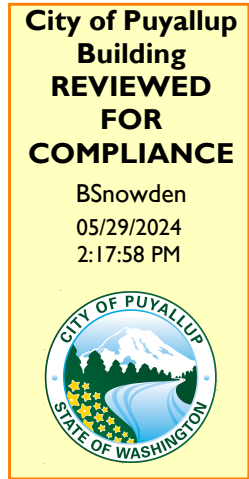
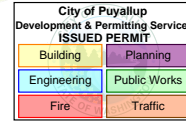


STRUCTURAL CALCULATIONS

Steel Storage Shelving
By Mobile Media Storage Solutions

JD Sports - Store #1315

South Hill Mall - Space #530
3500 South Meridian Street
Puyallup, Washington 98373



Calculations required to be provided by the Permittee on site for all Inspections

Prepared For:

Mobile Media Storage Solutions
45 Turner Drive - Suite #2A
Middletown, NY 10941



Please note: the calculations contained within justify the seismic resistance of the shelving systems for both vertical and lateral forces as required by the 2021 WSBC, ASCE 7-16, and ANSI/RMI-MH16.1 (2012). These storage shelves are not accessible to the general public

MOBILE MEDIA STORAGE SOLUTIONS

STEEL STORAGE SHELVING - LIGHT RETAIL

CODES: Current Editions of the: IBC & CBC & ASCE 7 & RMI

Design Inputs: Steel Storage Shelving: 10'H Mobile Shelf Units

Shelving Geometry -

Height of Shelving Unit =	10.0	ft	Steel Yield Stress =	33	ksi
Width of Shelving Unit =	4.0	ft	Modulus of Elast. =	29000	ksi
Depth of Shelving Unit =	2.0	ft			
Number of Shelves/Unit =	6		Eff. Length Factor =	1.7	
Vertical Shelf Spacing =	23.4	in	Unbraced Length,x =	23.4	in
Back to Back Units?	NO		Unbraced Length,y =	23.4	in
Are There Mobile Units?	YES		Type of Post?	14ga Upright Posts	
# of Units Per Anti-Tip?	1.5		Type of Beam?	DRL Low Profile	

Shelving Loading -

Live Load per Shelf =	9.4	psf	Display On Plaque Near Shelving Units
Maximum Weight per Shelf =	75	lbs	Per 2ft Deep Shelf
Dead Load per Shelf =	2.0	psf	Wire Grid Shelf Material
Weight of Each Post =	7.5	lbs	
Weight of Mobile Carriage =	50	lbs	
Floor Load Calculations:			
Total Load on Each "L" Post =	144	lbs	
Total Load On Each Unit =	627	lbs	

Seismic Information -

Importance Factor =	1.0	Not Open to the Public	SDC: D
Site Class =	D - Default		

Mapped Accel. Parameters:

$S_s = 1.264$	$F_a = 1.200$	$S_{ms} = 1.517$	$S_{ds} = 1.011$
$S_1 = 0.436$	$F_v = 1.864$	$S_{m1} = 0.813$	$S_{d1} = 0.542$

Structural System - ASCE 7 Section 15.5.3

Steel Storage Shelving:	R = 4	$a_p = 2.5$	$I_p = 1.0$
Average Roof Height =	20	ft	0'-0" For Ground Floor Location
Height of Base Attachment =	0	ft	Ground Floor
Shear Coeff Boundaries =	$V_{min} = 0.044$		
	$V_{max} = 0.253$		

Design Base Shear Coeff = $V_t = 0.177$ Adjusted For ASD

Lateral Force Distribution: per ASCE 7 Section 15.5.3.3

Total Dead Load per Shelf =	21.0	lbs
Total Live Load per Shelf =	75.2	lbs
Lateral DL Force per Shelf =	3.7	lbs
Lateral LL Force per Shelf =	13.3	lbs
67% of LL Force per Shelf =	8.9	lbs
Total DL Base Shear =	22.3	lbs
Total LL Base Shear =	79.8	lbs

LC1: Each Shelf is Loaded to 67% of its Live Weight

Cumulative Moment: 26337 in-lbs

Total Base Shear =	75.8	lbs
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Controlling Load Case By Inspection

