using exterior glue and complies with DOC PS-1 and DOC PS-2.
- (h) Screws used to attach wood structural panels are minimum No. 8 where structural members have a designation thickness of 54 mils or less and No. 10 where structural members have a designation thickness greater than 54 mils and comply with ASTM C1513.
- (i) Screws in the field of the panel are attached to intermediate supports at a maximum 12-in. (305 mm) spacing along the structural members.
- (j) Panels less than 12-in. (305-mm) wide are not used.
- (k) Maximum joist spacing is 24 in. (610 mm) on center.
- (l) Where diaphragms are designed as blocked, all panel edges are attached to structural members or panel blocking.
- (m) Where used as blocking, flat strap is a minimum thickness of 33 mils with a minimum width of 1-1/2 in. (38.1 mm) and is installed below the sheathing.
- (n) Where diaphragms are designed as blocked, the screws are installed through the sheathing to the blocking.
- (o) Fasteners along the edges in shear panels are placed from panel edges not less than

### F2.4.2 Available Strength

The available strength ( $\phi_v V_n$  or  $V_n/\Omega_v$ ) shall be determined from the nominal strength using the applicable safety factors and resistance factors given in this section in accordance with the applicable design method - ASD or LRFD as follows:

$$\Omega_v = 2.50 \quad (\text{ASD})$$

$$\phi_v = 0.60 \quad (\text{LRFD})$$

### F2.4.3 Design Deflection

The deflection of a diaphragm with wood structural panel sheathing shown in Table F2.4-1 shall be determined by principles of mechanics considering the deformation of the sheathing and its attachment, chords and collectors.

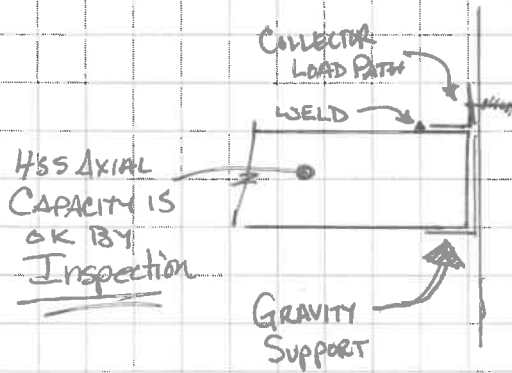
**Table F2.4-1**  
Nominal Shear Strength (v<sub>n</sub>) per Unit Length for Diaphragms Sheathed With Wood Structural Panel Sheathing<sup>1,2</sup>  
United States and Mexico (lb/ft)

Sheathing	Thickness (in.)	Blocked				Unblocked	
		Screw spacing at diaphragm boundary edges and at all continuous panel edges (in.)				Screws spaced maximum of 6 in. on all supported edges	
		6	4	2.5	2	Load perpendicular to unblocked edges and continuous panel joints	All other configurations
Screw spacing at all other panel edges (in.)							
		6	6	4	3		
Structural I	3/8	768	1022	1660	2045	685	510
	7/16	768	1127	1800	2255	755	565
	15/32	925	1232	1970	2465	825	615
C-D, C-C and other graded wood structural panels	3/8	690	920	1470	1840	615	460
	7/16	760	1015	1620	2030	680	505
	15/32	832	1110	1770	2215	740	555

1. For SI: 1" = 25.4 mm, 1 ft = 0.305 m, 1 lb = 4.45 N

2. For diaphragms sheathed with wood structural panels, tabulated R<sub>n</sub> values are applicable for short-term load duration (seismic loads).

CONNECTION OF COLLECTOR (HSS) TO (E) CONC. COL.



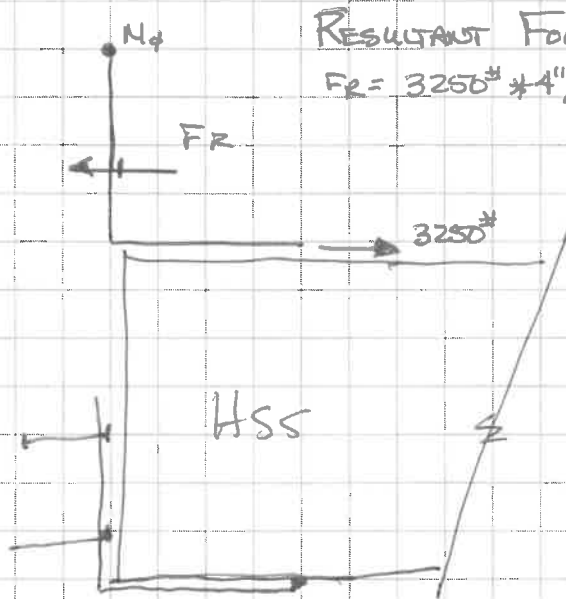
$$\begin{aligned} \text{COLLECTOR CONN. LOAD} &= \Omega_o F_p \\ &= 2.5 (1.3K) \\ &= 3,250^{\#} \text{ (LRFD)} \end{aligned}$$

CHECK WELD

$$\begin{aligned} \phi R_n &= 1.392 (D)(L) \text{ PER AISC manual} \\ \phi R_n &= 1.392 (3)(2.75 \text{ "NET}) \\ \phi R_n &= 11.5K \\ \uparrow \text{DCR} &= 0.28 \end{aligned}$$

NOTE: LOADS BEARING IN COMPRESSION ARE SIMILAR

CHECK ANCHORS INTO COLUMNS  
SEE FOLLOWING PAGES FOR ANCHOR CALC OUTPUT



RESULTANT FORCE TO INCLUDE Eccentric LOAD  $\frac{1}{2}$   
 $F_R = 3250^{\#} * 4 \text{ "}/2 = 5200^{\#}$  Consider Prying




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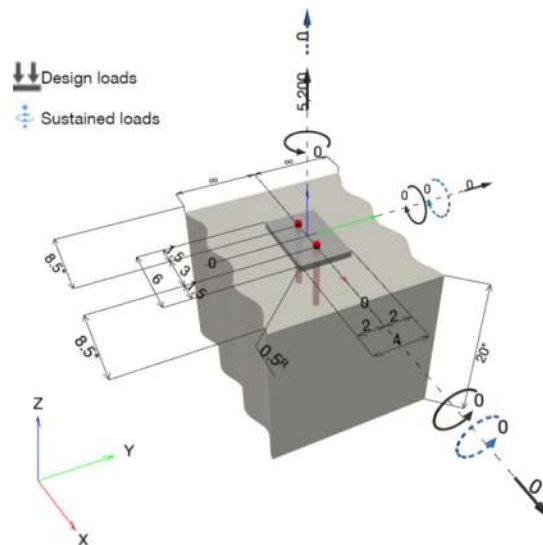
Specifier's comments:

## 1 Input data

<b>Anchor type and diameter:</b>	<b>HIT-HY 200 V3 + HAS-V-36 (ASTM F1554 Gr.36) 1/2</b>	
Item number:	2198022 HAS-V-36 1/2"x6-1/2" (element) / 2334276 HIT-HY 200-R V3 (adhesive)	
Effective embedment depth:	$h_{ef,opti} = 4.797$ in. ( $h_{ef,limit} = 10.000$ in.)	
Material:	ASTM F1554 Grade 36	
Evaluation Service Report:	ESR-4868	
Issued   Valid:	11/1/2022   11/1/2024	
Proof:	Design Method ACI 318-19 / Chem	
Stand-off installation:	$e_b = 0.000$ in. (no stand-off); $t = 0.500$ in.	
Anchor plate <sup>R</sup> :	$l_x \times l_y \times t = 6.000$ in. x $4.000$ in. x $0.500$ in.; (Recommended plate thickness: not calculated)	
Profile:	no profile	
Base material:	cracked concrete, 4000, $f'_c = 4,000$ psi; $h = 20.000$ in., Temp. short/long: 32/32 °F	
<b>Installation:</b>	<b>hammer drilled hole, Installation condition: Dry</b>	
Reinforcement:	tension: not present, shear: not present; no supplemental splitting reinforcement present	
	edge reinforcement: none or < No. 4 bar	
Seismic loads (cat. C, D, E, or F)	Tension load: yes (17.10.5.3 (d))	
	Shear load: yes (17.10.6.3 (c))	

<sup>R</sup> - The anchor calculation is based on a rigid anchor plate assumption.

## Geometry [in.] & Loading [lb, in.lb]





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1.1 Design results

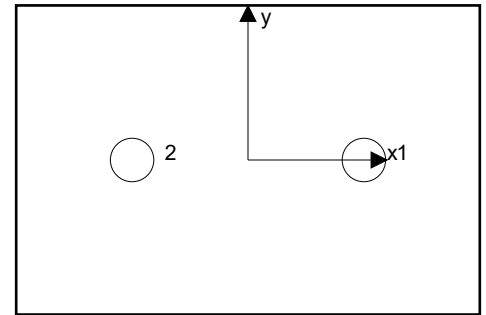
Case	Description	Forces [lb] / Moments [in.lb]	Seismic	Max. Util. Anchor [%]
1	Combination 1	N = 5,200; V <sub>x</sub> = 0; V <sub>y</sub> = 0; M <sub>x</sub> = 0; M <sub>y</sub> = 0; M <sub>z</sub> = 0;	yes	100

2 Load case/Resulting anchor forces

Anchor reactions [lb]

Tension force: (+Tension, -Compression)

Anchor	Tension force	Shear force	Shear force x	Shear force y
1	2,600	0	0	0
2	2,600	0	0	0



max. concrete compressive strain: - [%]  
 max. concrete compressive stress: - [psi]  
 resulting tension force in (x/y)=(0.000/0.000): 0 [lb]  
 resulting compression force in (x/y)=(0.000/0.000): 0 [lb]

Anchor forces are calculated based on the assumption of a rigid anchor plate.

