Drainage Report

Puyallup High School Portables

711, 721 & 701 West Main Puyallup, WA 98371

Prepared for

Puyallup School District c/o Studio Meng Strazzara 2001 Western Ave, Suite 200 Seattle, WA 98121 206.587.3797

Prepared by

JMJ Team 905 Main Street, Suite 200 Sumner, WA 98390 206.596.2020 Justin Jones, PE

October 3, 2024



PROJECT ENGINEER'S CERTIFICATION

"I hereby state that this Drainage Control Plan for the Puyallup High School Portables has been prepared by me or under my supervision and meets minimum standard of care and expertise which is usual and customary in this community for professional engineers. I understand that the City of Puyallup does not and will not assume liability for the sufficiency, suitability, or performance of drainage facilities prepared by me."

Justin Jones, PE





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PROJECT OVERVIEW AND VICINITY MAP

The Puyallup High School Portables project is located at the intersection of West Main and 7th Street SW in the City of Puyallup. The project site includes parcels 5870000231, 5870000190, 5870000200, and 5870000171, with a total lot area of 1.00 AC. The project has a total site area of 0.38 acres. The site is currently developed as a PF – Public Facilities lot. New development on-site includes the construction of 3 portable classroom buildings, open-graded gravel pad, and the construction of permeable asphalt walkways. The stormwater approach is to fully infiltrate runoff on-site.



Vicinity Map



Proposed Site Area Map

EXISTING CONDITIONS SUMMARY

The Puyallup High School Portables project has a lot area of 1.00 acre. The existing site consists of landscaping, asphalt parking lot, and existing portables east of the parking lot. The site is fairly flat and has a slight slope towards the north and west side of the property.

The existing storm system consists of downspout dispersion and gravity pipe conveyance system. Runoff from roof disperses onto parking lot and is captured via Contech Catch Basin Inlet Filter that connects to the City of Puyallup stormwater system along West Main. Runoff is then conveyed to the Puyallup River via gravity pipe conveyance system.

The site is located within Lahar Hazard area.

There are no critical areas within site.

PROPOSED CONDITIONS SUMMARY

The proposed development is located in the landscaped area west of the existing parking lot. New development includes the construction of 3 portable classroom buildings, perforated aluminum landing, and site improvements.

The proposed development will result in an addition of 8,678 SF of new impervious surfaces within the project site area. Total land disturbing activity on-site to be approximately 16,850 SF. Minimum requirements 1-9 will apply to this project. Lot Coverage Table has been provided in the report following.

Site improvements include the construction of permeable open-graded gravel pad, permeable asphalt walkways, landscaping, and stormwater conveyance and infiltration trenches. The portables will also have utility service connections for power and communications.

Stormwater runoff from the new portables will be collected via roof downspouts and conveyed to infiltration trenches to be fully infiltrated. Runoff from aluminum landing will drain through the perforated surface and be collected on the permeable gravel pad where stormwater will fully infiltrate into native soils. Runoff from permeable asphalt walkways will infiltrate through the porous surface and fully infiltrate into native soils.

Infiltration suitability was evaluated during the wet season (December 1st - April 1st) to determine infiltration rate and groundwater separation. Small PIT tests and groundwater monitoring were performed in accordance with the 2019 Stormwater Management Manual for Western Washington (DOE Manual) to determine infiltration feasibility. The infiltration rate was determined to be 0.64 in/hr (corrected). Infiltration Report has been provided in Appendix D. Fine sandy loam soil was observed during PIT test. This is consistent with measured infiltration rate and USDA soil survey.

LOT COVERAGE

The following tables show the existing and proposed lot coverage for the Puyallup High School Portables project site.

Existing Lot Coverage – 43,574 SF (1.00 AC) Lot Area							
Coverage Area (SF) Area (Acres) % of Site							
Impervious							
Roof	1,722	0.04					
Concrete Sidewalk	964	0.03					
Asphalt Parking Lot	6,686	0.15					
Total Site Impervious	9,372	0.22	22.0%				
Pervious							
Landscape	34,202	0.78					
Total Site Pervious	34,202	0.78	78.0%				

Proposed Lot Coverage – 43,574 SF (1.00 AC) Lot Area						
Coverage Area (SF) Area (Acres) % of Site						
Impervious						
Ex. Roof	1,722	0.04				
Ex. Concrete Sidewalk	964	0.03				
Ex. Asphalt Parking Lot	6,686	0.15				
New Roof	5,785	0.12				
New Permeable Asphalt Sidewalk	663	0.02				
New Permeable Gravel Pad	1,570	0.04				
New Perforated Aluminum Landing	660	0.02				
Total New Impervious	8,678	0.20	20.0%			
Total Site Impervious	18,050	0.42	42.0%			
Pervious						
Landscape	25,524	0.58				
Total Site Pervious	25,524	0.58	58.0%			

SUMMARY OF MINIMUM REQUIREMENTS

The City of Puyallup adopts the 2019 Stormwater Management Manual for Western Washington (DOE Manual). Volume 1 of the DOE Manual describes the minimum requirements for a development project. Using the flowchart below, Minimum Requirements #1-9 applies to the project site.





MINIMUM REQUIREMENT 1: PREPARATION OF STORMWATER SITE PLANS

Stormwater Site Plan drawings have been prepared per the City of Puyallup development codes and the 2019 Stormwater Management Manual for Western Washington (DOE Manual), see Appendix A.

MINIMUM REQUIREMENT 2: CONSTRUCTION STORMWATER POLLUTION PREVENTION

A Temporary Erosion and Sediment Control Plan has been prepared per the City of Puyallup development codes and the 2019 DOE Manual and is included in this report, see Appendix A. Construction Stormwater Pollution Prevention measures may include storm drain inlet protection; construction entrance; silt fence and a sediment trap.

MINIMUM REQUIREMENT 3: SOURCE CONTROL OF POLLUTION

Source control BMPs will be implemented to minimize stormwater contamination and help comply with the DOE Manual. BMP's for the project may include:

- Inspect and clean treatment BMPs, conveyance systems, and catch basins as needed, and determine necessary O & M Improvements.
- Clean catch basins when the depth of deposits reaches 60-percent of the sump depth as measured from the bottom of basin to the invert of the lowest pipe into or out of the basin.
- Clean woody debris in a catch basin as frequently as needed to ensure proper operation of the catch basin.

MINIMUM REQUIREMENT 4: PRESERVATION OF NATURAL DRAINAGE SYSTEMS AND OUTFALLS

Natural drainage for the developed site area surface flows towards the north and west side of the site and infiltrates into native soil. The project proposes to maintain natural drainage patterns and discharge at natural location.

MINIMUM REQUIREMENT 5: ONSITE STORMWATER MANAGEMENT

Per Figure I-3.3 of the 2019 DOE Manual, the Puyallup High School Portables project is required to either meet LID Performance Standards or utilize List #3 to determine appropriate stormwater management BMPs for various surfaces. This project proposes to meet LID Performance Standards.



Figure I-3.3: Flow Chart for Determining MR #5 Requirements

To meet LID Performance Standards, stormwater discharges must match developed discharge durations to predeveloped discharge rates from 8% of the 2-year peak flow to the full 50-year flow.

The following BMPs were considered for the site:

- Roofs:
 - Downspout Full Infiltration:

Downspout Full Infiltration was evaluated and was deemed feasible for the site. Runoff from proposed roof areas will be routed to downspout infiltration trenches and infiltrate 100% of roof runoff into native soils. The infiltration trenches have been sized utilizing 2019 DOE Manual sizing criteria as follow:

- Soil Type: Fine sand, loamy sand
- Min. Length Required per Portables: 145 LF
 - 75 LF per 1,000 SF of Roof Area
 - 1,929 SF / 1,000 SF = 1.93 x 75 LF = 144.7 LF -> 145 LF
- Trench Width x Depth: 2-feet x 1.5-feet
- Minimum 1-foot of separation between the bottom of the infiltration gallery and the seasonal high groundwater level.

145 LF of trench was determined to be the minimum length needed to fully infiltrate runoff from a single portable. 300 LF of infiltration trench was proposed to manage runoff from two (2) portables. 147 LF of infiltration trench was proposed to manage runoff from a single portable.

- Other Hard Surfaces:
 - <u>Permeable Pavements:</u>

Permeable Pavements were evaluated for the management of runoff from the gravel pad and asphalt walkway. This BMP was deemed feasible for the project. Runoff will permeate through the open-graded gravel pad and asphalt walkway and fully infiltrate into native soils. The permeable pavements have been sized utilizing the WWHM model based on the following criteria:

- Infiltration rate: 0.64 in/hr
- Layers for each surface type:
 - Gravel Pad: 10" Open-Graded Gravel (0.33 porosity)
 - Asphalt Walkways: 4" Porous Asphalt (0.33 porosity)
 6" Permeable Ballast (0.33 porosity)

 Minimum 1-foot of separation between the bottom of the permeable pavement and the seasonal high groundwater level.

The modeling determined that the proposed layers were sufficient to infiltrate 100% of runoff. See Appendix C for WWHM modeling.

- Lawn and Landscaped Areas:
 - This project is required to retain and protect undisturbed soil in areas not being developed and, prior to completion of the project, amend all new, replaced, and disturbed topsoil (including construction lay-down areas) with organic matter in accordance with BMP T5.13 of the 2019 DOE Manual.

This project proposes to infiltrate 100% of influent runoff on-site, resulting in no net gain of stormwater discharge from the developed site; therefore, this project meets or exceeds the LID Performance Threshold.

MINIMUM REQUIREMENT 6: RUNOFF TREATMENT

Per the 2019 DOE Manual, Runoff Treatment is required if the site Threshold Discharge Area (TDA) has a total of 5,000 SF of pollution generating hard surfaces (PGHS) or 3/4 acres of pollution generating pervious surfaces (PGPS). The Puyallup High School Portables project does not meet these thresholds as the site does not propose any PGHS or PGPS; therefore, runoff treatment is not required on-site.

MINIMUM REQUIREMENT 7: FLOW CONTROL

Per 2019 DOE Manual, Flow Control BMPs are required if the site TDA meets any of the following thresholds:

- TDAs that have a total of 10,000 SF or more of effective impervious surfaces, or
- TDAs that convert 3/4 acres or more of native vegetation, pasture, scrub/shrub, or unmaintained nonnative vegetation to lawn or landscape, or convert 2.5 acres or more of native vegetation to pasture, and from which there is a surface discharge in a natural or man-made conveyance system from the TDA, or
- TDAs that through a combination of effective hard surfaces and converted vegetation areas cause a 0.15 cubic feet per second (cfs) or greater increase in the 100-year flow frequency as estimated using an approved continuous simulation model and 15-minute time step.

Effective impervious surfaces can be defined as those impervious surfaces that are connected via sheet flow or discrete conveyance to a drainage system. Impervious surfaces are considered ineffective if approved runoff modeling methods indicate that the entire runoff file is infiltrated.

The Puyallup High School Portables project is proposing to infiltrate 100% of runoff file using an infiltration gallery and permeable pavements; therefore, all proposed impervious areas are deemed ineffective. Since the project is not proposing any effective impervious, TDA Thresholds stated above are not triggered and Flow Control BMPs are not required.

MINIMUM REQUIREMENT 8: WETLAND PROTECTION

This minimum requirement applies only to TDAs whose stormwater discharges to wetlands. This project does not propose to discharge stormwater to wetlands; therefore, this minimum requirement does not apply to the project.

MINIMUM REQUIREMENT 9: OPERATION AND MAINTENANCE

An operation and maintenance manual shall be provided for Stormwater Management BMPs in accordance with the 2019 DOE Manual. This manual will be developed prior to building occupancy.