Height:	Load:	% Per Level:	Lateral Force/Level:
h1 = 3 in	75 lbs	0.8%	F1 = 0.6 lbs
h2 = 26 in	75 lbs	7.2%	F2 = 5.4 lbs
h3 = 50 in	75 lbs	13.5%	F3 = 10.2 lbs
h4 = 73 in	75 lbs	19.8%	F4 = 15.0 lbs
h5 = 97 in	75 lbs	26.2%	F5 = 19.8 lbs
h6 = 120 in	75 lbs	32.5%	F6 = 24.6 lbs
h7 = 0 in	0 lbs	0.0%	F7 = 0.0 lbs
h8 = 0 in	0 lbs	0.0%	F8 = 0.0 lbs
h9 = 0 in	0 lbs	0.0%	F9 = 0.0 lbs
h10 = 0 in	0 lbs	0.0%	F10 = 0.0 lbs
h11 = 0 in	0 lbs	0.0%	F11 = 0.0 lbs
h12 = 0 in	0 lbs	0.0%	F12 = 0.0 lbs
h13 = 0 in	0 lbs	0.0%	F13 = 0.0 lbs
h14 = 0 in	0 lbs	0.0%	F14 = 0.0 lbs
h15 = 0 in	0 lbs	0.0%	F15 = 0.0 lbs
		Sum = 100%	75.8 lbs

LC 2: Top Shelf Only is Loaded to 100% of its Live Weight

Total Base Shear = 35.6 lbs Does Not Control

By inspection, the force distribution for intermediate shelves without live load (case 2) is negligible. Calculate the moment for each column based on the total seismic base shear for each shelf being loaded to 67% of its allowable live weight. The column at the center of the shelving system is the worst case for this condition.

Column Calculations - Combined Bending and Axial

Post Type:

Double Rivet "L" or "T" Post

Width =	1.5	in	$r_x =$	0.470	in
Depth =	1.5	in	$S_x =$	0.040	in ³
Thickness =	0.075	in	$I_x =$	0.060	in ⁴
E =	29000	ksi	$A_p =$	0.220	in ²
			$A_e =$	0.157	in ²

Column Bending Calculations -

Max Column Moment =	18.3	ft-lbs	For L Post
Allowable Bending Stress =	19.8	ksi	
Bending Stress on Column =	5.5	ksi	Bending Stress OK

Column Deflection Calculations -

Max Deflection =	0.306	in	At Top of Unit
Deflection Ratio =	392		L/ Δ
Allowable Deflection =	6	in	Max Deflection = 5% of Height
			Deflection OK

Shelf Rivet Connection -

Diameter of Rivet =	0.25	in	
Shear on Each Rivet =	293.2	lbs	
Brg Capacity of Rivet =	787.5	lbs	Brg Stress OK
Allowable Shear Stress =	13.2	ksi	
Shear Stress on Rivet =	6.0	ksi	Shear Stress OK

Column Axial Calculations -

Per "L" Post

DL + PL =	144	lbs	RMI Load Combination #1
DL + PL + EQ =	252	lbs	RMI Load Combination #6

Column Capacity Calculations -

Controlling Buckling Stress =	23.5	ksi	
Allowable Comp. Stress =	18.3	ksi	
Factor of Safety for Comp. =	1.80		
Nominal Column Capacity =	2878	lbs	
Allowable Column Capacity =	1599	lbs	
Static Axial Load on Column =	144	lbs	Axial Load OK

Combined Bending And Axial Forces -

Critical Buckling Load =	10852	lbs	
Axial Stress Unity =	0.158		Magnification Factor = 0.976
Bending Stress Unity =	0.242		$C_m =$ 0.85

Combined Stress Unity = 0.400	Column is Adequate
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Overtipping and Anti-Tip Calculations

Overtipping Forces -

Total Weight = 428 lbs Load Case 1: Dead Load + 67% Live Load
Total Lateral Force = 76 lbs

Overtipping Force = 552 ft*lbs Controlling Overtipping Force

Total Weight = 201 lbs Load Case 2: Dead Load + 100% Top Shelf
Total Lateral Force = 36 lbs

Overtipping Force = 288 ft*lbs Does Not Control

Tension Force per Anchor = 178 lbs
Shear Force per Anchor = 38 lbs

USE: 'Hilti' HUS-EZ (or equivalent) POST INSTALLED ANCHOR BOLTS

Allowable Tension Force = 736 lbs For Concrete Slab on Grade
Allowable Shear Force = 1056 lbs 3/8" Diameter x 2.5" Embedment