3 Tension load

	Load N <sub>ua</sub> [lb]	Capacity $\phi N_n$ [lb]	Utilization $\beta_N = N_{ua} / \phi N_n$	Status
Steel Strength*	2,600	6,172	43	OK
Bond Strength**	5,200	5,223	100	OK
Sustained Tension Load Bond Strength*	N/A	N/A	N/A	N/A
Concrete Breakout Failure**	5,200	6,655	79	OK

\* highest loaded anchor    \*\*anchor group (anchors in tension)


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**3.1 Steel Strength**

$N_{sa}$  = ESR value refer to ICC-ES ESR-4868  
 $\phi N_{sa} \geq N_{ua}$  ACI 318-19 Table 17.5.2

**Variables**

$A_{se,N}$ [in. <sup>2</sup> ]	$f_{uta}$ [psi]
0.14	58,000

**Calculations**

$N_{sa}$ [lb]
8,230

**Results**

$N_{sa}$ [lb]	$\phi_{steel}$	$\phi N_{sa}$ [lb]	$N_{ua}$ [lb]
8,230	0.750	6,172	2,600



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## 3.2 Bond Strength

$$N_{ag} = \left( \frac{A_{Na}}{A_{Na0}} \right) \Psi_{ec1,Na} \Psi_{ec2,Na} \Psi_{ed,Na} \Psi_{cp,Na} N_{ba} \quad \text{ACI 318-19 Eq. (17.6.5.1b)}$$

$$\phi N_{ag} \geq N_{ua} \quad \text{ACI 318-19 Table 17.5.2}$$

$$A_{Na} \text{ see ACI 318-19, Section 17.6.5.1, Fig. R 17.6.5.1(b)}$$

$$A_{Na0} = (2 c_{Na})^2 \quad \text{ACI 318-19 Eq. (17.6.5.1.2a)}$$

$$c_{Na} = 10 d_a \sqrt{\frac{\tau_{uncr}}{1100}} \quad \text{ACI 318-19 Eq. (17.6.5.1.2b)}$$

$$\Psi_{ec,Na} = \left( \frac{1}{1 + \frac{e_N}{c_{Na}}} \right) \leq 1.0 \quad \text{ACI 318-19 Eq. (17.6.5.3.1)}$$

$$\Psi_{ed,Na} = 0.7 + 0.3 \left( \frac{c_{a,min}}{c_{Na}} \right) \leq 1.0 \quad \text{ACI 318-19 Eq. (17.6.5.4.1b)}$$

$$\Psi_{cp,Na} = \text{MAX} \left( \frac{c_{a,min}}{c_{ac}}, \frac{c_{Na}}{c_{ac}} \right) \leq 1.0 \quad \text{ACI 318-19 Eq. (17.6.5.5.1b)}$$

$$N_{ba} = \lambda_a \cdot \tau_{k,c} \cdot \alpha_{N,seis} \cdot \pi \cdot d_a \cdot h_{ef} \quad \text{ACI 318-19 Eq. (17.6.5.2.1)}$$

## Variables

$\tau_{k,c,uncr}$ [psi]	$d_a$ [in.]	$h_{ef}$ [in.]	$c_{a,min}$ [in.]	$\alpha_{overhead}$	$\tau_{k,c}$ [psi]
2,327	0.500	4.797	8.500	1.000	1,190
$e_{c1,N}$ [in.]	$e_{c2,N}$ [in.]	$c_{ac}$ [in.]	$\lambda_a$	$\alpha_{N,seis}$	
0.000	0.000	8.542	1.000	0.990	

## Calculations

$c_{Na}$ [in.]	$A_{Na}$ [in. <sup>2</sup> ]	$A_{Na0}$ [in. <sup>2</sup> ]	$\Psi_{ed,Na}$
7.239	253.06	209.62	1.000
$\Psi_{ec1,Na}$	$\Psi_{ec2,Na}$	$\Psi_{cp,Na}$	$N_{ba}$ [lb]
1.000	1.000	1.000	8,875

## Results

$N_{ag}$ [lb]	$\phi_{bond}$	$\phi_{seismic}$	$\phi_{nonductile}$	$\phi N_{ag}$ [lb]	$N_{ua}$ [lb]
10,714	0.650	0.750	1.000	5,223	5,200



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## 3.3 Concrete Breakout Failure

$$N_{cbg} = \left( \frac{A_{Nc}}{A_{Nc0}} \right) \psi_{ec,N} \psi_{ed,N} \psi_{c,N} \psi_{cp,N} N_b \quad \text{ACI 318-19 Eq. (17.6.2.1b)}$$

$$\phi N_{cbg} \geq N_{ua} \quad \text{ACI 318-19 Table 17.5.2}$$

$A_{Nc}$  see ACI 318-19, Section 17.6.2.1, Fig. R 17.6.2.1(b)

$$A_{Nc0} = 9 h_{ef}^2 \quad \text{ACI 318-19 Eq. (17.6.2.1.4)}$$

$$\psi_{ec,N} = \left( \frac{1}{1 + \frac{2 e_N}{3 h_{ef}}} \right) \leq 1.0 \quad \text{ACI 318-19 Eq. (17.6.2.3.1)}$$

$$\psi_{ed,N} = 0.7 + 0.3 \left( \frac{c_{a,min}}{1.5 h_{ef}} \right) \leq 1.0 \quad \text{ACI 318-19 Eq. (17.6.2.4.1b)}$$

$$\psi_{cp,N} = \text{MAX} \left( \frac{c_{a,min}}{c_{ac}}, \frac{1.5 h_{ef}}{c_{ac}} \right) \leq 1.0 \quad \text{ACI 318-19 Eq. (17.6.2.6.1b)}$$

$$N_b = k_c \lambda_a \sqrt{f'_c} h_{ef}^{1.5} \quad \text{ACI 318-19 Eq. (17.6.2.2.1)}$$

## Variables

$h_{ef}$ [in.]	$e_{c1,N}$ [in.]	$e_{c2,N}$ [in.]	$c_{a,min}$ [in.]	$\psi_{c,N}$
4.797	0.000	0.000	8.500	1.000
$c_{ac}$ [in.]	$k_c$	$\lambda_a$	$f'_c$ [psij]	
8.542	17	1.000	4,000	

## Calculations

$A_{Nc}$ [in. <sup>2</sup> ]	$A_{Nc0}$ [in. <sup>2</sup> ]	$\psi_{ec1,N}$	$\psi_{ec2,N}$	$\psi_{ed,N}$	$\psi_{cp,N}$	$N_b$ [lb]
250.30	207.12	1.000	1.000	1.000	1.000	11,297

## Results

$N_{cbg}$ [lb]	$\phi_{concrete}$	$\phi_{seismic}$	$\phi_{nonductile}$	$\phi N_{cbg}$ [lb]	$N_{ua}$ [lb]
13,652	0.650	0.750	1.000	6,655	5,200





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### 4 Shear load

	Load $V_{ua}$ [lb]	Capacity $\phi V_n$ [lb]	Utilization $\beta_v = V_{ua} / \phi V_n$	Status
Steel Strength*	N/A	N/A	N/A	N/A
Steel failure (with lever arm)*	N/A	N/A	N/A	N/A
Pryout Strength (Bond Strength controls)*	N/A	N/A	N/A	N/A
Concrete edge failure in direction **	N/A	N/A	N/A	N/A

\* highest loaded anchor    \*\*anchor group (relevant anchors)

### 5 Warnings

- The anchor design methods in PROFIS Engineering require rigid anchor plates per current regulations (AS 5216:2021, ETAG 001/Annex C, EOTA TR029 etc.). This means load re-distribution on the anchors due to elastic deformations of the anchor plate are not considered - the anchor plate is assumed to be sufficiently stiff, in order not to be deformed when subjected to the design loading. PROFIS Engineering calculates the minimum required anchor plate thickness with CBFEM to limit the stress of the anchor plate based on the assumptions explained above. The proof if the rigid anchor plate assumption is valid is not carried out by PROFIS Engineering. Input data and results must be checked for agreement with the existing conditions and for plausibility!
- Condition A applies where the potential concrete failure surfaces are crossed by supplementary reinforcement proportioned to tie the potential concrete failure prism into the structural member. Condition B applies where such supplementary reinforcement is not provided, or where pullout or pryout strength governs.
- Design Strengths of adhesive anchor systems are influenced by the cleaning method. Refer to the INSTRUCTIONS FOR USE given in the Evaluation Service Report for cleaning and installation instructions.
- For additional information about ACI 318 strength design provisions, please go to <https://submittals.us.hilti.com/PROFISAnchorDesignGuide/>
- "An anchor design approach for structures assigned to Seismic Design Category C, D, E or F is given in ACI 318-19, Chapter 17, Section 17.10.5.3 (a) that requires the governing design strength of an anchor or group of anchors be limited by ductile steel failure. If this is NOT the case, the connection design (tension) shall satisfy the provisions of Section 17.10.5.3 (b), Section 17.10.5.3 (c), or Section 17.10.5.3 (d). The connection design (shear) shall satisfy the provisions of Section 17.10.6.3 (a), Section 17.10.6.3 (b), or Section 17.10.6.3 (c)."
- Section 17.10.5.3 (b) / Section 17.10.6.3 (a) require the attachment the anchors are connecting to the structure be designed to undergo ductile yielding at a load level corresponding to anchor forces no greater than the controlling design strength. Section 17.10.5.3 (c) / Section 17.10.6.3 (b) waive the ductility requirements and require the anchors to be designed for the maximum tension / shear that can be transmitted to the anchors by a non-yielding attachment. Section 17.10.5.3 (d) / Section 17.10.6.3 (c) waive the ductility requirements and require the design strength of the anchors to equal or exceed the maximum tension / shear obtained from design load combinations that include E, with E increased by  $\omega_0$ .
- Installation of Hilti adhesive anchor systems shall be performed by personnel trained to install Hilti adhesive anchors. Reference ACI 318-19, Section 26.7.

**Fastening meets the design criteria!**



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Company:		Page:	7
Address:		Specifier:	
Phone   Fax:		E-Mail:	
Design:	Concrete - Feb 9, 2024	Date:	2/9/2024
Fastening point:			

## 6 Installation data

Profile: no profile

Hole diameter in the fixture:  $d_f = 0.562$  in.

Plate thickness (input): 0.500 in.

Recommended plate thickness: not calculated

Drilling method: Hammer drilled

Cleaning: Compressed air cleaning of the drilled hole according to instructions for use is required

Anchor type and diameter: HIT-HY 200 V3 + HAS-V-36 (ASTM F1554 Gr.36) 1/2

Item number: 2198022 HAS-V-36 1/2"x6-1/2" (element) / 2334276 HIT-HY 200-R V3 (adhesive)

Maximum installation torque: 360 in.lb

Hole diameter in the base material: 0.562 in.

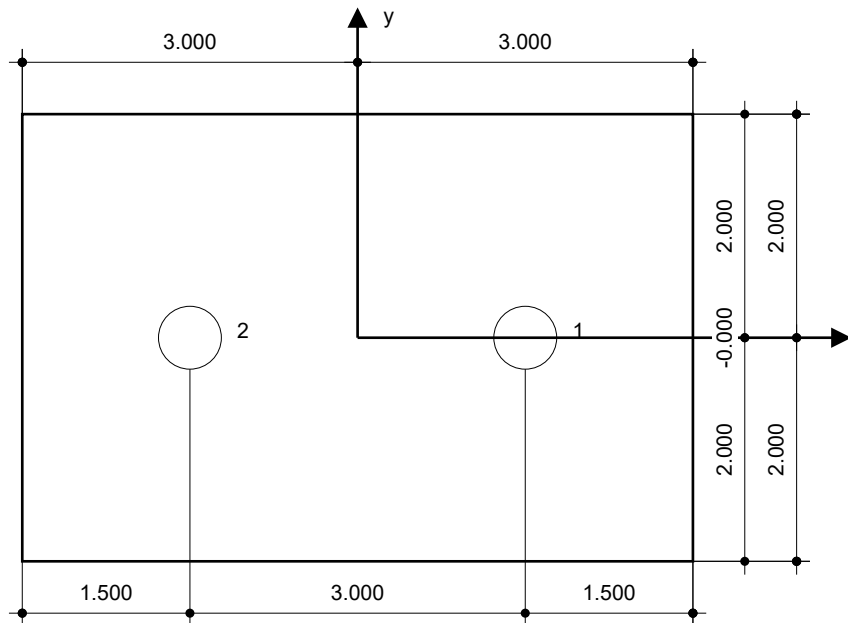
Hole depth in the base material: 4.797 in.