APPENDIX A



Total Lot Area	43,574 SF	(1.00 AC)	
Coverage	Area (SF)	Area (AC)	% of Site
Impervious			
Roof	1,722	0.04	
Concrete Sidewalk	964	0.03	
Asphalt Parking Lot	6,686	0.15	
Total Site Impervious	9,372	0.22	22.0%
Pervious			
Landscape	34,202	0.78	
Total Site Pervious	34,202	0.78	78.0%



۲	Column
®	Bollard
Ø	Gate Post
T	Communications Vault
(\mathbb{T})	Communications Manhole
Т	Telephone Cabinet
л	Sign
	Mailbox
\sim	Flag Pole
\bigcirc	Deciduous Tree
X	Evergreen Tree
TPN	Tax Parcel Number
FF	Finish Floor Elevation
	Road Centerline
SD SD	Storm Drain Line
SS SS	Sanitary Sewer Line
W	Buried Water Line
G	Buried Gas Line
——BPBP	Buried Power Line
TEL TEL	Buried Telecommunications Line
	Overhead Power Line
_00	Chain Link Fence
	Wood Fence
——————————————————————————————————————	Record Storm Line
——————————————————————————————————————	Record Sanitary Line
	Asphalt Surface
	Concrete Surface

HORIZONTAL DATUM

Washington Plane Coordinate System, South Zone, NAD 83/2011

Based on GPA observation utilizing the Washington State Reference Network (WSRN) Measured south 88°57'44" east between two found monuments along west main st. at the intersections with 8th st nw and 7th st nw

Gravel Surface

VERTICAL DATUM

NAVD88

Based on GPS observation utilizing the WSRN with NGS GEOID18 Loaded

Temporary Benchmark Elevation = 41.76 Description: Rebar & Control Cap #12 Located at the intersection of West Main & 7th ST NW SE of the radial curb line

SITE DATA

Total Lot Area:

• Total Project Site Area:

0 20 40 FEET 1" = 20'

16,587 SF (0.38 AC)

PF- Public Facilities

43,574 SF (1.00 AC)

- 5870000171, 5870000190, 5870000200, 5870000231 Tax Parcel Numbers:
- Zoning:

- APPROVED
- DEVELOPMENT ENGINEERING
- DATE NOTE: THIS APPROVAL IS VOID AFTER 180 DAYS FROM APPROVAL DATE. THE CITY WILL NOT BE RESPONSIBLE FOR ERRORS AND/OR OMISSIONS ON THESE PLANS. FIELD CONDITIONS MAY DICTATE CHANGES TO THESE PLANS AS



DETERMINED BY THE DEVELOPMENT ENGINEERING

ARCHITECT studicmeng STRAZZARA 2001 WESTERN AVE, STE# 200, SEATTLE, WA 98121 www.studioms.com | P: 206.587.3797 CONSULTANT JMJ Team 905 Main Street, Suite #200 Sumner, WA 98390 (206) 596-2020 CLIENT/OWNER D PUYALLUP SCHOOL DISTRICT A Tradition of Excellence TITLE PUYALLUP HS NEW PORTABLES 2023 STAMP ALLA. UIVAL . 10-03-24 ISSUED: DATE CONDITIONAL USE PERMIT OCT, 11 2023 CUP CC#1 RESPONSE APR, 5 2024 BUILDING PERMIT SET MAY 3, 2024 JULY 10, 2024 ROW PERMIT SET ROW PERMIT SET REV. 1 AUG 20, 2024 ROW PERMIT SET REV. 2 OCT 02, 2024 PERMIT CC#1 RESPONSE OCT 03, 2024 EXISTING SITE PLAN Building Permit #: CUP #: PLCUP20230109 Owner's Project #: 2023106 Architect's Project #: MO Drawn By Checked By JJ C.01





LEGEND

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Existing Gravel Pavement
Existing Concrete Pavement
Property Line
Parcel Line
Silt Fence
Existing Fence to be Removed
Existing Overhed Power Line
Existing Sewer Line
Existing Storm Line
Existing Water Line
Existing Gas Line
Existing Building Line
Existing Chainlink Fence Line
Tree Protection Fence Line
Existing Tree
Existing Type II Storm Manhole
Existing Type I Storm Catch Bas
Existing Sewer Manhole
Existing Light Pole

Construction Entrance

Vegetation To Be Removed

Concrete To Be Removed

Asphalt To Be Removed

Existing Asphalt Pavement

TESC NOTES

1. Contractor to install TESC measures as necessary to ensure stormwater leaving the site is free of settleable solids.

Existing Power Pole

- 2. Install and maintain construction entrance per City of Puyallup Standard Detail 05.01.01 and install wheel wash as needed per Washington DOE BMP C106.
- 3. Install silt fence per City of Puyallup Standard Detail 02.03.02. Silt Fence to mark clearing limits in the field.
- 4. Maintain and Install storm drain inlet protection in all existing catch basins within the project vicinity per WSDOT Standard Plan I-40.20-00 and storm drain barriers per City of Puyallup Standard Details 02.03.05 and 02.03.06. Catch Basins within drivable areas are only to use the storm drain inlet protection, and not City Standard 02.03.05 and 02.03.06.
- 5. Roads shall be cleared thoroughly as needed to protect stormwater infrastructure and downstream water resources. Sediment shall be removed from roads by shoveling or pickup sweeping and be transported to a controlled sediment disposal area.
- 6. Exposed soils shall be watered as necessary to prevent dust from leaving the site.
- 7. Concrete handling and equipment washing in accordance with DOE BMP C151.
- 8. Disturbed soils to be amended per DOE BMP T5.13
- 9. If necessary, alternative sediment control methods shall be submitted by the contractor for review and approval prior to construction.
- 10. A CESCL shall be present on-site or on-call for the duration of construction operations.
- 11. Install tree protection fence per City of Puyallup Detail on Sheet C-03.

DEMOLITION NOTES

- Vegetation to be Removed: 16,750 SF
- Concrete to be Removed: 75 SF
- Disturbed Area On-site: 16,850 SF

APPROVED
BY CITY OF PUYALLUP DEVELOPMENT ENGINEERING
DATE
NOTE: THIS APPROVAL IS VOID AFTER 180 DAYS FROM APPROVAL DATE. THE CITY WILL NOT BE RESPONSIBLE FOR ERRORS AND/OR OMISSIONS ON THESE PLANS. FIELD CONDITIONS MAY DICTATE CHANGES TO THESE PLANS AS DETERMINED BY THE DEVELOPMENT ENGINEERING MANAGER.
CALL TWO BUSINESS DAYS BEFORE YOU DIG 1-800-424-5555
UTILITIES UNDERGROUND LOCATION CENTER











OF ALLUP	GRADING, E SEDIMENTATION		EROSION, AND N CONTROL NO)TES	
ENGINEERING and	DRAWN BY JIM ERWIN-SVOBODA	CHECKED BY LINDA LIAN	APPROVED BY COLLEEN HARRIS	REVISED B XXXX	Ŷ	CITY STANDARD
DEPARTMENTS	FILE NAME F:\DWG\COMMON\STDS\CITY\2009\05_GRD\05.01\05.02.01		DATE APPROVED 07/01/2009	DATE REVISED XX/XX/XX	SCALE 1:1	05.02.01

APPROVED









VIEW 1



VIEW 2

LEGEND

Existing Asphalt

Existing Concrete

Proposed Permeable Asphalt

Proposed Open-Graded Gravel

Proposed Landscape Area

Proposed Infiltration Trench

Restored Asphalt Walkway

Proposed Yard Drain

Proposed Cleanout

Existing Catch Basin

Proposed Storm Drain Line

Existing Storm Drain Line

Proposed Grass

Proposed Perforated Aluminum Landing

Proposed Catch Basin Type 1, Open Grate



SITE DATA

- Total Lot Area:
- 16,587 SF (0.38 AC) • Total Project Site Area:
- 5870000171, 5870000191, 5870000200 Tax Parcel Numbers:
- Zoning:

PROPOSED LOT COVERAGE

PF- Public Facilities

43,574 SF (1.00 AC)

Total Lot Area	43,574 SF (1.00 AC)		
Coverage	Area (SF)	Area (AC)	% of Site
Impervious			
Ex. Roof	1,722	0.04	
Ex. Concrete Sidewalk	964	0.03	
Ex. Asphalt Parking Lot	6 <i>,</i> 686	0.15	
New Roof	5,785	0.12	
New Permeable Asphalt Sidewalk	663	0.02	
New Open-Graded Gravel Pad	1,570	0.04	
New Perforated Aluminum Landing	660	0.02	
Total New Impervious	8,678	0.20	20.0%
Total Site Impervious	18,050	0.42	42.0%
Pervious			
Landscape	25,524	0.58	
Total Site Pervious	25,524	0.58	58.0%

CONSTRUCTION NOTES

- 1. Install Open-Graded gravel pad per Section A on Sheet C.06.
- 2. Install Permeable Asphalt Sidewalk per Section B on Sheet C.06.
- 3. Install Infiltration Trench per Downspout Infiltration Trench Detail on Sheet C.06.
- 4. Disturbed soils to be amended per City of Puyallup Std. Dtl. 01.02.08a on Sheet C.07.
- 5. Install Sidewalk per City of Puyallup Std. Dtl. 01.02.01 on Sheet C.07.
- 6. Install Downspout Overflow per Downspout Infiltration Trench Detail on Sheet C.06.
- 7. Proposed ADA ramps on W Main to be barricaded and signed to prevent pedestrians from crossing W Main. Once roadway is closed to vehicle traffic with the proposed one year pilot these restrictions can be removed. A crosswalk at this location (with vehicle traffic present) does not meet engineering standards.
- 8. Install Cleanouts per City of Puyallup Std. Dtl. 02.01.09 on Sheet C.07.

LANDSCAPE NOTE

. All planting areas shall be mulched with a uniform four (4") inch layer of organic compost mulch material or wood chips over a properly cleaned, amended and graded subsurface.

	APPROVED
	BY CITY OF PUYALLUP DEVELOPMENT ENGINEERING
	DATE
0 10 20 FEET 1" = 10'	CALL TWO BUSINESS DAYS BEFORE YOU DIG 1-800-424-5555 UTILITIES UNDERGROUND LOCATION CENTER





LEGEND

	Existing Asphalt
	Existing Concrete
	Proposed Permeable Asphalt
	Proposed Open-Graded Gravel
	Proposed Perforated Aluminum Landing
	Proposed Infiltration Trench
	Proposed Catch Basin Type 1, Open Grate
	Proposed Yard Drain
69	Proposed Cleanout
	Existing Catch Basin
FF	Finished Floor Elevation
SE	Spot Elevation
ME	Match Existing Elevation
FW	Face of Walk Elevation
BW	Back of Walk Elevation
ТС	Top of Curb Elevation
BC	Bottom of Curb Elevation
GB	Grade Break

GENERAL NOTES

1 Landing shall not exceed 2.0% running or cross slope.

- 2 All sidewalk ramps shall not exceed 8.33% running slope or 2.0% cross slope.
- 3. Install 6" Cement Concrete Traffic Curb per WSDOT Std. Plan F-10.12-04. See Sheet C.07 for Detail.
- 4. Install Concrete Sidewalk per City of Puyallup Std. Detail 01.02.01. See Sheet C.07 for Detail.





DETERMINED BY THE DEVELOPMENT ENGINEERING

MANAGER.





OPEN-GRADED GRAVEL

SECTION

1'' = 1'



PERMEABLE ASPHALT SECTION 1'' = 1'

CITY OF PUYALLUP STORMWATER NOTES

1. All work in City right-of-way requires a permit from the City of Puyallup. Prior to any work commencing, the general contractor shall arrange for a preconstruction meeting at the Development Services Center to be attended by all contractors that will perform work shown on the engineering plans, representatives from all applicable Utility Companies, the project owner and appropriate City staff. Contact Engineering Services to schedule the meeting (253) 841-5568. The contractor is responsible to have their own approved set of plans at the meeting.

- 2. After completion of all items shown on these plans and before acceptance of the project, the contractor shall obtain a "punch list" prepared by the City's inspector detailing remaining items of work to be completed. All items of work shown on these plans shall be completed to the satisfaction of the City prior to acceptance of the water system and provision of sanitary sewer service.
- 3. All materials and workmanship shall conform to the Standard Specifications for Road, Bridge, and Municipal Construction (hereinafter referred to as the "Standard Specifications"), Washington State Department of Transportation and American Public Works Association, Washington State Chapter, latest edition, unless superseded or amended by the City of Puyallup City Standards for Public Works Engineering and Construction (hereinafter referred to as the "City Standards"). 4. A copy of these approved plans and applicable city developer specifications and details shall be on site during construction.
- 5. Any revisions made to these plans must be reviewed and approved by the developer's engineer and the Engineering Services Staff prior to any implementation in the field. The City shall not be responsible for any errors and/or omissions on these plans.
- 6. The contractor shall have all utilities verified on the ground prior to any construction. Call (811) at least two working days in advance. The owner and his/her engineer shall be contacted immediately if a conflict exists.
- 7. Any structure and/or obstruction which require removal or relocation relating to this project, shall be done so at the developer's expense.
- 8. During construction, all existing and newly installed drainage structures shall be protected from sediments.
- 9. All storm manholes shall conform to City Standard Detail No. 02.01.01. Flow control manhole/oil water separator shall conform to City Standard Detail No. 02.01.06 and 02.01.07. 10. Manhole ring and cover shall conform to City Standard Detail 06.01.02.
- 11. Catch basins Type I shall conform to City Standard Detail No.02.01.02 and 02.01.03 and shall be used only for depths less than 5 feet from top of the grate to the invert of the storm pipe.
- 12. Catch basins Type II shall conform to City Standard Detail No.02.01.04 and shall be used for depths greater than 5 feet from top of the grate to invert of the storm pipe.