Vertical Seismic Force = 30.3 lbs
Overstrength Factor = 2 For Anchoring to Concrete

Combined Loading = 0.484 Floor Anchors are Adequate

Mobile Carriage OR Baseplate Connection For Static Units -

Type of Connection = **Mobile Carriage** OR **14ga Baseplate at Static Units**

Tension per Side = 267 lbs
Capacity of (1) Tek Screw = 394 lbs

(2) #12 Screws Are Adequate

Tension Cap. of Baseplate Leg = 2030 lbs

Baseplate Thickness OK

(Yielding in Net / Fracture in Gross)

Anti-Tip Arm and Track Design -

Anti-Tip Yield Stress = 16 ksi 6063-T5
Thickness Anti-Tip = 0.12 in
Width of Anti-Tip = 0.43 in
Section Modulus of Leg = 0.0092 in³

Allowable Stress on Leg = 12.61 ksi
Bending Stress on Leg = 9.32 ksi

Anti-Tip Stress Unity = 0.739 Bending Stress OK

Section Modulus of Track = 0.090 in³
Spacing of Track A.B's = 24 in

Allowable Alumn. Stress = 12.61 ksi 6063-T5
Bending Stress on Track = 8.90 ksi

Track Stress Unity = 0.706 Bending Stress OK

Shelf Beam Calculations

Shelf Beam Calculations:

DRL Low Profile

Steel Yield Stress =	33	ksi	Shelf DL =	2.0	psf
Modulus of Elast. =	29000	ksi	Shelf LL =	9.40	psf

Beam Type:	<u>DRL</u>	<u>DRH</u>	<u>DRC</u>	
Area of Beam =	0.168	0.277	0.445	in ²
Section Modulus of Beam =	0.020	0.219	0.346	in ³
Moment of Inertia of Beam =	0.014	0.220	0.477	in ⁴

Shelf Width =	4.0	ft	Allowable Bending Stress =	19.3	ksi
Shelf Depth =	2.0	ft	Allowable Shear Stress =	13.2	ksi
Total Load/Shelf =	91	lbs			
Distributed Load =	11.4	plf			

Beam Type:	<u>DRL</u>	<u>DRH</u>	<u>DRC</u>	
Maximum Design Moment =	22.8			ft-lbs
Maximum Design Shear =	22.8			lbs
Beam Bending Stresses =	13.9			ksi
Beam Shear Stresses =	0.14			ksi

Bending Stress Unity = 0.720
Shear Stress Unity = 0.010

Bending Stress OK

Shear Stress OK

Max Allowable Deflection =	0.267	in	L/180
Maximum Beam Deflection =	0.163	in	Deflection OK

Shelf Beam Rivet Check:

Diameter of Rivet =	0.25	in
Post Moment Shear on Rivet =	293.2	lbs
Beam Shear on Rivet =	22.8	lbs
Resultant Shear =	294.0	lbs

Brg Capacity of Rivet = 787.5 lbs

Brg Stress OK

Allowable Shear Stress =	13.2	ksi
Shear Stress on Rivet =	6.0	ksi

Shear Stress OK

Slab Bearing & Uplift Calculations

Slab Design Properties -

Minimum Concrete Strength =	2500	psi	Assumed
Thickness of Concrete Slab =	4	in	Assumed
Weight of Concrete Slab =	50	psf	
Allowable Bearing Pressure =	500	psf	Assumed
Bearing Loads On Post =	80	lbs	Dead Load
	226	lbs	Live Load
	276	lbs	EQ Load
Uplift Loads on Post =	178	lbs	Resultant Uplift

Slab Bearing Capacity -

Depth of Post on Slab =	1.5	in	
Factored Bearing Load =	852	lbs	
Required Bearing Area =	167.70	in ²	12.95 inches per side
Critical Section =	3.72	in	For Bending
Soil Pressure on Crit. Section =	731.7	plf	Along Critical Length
Section Modulus =	32.0	in ³	Plain Concrete per Foot
Shear Area =	22	in	
Conc. Shear Stress =	9.7	psi	
Allowable Shear Stress =	73.2	psi	Shear Stress OK
Conc. Bending Stress =	13.2	psi	
Allowable Bending Stress =	137.5	psi	Bending Stress OK