Minimum thickness of the base material: 6.047 in.

1/2 Hilti HAS Carbon steel threaded rod with Hilti HIT-HY 200 V3 Safe Set System

### 6.1 Recommended accessories

Drilling	Cleaning	Setting
<ul style="list-style-type: none"> <li>Suitable Rotary Hammer</li> <li>Properly sized drill bit</li> </ul>	<ul style="list-style-type: none"> <li>Compressed air with required accessories to blow from the bottom of the hole</li> <li>Proper diameter wire brush</li> </ul>	<ul style="list-style-type: none"> <li>Dispenser including cassette and mixer</li> <li>Torque wrench</li> </ul>



Coordinates Anchor [in.]

Anchor	x	y	c <sub>-x</sub>	c <sub>+x</sub>	c <sub>-y</sub>	c <sub>+y</sub>
1	1.500	-0.000	11.500	8.500	-	-
2	-1.500	-0.000	8.500	11.500	-	-



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Company:		Page:	8
Address:		Specifier:	
Phone   Fax:		E-Mail:	
Design:	Concrete - Feb 9, 2024	Date:	2/9/2024
Fastening point:			

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## 7 Remarks; Your Cooperation Duties

- Any and all information and data contained in the Software concern solely the use of Hilti products and are based on the principles, formulas and security regulations in accordance with Hilti's technical directions and operating, mounting and assembly instructions, etc., that must be strictly complied with by the user. All figures contained therein are average figures, and therefore use-specific tests are to be conducted prior to using the relevant Hilti product. The results of the calculations carried out by means of the Software are based essentially on the data you put in. Therefore, you bear the sole responsibility for the absence of errors, the completeness and the relevance of the data to be put in by you. Moreover, you bear sole responsibility for having the results of the calculation checked and cleared by an expert, particularly with regard to compliance with applicable norms and permits, prior to using them for your specific facility. The Software serves only as an aid to interpret norms and permits without any guarantee as to the absence of errors, the correctness and the relevance of the results or suitability for a specific application.
- You must take all necessary and reasonable steps to prevent or limit damage caused by the Software. In particular, you must arrange for the regular backup of programs and data and, if applicable, carry out the updates of the Software offered by Hilti on a regular basis. If you do not use the AutoUpdate function of the Software, you must ensure that you are using the current and thus up-to-date version of the Software in each case by carrying out manual updates via the Hilti Website. Hilti will not be liable for consequences, such as the recovery of lost or damaged data or programs, arising from a culpable breach of duty by you.

# **BSE**

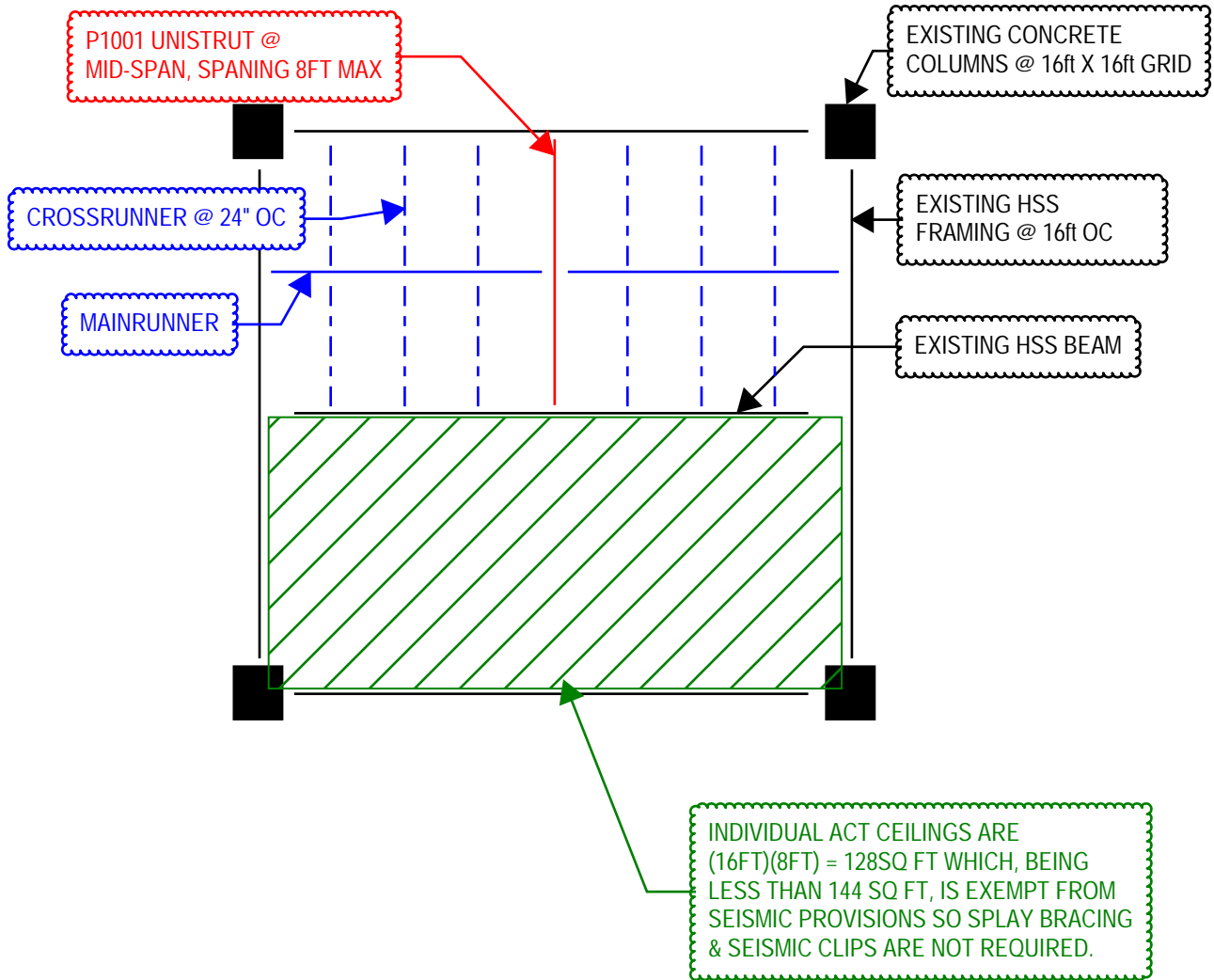
**B**rienen **S**tructural **E**ngineers, P.S.

## UPS ROOM CEILING DESIGN

# BSE

Brienen Structural Engineers, P.S.

## FRAMING INTENT:



# BEAM LOADING FROM UNISTRUT WEBSITE

(<https://www.atkore.com/Products/Strut-and-Fittings/Unistrut/1-58-Strut-and-Fittings/Strut-Channel/P1000-Series/P1001>)

## Beam Loading

Beam Loading - P1001						
Span (in)	Max Allow. Uniform Load (lbs)	Deflection at Uniform load (in)	Uniform Loading at Deflection			Lateral Bracing Reduction Factor
			Span/180 (lbs)	Span/240 (lbs)	Span/360 (lbs)	
24	* 3,500	0.02	* 3,500	* 3,500	* 3,500	1.00
36	3,190	0.07	3,190	3,190	3,190	1.00
48	2,390	0.13	2,390	2,390	2,390	1.00
60	1,910	0.20	1,910	1,910	1,620	0.97
72	1,600	0.28	1,600	1,600	1,130	0.93
84	1,370	0.39	1,370	1,240	830	0.89
96	1,200	0.51	1,200	950	630	0.85
108	1,060	0.64	1,000	750	500	0.81
120	960	0.79	810	610	410	0.78
144	800	1.14	560	420	280	0.70
168	680	1.53	410	310	210	0.63
192	600	2.02	320	240	160	0.56
216	530	2.54	250	190	130	0.49
240	480	3.16	200	150	100	0.44
Note	*Load limited by weld shear					

1200LBS(0.85) = 1020LBS  
 CEILING TRIBUTARY LOAD IS (3PSF)(4FT)(8FT) = 96LBS WHICH  
 LEAVES 924LBS OF LOAD FOR THE CABLE TRAY.  
 ASSUMING CABLE TRAY COULD BE A POINT LOAD IN THE CENTER  
 OF THE SPAN, ALLOWABLE LOAD IS REDUCED BY 50% = 462LBS

# UNISTRUT®

## BEAM LOAD CALCULATION GUIDE

### GUIDE FOR CALCULATING BEAM LOADS FOR UNISTRUT CHANNEL

Loads in the Beam Load Tables for UNISTRUT metal framing channel are given as a total uniform load (W) in pounds. For the more familiar uniform load (w) in pounds per foot or pounds per inch, divide the table load by the span.

Loads under the column headings of "Span/180", "Span/240" and "Span/360" are provided for installations in which deflection (sag) of the loaded UNISTRUT channel must be limited. These ratios are standard engineering practice and, when applicable, are usually given by the Professional Engineer of Record or the Project Specifications. Actual deflection from these preset ratios equals the span (inches or feet) divided by the number 180, 240 or 360. When designing to one of these deflection limits, the allowed uniform load is generally less than the values under the column heading "Maximum Allowed Uniform Load". For further information or assistance on this issue, please contact us.

All 5 notes below the beam load tables must be followed to obtain the final usable load on the channel. Failure to do so produces the wrong working load. These notes require adjustments to the Maximum Allowed Uniform Load for:

- Pierced Channel (if applicable)
- Unbraced Length
- Channel Weight
- Midspan Point Loads (if applicable)

Use the following 5 steps to accurately determine the allowed working load of UNISTRUT channel:

1. **STEP #1:** Determine Maximum Allowed Uniform Load from Load Table
2. **STEP #2:** Multiply the Applicable Pierced Hole Factor (only if using a Beam Load Table for the solid channel)
  - 0.95 for "KO"
  - 0.90 for "HS" & "H3"
  - 0.85 for "T", "SL" & "WT"
  - 0.70 for "DS"
3. **STEP #3:** Multiply by the Unbraced Length Factor
4. **STEP #4:** Subtract the Channel Weight
5. **STEP #5:** Multiply by 50% for Midspan Loading (if applicable)

The result after step #4 is the net allowed total uniform load in pounds. The result after step #5 is the allowed midspan point load.



# RCA Rigid Connector Angles

PRCTI20240333

The Simpson Strong-Tie® rigid connector angle is a general purpose clip angle designed for a wide range of cold-formed steel construction applications. With prepunched holes for fastener attachment, these L-shaped clips save time and labor on the job.

**Features:**

- Use with miscellaneous header/sill connections to jamb studs, jamb stud reinforcement at track, u-channel bridging, stud-blocking, bypass curtain-wall framing, joist connections and other versatile options
- Easy to install, with prepunched holes for quick and accurate fastener attachment

**Material:** RCAXXX/54 — 54 mil (16 ga.), 50 ksi  
 RCAXXX/68 — 68 mil (14 ga.), 50 ksi  
 RCAXXX/97 — 97 mil (12 ga.), 50 ksi  
 (Note: “XXX” is model number shown below.)