13. Cast iron or ductile iron frame and grate shall conform to City Standard Detail No.02.01.05. Grate shall be marked with "drains to stream". Solid catch basin lids (square unless noted as round) shall conform to WSDOT Standard Plan B-30.20-04 (Olympic Foundry No. SM60 or equal). Vaned grates shall conform to WSDOT Standard Plan B-30.30-03 (Olympic Foundry o. SM60V or equal).

- 14. Stormwater pipe shall be only PVC, concrete, ductile iron, or dual walled Polypropylene pipe.
- a. The use of any other type shall be reviewed and approved by the Engineering Services Staff prior to installation.
- b. PVC pipe shall be per ASTM D3034, SDR 35 for pipe size 15-inch and smaller and F679 for pipe sizes 18 to 27 inch. Minimum cover on PVC pipe shall be 3.0 feet.
- c. Concrete pipe shall conform to the WSDOT Standard Specifications for concrete underdrain pipe. Minimum cover on concrete pipe shall not less than 3.0 feet.
- d. Ductile iron pipe shall be Class 50, conforming to AWWA C151. Minimum cover on ductile iron pipe shall be 1.0 foot.
- e. Polypropylene Pipe (PP) shall be dual walled, have a smooth interior and exterior corrugations and meet WSDOT 9-05.24(1). 12-inch through 30-inch pipe shall meet or exceed ASTM F2736 and AASHTO M330, Type S, or Type D. 36-inch through 60-inch pipe shall meet or exceed ASTM F2881 and AASHTO M330, Type S, or Type D. Testing shall be per ASTM F1417. Minimum cover over Polypropylene pipe shall be 3-feet.
- 15. Trenching, bedding, and backfill for pipe shall conform to City Standard Detail No. 06.01.01.
- 16. Storm pipe shall be a minimum of 10 feet away from building foundations and/or roof lines.
- 17. All storm pipe shall be tested and inspected for acceptance as outlined in Section 209 of the City of Puyallup Stormwater Management Standards.
- 18. All temporary sedimentation and erosion control measures, and protective measures for critical areas and significant trees shall be installed prior to initiating any construction activities.
- 19. Registration is required for all Class V UIC wells within public drainage tracts or public rightof-way and must be submitted sixty (60) days prior to well construction. A copy of the online registration shall be submitted to the City prior to construction.



Subgrade Shall be Compacted

to 90-92% of Max. Dry Density

& Shall be Firm & Unyielding

















STDS\STR\01.02.08



UTILITIES UNDERGROUND LOCATION CENTER



APPENDIX B





PHS Portables Vicinity Map Figure 1



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NOT TO SCALE

PHS Portables Drainage Basin Map

Figure 2



NOT TO SCALE

Downstream Drainage Map Figure 3



 (\bigcirc)

NOT TO SCALE



PROPOSED BASINS

<u>Subbasin 1:</u>		
Impervious:		
Roof:	5,785 SF	
Total:	5,785 SF	(0.13 AC)
Subbasin 2:		
Impervious:		
Perm. Gravel:	1,570 SF	
Landing:	660 SF	
Total:	2,230 SF	(0.05 AC)
Subbasin 3:		
Impervious:		
Perm. Asphalt:	663 SF	
Total:	663 SF	(0.02 AC)

PHS Portables

Proposed Basin Map Figure 4

APPENDIX C

<section-header>

General Model Information

WWHM2012 Project Name: Combined Basins

Site Name: Site Address:

City:	
Report Date:	10/4/2024
Gage:	40 IN EAST
Data Start:	10/01/1901
Data End:	09/30/2059
Timestep:	15 Minute
Precip Scale:	1.000
Version Date:	2023/01/27
Version:	4.2.19

POC Thresholds

Low Flow Threshold for POC1:	50 Percent of the 2 Year
High Flow Threshold for POC1:	50 Year

Landuse Basin Data Predeveloped Land Use

Basin 1

Bypass:	No
GroundWater:	No
Pervious Land Use C, Forest, Flat	acre 0.2
Pervious Total	0.2
Impervious Land Use	acre
Impervious Total	0
Basin Total	0.2

Mitigated Land Use

Portable Roofs

Bypass:	No
GroundWater:	No
Pervious Land Use	acre
Pervious Total	0
Impervious Land Use ROOF TOPS FLAT	acre 0.13
Impervious Total	0.13
Basin Total	0.13

Routing Elements Predeveloped Routing
Mitigated Routing

Gravel Trench Bed 1

Bottom Length: Bottom Width: Trench bottom slope Trench Left side slope Trench right side slope Material thickness of f Pour Space of materia Material thickness of s Pour Space of materia Material thickness of t Pour Space of materia Infiltration On	1: e 0: e 2: irst layer: al for first layer: second layer: al for second layer: hird layer: al for third layer:	29.90 ft. 29.90 ft. 0 To 1 0 To 1 0 To 1 1.5 0.33 0 0 0 0
Infiltration rate: Infiltration safety facto Total Volume Infiltrate Total Volume Through Total Volume Through Percent Infiltrated: Total Precip Applied to Total Evap From Facil Discharge Structure Riser Height: Riser Diameter: Element Flows To: Outlet 1	r: d (ac-ft.): n Riser (ac-ft.): n Facility (ac-ft.): o Facility: ity: 1.4 ft. 12 in. Outlet 2	1.43 0.45 55.331 0.077 55.408 99.86 0 0

Gravel Trench Bed Hydraulic Table

Stage(feet)	Area(ac.)	Volume(ac-ft.)	Discharge(cfs)	Infilt(cfs)
0.0000	0.020	0.000	0.000	0.000
0.0167	0.020	0.000	0.000	0.013
0.0333	0.020	0.000	0.000	0.013
0.0500	0.020	0.000	0.000	0.013
0.0667	0.020	0.000	0.000	0.013
0.0833	0.020	0.000	0.000	0.013
0.1000	0.020	0.000	0.000	0.013
0.1167	0.020	0.000	0.000	0.013
0.1333	0.020	0.000	0.000	0.013
0.1500	0.020	0.001	0.000	0.013
0.1667	0.020	0.001	0.000	0.013
0.1833	0.020	0.001	0.000	0.013
0.2000	0.020	0.001	0.000	0.013
0.2167	0.020	0.001	0.000	0.013
0.2333	0.020	0.001	0.000	0.013
0.2500	0.020	0.001	0.000	0.013
0.2667	0.020	0.001	0.000	0.013
0.2833	0.020	0.001	0.000	0.013
0.3000	0.020	0.002	0.000	0.013
0.3167	0.020	0.002	0.000	0.013
0.3333	0.020	0.002	0.000	0.013
0.3500	0.020	0.002	0.000	0.013
0.3667	0.020	0.002	0.000	0.013
0.3833	0.020	0.002	0.000	0.013

0.4000 0.4167 0.4333 0.4500 0.4667 0.4833 0.5000 0.5167 0.5333 0.5500 0.5667 0.5833 0.6000 0.6167 0.6333 0.6500 0.6667 0.6833 0.7000 0.7167 0.7232	0.020 0.020	0.002 0.002 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.005	0.000 0	$\begin{array}{c} 0.013\\ 0.0013\\ 0.0013\\ 0.0013\\ 0.0013\\ 0.0013\\ 0.0013\\ 0.0013\\ 0.0013\\ 0$
0.7333 0.7500 0.7667 0.7833 0.8000 0.8167 0.8333 0.8500 0.8667 0.8833 0.9000 0.9167 0.9333 0.9500 0.9667 0.9833 1.0000 1.0167 1.0333 1.0500 1.0667 1.0833 1.1000	0.020 0.	0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.006 0.006 0.006 0.006 0.006 0.006 0.006 0.006 0.006 0.006 0.006 0.006 0.006 0.006 0.006 0.007 0.007 0.007 0.007 0.007 0.007	0.000 0	0.013 0
1.1167 1.1333 1.1500 1.1667 1.1833 1.2000 1.2167 1.2333 1.2500 1.2667 1.2833 1.3000 1.3167 1.3333 1.3500	0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020 0.020	0.007 0.007 0.007 0.008 0.009 0.009	0.000 0.0000 0.000 0.000 0.000 0.000	$\begin{array}{c} 0.013\\ 0.013\\ 0.013\\ 0.013\\ 0.013\\ 0.013\\ 0.013\\ 0.013\\ 0.013\\ 0.013\\ 0.013\\ 0.013\\ 0.013\\ 0.013\\ 0.013\\ 0.013\\ 0.013\\ 0.013\\ 0.013\\ 0.013\end{array}$

1.3667	0.020	0.009	0.000	0.013
1.3833	0.020	0.009	0.000	0.013
1.4000	0.020	0.009	0.000	0.013
1.4167	0.020	0.009	0.022	0.013
1.4333	0.020	0.009	0.064	0.013
1.4500	0.020	0.009	0.118	0.013
1.4667	0.020	0.009	0.182	0.013
1.4833	0.020	0.010	0.254	0.013
1.5000	0.020	0.010	0.333	0.013

Open-Graded Gravel

Infiltration On Infiltration rate:

Percent Infiltrated:

Pour Space of material for third layer:

Total Volume Through Riser (ac-ft.):

Total Volume Through Facility (ac-ft.):

Infiltration safety factor: Total Volume Infiltrated (ac-ft.):

Total Precip Applied to Facility:

Total Evap From Facility:

Pavement Area:0.0511 acre.Pavement Length:47.20 ft.Pavement Width:47.20 ft.Pavement width:Pavement slope 1:0 To 1Pavement thickness:0.83Pour Space of Pavement:0.33Material thickness of second layer:0Pour Space of material for second layer:0Material thickness of third layer:0

0

0

0

1.43

0.45 20.256

20.256

100

1.359

Permeable Asphalt Pavement Area:0.0152 acre.Pavement Length:132.60 ft. Pavement Width: 5.00 ft. Pavement slope 1:0 To 1

Pavement thickness:	0.33
Pour Space of Pavement:	0.33
Material thickness of second layer:	0.5
Pour Space of material for second layer:	0.33
Material thickness of third layer:	0
Pour Space of material for third layer:	0
Infiltration On	
Infiltration rate:	1.43
Infiltration safety factor:	0.45
Total Volume Infiltrated (ac-ft.):	5.827
Total Volume Through Riser (ac-ft.):	0
Total Volume Through Facility (ac-ft.):	5.827
Percent Infiltrated:	100
Total Precip Applied to Facility:	0
Total Evap From Facility:	0.404
-	

Analysis Results



Annual Year	Peaks for Predeveloped Predeveloped	and Mitigated.	POC #1
1902	0.000	0.000	
1903	0.000	0.000	
100/	0.000	0.000	
1904	0.003	0.000	
1905	0.000	0.000	
1906	0.000	0.000	
1907	0.001	0.000	
1908	0.000	0.000	
1909	0.000	0.000	
1910	0.001	0.000	
1911	0.000	0.000	
1912	0.011	0.006	
1913	0.000	0.000	
1914	0.000	0.000	
1915	0.000	0.000	
1916	0.001	0.000	
1917	0.000	0.000	
1918	0.000	0.000	
1919	0.000	0.000	
1920	0.001	0.000	
1921	0.000	0.000	
1922	0.002	0.000	
1923	0.000	0.000	
1924	0,000	0.000	
1925	0,000	0.000	
1926	0,000	0.000	
1927	0,000	0.000	
1928	0.000	0.000	
1929	0.001	0.000	
1930	0.000	0.000	
1931	0,000	0.000	
1932	0.000	0.000	
1033	0.000	0.000	
1934	0.002	0.000	
1035	0.002	0.000	
1936	0.000	0.000	
1937	0.000	0.000	
1938	0.000	0.000	
1030	0.000	0.000	
1940	0.000	0.000	
1941	0,000	0.000	
1942	0.000	0.000	
1943	0.000	0.000	
1940	0.000	0.000	
10/5	0.001	0.002	
10/6	0.000	0.000	
10/7	0.001	0.000	
10/18	0.000	0.000	
10/0	0.000	0.014	
1050	0.000	0.003	
1051		0.000	
1050	0.000	0.000	
1902	0.003	0.041	
1900	0.002	0.030	
1904	0.000	0.000	
1955	0.000	0.000	
1956	0.000	0.000	
1957	0.000	0.000	