Slab Uplift Capacity -

Required Area to Resist Uplift =	5.93	ft ²	
Length of Slab Req'd =	1.48	ft	Assume Full Shelf Width x Req'd Length
Worst Case Length of Slab =	4.00	ft	Maximum of Width or Length Req'd
Distance to Anchor Bolt =	2.00	ft	
Shear Force on 1ft Strip =	140.0	lbs	
Allowable Shear Force =	1760.0	lbs	Shear OK
Bending Moment on 1ft Strip =	140.0	ft-lbs	
Allowable Bending Moment =	366.7	ft-lbs	Bending OK

MOBILE MEDIA STORAGE SOLUTIONS

STEEL STORAGE SHELVING - LIGHT RETAIL

CODES: Current Editions of the: IBC & CBC & ASCE 7 & RMI

Design Inputs: Steel Storage Shelving: 12'H Freestanding Units

Shelving Geometry -

Height of Shelving Unit =	12.0	ft	Steel Yield Stress =	33	ksi
Width of Shelving Unit =	5.0	ft	Modulus of Elast. =	29000	ksi
Depth of Shelving Unit =	2.0	ft (MAX)			
Number of Shelves/Unit =	7		Eff. Length Factor =	1.7	
Vertical Shelf Spacing =	23.5	in	Unbraced Length,x =	23.5	in
Back to Back Units?	NO		Unbraced Length,y =	23.5	in
Are There Mobile Units?	NO		Type of Post?	14ga Upright Posts	
# of Units Per Anti-Tip?	NA		Type of Beam?	DRL Low Profile	

Shelving Loading -

Live Load per Shelf =	7.5	psf	Display On Plaque Near Shelving Units
Maximum Weight per Shelf =	75	lbs	Per 2ft (MAX) Deep Shelf
Dead Load per Shelf =	2.0	psf	Wire Grid Shelf Material
Weight of Each Post =	9.0	lbs	
Weight of Mobile Carriage =	0	lbs	
Floor Load Calculations:			
Total Load on Each "L" Post =	175	lbs	
Total Load On Each Unit =	701	lbs	

Seismic Information -

Importance Factor -	1.0	Not Open to the Public	SDC: D
Site Class -	D - Default		

Mapped Accel. Parameters:

$S_s = 1.264$	$F_a = 1.200$	$S_{ms} = 1.517$	$S_{ds} = 1.011$
$S_1 = 0.436$	$F_v = 1.864$	$S_{m1} = 0.813$	$S_{d1} = 0.542$

Structural System - ASCE 7 Section 15.5.3

Steel Storage Shelving:	R = 4	$a_p = 2.5$	$I_p = 1.0$
Average Roof Height =	20	ft	0'-0" For Ground Floor Location
Height of Base Attachment =	0	ft	Ground Floor
Shear Coeff Boundaries =	$V_{min} = 0.044$		
	$V_{max} = 0.253$		

Design Base Shear Coeff =	$V_t = 0.177$	Adjusted For ASD
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Lateral Force Distribution: per ASCE 7 Section 15.5.3.3

Total Dead Load per Shelf =	25.1	lbs
Total Live Load per Shelf =	75	lbs
Lateral DL Force per Shelf =	4.4	lbs
Lateral LL Force per Shelf =	13.3	lbs
67% of LL Force per Shelf =	8.9	lbs
Total DL Base Shear =	31.1	lbs
Total LL Base Shear =	92.9	lbs

LC1: Each Shelf is Loaded to 67% of its Live Weight

Cumulative Moment: 38785 in-lbs

Total Base Shear =	93.4	lbs
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Controlling Load Case By Inspection