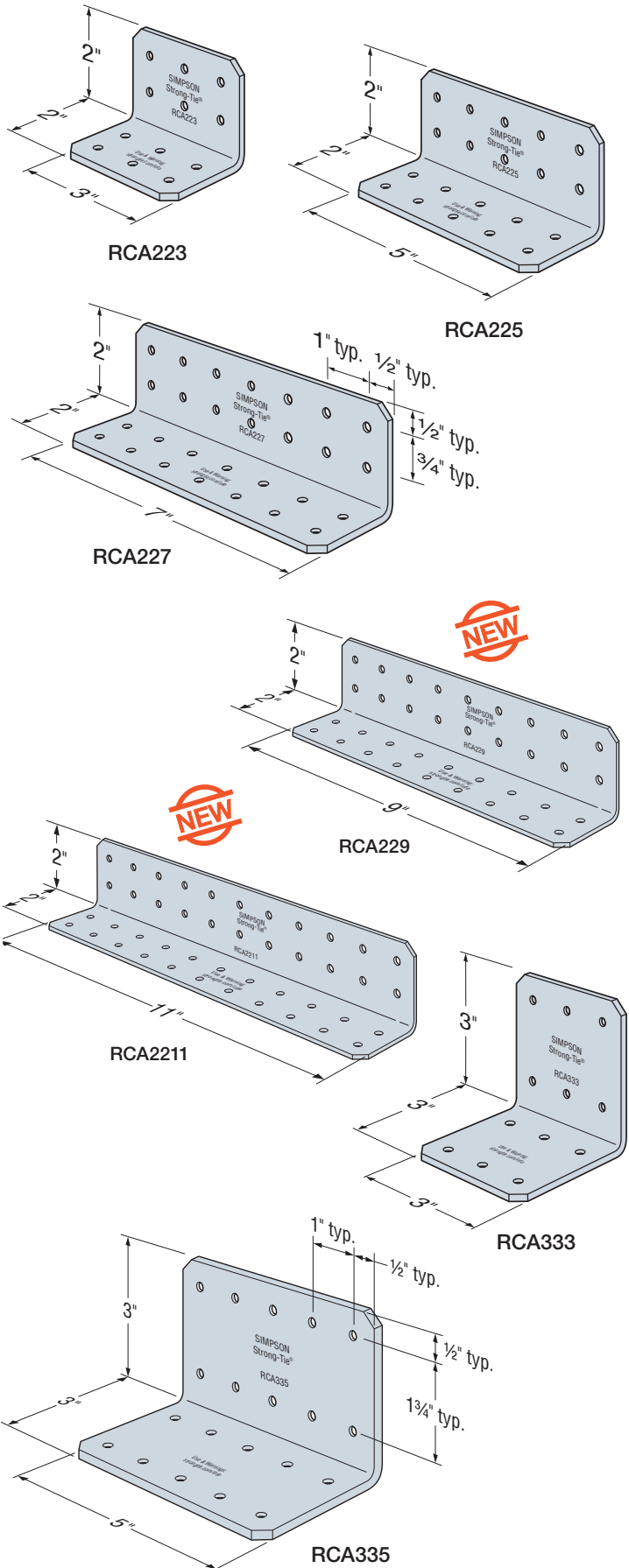
**Finish:** Galvanized (G90)

**Installation:**

- Use all specified anchors/fasteners

## Ordering Information

Model No.	Ordering SKU	Bucket Quantity
RCA223/54	RCA223/54-R150	150
RCA223/68	RCA223/68-R125	125
RCA223/97	RCA223/97-R90	90
RCA225/54	RCA225/54-R90	90
RCA225/68	RCA225/68-R75	75
RCA225/97	RCA225/97-R55	55
RCA227/54	RCA227/54-R65	65
RCA227/68	RCA227/68-R55	55
RCA227/97	RCA227/97-R40	40
RCA229/54	RCA229/54-R50	50
RCA229/68	RCA229/68-R50	50
RCA229/97	RCA229/97-R35	35
RCA2211/54	RCA2211/54-R45	45
RCA2211/68	RCA2211/68-R40	40
RCA2211/97	RCA2211/97-R30	30
RCA333/54	RCA333/54-R100	100
RCA333/68	RCA333/68-R85	85
RCA333/97	RCA333/97-R60	60
RCA335/54	RCA335/54-R60	60
RCA335/68	RCA335/68-R50	50
RCA335/97	RCA335/97-R35	35



Rigid Connectors

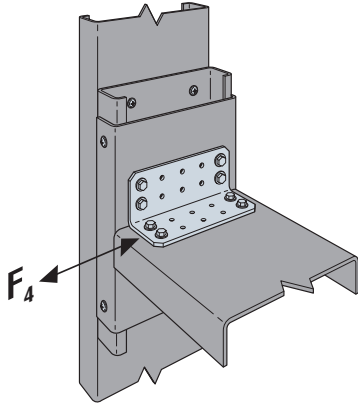
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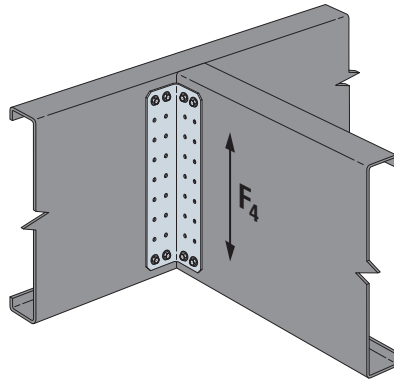
# RCA Rigid Connector Angles

PRCTI20240333

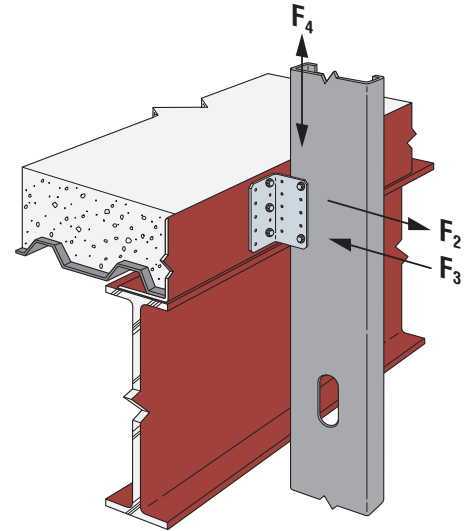
Rigid Connectors



Typical RCA225 Installation at Sill/Jamb



Typical RCA229 Installation at Joist Connection



Typical RCA335 Installation at Bypass Framing

## Screw Patterns for Rigid Connector Angles

Models	Pattern 3A	Pattern 3B	Pattern 3C		
RCA223/54 RCA223/68 RCA223/97 RCA333/54 RCA333/68 RCA333/97					
Models	Pattern 5A	Pattern 5B	Pattern 5C	Pattern 5D	Pattern 5E
RCA225/54 RCA225/68 RCA225/97 RCA335/54 RCA335/68 RCA335/97					
Models	Pattern 7A	Pattern 7B	Pattern 7C	Pattern 7D	Pattern 7E
RCA227/54 RCA227/68 RCA227/97					
Models	Pattern 9A	Pattern 9B	Pattern 9C	Pattern 9D	Pattern 9E
RCA229/54 RCA229/68 RCA229/97					
Models	Pattern 11A	Pattern 11B	Pattern 11C	Pattern 11D	Pattern 11E
RCA2211/54 RCA2211/68 RCA2211/97					

# RCA Rigid Connector Angles

PRCTI20240333

## RCA Rigid Connector Angles Allowable Loads (lb.)

Model	No. of #10 Screws <sup>5,6</sup>	Screw Pattern	Stud Framing Thickness <sup>11</sup>								
			33 mil (20 ga.)			43 mil (18 ga.)			54 mil (16 ga.)		
			F <sub>2</sub>	F <sub>3</sub>	F <sub>4</sub>	F <sub>2</sub>	F <sub>3</sub>	F <sub>4</sub>	F <sub>2</sub>	F <sub>3</sub>	F <sub>4</sub>
RCA223/54	3	3A	205	495	200	205	590	310	205	590	620
	4	3B	205	580	390	205	580	605	205	580	1,095
	6	3C	205	865	480	205	865	740	205	865	1,095
RCA223/68	3	3A	310	495	200	310	765	310	310	815	620
	4	3B	310	660	390	310	805	605	310	805	1,210
	6	3C	310	990	480	310	1,320	605	310	1,205	1,350
RCA223/97	3	3A	495	495	200	630	1,020	630	630	1,415	620
	4	3B	630	660	390	630	1,020	630	630	1,265	1,210
	6	3C	630	990	480	630	1,530	740	630	1,895	1,485
RCA225/54	2	5A	330	330	265	340	390	410	340	390	815
	4	5B	340	580	535	340	580	830	340	580	1,660
	5	5C	340	825	460	340	980	705	340	980	1,310
	8	5D	340	1,155	915	340	1,155	1,420	340	1,155	1,825
	10	5E	340	1,445	1,035	340	1,445	1,600	340	1,445	1,825
RCA225/68	2	5A	330	330	265	510	510	410	520	545	815
	4	5B	520	660	535	520	805	830	520	805	1,660
	5	5C	520	825	460	520	1,275	705	520	1,360	1,415
	8	5D	520	1,320	915	520	1,605	1,420	520	1,605	2,255
	10	5E	520	1,650	1,035	520	2,010	1,600	520	2,010	2,255
RCA225/97	2	5A	330	330	265	510	510	410	1,020	945	815
	4	5B	660	660	535	1,020	1,020	830	1,050	1,265	1,660
	5	5C	825	825	460	1,050	1,275	705	1,050	2,360	1,415
	8	5D	1,050	1,320	915	1,050	2,040	1,420	1,050	2,525	2,835
	10	5E	1,050	1,650	1,035	1,050	2,550	1,600	1,050	3,155	3,200
RCA227/54	4	7A	475	660	545	475	785	840	475	785	1,675
	4	7B	475	580	595	475	580	920	475	580	1,840
	7	7C	475	1,155	765	475	1,280	1,185	475	1,280	1,685
	8	7D	475	1,155	1,120	475	1,155	1,730	475	1,155	2,555
	14	7E	475	2,025	1,685	475	2,025	2,555	475	2,025	2,555
RCA227/68	4	7A	660	660	545	725	1,020	840	725	1,090	1,675
	4	7B	660	660	595	725	805	920	725	805	1,840
	7	7C	725	1,155	765	725	1,780	1,185	725	1,780	2,370
	8	7D	725	1,320	1,120	725	1,605	1,730	725	1,605	3,155
	14	7E	725	2,310	1,685	725	2,810	2,605	725	2,810	3,155
RCA227/97	4	7A	660	660	545	1,020	1,020	840	1,470	1,890	1,675
	4	7B	660	660	595	1,020	1,020	920	1,470	1,265	1,840
	7	7C	1,155	1,155	765	1,470	1,785	1,185	1,470	3,080	2,370
	8	7D	1,320	1,320	1,120	1,470	2,040	1,730	1,470	2,525	3,460
	14	7E	1,470	2,310	1,685	1,470	3,570	2,605	1,470	4,420	4,490
RCA229/54	4	9A	615	660	595	615	1,020	920	615	1,100	1,840
	4	9B	615	660	620	615	815	960	615	815	1,920
	9	9C	615	1,485	1,105	615	2,295	1,705	615	2,475	3,410
	8	9D	615	1,320	1,210	615	1,630	1,865	615	1,630	3,735
	18	9E	615	2,970	2,375	615	3,665	3,670	615	3,665	4,715
RCA229/68	4	9A	660	660	595	935	1,020	920	935	1,525	1,840
	4	9B	660	660	620	935	1,020	960	935	1,130	1,920
	9	9C	935	1,485	1,105	935	2,295	1,705	935	3,435	3,410
	8	9D	935	1,320	1,210	935	2,040	1,865	935	2,260	3,735
	18	9E	935	2,970	2,375	935	4,590	3,670	935	5,090	5,750
RCA229/97	4	9A	660	660	595	1,020	1,020	920	1,890	2,040	1,840
	4	9B	660	660	620	1,020	1,020	960	1,890	1,610	1,920
	9	9C	1,485	1,485	1,105	1,890	2,295	1,705	1,890	4,590	3,410
	8	9D	1,320	1,320	1,210	1,890	2,040	1,865	1,890	3,220	3,735
	18	9E	1,890	2,970	2,375	1,890	4,590	3,670	1,890	7,240	7,340

EA SIDE OF UNISTRUT

Rigid Connectors

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See footnotes on p. 106.