1958 1959 1960 1961 1962 1963 1964 1965 1966 1967 1968 1969 1970 1971 1972 1973 1974 1975 1976 1977 1978 1979	0.002 0.000 0.002 0.000 0.000 0.000 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.002 0.002 0.002 0.000 0.001 0.001	0.011 0.000 0.000 0.011 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.023 0.023 0.032 0.000
1980 1981 1982 1983 1984 1985 1986 1987 1988 1989 1990 1991 1992 1993 1994 1995 1996 1997 1998 1999 2000	0.001 0.000 0.001 0.001 0.002 0.002 0.000 0.001 0.000 0.000 0.001 0.000 0.000 0.001 0.000 0.000 0.001 0.000 0.000 0.001 0.000 0	0.000 0
2001 2002 2003 2004 2005 2006 2007 2008 2009 2010 2011 2012 2013 2014 2015	0.000 0.003 0.000 0.005 0.0001 0.001	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.025 0.000

2016 2017	0.000 0.000	0.000 0.053
2018 2019	0.002 0.002	$0.000 \\ 0.045$
2020	0.001	0.000
2021 2022	0.001	0.000
2023	0.000	0.000
2024 2025	0.009	0.015
2026	0.000	0.000
2028	0.000	0.000
2029	0.000	0.000
2031	0.000	0.000
2032 2033	0.000 0.000	$0.000 \\ 0.000$
2034	0.000	0.000
2035 2036	0.001	0.026
2037	0.000	0.000
2038	0.000	0.000
2040 2041	0.000	0.000
2042	0.001	0.030
2043 2044	0.001 0.001	$0.000 \\ 0.000$
2045	0.000	0.000
2046 2047	0.000	0.000
2048	0.000	0.000
2049	0.000	0.000
2051 2052	0.001	0.010 0.000
2053	0.000	0.000
2054 2055	0.001	0.033
2056	0.000	0.000
2058	0.000	0.000
2059	0.003	0.000

Ranked Annual Peaks

Ranked Annual Peaks for Predeveloped and Mitigated. POC #1 Rank Predeveloped Mitigated

Rank	Predeveloped	Mitigated
1	0.0106	0.0525
2	0.0089	0.0521
3	0.0055	0.0450
4	0.0035	0.0407
5	0.0029	0.0379
6	0.0028	0.0333
7	0.0026	0.0318
8	0.0024	0.0297
9	0.0022	0.0278
10	0.0022	0.0264

11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35	0.0020 0.0018 0.0017 0.0016 0.0016 0.0015 0.0015 0.0015 0.0014 0.0014 0.0014 0.0010 0.0010 0.0010 0.0010 0.0009 0.0008 0.00	0.0247 0.0234 0.0149 0.0140 0.0110 0.0110 0.0106 0.0005 0.0000
37 38 39	0.0007 0.0007 0.0007	0.0000 0.0000 0.0000
40 41 42 43	0.0007 0.0007 0.0007 0.0007	0.0000 0.0000 0.0000 0.0000
44 45 46 47	0.0007 0.0007 0.0006 0.0006	$\begin{array}{c} 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\end{array}$
48 49 50 51	0.0006 0.0006 0.0006 0.0006	$\begin{array}{c} 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\end{array}$
52 53 54 55	0.0006 0.0006 0.0006 0.0005	0.0000 0.0000 0.0000 0.0000
56 57 58 59	0.0005 0.0004 0.0004	0.0000 0.0000 0.0000
60 61 62	0.0004 0.0004 0.0004 0.0004	0.0000 0.0000 0.0000 0.0000
63 64 65 66	0.0004 0.0004 0.0004 0.0004	$\begin{array}{c} 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\end{array}$
67 68	0.0003 0.0003	$0.0000 \\ 0.0000$

69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 90 91 92 93 94 95 96 97 98 99 100	0.0003 0.0002 0.0002	0.0000 0.00
103 104 105 106 107 108 109 110 111 112 113 114 115 116 117 118 119 120 121 122 123 124 125	0.0002 0.0002	0.0000 0.00
126	0.0002	0.0000

127	0.0002	0.0000
128	0.0002	0.0000
129	0.0002	0.0000
130	0.0002	0.0000
132	0.0002	0.0000
133	0.0002	0.0000
134	0.0002	0.0000
135	0.0002	0.0000
136	0.0002	0.0000
137	0.0002	0.0000
138	0.0002	0.0000
139	0.0002	0.0000
140	0.0002	0.0000
141	0.0002	0.0000
142	0.0002	0.0000
143	0.0002	0.0000
144	0.0002	0.0000
145	0.0002	0.0000
147	0.0002	0.0000
148	0.0002	0.0000
149	0.0002	0.0000
150	0.0002	0.0000
151	0.0002	0.0000
152	0.0002	0.0000
153	0.0002	0.0000
154	0.0002	0.0000
155	0.0002	0.0000
150	0.0002	0.0000
158	0.0002	0.0000
100	0.0002	0.0000

LID Duration Flows The Facility PASSED

Flow(cfs)	Predev	Mit	Percentage	Pass/Fail
0.0000	101494	307	0	Pass
0.0000	99444	307	0	Pass
0.0000	95732	307	0	Pass
0.0000	93793	307	0	Pass
0.0000	90469	307	0	Pass
0.0000	88696	307	0	Pass
0.0000	87034	307	0	Pass
0.0000	83655	307	0	Pass
0.0000	82159	305	0	Pass
0.0000	79168	304	0	Pass
0.0000	77505	304	0	Pass
0.0000	76065	304	0	Pass
0.0000	72796	304	0	Pass
0.0000	71356	304	0	Pass
0.0000	68420	304	0	Pass
0.0000	66869	304	0	Pass
0.0000	65262	304	0	Pass
0.0001	62547	304	0	Pass
0.0001	61329	304	0	Pass
0.0001	59002	304	0	Pass
0.0001	57894	304	0	Pass
0.0001	57007	304	0	Pass
0.0001	55190	304	0	Pass
0.0001	54309	304	0	Pass
0.0001	52675	304	0	Pass
0.0001	51888	304	0	Pass
0.0001	51179	304	0	Pass
0.0001	49678	304	0	Pass
0.0001	48946	304	0	Pass
0.0001	47445	303	0	Pass
0.0001	46669	303	0	Pass
0.0001	45229	303	0	Pass
0.0001	44509	303	0	Pass
0.0001	43850	302	0	Pass
0.0001	42370	302	0	Pass
0.0001	41683	302	0	Pass
0.0001	40105	302	0	Pass
0.0001	39429	301	0	Pass
0.0001	38659	301	0	Pass
0.0001	37334	301	0	Pass
0.0001	36636	301	0	Pass
0.0001	35207	301	0	Pass
0.0001	34454	301	0	Pass
0.0001	33817	301	0	Pass
0.0001	32465	301	0	Pass
0.0001	31789	301	0	Pass
0.0001	30553	301	0	Pass
0.0001	29910	301	1	Pass
0.0001	29224	301	1	Pass
0.0001	28072	301	1	Pass
0.0001	2/495	301	1	Pass
0.0001	26277	301	1	Pass
0.0001	25728	301	1	Pass

0.0001	25191	301	1	Pass
0.0001	24149	301	1	Pass
0.0001	23706	301	1	Pass
0.0001	22753	301	1	Pass
0.0001	22177	301	1	Pass
0.0001	21628	300	1	Pass
0.0001	20687	300	1	Pass
0.0001	20166	300	1	Pass
0.0001	19074	300	1	Pass
0.0001	18598	300	1	Pass
0.0001	18182	300	1	Pass
0.0001	17257	300	1	Pass
0.0001	16820	300	1	Pass
0.0001	16022	300	1	Pass
0.0001	15579	300	1	Pass
0.0001	15141	300	1	Pass
0.0001	14249	300	2	Pass
0.0001	13745	300	2	Pass
0.0001	12931	300	2	Pass
0.0001	12454	300	2	Pass
0.0001	12077	300	2	Pass
0.0001	11202	300	2	Pass
0.0001	10809	300	2	Pass
0.0001	10000	300	3	Pass
0.0001	9000	200	3	Pass Dass
0.0001	0701 8316	299	3	Pass
0.0001	7067	290	3	Pass Dass
0.0001	7185	208	J 4	Dass
0.0001	6859	208	4	Pass
0.0001	6116	298	4	Pass
0.0001	5778	200	5	Pass
0.0001	5465	298	5	Pass
0.0001	4802	298	6	Pass
0.0001	4434	298	õ	Pass
0.0002	3829	298	7	Pass
0.0002	3539	298	8	Pass
0.0002	3192	298	9	Pass
0.0002	2611	298	11	Pass
0.0002	2293	298	12	Pass
0.0002	1781	298	16	Pass
0.0002	1593	298	18	Pass
0.0002	1356	298	21	Pass
0.0002	793	298	37	Pass
0.0002	688	298	43	Pass
0.0002	676	298	44	Pass
0.0002	664	298	44	Pass

Duration Flows

The Duration Matching Failed

Flow(cfs)	Predev	Mit	Percentage	Pass/Fail
0.0002	664	298	44	Pass
0.0002	522	296	56	Pass
0.0002	439	296	67	Pass
0.0003	366	296	80	Pass
0.0003	308	295	95	Pass
0.0004	267	294	110	Pass
0.0004	249	293	117	Fail
0.0004	231	293	126	Fail
0.0005	203	292	143	Fail
0.0005	187	292	156	Fail
0.0005	168	292	173	Fail
0.0006	147	291	197	Fail
0.0006	129	291	225	Fail
0.0007	120	290	241	Fail
0.0007	108	289	267	Fail
0.0007	100	289	289	Fail
0.0008	93	289	310	Fail
0.0008	85	289	340	Fail
0.0009	79	287	363	Fail
0.0009	76	286	376	Fail
0.0009	72	285	395	Fail
0.0010	67	283	422	Fail
0.0010	63	283	449	Fail
0.0010	62	283	456	Fail
0.0011	58	283	487	Fail
0.0011	56	282	503	Fail
0.0012	55	281	510	Fail
0.0012	54	280	518	Fail
0.0012	51	278	545	Fail
0.0013	50	278	556	Fail
0.0013	49	278	567	Fail
0.0013	46	278	604	Fail
0.0014	45	278	617	Fail
0.0014	44	278	631	Fail
0.0015	43	276	641	Fail
0.0015	40	274	685	Fail
0.0015	38	273	718	Fail
0.0016	37	273	737	Fail
0.0016	36	272	755	Fail
0.0017	35	271	774	Fail
0.0017	33	270	818	Fail
0.0017	32	270	843	Fail
0.0018	29	270	931	Fail
0.0018	28	270	964	Fail
0.0018	28	269	960	Fail
0.0019	28	267	953	Fail
0.0019	28	267	953	Fail
0.0020	27	267	988	Fail
0.0020	27	267	988	Fail
0.0020	26	267	1026	Fail
0.0021	25	266	1064	Fail
0.0021	25	263	1052	Fail
0.0021	23	261	1134	Fail
0.0022	22	259	1177	Fail

0.0022	22	258	1172	Fail
0.0023	21	258	1228	Fail
0.0023	21	257	1223	Fail
0.0023	21	257	1223	Fail
0.0024	21	257	1223	Fail
0.0024 0.0025	21 20 20	256 255 255	1219 1275 1275	Fail Fail Fail
0.0025	20 20 19	255 255 254	1275 1275 1336	Fail Fail
0.0026	18	253	1405	Fail
0.0026	17	253	1488	Fail
0.0027	17	253	1488	Fail
0.0027	17	253	1488	Fail
0.0028	15	252	1679	Fail
0.0028	15	252	1679	Fail
0.0028	14	251	1792	Fail
0.0029	14	250	1785	Fail
0.0029	13	250	1923	Fail
0.0029	13	250	1923	Fail
0.0030	13	249	1915	Fail
0.0030 0.0031	13 13 12	249 248 247	1915 1907 2058	Fail Fail Fail
0.0031	12	247	2058	Fail
	12	246	2050	Fail
	12	245	2041	Fail
0.0032 0.0033	12 12 12	244 244	2033 2033	Fail Fail
0.0033	12	243	2025	Fail
0.0033	12	242	2016	Fail
0.0034 0.0034	12 12 12	241 239 239	2008 1991 1991	Fail Fail Fail
0.0035 0.0035	12 12 11	239 239 238	1991 2163	Fail Fail
0.0036	11	238	2163	Fail
0.0036	11	237	2154	Fail
0.0036	11	236	2145	Fail
0.0037	11	236	2145	Fail
0.0037	11	235	2136	Fail
0.0037	11	235	2136	Fail
0.0037	11	235	2136	Fail
0.0038	11	235	2136	Fail
0.0038	11	235	2136	Fail
0.0039	11	235	2136	Fail
0.0039	11	235	2136	Fail
0.0039	11	235	2136	Fail

The development has an increase in flow durations from 1/2 Predeveloped 2 year flow to the 2 year flow or more than a 10% increase from the 2 year to the 50 year flow.