Height:	Load:	% Per Level:	Lateral Force/Level:
h1 = 3 in	75 lbs	0.6%	F1 = 0.5 lbs
h2 = 27 in	75 lbs	5.2%	F2 = 4.8 lbs
h3 = 50 in	75 lbs	9.7%	F3 = 9.1 lbs
h4 = 74 in	75 lbs	14.3%	F4 = 13.3 lbs
h5 = 97 in	75 lbs	18.9%	F5 = 17.6 lbs
h6 = 121 in	75 lbs	23.4%	F6 = 21.9 lbs
h7 = 144 in	75 lbs	28.0%	F7 = 26.1 lbs
h8 = 0 in	0 lbs	0.0%	F8 = 0.0 lbs
h9 = 0 in	0 lbs	0.0%	F9 = 0.0 lbs
h10 = 0 in	0 lbs	0.0%	F10 = 0.0 lbs
h11 = 0 in	0 lbs	0.0%	F11 = 0.0 lbs
h12 = 0 in	0 lbs	0.0%	F12 = 0.0 lbs
h13 = 0 in	0 lbs	0.0%	F13 = 0.0 lbs
h14 = 0 in	0 lbs	0.0%	F14 = 0.0 lbs
h15 = 0 in	0 lbs	0.0%	F15 = 0.0 lbs
Sum = 100%			Total = 93.4 lbs

LC 2: Top Shelf Only is Loaded to 100% of its Live Weight

Total Base Shear = 44.4 lbs Does Not Control

By inspection, the force distribution for intermediate shelves without live load (case 2) is negligible. Calculate the moment for each column based on the total seismic base shear for each shelf being loaded to 67% of its allowable live weight. The column at the center of the shelving system is the worst case for this condition.

Column Calculations - Combined Bending and Axial

Post Type:

Double Rivet "L" or "T" Post

Width =	1.5	in	$r_x =$	0.470	in
Depth =	1.5	in	$S_x =$	0.040	in ³
Thickness =	0.075	in	$I_x =$	0.060	in ⁴
E =	29000	ksi	$A_p =$	0.220	in ²
			$A_e =$	0.157	in ²

Column Bending Calculations -

Max Column Moment =	22.7	ft-lbs	For L Post
Allowable Bending Stress =	19.8	ksi	
Bending Stress on Column =	6.8	ksi	Bending Stress OK

Column Deflection Calculations -

Max Deflection =	0.438	in	At Top of Unit
Deflection Ratio =	329		L/ Δ
Allowable Deflection =	7.2	in	Max Deflection = 5% of Height
			Deflection OK

Shelf Rivet Connection -

Diameter of Rivet =	0.25	in	
Shear on Each Rivet =	363.6	lbs	
Brg Capacity of Rivet =	787.5	lbs	Brg Stress OK
Allowable Shear Stress =	13.2	ksi	
Shear Stress on Rivet =	7.4	ksi	Shear Stress OK

Column Axial Calculations -

Per "L" Post

DL + PL =	175	lbs	RMI Load Combination #1
DL + PL + EQ =	343	lbs	RMI Load Combination #6

Column Capacity Calculations -

Controlling Buckling Stress =	23.4	ksi	
Allowable Comp. Stress =	18.3	ksi	
Factor of Safety for Comp. =	1.80		
Nominal Column Capacity =	2871	lbs	
Allowable Column Capacity =	1595	lbs	
Static Axial Load on Column =	175	lbs	Axial Load OK

Combined Bending And Axial Forces -

Critical Buckling Load =	10760	lbs	
Axial Stress Unity =	0.215		Magnification Factor = 0.971
Bending Stress Unity =	0.302		$C_m =$ 0.85

Combined Stress Unity = 0.516	Column is Adequate
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Overturning and Anti-Tip Calculations

Overturning Forces -

Total Weight = 528 lbs Load Case 1: Dead Load + 67% Live Load
Total Lateral Force = 93 lbs

Overturning Force = 806 ft*lbs Controlling Overturning Force

Total Weight = 251 lbs Load Case 2: Dead Load + 100% Top Shelf
Total Lateral Force = 44 lbs

Overturning Force = 407 ft*lbs Does Not Control

Tension Force per Anchor = 282 lbs
Shear Force per Anchor = 47 lbs

USE: 'Hilti' HUS-EZ (or equivalent) POST INSTALLED ANCHOR BOLTS

Allowable Tension Force = 736 lbs For Concrete Slab on Grade
Allowable Shear Force = 1056 lbs 3/8" Diameter x 2.5" Embedment

Vertical Seismic Force = 37.4 lbs
Overstrength Factor = 2 For Anchoring to Concrete