### 3.2.5.2 MATERIAL SPECIFICATIONS

Fastener designation	Fastener material	Fastener plating <sup>1</sup>	Steel washer or clip plating <sup>1,2</sup>	Washer or clip plating <sup>1,2</sup>
X-P*	Carbon Steel	5 µm Zinc	N/A	N/A
X-U*	Carbon Steel	5 µm Zinc	Carbon Steel	5 µm Zinc
DS/EDS	Carbon Steel	5 µm Zinc	N/A	N/A
X-C	Carbon Steel	5 µm Zinc	Carbon Steel	5 µm Zinc
X-R, X-CR <sup>3</sup>	SAE 316	N/A	SAE 316	N/A
X-C/ X-P/ X-PN/ X-S: G2/G3/B3	Carbon Steel	2-10 µm Zinc	N/A	N/A
X-CT Forming Nail	Carbon Steel	5 µm Zinc	N/A	N/A
BC X-C	Carbon Steel	5 µm Zinc	Carbon Steel	5 µm Zinc

1 The 5 µm zinc coating is in accordance with ASTM B 633, SC 1, Type III. Refer to Section 2.3.3.1 for more information.

2 Most fasteners have a plastic washer for guidance when installing. Not all fastener lengths have a pre-mounted steel washer. Refer to Section 3.2.2.4 for more information on available fasteners.

3. The X-CR and X-R fastener material is a proprietary material, which provides a corrosion resistance equivalent to SAE 316 stainless steel. The steel washer material is SAE 316 stainless steel.

\* More details about the innovative X-P and X-U fasteners can be found in Section 3.2.6.

### 3.2.5.3 TECHNICAL DATA

#### Allowable loads in normal weight concrete<sup>1,2</sup>

Fastener description	Fastener	Shank diameter in. (mm)	Minimum embedment in. (mm)	Concrete compressive strength							
				2000 psi		4000 psi		6000 psi		8000 psi	
				Tension lb (kN)	Shear lb (kN)	Tension lb (kN)	Shear lb (kN)	Tension lb (kN)	Shear lb (kN)	Tension lb (kN)	Shear lb (kN)
Premium Concrete Fastener	X-P	0.157 (4.0)	3/4 (19)	100 (0.44)	155 (0.69)	100 (0.44)	175 (0.78)	105 (0.47)	205 (0.91)	135 (0.60)	205 (0.91)
			1 (25)	165 (0.73)	220 (0.98)	180 (0.80)	225 (1.00)	150 (0.67)	300 (1.33)	150 (0.67)	215 (0.96)
			1-1/4 (32)	240 (1.07)	310 (1.38)	280 (1.25)	310 (1.38)	180 (0.80)	425 (1.89)	-	-
			1-1/2 (38)	310 (1.38)	420 (1.87)	-	-	-	-	-	-
Universal Knurled Shank Fasteners	X-U	0.157 (4.0)	3/4 (19)	100 (0.44)	125 (0.57)	100 (0.44)	125 (0.57)	105 (0.47)	205 (0.91)	-	-
			1 (25)	165 (0.73)	190 (0.85)	170 (0.76)	225 (1.00)	110 (0.49)	280 (1.25)	-	-
			1-1/4 (32)	240 (1.07)	310 (1.38)	280 (1.25)	310 (1.38)	180 (0.80)	425 (1.89)	-	-
			1-1/2 (38)	275 (1.22)	420 (1.87)	325 (1.45)	420 (1.87)	-	-	-	-
Standard Fastener (Black collated strip or guidance washer)	X-C	0.138 (3.5)	3/4 (19)	45 (0.20)	75 (0.33)	65 (0.29)	105 (0.47)	95 (0.42)	195 (0.87)	-	-
			1 (25)	85 (0.38)	150 (0.67)	160 (0.71)	200 (0.89)	105 (0.47)	270 (1.20)	-	-
			1-1/4 (32)	130 (0.58)	210 (0.93)	270 (1.20)	290 (1.29)	165 (0.73)	325 (1.45)	-	-
			1-1/2 (38)	175 (0.78)	260 (1.16)	270 (1.20)	360 (1.60)	-	-	-	-
Heavy Duty Fastener	DS	0.177 (4.5)	3/4 (19)	50 (0.22)	120 (0.53)	125 (0.56)	135 (0.60)	-	-	-	-
			1 (25)	130 (0.58)	195 (0.87)	155 (0.69)	240 (1.07)	-	-	-	-
			1-1/4 (32)	220 (0.98)	385 (1.71)	270 (1.20)	425 (1.89)	-	-	-	-
			1-1/2 (38)	300 (1.33)	405 (1.80)	355 (1.58)	450 (2.00)	-	-	-	-
Stainless Steel Fastener	X-CR	0.145 (3.7)	3/4 (19)	30 (0.13)	40 (0.18)	65 (0.29)	40 (0.18)	-	-	-	-
			1 (25)	55 (0.24)	185 (0.82)	120 (0.53)	190 (0.85)	100 (0.44)	170 (0.76)	-	-
			1-1/4 (32)	110 (0.49)	290 (1.29)	125 (0.56)	300 (1.33)	120 (0.53)	440 (1.96)	-	-
			1-1/2 (38)	265 (1.18)	405 (1.80)	350 (1.56)	450 (2.00)	-	-	-	-
Gas Fastener	X-C B3, X-C G3	0.118 (3.0)	3/4 (19)	110 (0.5)	190 (0.9)	110 (0.5)	190 (0.9)	110 (0.5)	190 (0.9)	-	-
Premium Gas Fastener	X-GHP, X-P 17 G2, X-P 20 G2, X-P G3, X-P B3	0.118 (3.0)	5/8 (16)	-	-	50 (0.2)	120 (0.5)	50 (0.2)	90 (0.4)	-	-
			3/4 (19)	80 (0.4)	120 (0.5)	-	-	-	-	-	-
Forming Fastener	X-CT 47 <sup>3</sup>	0.145 (3.7)	1 (25)	60 (0.27)	65 (0.29)	-	-	-	-	-	-
	X-CT 62 <sup>3</sup>	0.145 (3.7)	1 (25)	75 (0.33)	75 (0.33)	-	-	-	-	-	-

(2) HILTI X-U ANCHORS EMBEDDED 1" MIN EA SIDE & END OF UNISTRUT

1 The tabulated allowable load values are for the low-velocity fasteners only, using a safety factor that is greater than or equal to 5.0, calculated in accordance with ICC-ES AC70. Wood or steel members connected to the substrate must be investigated in accordance with accepted design criteria.

2 Multiple fasteners are recommended for any attachment.

3 For temporary fastening of formwork only.

**Allowable loads in minimum ASTM A36 ( $F_y \geq 36$  ksi,  $F_u \geq 58$  ksi) steel<sup>1,2,4,5</sup>**

Fastener description	Fastener	Shank diameter in. (mm)	Steel thickness (in.)												
			1/8		3/16		1/4		3/8		1/2		≥3/4		
			Tension lb (kN)	Shear lb (kN)	Tension lb (kN)	Shear lb (kN)	Tension lb (kN)	Shear lb (kN)	Tension lb (kN)	Shear lb (kN)	Tension lb (kN)	Shear lb (kN)	Tension lb (kN)	Shear lb (kN)	
Universal knurled shank*	X-U <sup>6</sup>	0.157 (4.0)	-	-	535 (2.38)	720 (3.20)	775 (3.45)	720 (3.20)	935 (4.16)	720 (3.20)	900 (4.00)	720 (3.20)	350 (1.56)	375 (1.67)	
Stepped-shank knurling-lengthwise	X-U 15 <sup>7</sup>	0.145 (3.7)	-	-	155 (0.69)	395 (1.76)	230 (1.03)	395 (1.76)	420 (1.90)	450 (2.00)	365 (1.62)	500 (2.22)	365 (1.62)	400 (1.78)	
Standard knurled shank	X-S13	0.145 (3.7)	140 (0.62)	300 (1.33)	(2) HILTI X-U ANCHORS EA SIDE & END OF UNISTRUT						450 (2.00)	-	-	-	-
Drywall smooth shank w/metal top hat washer	X-S16	0.145 (3.7)	-	-							225 (1.00)	420 (1.87)	225 (1.00)	430 (1.91)	225 (1.00)
Heavy duty knurled shank	EDS <sup>3</sup>	0.177 (4.5)	-	-	305 (1.36)	615 (2.67)	625 (2.78)	870 (3.87)	715 (3.18)	870 (3.87)	890 (3.96)	960 (4.27)	400 (1.78)	655 (2.91)	
Heavy duty smooth shank	DS	0.177 (4.5)	-	-	365 (1.62)	725 (3.22)	580 (2.58)	725 (3.22)	695 (3.09)	725 (3.22)	735 (3.27)	860 (3.83)	-	-	
Stainless steel smooth shank	X-R <sup>10</sup>	0.145 (3.7)	-	-	460 (2.05)	460 (2.05)	615 (2.74)	500 (2.22)	-	-	-	-	-	-	
	X-R <sup>8,10</sup>	0.145 (3.7)	300 (1.33)	190 (0.85)	615 (2.74)	495 (2.20)	760 (3.38)	500 (2.22)	220 (0.98)	325 (1.45)	225 (1.00)	335 (1.49)	-	-	
Standard gas fastener for steel	X-EGN 14 <sup>9</sup> , X-S 14 B3	0.118 (3.0)	140 (0.6)	230 (1.0)	220 (1.0)	245 (1.1)	225 (1.0)	290 (1.3)	280 (1.2)	330 (1.5)	280 (1.2)	330 (1.5)	280 (1.2)	330 (1.5)	
Standard gas fastener for steel	X-EGN 14 <sup>8,9</sup> , X-S 14 B38	0.118 (3.0)	-	-	220 (1.0)	295 (1.3)	260 (1.2)	355 (1.6)	280 (1.2)	385 (1.7)	280 (1.2)	385 (1.7)	280 (1.2)	385 (1.7)	
Premium gas fastener	X-GHP, X-P G3, X-P B3	0.118 (3.0)	125 (0.6)	230 (1.0)	170 (0.8)	245 (1.1)	200 (0.9)	230 (1.0)	250 (1.1)	255 (1.1)	-	-	-	-	