The development has an increase in flow durations for more than 50% of the flows for the range of the duration analysis.

Water Quality

Water QualityWater Quality BMP Flow and Volume for POC #1On-line facility volume:0 acre-feetOn-line facility target flow:0 cfs.Adjusted for 15 min:0 cfs.Off-line facility target flow:0 cfs.Adjusted for 15 min:0 cfs.O cfs.0 cfs.

LID Report

LID Technique	Used for Treatment ?	Total Volume Needs Treatment (ac-ft)	Volume Through Facility (ac-ft)	Infiltration Volume (ac-ft)	Cumulative Volume Infiltration Credit	Percent Volume Infiltrated	Water Quality	Percent Water Quality Treated	Comment
Gravel Trench Bed 1 POC		50.42				99.86			
Open-Graded Gravel POC		18.43				100.00			
Permeable Asphalt POC		5.30				100.00			
Total Volume Infiltrated		74.16	0.00	0.00		99.91	0.00	0%	No Treat. Credit
Compliance with LID Standard 8% of 2-yr to 50% of 2-yr									Duration Analysis Result = Passed

Model Default Modifications

Total of 0 changes have been made.

PERLND Changes

No PERLND changes have been made.

IMPLND Changes

No IMPLND changes have been made.

Appendix Predeveloped Schematic

	霘	Basin 0.20ac	1			

Mitigated Schematic



Predeveloped UCI File

Mitigated UCI File

RUN

GLOBAL WWHM4 model simulation
 START
 1901 10 01
 END
 2059 09 30

 RUN INTERP OUTPUT LEVEL
 3
 0
 RESUME 0 RUN 1 UNIT SYSTEM 1 END GLOBAL FILES <File> <Un#> <-----File Name---->*** * * * <-ID-> WDM 26 Combined Basins.wdm MESSU 25 MitCombined Basins.MES MitCombined Basins.L61 27 28 MitCombined Basins.L62 POCCombined Basinsl.dat 30 END FILES OPN SEOUENCE 4 17 INGRP INDELT 00:15 IMPLND IMPLND RCHRES 1 IMPLND 18 2 3 RCHRES RCHRES 1 COPY COPY 501 DISPLY 1 END INGRP END OPN SEQUENCE DISPLY DISPLY-INF01 # - #<----Title---->***TRAN PIVL DIG1 FIL1 PYR DIG2 FIL2 YRND
1 Open-Graded Gravel MAX 1 2 30 9 END DISPLY-INFO1 END DISPLY COPY TIMESERIES # - # NPT NMN *** 1 501 1 END TIMESERIES END COPY GENER OPCODE # # OPCD *** END OPCODE PARM K *** # # END PARM END GENER PERLND GEN-INFO <PLS ><-----Name---->NBLKS Unit-systems Printer *** User t-series Engl Metr *** # - # * * * in out END GEN-INFO *** Section PWATER*** ACTIVITY # - # ATMP SNOW PWAT SED PST PWG PQAL MSTL PEST NITR PHOS TRAC *** END ACTIVITY PRINT-INFO

- # ATMP SNOW PWAT SED PST PWG PQAL MSTL PEST NITR PHOS TRAC ******** END PRINT-INFO PWAT-PARM1 <PLS > PWATER variable monthly parameter value flags *** # - # CSNO RTOP UZFG VCS VUZ VNN VIFW VIRC VLE INFC HWT *** END PWAT-PARM1 PWAT-PARM2 WAI-FARM2
<PLS > PWATER input info: Part 2 ***
- # ***FOREST LZSN INFILT LSUR SLSUR <PLS > KVARY AGWRC END PWAT-PARM2 PWAT-PARM3 <PLS > PWATER input info: Part 3 ***
- # ***PETMAX PETMIN INFEXP INFILD DEEPFR BASETP AGWETP END PWAT-PARM3 PWAT-PARM4 <PLS > PWATER input info: Part 4 *** # - # CEPSC UZSN NSUR INTFW IRC LZETP *** END PWAT-PARM4 PWAT-STATE1 <PLS > *** Initial conditions at start of simulation ran from 1990 to end of 1992 (pat 1-11-95) RUN 21 *** # - # *** CEPS SURS UZS IFWS LZS AGWS GWVS END PWAT-STATE1 END PERLND IMPLND GEN-INFO <PLS ><-----Name----> Unit-systems Printer *** User t-series Engl Metr *** # - # in out *** ROOF TOPS/FLAT111270Porous Pavement111270Porous Pavement111270 0 4 17 18 END GEN-INFO *** Section IWATER*** ACTIVITY # - # ATMP SNOW IWAT SLD IWG IQAL *** 4 17 18 END ACTIVITY PRINT-INFO <ILS > ******* Print-flags ******* PIVL PYR 4 17 18 END PRINT-INFO IWAT-PARM1 <PLS > IWATER variable monthly parameter value flags *** # - # CSNO RTOP VRS VNN RTLI * * * 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 4 17 18 END IWAT-PARM1 IWAT-PARM2
 <PLS >
 IWATER input info: Part 2
 *

 # - # ***
 LSUR
 SLSUR
 NSUR
 RETSC

 4
 400
 0.01
 0.1
 0.1

 .7
 400
 0.01
 0.1
 0.1
 <PLS > * * * RETSC 17

400 0.01 0.1 0.1 18 END IWAT-PARM2 IWAT-PARM3 IWATER input info: Part 3 * * * <PLS > # - # ***PETMAX PETMIN 0 4 0 17 0 0 18 0 0 END IWAT-PARM3 IWAT-STATE1 <PLS > *** Initial conditions at start of simulation # - # *** RETS SURS 4 0 0 0 17 0 0 0 18 END IWAT-STATE1 END IMPLND SCHEMATIC <--Area--> <-Target-> MBLK *** <-factor-> <Name> # Tbl# *** <-Source-> <Name> # Portable Roofs*** 0.13 RCHRES 3 0.0152 RCHRES 2 0.0511 PCHRES 1 IMPLND 4 5 IMPLND 18 IMPLND 17 2 5 0.0511 1 5 RCHRES ******Routing***** COPY115COPY50117COPY50117COPY50117 IMPLND 4 0.13 RCHRES 3 1 RCHRES 1 1 RCHRES 2 1 END SCHEMATIC NETWORK <-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Target vols> <-Grp> <-Member-> *** <Name> # <Name> # #<-factor->strg <Name> # # <Name> # # *** COPY 501 OUTPUT MEAN 1 1 48.4 DISPLY 1 INPUT TIMSER 1 <-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Target vols> <-Grp> <-Member-> *** <Name> # <Name> # #<-factor->strg <Name> # # <Name> # # *** END NETWORK RCHRES GEN-INFO Name Nexits Unit Systems Printer * * * RCHRES # - #<----> User T-series Engl Metr LKFG * * * * * * in out
 Open-Graded Grav-008
 2
 1
 1
 28

 Permeable Asphal-009
 2
 1
 1
 28

 Gravel Trench Be-004
 2
 1
 1
 28
 1 0 1 2 0 1 3 0 1 END GEN-INFO *** Section RCHRES*** ACTIVITY # - # HYFG ADFG CNFG HTFG SDFG GQFG OXFG NUFG PKFG PHFG *** 1 0 0 0 0 0 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 2 1 3 1 END ACTIVITY PRINT-INFO * * * * * * * * *

2 3 END PRINT	4 0 4 0 -INFO	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 9 1 9	
HYDR-PARM RCHRES # - #	1 Flags for VC A1 A2 FG FG FG * * *	c each HYDR A3 ODFVFG FG possib * * *	Section for each le exit * * *	*** ODGTFG *** possib * *	for each le exit	FUNCT possil	*** for each ble exit **
1 2 3 END HYDR-	0 1 0 0 1 0 0 1 0 PARM1	$\begin{array}{ccccc} 0 & 4 & 5 \\ 0 & 4 & 5 \\ 0 & 4 & 5 \end{array}$	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	2 2 2 2 2 2	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
HYDR-PARM # - #	2 FTABNO	LEN	DELTH	STCOR	KS	DB50	* * *
<>< 1 2 3 END HYDR-	>< 1 2 3 PARM2	0.01 0.03 0.01	0.0 0.0 0.0 0.0	<>< 0.0 0.0 0.0	>< 0.5 0.5 0.5	0.0 0.0 0.0	* * *
HYDR-INIT RCHRES # - # *	Initial c *** VOL ** ac-ft >	conditions Initia for eac <><	for each H l value h possible ><>	HYDR sectio of COLIND e exit	n Initia for eac *** <><	l value h possible	*** of OUTDGT e exit <>
1 2 3 END HYDR- END RCHRES	0 0 0 INIT	$\begin{array}{c} 4.0\\ 4.0\\ 4.0\end{array}$	5.0 0.0 5.0 0.0 5.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0
SPEC-ACTION END SPEC-AC FTABLES FTABLE 92 5	S TIONS 3						
Depth (ft) 0.00000 0.016667 0.033333 0.050000 0.066667 0.083333 0.100000 0.116667 0.133333 0.150000 0.166667 0.183333 0.200000 0.216667 0.233333 0.250000 0.266667 0.283333 0.300000 0.316667 0.333333 0.350000 0.366667 0.383333 0.400000 0.416667 0.433333 0.450000 0.46667 0.483333 0.500000	Area (acres) 0.020524	Volume (acre-ft) 0.00000 0.000113 0.000226 0.000339 0.000452 0.000564 0.000677 0.000790 0.000903 0.001016 0.001129 0.001242 0.001242 0.001355 0.001467 0.001580 0.001693 0.001693 0.001693 0.001693 0.001806 0.001919 0.002248 0.002258 0.002258 0.0022596 0.0022709 0.002822 0.002822 0.002935 0.003048 0.003161 0.003274 0.003386	Outflow1 (cfs) 0.000000 0.000000 0.000000 0.000000 0.000000	Outflow2 (cfs) 0.000000 0.013317	Velocity (ft/sec)	Travel T: (Minute	ime*** es)***