Combined Loading = 0.766 Floor Anchors are Adequate

Mobile Carriage OR Baseplate Connection For Static Units -

Type of Connection = **NONE** OR **14ga Baseplate at Static Units**

Tension per Side = 282 lbs Static Baseplate Connection
Capacity of (1) Tek Screw = 394 lbs **(2) #12 Screws Are Adequate**

Tension Cap. of Baseplate Leg = 2030 lbs **Baseplate Thickness OK**
(Yielding in Net / Fracture in Gross)

Anti-Tip Arm and Track Design -

Anti-Tip Yield Stress = 16 ksi 6063-T5
Thickness Anti-Tip = 0.12 in
Width of Anti-Tip = 0.43 in
Section Modulus of Leg = 0.0092 in³

Allowable Stress on Leg = N/A ksi
Bending Stress on Leg = N/A ksi

Anti-Tip Stress Unity = N/A N/A

Section Modulus of Track = 0.090 in³
Spacing of Track A.B's = N/A in

Allowable Alumn. Stress = N/A ksi 6063-T5
Bending Stress on Track = N/A ksi

Track Stress Unity = N/A N/A

Shelf Beam Calculations

Shelf Beam Calculations:

DRL Low Profile

Steel Yield Stress =	33	ksi	Shelf DL =	2.0	psf
Modulus of Elast. =	29000	ksi	Shelf LL =	7.50	psf
Beam Type:	<u>DRL</u>	<u>DRH</u>	<u>DRC</u>		
Area of Beam =	0.168	0.277	0.445	in ²	
Section Modulus of Beam =	0.020	0.219	0.346	in ³	
Moment of Inertia of Beam =	0.014	0.220	0.477	in ⁴	
Shelf Width =	5.0	ft	Allowable Bending Stress =	19.8	ksi
Shelf Depth =	2.0	ft	Allowable Shear Stress =	13.2	ksi
Total Load/Shelf =	95	lbs			
Distributed Load =	9.5	plf			

Beam Type:	<u>DRL</u>	<u>DRH</u>	<u>DRC</u>	
Maximum Design Moment =	29.7			ft-lbs
Maximum Design Shear =	23.8			lbs
Beam Bending Stresses =	18.1			ksi
Beam Shear Stresses =	0.14			ksi

Bending Stress Unity = 0.913
Shear Stress Unity = 0.011

Bending Stress OK

Shear Stress OK

Max Allowable Deflection = 0.333 in
Maximum Beam Deflection = 0.331 in

L/180

Deflection OK

Shelf Beam Rivet Check:

Diameter of Rivet = 0.25 in
Post Moment Shear on Rivet = 363.6 lbs
Beam Shear on Rivet = 23.8 lbs
Resultant Shear = 364.4 lbs

Brg Capacity of Rivet = 787.5 lbs

Brg Stress OK

Allowable Shear Stress = 13.2 ksi
Shear Stress on Rivet = 7.4 ksi

Shear Stress OK

Wall Supported Unit Calculations

Seismic Force at Top of Units -

Average Roof Height = 20.0 ft

Height of Attachment = 12.0 ft

Shear Coeff Boundaries = $V_{min} = 0.303$

$V_{max} = 1.618$

Design Base Shear Coeff = $V_t = 0.397$ Adjusted For ASD

Total Weight per Unit = 470 lbs

Lateral Force at Top/Bottom = 93 lbs

Standard Stud Spacing = 16 in

Wall Connections per Unit = 2 (to nearest stud each side of T post)

Tek Screw Capacity = 84 lbs

Tension Cap. for #10 Screw in 20ga Stud

Force Per Connection = 47 lbs

Screw Capacity OK

Light Gage Steel Stud Wall Framing

Stud Design Data -

Height of Wall Studs =	16.0	ft	Int. Non-Brg - Worst Case Ht Assumed
Location of Point Load =	12.0	ft	
Design Lateral Load =	46.6	lbs	From Shelving Unit
Additional Lateral Load =	5.0	psf	Interior Seismic Force
Design Axial Load =	85.3	lbs	Dead Load of Wall Framing
Spacing of Studs =	16.0	in	

TRY: 3-5/8" x 1-5/8" x 20ga Studs @ 16" o.c. (Worst Case Assumed)