- The tabulated allowable load values are for the low-velocity fasteners only, using a safety factor that is greater than or equal to 5.0, calculated in accordance with ICC-ES AC70. Wood or steel members connected to the substrate must be investigated in accordance with accepted design criteria.
- Low-velocity fasteners shall be driven to where the point of the fastener penetrates through the steel base material in accordance with Section 3.2.2.3, except as noted in this table.
- EDS fasteners installed into greater than 1/2" thick steel require 1/2" minimum penetration.
- Multiple fasteners are recommended for any attachment.
- Refer to guidelines for fastening to steel, Section 3.2.2, for application limits.
- Tabulated allowable load values provided for 3/4" steel are based upon minimum point penetration of 1/2" into the steel. If 1/2" point penetration into the steel is not achieved, but a point penetration of at least 3/8" is obtained, the tabulated tension value should be reduced by 20 percent and the tabulated shear load should be reduced by 8 percent.
- X-U 15 fasteners installed into greater than 3/8" thick steel require 15/32" minimum penetration into the steel.
- Based on testing with  $F_y = 50$  ksi base material.
- Fasteners installed into 3/8" or thicker base steel require 0.320" minimum penetration depth into the steel.
- Fasteners installed into 3/8" or thicker base require 0.38" minimum penetration depth into the steel.

**Allowable tensile pullover and shear bearing load capacities for steel framing with power driven fasteners<sup>1,2,3,4</sup>**

Fastener description	Fastener	Head dia. in. (mm)	Sheet steel thickness													
			14 ga.		16 ga.		18 ga.		20 ga.		22 ga.		24 ga.		25/26 ga.	
			Tension lb (kN)	Shear lb (kN)	Tension lb (kN)	Shear lb (kN)	Tension lb (kN)	Shear lb (kN)	Tension lb (kN)	Shear lb (kN)	Tension lb (kN)	Shear lb (kN)	Tension lb (kN)	Shear lb (kN)	Tension lb (kN)	Shear lb (kN)
0.157" shank with or w/o plastic washers or MX collation	X-U, X-P	0.322 (8.2)	825 (3.67)	1,085 (4.83)	685 (3.05)	720 (3.20)	490 (2.18)	525 (2.34)	360 (1.60)	445 (1.98)	300 (1.33)	330 (1.47)	205 (0.91)	255 (1.13)	120 (0.53)	145 (0.64)
0.145" shank with or w/o plastic washers or MX collation	X-C, X-R	0.322 (8.2)	-	985 (4.38)	685 (3.05)	720 (3.20)	490 (2.18)	515 (2.29)	360 (1.60)	440 (1.96)	300 (1.33)	310 (1.38)	205 (0.91)	235 (1.05)	120 (0.53)	145 (0.64)
0.177" shank without washer	DS, EDS	0.322 (8.2)	965 (4.29)	1,085 (4.83)	810 (3.60)	815 (3.63)	625 (2.78)	535 (2.38)	460 (2.05)	465 (2.07)	360 (1.60)	350 (1.56)	300 (1.33)	260 (1.16)	240 (1.07)	180 (0.80)
0.145" shank with plastic top hat washers	X-S13 THP, X-S16 TH	0.322 (8.2)	-	985 (4.38)	685 (3.05)	720 (3.20)	490 (2.18)	515 (2.29)	360 (1.60)	440 (1.96)	300 (1.33)	310 (1.38)	205 (0.91)	235 (1.05)	120 (0.53)	145 (0.64)
0.118" shank with MX collation	X-EGN, X-GN, X-GHP	0.276 (6.8)	-	-	-	-	325 (1.45)	390 (1.73)	265 (1.18)	335 (1.49)	250 (1.11)	235 (1.05)	170 (0.76)	185 (0.82)	100 (0.44)	125 (0.56)

- Allowable load values are based on a safety factor of 3.0.
- Allowable pullover capacities of sheet steel should be compared to the allowable fastener tensile load capacities in concrete, steel, and masonry to determine controlling resistance load.
- Allowable shear bearing capacities of sheet steel should be compared to allowable fastener shear capacities in concrete, steel and masonry to determine controlling resistance load.
- Data is based on the following minimum sheet steel properties,  $F_y = 33$  ksi,  $F_u = 45$  ksi (ASTM A653 material).

\* More details about the innovative X-U fastener can be found in Section 3.2.6.

**Ceiling Design****Ceiling Weight, W**

- USG Donn Brand Framing
- (1) Layer 3/4" USG Mars ACT
- Finishes, MEP, Misc

**PSF**

1

1

1

 $W_{MAX} \approx 3 \text{ PSF}$ 
**Seismic Force per ASCE**

$$a_p = \boxed{1}$$

$$S_{DS} = \boxed{1.006}$$

$$R_p = \boxed{2.5}$$

$$I_p = \boxed{1}$$

$$z/h = \boxed{1}$$

$$F_d = \frac{0.4a_p S_{DS} W I_p}{R_p} \left(1 + 2 \frac{z}{h}\right)$$

$$F_d = 0.483W \quad (\text{LRFD}) \quad \longrightarrow \quad E_{ASD} = 0.7F_d = \boxed{0.338W} \quad (\text{ASD})$$

 $E_{MAX} = 1 \text{ PSF}$

# BSE

**B**rienen **S**tructural **E**ngineers, P.S.

**ACT:**

Grid System = USG Donn Brand Advancespan

Panel = USG 2ft x 4ft 3/4in Mars 88189CR

System Weight = 3.0 PSF

Total Ceiling Area per grid is <144sq ft so Seismic Provisions are not required.

Main Runner Spacing = 4' oc

Main Runner Distributed Loads  $w_{max} = 3.0 \text{ PSF} \times 4' = 12 \text{ PLF}$

Use Main Runner DXAS, Allowable Load =  $12\text{PLF} \geq w_{max} \rightarrow \text{OK}$

Cross Runner Span = 4' max between main runners @ 2' oc

Use Cross Runner DXL424

Main Runner and Cross Runner Info Attached.

# USG MARS™ HEALTHCARE ACOUSTICAL PANELS CLIMAPLUS™ PERFORMANCE WITH CLEAN ROOM, HIGH-NRC AND AIRCARE™ COATING OPTIONS

PRCTI20240333



USG Mars™ Healthcare  
Acoustical Panels with ClimaPlus™  
Performance/USG Donn® Brand DX®/  
DXL™ Acoustical Suspension System

Photo this page:  
Chinook Regional Hospital  
Architect: Perkins + Will / KRA / Group2 / Stuart Olson  
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GO TO [USG.COM](http://USG.COM) OR [CGCINC.COM](http://CGCINC.COM)



White  
050

## FEATURES AND BENEFITS

- Water-repellent membrane designed to be durable and safe with common disinfectants.\*\*
- Washable and soil-resistant finish. Impact and scratch resistant.
- Acoustics and cleanability exceed FGI guidelines for healthcare.
- Meets USDA/FSIS guidelines for use in food-processing areas.
- Achieves FDA standards for smoothness, durability and cleanability.
- Clean Room tested to ISO 5 (Class 100) (Items 86169CR, 88189CR, 86684CR, 88683CR).
- ClimaPlus™ 30-year limited system warranty against visible sag, mold and mildew.
- AirCare™ coating applied to face and back reduces 75% of formaldehyde over a 10-year period.<sup>4</sup>
- GREENGUARD Gold certified for low emitting performance.
- Balanced Acoustics. High-NRC and High-CAC provide excellent sound control that assist in addressing HIPAA standards.
- USG Mars™ Healthcare Acoustical Panels is part of the Ecoblueprint™ portfolio — meeting today's sustainability standards. For sustainability documentation go to [USG.com](http://USG.com) or [CGCInc.com](http://CGCInc.com).

## APPLICATIONS

- Kitchen and food-prep areas
- Lavatories and restrooms
- Laboratories and Clean Rooms
- Nurses' stations/  
waiting rooms
- Treatment/patient  
rooms

## SUBSTRATE

- Wet-formed  
mineral fiber

Fine-Textured Panel

# USG MARS™ HEALTHCARE ACOUSTICAL PANELS

CLIMAPLUS™ PERFORMANCE – NEW CLEAN ROOM, HIGH-NRC AND AIRCARE™  
COATING OPTIONS

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PRODUCT CERTIFIED  
FOR LOW CHEMICAL  
EMISSIONS:  
ULCOM/CG  
UL2818