0.516667 0.533333 0.550000 0.566667 0.583333 0.600000 0.616667 0.633333 0.650000 0.666667 0.683333 0.700000 0.716667 0.733333 0.750000 0.766667 0.783333 0.750000 0.816667 0.833333 0.800000 0.816667 0.833333 0.900000 0.916667 0.933333 0.900000 0.916667 0.983333 1.000000 1.016667 1.033333 1.000000 1.016667 1.033333 1.050000 1.066667 1.083333 1.000000 1.116667 1.083333 1.100000 1.166667 1.083333 1.100000 1.16667 1.233333 1.250000 1.26667 1.233333 1.250000 1.216667 1.233333 1.200000 1.216667 1.33333 1.200000 1.26667 1.233333 1.200000 1.26667 1.233333 1.250000 1.26667 1.2667 1.2667 1.2667 1.2667 1.2667 1.2677 1.2757 1.2757 1.2757 1.2757 1.2757 1.2757 1.2757 1.2	0.020524 0.02	0.003499 0.003612 0.003725 0.003838 0.003951 0.004064 0.004177 0.004289 0.004289 0.004515 0.004628 0.004741 0.004967 0.005080 0.005192 0.005305 0.005418 0.005757 0.005644 0.005757 0.005870 0.005983 0.006966 0.006208 0.006321 0.006321 0.006434 0.006547 0.006660 0.006208 0.006321 0.006434 0.006547 0.0066434 0.006547 0.0066886 0.006999 0.007111 0.007224 0.007337 0.007450 0.007763 0.007763 0.007763 0.007763 0.007763 0.007759 0.007753 0.007753 0.007450 0.007753 0.007753 0.007753 0.007450 0.007902 0.008014 0.008127 0.008466 0.008579 0.008466 0.008579 0.008466 0.008579 0.008466 0.008579 0.008420 0.009482 0.009482 0.00930 0.009482 0.00930 0.009482 0.00930 0.009482 0.00930 0.009482 0.00930 0.009482 0.00930 0.009482 0.00930 0.009482 0.00930 0.009482 0.00930 0.009482 0.00930 0.009482 0.00930 0.009482 0.00930 0.009482 0.00930 0.009482 0.00930 0.009482 0.00930 0.009482 0.00930 0.009482 0.00930 0.009482 0.009482 0.009482 0.009482 0.009482 0.009482 0.009482 0.009482 0.009482 0.009482 0.009482 0.009482 0.009482 0.009482 0.009482 0.009482 0.00948	0.000000 0.00	0.013317 0.0131		
1.483333 1.500000 1.516667 END FTABL	0.020524 0.020524 0.020524 0.020524 E 3	0.010046 0.010159 0.010501	0.182234 0.254292 0.333520 0.418946	0.013317 0.013317 0.013317 0.013317		
FTABLE 91 5 Depth (ft) 0.000000 0.005556 0.011111 0.016667	1 Area (acres) 0.051144 0.051144 0.051144	Volume (acre-ft) 0.000000 0.000094 0.000188 0.000281	Outflow1 (cfs) 0.000000 0.000000 0.000000 0.000000	Outflow2 (cfs) 0.000000 0.033186 0.033186 0.033186	Velocity (ft/sec)	Travel Time*** (Minutes)***

0.022222	0.051144	0.000375	0.00000	0.033186
0.027778	0.051144	0.000469	0.000000	0.033186
0.033333	0.051144 0.051144	0.000563	0.000000	0.033186
0.044444	0.051144	0.000750	0.000000	0.033186
0.050000	0.051144	0.000844	0.000000	0.033186
0.055556	0.051144	0.000938	0.00000	0.033186
0.061111	0.051144	0.001031	0.00000	0.033186
0.066667	0.051144	0.001125	0.000000	0.033186
0.072222	0.051144	0.001219	0.000000	0.033186
0.077778	0.051144 0.051144	0.001313	0.000000	0.033186
0.088889	0.051144	0.001400	0.000000	0.033186
0.094444	0.051144	0.001594	0.000000	0.033186
0.100000	0.051144	0.001688	0.00000	0.033186
0.105556	0.051144	0.001782	0.000000	0.033186
0.111111	0.051144	0.001875	0.000000	0.033186
0.110007 0.122222	0.051144 0.051144	0.001969	0.000000	0.033186
0.127778	0.051144	0.002157	0.000000	0.033186
0.133333	0.051144	0.002250	0.000000	0.033186
0.138889	0.051144	0.002344	0.00000	0.033186
0.144444	0.051144	0.002438	0.000000	0.033186
0.150000	0.051144	0.002532	0.000000	0.033186
0.155556	0.051144 0.051144	0.002625	0.000000	0.033186
0.166667	0.051144	0.002719	0.000000	0.033186
0.172222	0.051144	0.002907	0.000000	0.033186
0.177778	0.051144	0.003000	0.00000	0.033186
0.183333	0.051144	0.003094	0.000000	0.033186
0.188889	0.051144	0.003188	0.000000	0.033186
0.194444	0.051144 0 051144	0.003282 0.003376	0.000000	0.033186
0.205556	0.051144	0.003469	0.000000	0.033186
0.211111	0.051144	0.003563	0.00000	0.033186
0.216667	0.051144	0.003657	0.000000	0.033186
0.222222	0.051144	0.003751	0.000000	0.033186
0.22///8	0.051144 0.051144	0.003844	0.000000	0.033186
0.238889	0.051144	0.004032	0.000000	0.033186
0.244444	0.051144	0.004126	0.00000	0.033186
0.250000	0.051144	0.004219	0.00000	0.033186
0.255556	0.051144	0.004313	0.000000	0.033186
0.261111	0.051144 0.051144	0.004407 0.004501	0.000000	0.033186
0.272222	0.051144	0.004594	0.000000	0.033186
0.277778	0.051144	0.004688	0.000000	0.033186
0.283333	0.051144	0.004782	0.00000	0.033186
0.288889	0.051144	0.004876	0.000000	0.033186
0.294444	0.051144	0.004970	0.000000	0.033186
0.305556	0.051144 0.051144	0.005157	0.000000	0.033186
0.311111	0.051144	0.005251	0.000000	0.033186
0.316667	0.051144	0.005345	0.00000	0.033186
0.322222	0.051144	0.005438	0.00000	0.033186
0.327778	0.051144	0.005532	0.000000	0.033186
0.338889	0.051144 0.051144	0.005720	0.000000	0.033186
0.344444	0.051144	0.005813	0.000000	0.033186
0.350000	0.051144	0.005907	0.00000	0.033186
0.355556	0.051144	0.006001	0.000000	0.033186
0.361111	0.051144	0.006095	0.000000	0.033186
0.372222	0.051144 0.051144	0.006188	0.000000	0.033186
0.377778	0.051144	0.006376	0.000000	0.033186
0.383333	0.051144	0.006470	0.000000	0.033186
0.388889	0.051144	0.006564	0.00000	0.033186
0.394444	0.051144	0.006657	0.00000	0.033186
0.400000	0.051144 0.051144	0.006/51 0.006845	0.000000	0.033186

0.411111 0.416667 0.422222 0.427778 0.433333 0.438889 0.444444 0.450000 0.455556 0.461111 0.466667 0.472222 0.477778 0.483333 0.488889 0.494444 0.500000 END FTABLE	0.051144 0.051144 0.051144 0.051144 0.051144 0.051144 0.051144 0.051144 0.051144 0.051144 0.051144 0.051144 0.051144 0.051144 0.051144 0.051144 0.051144 0.051144 2.2	0.006939 0.007032 0.007126 0.007220 0.007314 0.007407 0.007501 0.007595 0.007689 0.007782 0.007876 0.007970 0.008064 0.008157 0.008251 0.008345 0.008439	0.000000 0.000000	0.033186 0.033186 0.033186 0.033186 0.033186 0.033186 0.033186 0.033186 0.033186 0.033186 0.033186 0.033186 0.033186 0.033186 0.033186 0.033186 0.033186 0.033186 0.033186			
Depth (ft) 0.00000 0.005556 0.01111 0.016667 0.022222 0.027778 0.033333 0.038889 0.044444 0.050000 0.055556 0.06111 0.066667 0.072222 0.077778 0.083333 0.088889 0.094444 0.100000 0.105556 0.11111 0.116667 0.122222 0.127778 0.133333 0.138889 0.144444 0.150000 0.155556 0.161111 0.166667 0.172222 0.127778 0.133333 0.138889 0.144444 0.150000 0.155556 0.161111 0.166667 0.172222 0.177778 0.183333 0.188889 0.194444 0.200000 0.205556 0.211111 0.216667 0.2222778 0.233333 0.238889 0.244444 0.250000 0.255556 0.261111	Area (acres) 0.015220	Volume (acre-ft) 0.000000 0.00028 0.000056 0.000084 0.000112 0.000140 0.000195 0.000223 0.000251 0.000279 0.000307 0.000307 0.000335 0.000363 0.000391 0.000414 0.000474 0.000474 0.000502 0.000558 0.000520 0.000558 0.0000558 0.0000558 0.0000558 0.0000558 0.0000558	Outflow1 (cfs) 0.000000 0.000000 0.000000 0.000000 0.000000	Outflow2 (cfs) 0.000000 0.009876	Velocity (ft/sec)	<pre>Travel Time*** (Minutes)***</pre>	

$\begin{array}{c} 0.266667 & 0.015220 & 0 \\ 0.272222 & 0.015220 & 0 \\ 0.283333 & 0.015220 & 0 \\ 0.283333 & 0.015220 & 0 \\ 0.288889 & 0.015220 & 0 \\ 0.294444 & 0.015220 & 0 \\ 0.30000 & 0.015220 & 0 \\ 0.305556 & 0.015220 & 0 \\ 0.31111 & 0.015220 & 0 \\ 0.316667 & 0.015220 & 0 \\ 0.322222 & 0.015220 & 0 \\ 0.327778 & 0.015220 & 0 \\ 0.33333 & 0.015220 & 0 \\ 0.338889 & 0.015220 & 0 \\ 0.344444 & 0.015220 & 0 \\ 0.35556 & 0.015220 & 0 \\ 0.366667 & 0.015220 & 0 \\ 0.366667 & 0.015220 & 0 \\ 0.366667 & 0.015220 & 0 \\ 0.366667 & 0.015220 & 0 \\ 0.366667 & 0.015220 & 0 \\ 0.366667 & 0.015220 & 0 \\ 0.377778 & 0.015220 & 0 \\ 0.388889 & 0.015220 & 0 \\ 0.388889 & 0.015220 & 0 \\ 0.388889 & 0.015220 & 0 \\ 0.394444 & 0.015220 & 0 \\ 0.400000 & 0.015220 & 0 \\ 0.405556 & 0.015220 & 0 \\ 0.41111 & 0.015220 & 0 \\ 0.422222 & 0.015220 & 0 \\ 0.427778 & 0.015220 & 0 \\ 0.427778 & 0.015220 & 0 \\ 0.43333 & 0.015220 & 0 \\ 0.438889 & 0.015220 & 0 \\ 0.444444 & 0.015220 & 0 \\ 0.45556 & 0.015220 & 0 \\ 0.438889 & 0.015220 & 0 \\ 0.438889 & 0.015220 & 0 \\ 0.438889 & 0.015220 & 0 \\ 0.444444 & 0.015220 & 0 \\ 0.466667 & 0.015220 & 0 \\ 0.477222 & 0.015220 & 0 \\ 0.466667 & 0.015220 & 0 \\ 0.488889 & 0.015220 & 0 \\ 0.488889 & 0.015220 & 0 \\ 0.488889 & 0.015220 & 0 \\ 0.494444 & 0.015220 & 0 \\ 0.4948889 & 0.015220 & 0 \\ 0.494444 & 0.015220 & 0 \\ 0.494444 & 0.0152$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.009876 0.00	
EXT SOURCES <-Volume-> <member> Ssy <name> # <name> # ten WDM 2 PREC ENG WDM 2 PREC ENG WDM 1 EVAP ENG WDM 1 EVAP ENG WDM 1 EVAP ENG WDM 1 EVAP ENG</name></name></member>	rsSgap <mult>Tran a strg<-factor->strg L 1 L 1 L 1 L 1 L 1 L 1 L 1 L 1</mult>	n <-Target vols> <-Gr s <name> # # PERLND 1 999 EXTN IMPLND 1 999 EXTN PERLND 1 999 EXTN IMPLND 1 999 EXTN RCHRES 1 EXTN RCHRES 2 EXTN</name>	<pre>p> <-Member-> ***</pre>
END EXT SOURCES			
EXT TARGETS <-Volume-> <-Grp> <-Mem <name> # <name RCHRES 3 HYDR RO RCHRES 3 HYDR O RCHRES 3 HYDR O RCHRES 3 HYDR STAGE COPY 1 OUTPUT MEAN COPY 501 OUTPUT MEAN RCHRES 1 HYDR RO RCHRES 1 HYDR O RCHRES 1 HYDR O</name </name>	ber-> <mult>Tran + #<-factor->stry 1 1 1 2 1 1 1 1 1 1 1 48.4 1 1 48.4 1 1 48.4 1 1 1 2 1 1 1 1 1 2 1 1 1 1 1 1 1 1 1</mult>	n <-Volume-> <member> g <name> # <name> WDM 1000 FLOW WDM 1001 FLOW WDM 1002 FLOW WDM 1003 STAG WDM 701 FLOW WDM 801 FLOW WDM 1004 FLOW WDM 1005 FLOW WDM 1006 FLOW</name></name></member>	Tsys Tgap Amd *** tem strg strg*** ENGL REPL ENGL REPL ENGL REPL ENGL REPL ENGL REPL ENGL REPL ENGL REPL ENGL REPL ENGL REPL ENGL REPL