Width =	3.625	in	rx =	1.450	in
Depth =	1.625	in	ry =	0.616	in
Thickness =	0.035	in	Sx =	0.268	in ³
Fy =	33	ksi	Ix =	0.551	in ⁴
E =	29000	ksi	Ap =	0.262	in ²
K =	1.0		Unbraced Length X =	16	ft
			Unbraced Length Y =	4	ft

Stud Capacity -

Buckling Stress, X =	16.32	ksi
Buckling Stress, Y =	47.14	ksi
Allowable Buckling Stress =	16.32	ksi
Nominal Axial Strength =	4277	lbs
Factor of Safety =	1.92	
Allowable Axial Load =	2228	lbs

Maximum Design Moment =	353.3	ft-lbs
Maximum Design Shear =	88.3	lbs

Allowable Bending Stress =	21.78	ksi
Actual Bending Stress =	15.82	ksi

Bending Stress OK

Allowable Shear Stress =	13.20	ksi
Actual Shear Stress =	0.34	ksi

Shear Stress OK

Allowable Axial Stress =	8.50	ksi
Actual Axial Stress =	0.33	ksi

Axial Stress OK

Combined Stress Unity = 0.76

Combined Stress OK

Slab Bearing & Uplift Calculations

Slab Design Properties -

Minimum Concrete Strength =	2500	psi	Assumed
Thickness of Concrete Slab =	4	in	Assumed
Weight of Concrete Slab =	50	psf	
Allowable Bearing Pressure =	500	psf	Assumed
Bearing Loads On Post =	79	lbs	Dead Load
	263	lbs	Live Load
	403	lbs	EQ Load
Uplift Loads on Post =	282	lbs	Resultant Uplift

Slab Bearing Capacity -

Depth of Post on Slab =	1.5	in	
Factored Bearing Load =	1090	lbs	
Required Bearing Area =	214.38	in ²	14.64 inches per side
Critical Section =	4.57	in	For Bending
Soil Pressure on Crit. Section =	732.4	plf	Along Critical Length
Section Modulus =	32.0	in ³	Plain Concrete per Foot
Shear Area =	22	in	
Conc. Shear Stress =	12.4	psi	
Allowable Shear Stress =	73.2	psi	Shear Stress OK
Conc. Bending Stress =	19.9	psi	
Allowable Bending Stress =	137.5	psi	Bending Stress OK

Slab Uplift Capacity -

Required Area to Resist Uplift =	9.40	ft ²	
Length of Slab Req'd =	1.88	ft	Assume Full Shelf Width x Req'd Length
Worst Case Length of Slab =	5.00	ft	Maximum of Width or Length Req'd
Distance to Anchor Bolt =	2.50	ft	
Shear Force on 1ft Strip =	175.0	lbs	
Allowable Shear Force =	1760.0	lbs	Shear OK
Bending Moment on 1ft Strip =	218.8	ft-lbs	
Allowable Bending Moment =	366.7	ft-lbs	Bending OK

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Company:	Eclipse Engineering, PC	Page:
Address:		Specifier:
Phone Fax:		E-Mail:
Design:	3/8" HUS-EZ	Date:
Fastening point:		

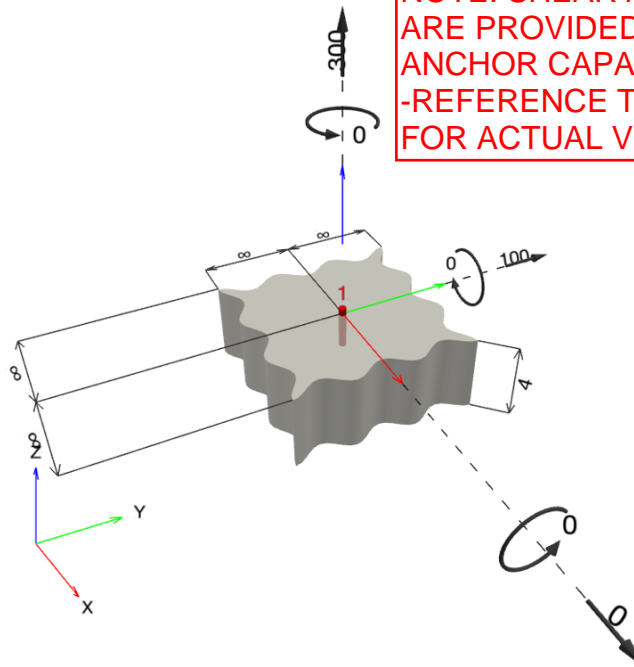
Specifier's comments:

1 Input data



Anchor type and diameter:	KWIK HUS-EZ (KH-EZ) 3/8 (2 1/2)
Item number:	418057 KH-EZ 3/8"x3"
Effective embedment depth:	$h_{ef,act} = 1.860$ in., $h_{nom} = 2.500$ in.
Material:	Carbon Steel
Evaluation Service Report:	ESR-3027
Proof:	Design Method ACI 318
Stand-off installation:	
Profile:	
Base material:	cracked concrete, 2500, $f'_c = 2,500$ psi; $h = 4.000$ in.
Installation:	hammer drilled hole, Installation condition: Dry
Reinforcement:	tension: not present, shear: not present; no supplemental splitting reinforcement present
	edge reinforcement: none or < No. 4 bar
Seismic loads (cat. C, D, E, or F)	Tension load: yes (17.10.5.3 (d))
	Shear load: yes (17.10.6.3 (c))

Geometry [in.] & Loading [lb, in.lb]



NOTE: SHEAR AND TENSION FORCES ARE PROVIDED TO CALCULATE ANCHOR CAPACITY -REFERENCE THE CALCULATIONS FOR ACTUAL V & T AND UNITY CHECK



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Company: Eclipse Engineering, PC
 Address:
 Phone | Fax: |
 Design: 3/8" HUS-EZ
 Fastening point:

Page:
 Specifier:
 E-Mail:
 Date:

2 Proof I Utilization (Governing Cases)

Loading	Proof	Design values [lb]		Utilization	Status
		Load	Capacity	β_N / β_V [%]	
Tension	Concrete Breakout Failure	300	1,051	29 / -	OK
Shear	Pryout Strength	100	1,509	- / 7	OK

Loading	β_N	β_V	ζ	Utilization $\beta_{N,V}$ [%]	Status
Combined tension and shear loads	0.285	0.066	5/3	14	OK

Convert to ASD =
 Multiply by 0.7

3 Warnings

- Please consider all details and hints/warnings given in the detailed report!

Fastening meets the design criteria!

⚠ This is a beta release of the new ATC Hazards by Location website. Please [contact us](#) with feedback.

ℹ The ATC Hazards by Location website will not be updated to support ASCE 7-22. [Find out why.](#)

ATC Hazards by Location

Search Information

Address: 3500 S Meridian, Puyallup, WA 98373, USA
Coordinates: 47.1580315, -122.2973003
Elevation: 431 ft
Timestamp: 2023-12-11T12:20:46.900Z
Hazard Type: Seismic
Reference Document: ASCE7-16
Risk Category: II
Site Class: D-default



Basic Parameters

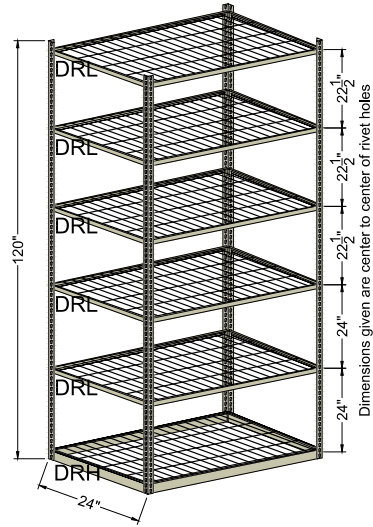
Name	Value	Description
S_S	1.264	MCE_R ground motion (period=0.2s)
S_1	0.436	MCE_R ground motion (period=1.0s)
S_{MS}	1.517	Site-modified spectral acceleration value
S_{M1}	* null	Site-modified spectral acceleration value
S_{DS}	1.011	Numeric seismic design value at 0.2s SA
S_{D1}	* null	Numeric seismic design value at 1.0s SA

* See Section 11.4.8

Additional Information

Name	Value	Description
SDC	* null	Seismic design category
F_a	1.2	Site amplification factor at 0.2s
F_v	* null	Site amplification factor at 1.0s
CR_S	0.914	Coefficient of risk (0.2s)
CR_1	0.898	Coefficient of risk (1.0s)

10'H UNITS



12'H UNITS