UL Classified

Edge	Panel Size	Fire Rating	Item No.	NRC	CAC Min.	LR <sup>2</sup>	Color	Grid Options	VOC Emissions	Anti-Mold & Mildew/Sag Resistance	Recycled Content <sup>1</sup>	Panel Cost
USG MARS™ HEALTHCARE HIGH-NRC PANELS 85/35 Plant-Based Binder <sup>6</sup>	SQ	Class A	2'x2'x7/8" <b>86256</b>	0.85	35	0.90	White	A,B,C,D,E,F	Low		70%	\$\$
	2'x4'x7/8" <b>88256</b>		0.85	35	0.90	White	A,B,D,E,F	Low		70%	\$\$	
USG MARS™ HEALTHCARE HIGH-NRC/ HIGH-CAC PANELS 80/40 Plant-Based Binder <sup>6</sup>	SLT	Class A	2'x2'x7/8" <b>86257</b>	0.85	35	0.90	White	G,H,I,J	Low		70%	\$\$
	FLB		2'x2'x7/8" <b>86258</b>	0.85	35	0.90	White	K,L,M,N	Low		70%	\$\$
USG MARS™ HEALTHCARE HIGH-NRC/ HIGH-CAC PANELS 80/40 Plant-Based Binder <sup>6</sup>	SQ	Class A	2'x2'x1" <b>86115</b>	0.80	40	0.90	White	A,B,C,D,E,F	Low		71%	\$\$
			2'x4'x1" <b>88115</b>	0.80	40	0.90	White	A,B,D,E,F	Low		71%	\$\$
	SLT	Class A	2'x2'x1" <b>86343</b>	0.80	40	0.90	White	G,H,I,J	Low		71%	\$\$
			2'x4'x1" <b>88343</b>	0.80	40	0.90	White	G,H,I,J	Low		71%	\$\$
	FLB	Class A	2'x2'x1" <b>86344</b>	0.80	40	0.90	White	K,L,M,N	Low		71%	\$\$
			2'x4'x1" <b>88344</b>	0.80	40	0.90	White	K,L,M,N	Low		71%	\$\$
USG MARS™ HEALTHCARE HIGH-NRC PANELS 80/35 Plant-Based Binder <sup>6</sup>	SQ	Class A	2'x2'x7/8" <b>86152</b>	0.80	35	0.90	White	A,B,C,D,E,F	Low		70%	\$\$
			2'x4'x7/8" <b>86340</b>	0.80	35	0.90	White	A,B,D,E,F	Low		70%	\$\$
	SLT	Class A	2'x2'x7/8" <b>86470</b>	0.80	35	0.90	White	G,H,I,J	Low		70%	\$\$
	FLB		2'x2'x7/8" <b>86750</b>	0.80	35	0.90	White	K,L,M,N	Low		70%	\$\$
USG MARS™ HEALTHCARE PANELS 75/35	SQ	Class A	2'x2'x3/4" <b>86169</b>	0.75	35	0.90	White	A,B,C,D,E,F	Low		69%	\$\$
			2'x4'x3/4" <b>88189</b>	0.75	35	0.90	White	A,B,D,E,F	Low		69%	\$\$
	SLT	Class A	2'x2'x3/4" <b>86684</b>	0.75	35	0.90	White	G,H,I,J	Low		69%	\$\$
			2'x4'x3/4" <b>88683</b>	0.75	35	0.90	White	G,H,I,J	Low		69%	\$\$
FLB	Class A	2'x2'x3/4" <b>86984</b>	0.75	35	0.90	White	K,L,M,N	Low		69%	\$\$	
		2'x4'x3/4" <b>88983</b>	0.75	35	0.90	White	K,L,M,N	Low		69%	\$\$	
USG MARS™ HEALTHCARE HIGH-CAC PANELS 60/40	SQ	Class A	2'x2'x3/4" <b>86270</b>	0.60	40	0.90	White	A,B,C,D,E,F	Low		71%	\$\$
			2'x4'x3/4" <b>88271</b>	0.60	40	0.90	White	A,B,D,E,F	Low		71%	\$\$
	SLT	Class A	2'x2'x3/4" <b>86272</b>	0.60	40	0.90	White	G,H,I,J	Low		71%	\$\$
	FLB		2'x2'x3/4" <b>86273</b>	0.60	40	0.90	White	K,L,M,N	Low		71%	\$\$
		Class A	2'x4'x3/4" <b>88273</b>	0.60	40	0.90	White	K,L,M,N	Low		71%	\$\$

**Low Emissions (VOC)**  
Third party (GREENGUARD Gold) certified for low-emitting performance, meets California Department of Public Health's (CDPH) Standard Method v1.2 - 2017 (CA Section 01350). 'Certificates of Compliance' for Low VOC Emissions are available on usg.com and at spot.ul.com.

**ClimaPlus™ Warranty Performance<sup>5</sup>**  
Contains a broad-spectrum antimicrobial additive on the face and back of the panel that provides resistance against the growth of mold and mildew. Includes sag-resistance performance.

**High Recycled Content**  
USG classifies High Recycled Content as greater than 50%. Total recycled content is based on product composition of postconsumer and preconsumer (postindustrial) recycled content per FTC guidelines.



# USG MARS™ HEALTHCARE ACOUSTICAL PANELS

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COATING OPTIONS

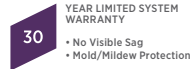
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EMISSIONS:  
ULCOM/GG  
UL2818



• No Visible Sag  
• Mold/Mildew Protection



UL Classified

Edge	Panel Size	Fire Rating	Item No.	NRC	CAC Min.	LR <sup>2</sup>	Color	Grid Options	VOC Emissions	Anti-Mold & Mildew/Sag Resistance	Recycled Content <sup>1</sup>	Panel Cost
SQ 	2'x2'x3/4"	Class A	<b>86169AIR</b>	0.75	35	0.90	White	A,B,C,D,E,F	Low		69%	\$\$
	2'x4'x3/4"	Class A	<b>88189AIR</b>	0.75	35	0.90	White	A,B,D,E,F	Low		69%	\$\$
SLT 	2'x2'x3/4"	Class A	<b>86684AIR</b>	0.75	35	0.90	White	G,H,I,J	Low		69%	\$\$
	2'x4'x3/4"	Class A	<b>88683AIR</b>	0.75	35	0.90	White	G,H,I,J	Low		69%	\$\$
FLB 	2'x2'x3/4"	Class A	<b>86984AIR</b>	0.75	35	0.90	White	K,L,M,N	Low		69%	\$\$
	2'x4'x3/4"	Class A	<b>88983AIR</b>	0.75	35	0.90	White	K,L,M,N	Low		69%	\$\$
SQ 	2'x2'x3/4"	Class A	<b>86169CR</b>	0.75	35	0.90	White	O	Low		68%	\$\$
	2'x4'x3/4"	Class A	<b>88189CR</b>	0.75	35	0.90	White	O	Low		68%	\$\$
SLT 	2'x2'x3/4"	Class A	<b>86684CR</b>	0.75	35	0.90	White	P	Low		68%	\$\$
	2'x4'x3/4"	Class A	<b>88683CR</b>	0.75	35	0.90	White	P	Low		68%	\$\$

USG MARS™ HEALTHCARE  
WITH AIRCARE™ COATING<sup>4</sup>  
75/35

USG MARS™ HEALTHCARE  
CLEAN ROOM PANELS  
75/35

**Low Emissions (VOC)**  
Third party (GREENGUARD Gold) certified for low-emitting performance, meets California Department of Public Health's (CDPH) Standard Method v1.2 - 2017 (CA Section 01350). 'Certificates of Compliance' for Low VOC Emissions are available on usg.com and at spot.ul.com.

**ClimaPlus™ Warranty Performance<sup>3</sup>**  
Contains a broad-spectrum antimicrobial additive on the face and back of the panel that provides resistance against the growth of mold and mildew. Includes sag-resistance performance.

**High Recycled Content**  
USG classifies High Recycled Content as greater than 50%. Total recycled content is based on product composition of postconsumer and preconsumer (postindustrial) recycled content per FTC guidelines.

# USG MARS™ HEALTHCARE ACOUSTICAL PANELS

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COATING OPTIONS

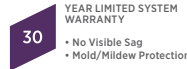
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## GRID PROFILE OPTIONS

<b>A</b> USG DX®	<b>B</b> USG DXW™	<b>C<sup>5</sup></b> USG Centricitee™ DXT™	<b>D</b> USG DXLA™
<b>E</b> USG ZXLA™	<b>F</b> USG AX™	<b>G</b> USG DX®	<b>H</b> USG DXLA™
<b>I</b> USG ZXLA™	<b>J</b> USG AX™	<b>K</b> USG Centricitee™ DXT™	<b>L</b> USG Fineline® DXF™
<b>M</b> USG Fineline® 1/8 DXFF™	<b>N</b> USG Identitee® DXI™	<b>O</b> USG CE™	<b>P</b> USG DXCE™

## PHYSICAL DATA/ FOOTNOTES

### Product literature

Data sheet: SC2585

### ASTM E1264 classification

ASTM E1264-22 Type IV, Form 1 & 2, Pattern E & G  
ASTM E1264-23 Type A, Form A2.1, Pattern E & G

### ASTM E84 and CAN/ULC S102 surface-burning characteristics Class A

Flame spread: 25 or less  
Smoke developed: 50 or less

### Weight

1.03-1.24 lb./sq. ft.

### Thermal resistance

R-2.2

### Maximum backloading

See *USG 30-Year Limited System Warranty Commercial Applications* (SC2102).

### Online tools

usgdesignstudio.com or cgcdesignstudio.com

### ASTM D2486 scrubability test

(standard test)

### ASTM D4828 washability test

(modified test)

### Water repellency

Cobb method (Tappi T441 om-84) Water Drop Test

### \*\*Maintenance

To clean panel, use a clean, white cloth with water or a mild detergent and wipe surface. To disinfect panel, lightly spray surface and wipe clean with a clean, white cloth. Acceptable colorless disinfectants include:

- Hydrogen peroxide
- Isopropyl alcohol
- Quaternary ammonium
- Sodium hypochlorite

Do not mix cleaners. Follow cleaner manufacturer's recommendations.

### USG Mars™ Healthcare Clean Room

- Field-cut edges of USG Mars™ Healthcare Clean Room panels may be sealed with white latex paint. Use square edge panels for all lay-in field-cut perimeter panels.

- Clean Room-rated applications require a suspension system with gasketed tee flanges such as USG Donn® Brand CE™.

- Tested to ISO Class 5 particle emissions, per ISO 14644, by UL Environment. Rating may decrease to ISO Class 7 or greater with airflow above 1 ACH, pressure fluctuations, or vibrations in the ceiling system.

- For more information, please reference test report from UL Environment.

### Metric sizes available

Contact sales for minimum quantities and lead times.

### Footnotes

1. For details, see USG Sustainability tool at usgdesignstudio.com or cgcdesignstudio.com.
2. LR values are shown as averages.
3. Panel face and back surfaces treated with a proprietary broad-spectrum antimicrobial standard formulation that inhibits and retards the growth of mold and mildew. For details, see *USG 30-Year Limited System Warranty Commercial Applications* (SC2102).
4. AirCare™ coating removes formaldehyde by an average of 75% over 10 years at an average indoor concentration of 13 ppb.
5. Maximum 2'x2' with SQ edge panels.
6. All USG Mars™ High NRC Acoustical Panels with a "plant-based binder" label contain up to 65% plant-based material in the binder. For more information please refer to the USG Mars™ Acoustical Panels Health Product Declaration, available at www.usg.com

WEIGHT FOR 88189CR IS THE LOWER END SINCE IT'S 3/4" THICK AS OPPOSED TO THE UPPER END BEING 7/8".