RCHRES	1	HYDR	STAGE	1	1	1	WDM	1007	STAG	; El	NGL	REPL
RCHRES	2	HYDR	RO	1	1	1	WDM	1008	FLOW	I El	NGL	REPL
RCHRES	2	HYDR	0	1	1	1	WDM	1009	FLOW	I El	NGL	REPL
RCHRES	2	HYDR	0	2	1	1	WDM	1010	FLOW	I El	NGL	REPL
RCHRES	2	HYDR	STAGE	1	1	1	WDM	1011	STAG	; El	NGL	REPL
END EXT	TAR	GETS										
MASS-LIN	K											
<volume> <-Grp></volume>		<-Member-> <mult-< td=""><td>-></td><td colspan="2"><target></target></td><td><-Grp></td><td><-Member</td><td>r->***</td></mult-<>		->	<target></target>		<-Grp>	<-Member	r->***			
<name></name>		<name></name>	# #<-factor->		<name></name>				<name></name>	# #***		
MASS-L	INK		5									
IMPLND		IWATER	SURO		0.08333	3	RCHRES	3		INFLOW	IVOL	
END MA	SS-	LINK	5									
MASS-T.	TNK		15									
	1 1 1 1 1	TWATER	SURO		0 08333	3	COPY			TNDIT	MEAN	
END MA	55-	TTNK	15		0.00555		0011			1111 0 1	1.177.77	
			10									
MASS-L	INK		17									
RCHRES		OFLOW	OVOL	1			COPY			INPUT	MEAN	
END MA	SS-	LINK	17									

END MASS-LINK

END RUN

Predeveloped HSPF Message File

Mitigated HSPF Message File

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www.clearcreeksolutions.com

APPENDIX D

Infiltration Testing Report

Puyallup High School Portables

711, 721 & 701 West Main Puyallup, WA

Prepared for

Puyallup School District c/o Studio Meng Strazzara 2001 Western Ave, Suite 200 Seattle, WA 98121 206.587.3797

Prepared by

JMJ TEAM 905 Main St, Suite 200 Sumner, WA 98390 206.596.2020 Justin Jones, PE


PROJECT ENGINEER'S CERTIFICATION

I hereby certify that this Infiltration Testing Report for Puyallup High School Portables has been prepared by me or under my supervision and meets minimum standards of the Department of Ecology Stormwater Management Manual for Western Washington.

Justin Jones, PE





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Appendix C: Department of Ecology PIT Procedure

Appendix D: Department of Ecology Factor of Safety Guidelines



SUMMARY

This report details the results of infiltration testing for use in the stormwater system design of Puyallup High School Portables located within Puyallup, WA. Two (2) Small-Scale Pilot Infiltration Tests (PIT) were conducted on site to determine the onsite stormwater infiltration rate. The test holes were excavated and backfilled by a licensed contractor and the PIT was completed in accordance with the Department of Ecology (ECY) Stormwater Management Manual for Western Washington (Stormwater Manual).

The PIT process evaluates the infiltration within a 12 SF area by first measuring the rate of water required to maintain a constant water elevation of approximately 12-inches in the test pit, and second by measuring the drawdown rate of the water within the test pit. The drawdown is done using a data logger.

The field data is then analyzed, and a factor of safety is applied to determine the stormwater design infiltration rate. Below is a summary of the results.

Test Pit and Ground Water Monitoring Location



Summary of Results

Per the PIT, the site soil is suitable for stormwater infiltration. Soil evaluations were not taken as the designed stormwater BMP is not intended to treat pollution generating surfaces.

Testing Test PIT		Results	ECY Threshold	
	Pit Depth	4.0-feet	N/A	
Ground Water	Test Hole 1 Groundwater Level	Ground Water Observed at 4.0'	N/A	
	Test Hole 2 Groundwater Level	Ground Water Observed at 3.5' Depth	N/A	
	Infiltration Rate Factor of Safety	0.45	N/A	
		Uncorrected: 1.43 inches per hour		
Infiltration Pate	Test Hole 1 Infiltration Rates	Design: 0.64 Inches per hour	≥ 0.3 inches per hour	
		Uncorrected: 4.42 inches per hour	≥ 0.3 inches per hour	
	Test Hole 2 Infiltration Rates	Design: 1.99 inches per hour		
	Test Hole 1 Lab Analysis	CEC Value: N/A	≥ 5.0 milliequivalents CEC/100g	
		Organic Content: N/A	≥ 1.0%	
Water Quality	Test Hole 2 Lab Analysis	CEC Value: N/A	≥ 5.0 milliequivalents CEC/100g	
		Organic Content: N/A	≥ 1.0%	

INFILTRATION TEST PROCEDURES

Below is the process taken for the Small-Scale PIT:

- □ Identify PIT locations based on the site survey of existing buildings and utilities as well as the potential locations of infiltration facilities based on the preliminary site plan.
- Obtain public and private utility locates. Prior to the PIT utility locates will be called to ensure there are no utilities present in the PIT locations.
- Excavation of PIT holes (approximately 3-feet x 4-feet x 2-feet deep). A 3-feet x 4-feet x 2-feet tall wood box is inserted into the test hole to ensure that the bottom surface area is exactly 12 SF. The box is backfilled to the top edge to ensure stability and infiltration only through the bottom of the test hole for the duration of the PIT.
- A soil sample is collected from the bottom of the hole to test treatment capability. A lab tests the cation exchange rate and organic matter content of soils. Lab results confirm if the soil is suitable for treatment based on Stormwater Manual criteria.
- □ A float system with a water hose connection is set into the center of the test hole. The float system is equipped with a leveling plate, a measuring ruler for visual inspection of water levels and a perforated pipe housing for the data collector.
- Using water transfer tanks or hose spigot as available, the test hole is filled to a 12-inch water depth that is maintained. The presoak period ensures that the soil has been fully saturated before conducting the PIT. A 1-hour stabilization test is performed after the presoak period to confirm soil stabilization. If the test yields 4 constant gallon per minute (GPM) readings that are conducted every 15-minutes, the stabilization of the soil is confirmed.
- A 1-hour GPM test is conducted per the Stormwater Manual. Using a water meter accurate to the nearest tenth of a gallon, a GPM flow rate is recorded every 15-minutes while the water level is maintained at a 12-inch depth. An infiltration rate (in/hr) can be determined using the GPM flow rate and the 12 SF bottom surface area of the hole.
- A drawdown test is performed per Stormwater Manual to determine the drawdown infiltration capability of the soil. A CRS451V (Pressure Transducer) is placed into the test hole and set to take pressure (PSI) readings every 10-minutes. The water source is shut off, and the pressure transducer will measure water drawdown for a 2-hour period. At the end of the period the sensors are removed from the test hole, the data is collected using a PC interface module and the HydroSci program to communicate with the sensor to retrieve the data.
- □ The wood box and the float system are removed from the test hole.
- □ The test hole is then over excavated to confirm there is no ground water mounding.
- □ The test pit then gets backfilled and restored to prior state of excavation.

FINDINGS AND RECOMMENDATIONS

Groundwater Conditions

The Stormwater Manual specifies minimum separations between the seasonal high groundwater elevation and the bottom of the infiltration facility based on different best management practices (BMP):

- Downspout Infiltration: 1-foot
- Permeable Pavement: 1-foot
- Infiltration Gallery: 1-foot
- Bioretention: 3-foot

Groundwater was monitored throughout the wet season. The known seasonal high groundwater level for Test Hole-1 was determined to be 4.0' below the existing grade of 42.1'. The known seasonal high groundwater level for Test Hole-2 was determined to be 3.55' below the existing grade of 41.6'. With known groundwater conditions for each test hole, there is adequate spacing between groundwater and BMPs. An overflow should be installed with BMP in case of large storm events.

Field Measured Infiltration Rate

The infiltration rate was collected using two methods during the PIT. The first method is to measure the gallons per minute flow rate required to maintain a constant water level in the test pit. The average of the flow rate measurements taken over an hour timeframe.

The second method is to measure the drawdown rate of the test pit. Measurements were taken both visually and with a data logger. The average of the drawdown measurements resulted in the following infiltration rates:



- Test Hole 1: 1.43 inches per hour
- Test Hole 2: 4.42 inches per hour



Design Infiltration Rate

Per the Stormwater Manual a minimum design infiltration rate of 0.3 inches per hour is required for onsite infiltration. The design infiltration rate takes the field measured infiltration rate and applies a factor of safety based on three correction factors. The three corrections are based on site variability, test method, and degree of influent control (See Appendix D).

Issue	Partial Correction Factor
Site variability and number of locations tested	CF _V = 0.33 to 1.0
Test Method	
Large-scale PIT	r CF _t = 0.75
Small-scale PIT	⊠ = 0.50
Other small-scale (e.g. Double ring, falling head)	⊠ = 0.40
Grain Size Method	▣ = 0.40
Degree of influent control to prevent siltation and bio-buildup	CF _m = 0.9

Total Correction Factor, $CF_T = CF_V \times CF_t \times CF_m$

Per the Stormwater Manual, a site variability correction of 1 is used. A correction of 0.5 for the small-scale PIT and 0.9 for the degree of influent are also used. A total correction factor of 0.45 is applied to the measured infiltration rate yielding a recommended design infiltration rates as follows:

- Test Hole 1: 0.64 inches per hour
- Test Hole 2: 1.99 inches per hour

Treatment Suitability

Per the Stormwater Manual the soils that stormwater is infiltrated into may be used for treatment of pollution generating surfaces if the soil meets specific requirements. Otherwise, a treatment layer is required to treat pollution generating surfaces. The treatment threshold of the infiltrated soil per the Stormwater Manual is a Cation Exchange Capacity greater than or equal to 5 milliequivalents CEC/100g and a minimum of 1.0% organic content.

This project does not propose to manage pollution generating hard surfaces runoff through an infiltration facility; therefore, soil treatment suitability was not evaluated.