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### SC2585/rev.10-23

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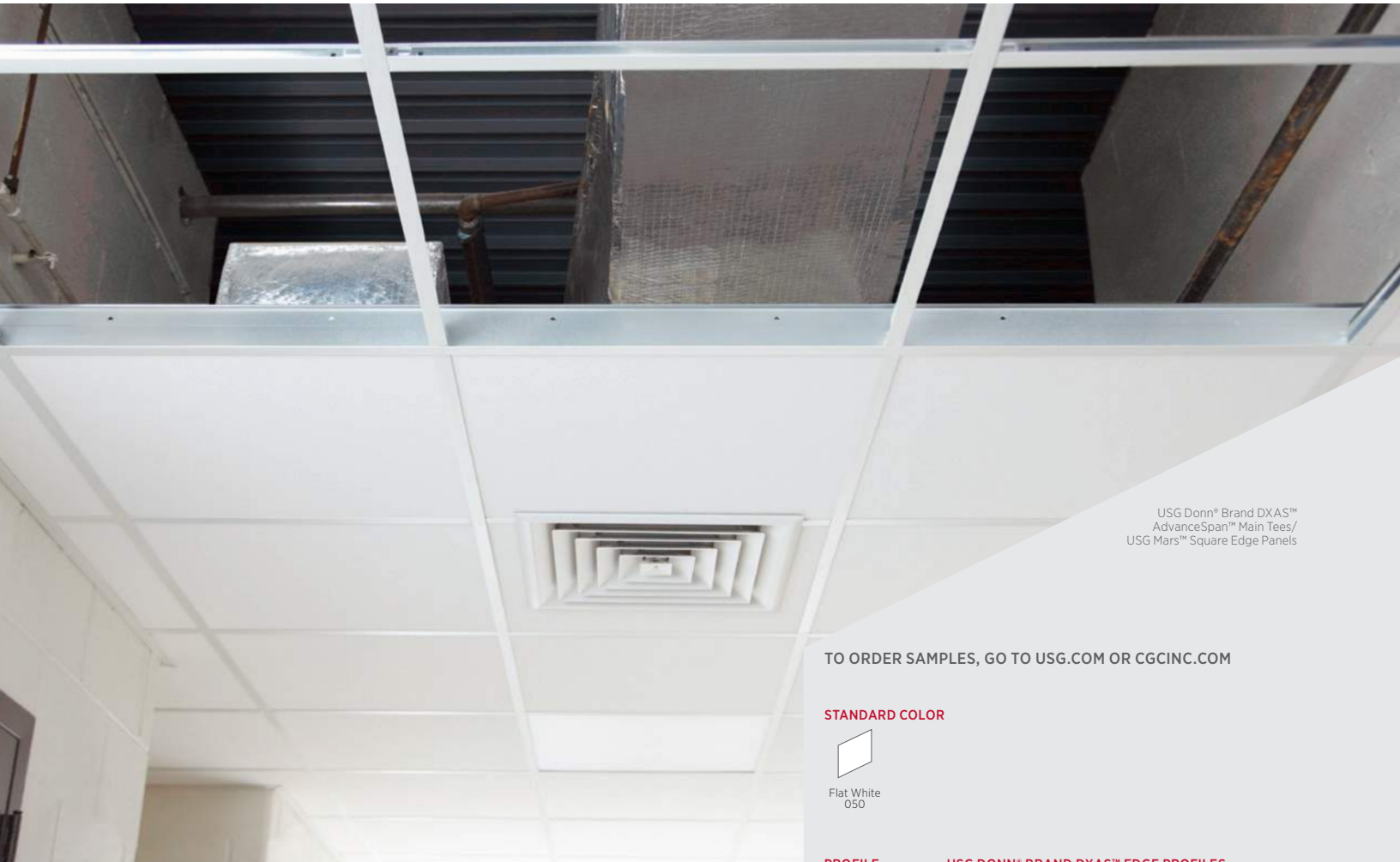
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Safety First! Follow good safety/industrial hygiene practices during installation. Wear appropriate personal protective equipment. Read SDS and literature before specification and installation.



# USG DONN® BRAND ADVANCESPAN™

USG DONN® BRAND DXAS™ AND DXTAS™ PROFILES



USG Donn® Brand DXAS™  
AdvanceSpan™ Main Tees/  
USG Mars™ Square Edge Panels

TO ORDER SAMPLES, GO TO [USG.COM](http://USG.COM) OR [CGCINC.COM](http://CGCINC.COM)

## STANDARD COLOR

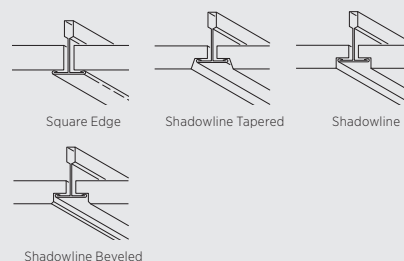


Flat White  
050

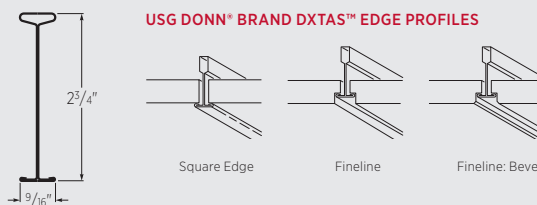
## PROFILE



## USG DONN® BRAND DXAS™ EDGE PROFILES



## USG DONN® BRAND DXTAS™ EDGE PROFILES



## FEATURES AND BENEFITS

- Spans up to 8' with no hanger wires.
- Ideal for healthcare, hospitality and multifamily applications with crowded plenum spaces.
- Seismic installation designs validated in ICC-ES Evaluation Report ESR-5136.
- Approved by OSHPD/HCAi for seismic applications.
- USG Donn® Brand DX®-15/16" and USG Donn® Brand Centricitee™ DXT™-9/16" face profiles available.
- Reversible structural wall channel works with both USG DX® and DXT™ profiles.
- Compatible with all standard USG DX® and DXT™ cross tees.
- Available with End Splice detail to speed up installation.
- USG Donn® Brand AdvanceSpan™ Suspension System is part of the Ecoblueprint™ portfolio — meeting today's sustainability standards. For sustainability documentation go to [USG.com](http://USG.com) or [CGCInc.com](http://CGCInc.com).

## APPLICATIONS

- Hospitals
- Multifamily dwellings
- Hotels
- Schools
- General interior use applications

**USG DONN® BRAND ADVANCESPAN™**  
 USG DONN® BRAND DXAS™ AND DXTAS™ PROFILES

ORDER SAMPLES/LITERATURE  
 USG: usg.com or samplitt@usg.com  
 CGC: contact Sales Representative

TECHNICAL SERVICES  
 800 USG.4YOU (874-4968)

FOR MOST UP-TO-DATE  
 TECHNICAL INFORMATION  
 AND LEED REPORT TOOL  
 usgdesignstudio.com  
 cgcdesignstudio.com



Declare® Labels on select finishes, see usg.com for more details and documentation.

Item No	Length	Height	Face Profile	Fire Rating	Recycled Content	Color	Max Unsupported Span at Rated Load	
							Intermediate Duty (12 lb./LF)	Heavy Duty (16 lb./LF)
<b>15/16" TEE SYSTEM</b>								
Main Tee 	<b>DXAS</b>	8'-6" 10'-6" 12'-6"	2-3/4"	15/16"	Class A	Flat White 050	8'-0"	7'-0"
	<b>DXAS-ES</b>	10'-0" 12'-0"	2-3/4"	15/16"	Class A	Flat White 050	8'-0"	7'-0"
Cross Tee 1" 	<b>DX216</b>	2' 600 mm	1" (25 mm)	15/16"	Class A	Flat White 050		
	<b>Cross Tee 1-1/2"</b>							
	<b>DXL424</b>	4' 1200 mm	1-1/2" (38 mm)	15/16"	Class A	Flat White 050		
	<b>DXL424HRC</b>			15/16"	Class A	Flat White 050		
	<b>DX422</b>			15/16"	Class A	Flat White 050		
	<b>DX422HRC</b>			15/16"	Class A	Flat White 050		
	<b>DX426HD</b>			15/16"	Class A	Flat White 050		
<b>9/16" TEE SYSTEM</b>								
Main Tee 	<b>DXTAS</b>	8'-6" 10'-6" 12'-6"	2-3/4"	9/16"	Class A	Flat White 050	8'-0"	7'-0"
	<b>DXTAS-ES</b>	10'-0" 12'-0"	2-3/4"	9/16"	Class A	Flat White 050	8'-0"	7'-0"
Cross Tee 1-1/2" 	<b>DXT222</b>	2' 600 mm	1-1/2" (38 mm)	9/16"	Class A	Flat White 050		
	<b>DXT222HRC</b>			9/16"	Class A	Flat White 050		
	<b>DXLT222</b>			9/16"	Class A	Flat White 050		
	<b>DXT422</b>	4' 1200 mm	1-1/2" (38 mm)	9/16"	Class A	Flat White 050		
	<b>DXT424</b>			9/16"	Class A	Flat White 050		
	<b>DXT424HRC</b>			9/16"	Class A	Flat White 050		
<b>MOLDING</b>								
	<b>Channel</b>	<b>Length</b>	<b>Height</b>	<b>Face Profile</b>	<b>Item No</b>	<b>Recycled Content</b>	<b>Color</b>	
		10'	2-7/8"	Reversible for 15/16" or 9/16"	<b>US44HRC</b>		Flat White 050	

\*Tested in accordance with ASTM C635 modified.

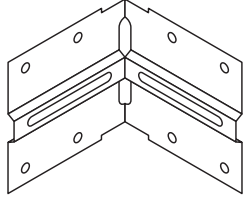
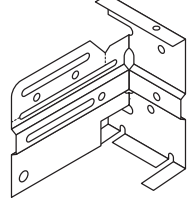
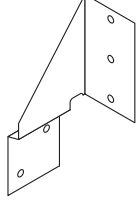
**Low Emissions (VOC)**  
 CDPH 01350 v1.2-2017 compliance on select finishes, see usg.com for more details and documentation.

**High Recycled Content**  
 USG classifies High Recycled Content as greater than 50%. Total recycled content is based on product composition of postconsumer and preconsumer (postindustrial) recycled content per FTC guidelines.

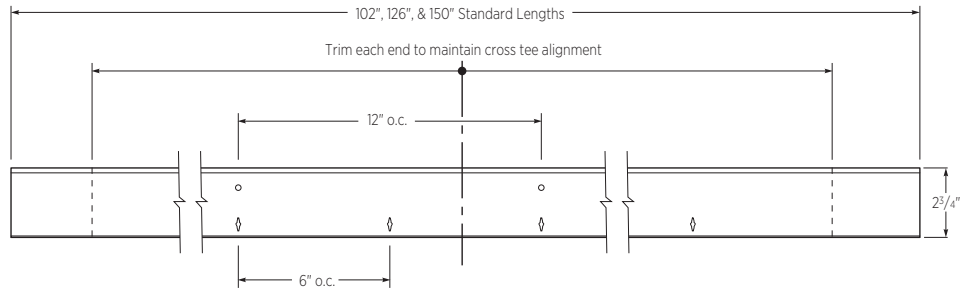


Declare® Labels on select finishes, see usg.com for more details and documentation.

**ACCESSORIES**

ASMTSP Splice Plate	US44CC Channel Clip	ASCBC Cross Brace Clip
		

**USG DONN® BRAND ADVANCESPAN™ MAIN TEE DETAILS**



**PHYSICAL DATA/ FOOTNOTES**

**Product literature and samples**  
 Data sheet: AC3324  
 Installation guide: AC3325  
 USG DXAS™ sample: 259499  
 USG DXTAS™ sample: 259500

**Material**  
 Min. G30 hot-dipped galvanized steel body and cap. Baked-on polyester paint.

**Online tools**  
 usgdesignstudio.com or cgcdesignstudio.com

**Compliance**  
 Third-party tested by Progressive Engineering Inc. in accordance with ASTM C635 (modified). Full-scale seismic testing conducted by University of California, Berkeley, Pacific Earthquake Engineering Research Center. Local building codes may vary; check with code official for compliance prior to installing.

**Limitations**  
 Interior applications only.

**Seismic Compliance**  
 AdvanceSpan™ is OSHPD/HCAI pre-approved per OPM-0462.

**ICC Evaluation Service, LLC Report Compliance**  
 For areas under ICC jurisdiction, see ICC-ES Evaluation Report ESR-5136 for allowable values and conditions of use. Reports are subject to reexamination, revision and possible cancellation. Refer to usg.com for most current version.

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