TEST PIT PHOTO DOCUMENTATION – TEST HOLE 1









Pre-Soak PIT

1-Hour GPM Test



Completed Drawdown





Overexcavate to Verify Groundwater Mounding

Backfill and Install Groundwater Monitoring

TEST PIT PHOTO DOCUMENTATION – TEST HOLE 2



3-feet x 4-feet x 2-feet PIT and Pre-Soak



1-Hour GPM Test



Overexcavate to Verify Groundwater Mounding



Backfill and Install Groundwater Monitoring

APPENDIX A

Project Location:	PHS Portables			3506 Initial Meter Reading				
Date of Test:	This For dasies	2/10/2024	Test start	ssoo mila meter nedang				
Date of rest.		2/10/2024	Test start					
Tost Bit Dimonsions:		Width (foot)	2	Longth (feet)	4	Depth (inches)	24	
Test Fit Dimensions.		width (leet)	3	Length (reet)	4	Depth (inches)	24	
Procoak:	12:00PM Start Pro soak	Abrs at 12-inch water column						
FICSOAK.	12.00FWI Start FIE SOak	4113 at 12-inch water column						
Weather Conditions	Clear	50° 5		-				
weather conditions.	Clear	50 F		-				
Infiltration Tests				-				
minuration rest.		Mater Calvera Maintained (inches)	10	-				
		Callege Declark:	7.40	-				
		Gallons Per Inch.	7.40	-			Flow	Infiltration
		Time(Minutes)	Volume (gallons)		low Poto (CDA	a)	(Gallons)	Pate (in /br)
		Time(windles)	volume (galions)	Motor Start	Notor End	(I) Flow (Callans)	(Galions)	Kate (III/III)
4.05 DNA Chart					WIELEI EIIU	Flow (Galiolis)	0.2	
4:05 PIVI Start		0		3581.9	3582.1	0.2	0.2	
		15		3584.7	3584.9	0.3	3.1	
		30		3587.9	3588.2	0.3	6.3	
		45		3591.0	3591.3	0.3	9.4	
		60		3594.2	3594.8	0.6	12.9	1./
Descudences To at 10 and 3								
Drawdown Test (Sensor):								
		JIVIJ 01 (CRS451V Sensors from						
Sensor Name:		Campbell Scientic)						
T (D)					1.1.1(1.1)			
Time (Decimal Hours)	Record Measurement Interval	Time Stamp	Record #	Reading (PSI)	Level (in)			
0.0000	0	4:05 PM	0	0.61668	17.0943696			
0.1667	10	4:15 PM	1	0.605066	16.77242952			
0.3333	20	4:25 PM	2	0.593788	16.45980336			
0.5000	30	4:35 PM	3	0.582971	16.15995612			
0.6667	40	4:45 PM	4	0.572547	15.8/100284			
0.8333	50	4:55 PM	5	0.562265	15.5859858			
1.0000	60	5:05 PM	6	0.552374	15.31180728			
1.1667	70	5:15 PM	7	0.542279	15.03197388			
1.3333	80	5:25 PM	8	0.532924	14.77265328			
1.5000	90	5:35 PM	9	0.52373	14.5177956			
1.6667	100	5:45 PM	10	0.514174	14.25290328			
1.8333	110	5:55 PM	11	0.505343	14.00810796			
2.0000	120	6:05 PM	12	0.497038	13.77789336			
2.1667	130	6:15 PM	13	0.488469	13.54036068			
2.3333	140	6:25 PM	14	0.479748	13.29861456			
2.5000	150	6:35 PM	15	0.471365	13.0662378			
2.6667	160	6:45 PM	16	0.463378	12.84483816			
2.8333	170	6:55 PM	17	0.455239	12.61922508			
3.0000	180	7:05 PM	18	0.447283	12.39868476			
3.1667	190	7:15 PM	19	0.439696	12.18837312			
3.3333	200	7:25 PM	20	0.431804	11.96960688			
3.5000	210	7:35 PM	21	0.424222	11.75943384			
3.6667	220	7:45 PM	22	0.416743	11.55211596			
3.8333	230	7:55 PM	23	0.409753	11.35835316			
4.0000	240	8:05 PM	24	0.4027	11.162844			
4.1667	250	8:15 PM	25	0.395456	10.96204032			
4.3333	260	8:25 PM	26	0.388569	10.77113268			
4.5000	270	8:35 PM	27	0.381685	10.5803082			
						Average Infiltration Rate:	1.43	
						Factor of Safety:	0.45	
						Design Infiltration Rate:	0.64	



Project Location:	PHS Library			4502 Initial Meter Reading				
Date of Test:		2/10/2024	Test start					
		_,,,		1				
Test Pit Dimensions		Width (feet)	3	Length (feet)	4	Depth (inches)	24	
		width (reet)	5	Lenger (reet)		Depth (menes)	21	
Presoak:	12:00PM Start Pre soak	4hrs at 12-inch water column						
Weather Conditions:	Clear	50° F						
Infiltration Test:								
		Water Column Maintained (inches):	12					
		Gallons Per Inch:	7.48					
							Flow	Infiltration
		Time(Minutes)	Volume (gallons)	1	low Rate (GPN	/)	(Gallons)	Rate (in/hr)
				Meter Start	Meter End	Flow (Gallons)		
4:15 PM Start		0		4702.0	4702.8	0.8	0.8	
		15		4711.5	4712.2	0.7	10.2	
		30		4721.7	4722.4	0.7	20.4	
		45		4732.2	4732.9	0.7	30.9	
		60		4742.9	4743.7	0.8	41.6	5.6
Drawdown Test (Sensor):								
		JMJ 02 (CRS451V Sensors from						
Sensor Name:		Campbell Scientic)						
Time (Decimal Hours)	Record Measurement Interval	Time Stamp	Record #	Reading (PSI)	Level (in)			
0.0000	0	4:05 PM	0	0.5816216	16.12255075			
0.1667	10	4:15 PM	1	0.5537774	15.35070953			
0.3333	20	4:25 PM	2	0.5248642	14.54923562			
0.5000	30	4:35 PM	3	0.4966844	13.76809157			
0.6667	40	4:45 PM	4	0.4701035	13.03126902			
0.8333	50	4:55 PM	5	0.4443737	12.31803896			
1.0000	60	5:05 PM	6	0.4201141	11.64556285			
1.1667	70	5:15 PM	7	0.3973055	11.01330846			
1.3333	80	5:25 PM	8	0.3752191	10.40107345			
1.5000	90	5:35 PM	9	0.3541772	9.817791984			
1.6667	100	5:45 PM	10	0.334096	9.26114112			
1.8333	110	5:55 PM	11	0.3144749	8.717244228			
2.0000	120	6:05 PM	12	0.2135902	5.920720344			
	1	l						
	1	l						
	1							
	1							
	1	1		+				
	1	1		+				
		1			1			
		1		1		Average Infiltration Rate:	4 47	
				1			4.42	
	1	1				Factor of Safety	0.45	
	1	1				. actor or surety.	0.45	
				1	1	Design Infiltration Rate:	1.99	
				1				





Puyallup School District PHS Portables Ground Water Monitoring Log

#	Location	Date	Groud Water Depth (Ft)
1	#1 - PHS Proposed Portable	1/12/2024	4.5'
2	#1 - PHS Proposed Portable	1/26/2024	4.3'
3	#1 - PHS Proposed Portable	2/10/2024	4.2'
4	#1 - PHS Proposed Portable	2/16/2024	4.0'
5	#1 - PHS Proposed Portable	3/1/2024	4.3'
6	#1 - PHS Proposed Portable	3/14/2024	4.0'
7	#1 - PHS Proposed Portable	3/25/2024	4.8'
8	#1 - PHS Proposed Portable	4/5/2024	5.1'
1	#2 - PHS Library	1/12/2024	4.3'
2	#2 - PHS Library	1/26/2024	4.1'
3	#2 - PHS Library	2/10/2024	3.6'
4	#2 - PHS Library	2/16/2024	3.5'
5	#2 - PHS Library	3/1/2024	3.8'
6	#2 - PHS Library	3/14/2024	3.7'
7	#2 - PHS Library	3/25/2024	4.0'
8	#2 - PHS Library	4/5/2024	3.8'

APPENDIX B



Stainless-Steel Vented Stand-Alone Pressure Transducer



Pressure Transducer Combined with a Recorder

R 😪 🕻 6

PRODUCT

High resolution and accuracy

Overview

The CRS451V consists of a submersible water-level and watertemperature sensor with its own time clock and memory to store the collected data—in a compact stainless-steel case. This data logging capability frees users to place the sensor in remote sites and let it collect data for long periods. HydroSci software is included and elegantly supports test setup, data retrieval, and data display. Long battery life and rugged construction mean you can trust the CRS451V to collect important data. Low cost and ease of use make it a good choice in a variety of applications. The CRS456V is the same as this, but with a titanium case.

Benefits and Features

- Sensors and data-collection features in one instrument case
- > Rugged stainless-steel case protects piezoresistive sensor
- Quality construction ensures product reliability
- > Fully temperature-compensated

Fast scan rate

-) Large data-storage capacity
- Long battery life
- > Easy-to-use software

Detailed Description

The CRS451V has several pressure range options.

HydroSci software is available for download. This software simplifies the process of configuring the CRS451V. Users can

configure the CRS451V to monitor surface water, ground water, or a standard pump test.

HydroSci software will display the data in tabular or graphical formats.

Specifications

Venting

Vented

Measurement Time

< 1.0 s

APPENDIX C

INFILTRATION TEST

The Washington State Department of Ecology Stormwater Manual provides testing procedures and best practices, which are described below.

- Testing should occur between December 1 and April 1.
- The horizontal and vertical locations of the PIT shall be surveyed by a licensed land surveyor and accurately shown on the design drawings.
- Excavate the test pit to the estimated elevation of the proposed infiltration into the native soil. Note that for some proposed BMPs, such as and <u>BMP T5.15: Per-meable Pavements</u>, this will be below the proposed finished grade. If the native soils will have to meet a minimum subgrade compaction requirement (for example, the road subgrade if using <u>BMP T5.15: Permeable Pavements</u>), compact the native soil to that requirement prior to testing. Lay back the slopes sufficiently to avoid caving and erosion during the test. Altern- atively, consider shoring the sides of the test pit.
- The horizontal surface area of the bottom of the test pit should be approximately 100 square feet. Document the size and geometry of the test pit.
- Install a vertical measuring rod (long enough to measure the ponded water depth, minimum 5- ft. long) marked in half-inch increments in the center of the pit bottom.
- Use a rigid 6-inch diameter pipe with a splash plate on the bottom to convey water to the test pit and reduce side-wall erosion or excessive disturbance of the test pit bottom. Excessive erosion and bottom disturbance will result in clogging of the infiltration receptor and yield lower than actual infiltration rates.
- Add water to the pit at a rate that will maintain a water level between 6 and 12 inches above the bottom of the pit. A rotameter can be used to measure the flow rate into the pit.

The depth should not exceed the proposed maximum depth of water expected in the completed BMP. For infiltration BMPs serving large drainage areas, designs with multiple feet of standing water can have infiltration tests with greater than 1 foot of standing water.

- Every 15-30 min, record the cumulative volume and instantaneous flow rate in gallons per minute necessary to maintain the water level at the same point on the measuring rod.
- Keep adding water to the pit until one hour after the flow rate into the pit has stabilized (constant flow rate; a goal of 5% or less variation in the total flow) while maintaining the same pond water level. The total of the pre-soak time plus one hour after the flow rate has stabilized should be no less than 6 hours.
- After the flow rate has stabilized for at least one hour, turn off the water and record the rate of infiltration (the drop rate of the standing water) in inches per hour from the measuring rod data, until the pit is empty. Consider running this falling head phase of the test several times to estimate the dependency of the infiltration rate with head.
- At the conclusion of testing, over-excavate the pit to see if the test water is mounded on shallow restrictive layers or if it has continued to flow deep into the subsurface. The depth of excavation varies depending on soil type and depth to the hydraulic restricting layer, and is determined by the

engineer or certified soils professional. Mounding is an indication that a mounding analysis is necessary.

DATA ANALYSIS

Calculate and record the initial K_{sat} rate in inches per hour in 30 minutes or one-hour increments until one hour after the flow has stabilized.

Use statistical/trend analysis to obtain the hourly flow rate when the flow stabilizes. This would be the lowest hourly flow rate. *Example:*

The area of the bottom of the test pit is 8.5-ft. by 11.5-ft. (97.75 sq. ft.).

Water flow rate was measured and recorded at intervals ranging from 15 to 30 minutes throughout the test. Between 400 minutes and 1,000 minutes the flow rate stabilized between 10 and 12.5 gal- lons per minute or 600 to 750 gallons per hour, or 80.2 to 100 ft³ per hour. Dividing this rate by the surface area gives an initial K_{sat} of 9.8 to 12.3 inches per hour.

K_{sat} Determination Option 2: Small Scale Pilot Infiltration Test (PIT)

A small-scale PIT can be substituted for <u>Ksat Determination Option 1: Large Scale Pilot Infiltration</u> <u>Test (PIT)</u> in any of the following instances:

- The drainage area to the infiltration BMP is less than 1 acre.
- The testing is for <u>BMP T7.30: Bioretention</u> or <u>BMP T5.15: Permeable Pavements</u> that either serve small drainage areas and/or are widely dispersed throughout a project site.
- The site has a high infiltration rate (>4 in/hr), making a large scale PIT difficult, and the site geo- technical investigation suggests uniform subsurface characteristics.

INFILTRATION TEST

Use the same procedures described above in <u>Ksat Determination Option 1: Large Scale Pilot Infiltra-tion Test</u> (<u>PIT</u>), with the following changes:

- The horizontal surface area of the bottom of the test pit should be 12 to 32 square feet. It may be circular or rectangular. Document the size and geometry of the test pit.
- The rigid pipe with a splash plate used to convey water to the pit may be a 3-inch diameter pipe for pits on the smaller end of the recommended surface area, or a 4-inch pipe for pits on the larger end of the recommended surface area.
- Pre-soak period: Add water to the pit so that there is standing water for at least 6 hours. Maintain the pre-soak water level at least 12 inches above the bottom of the pit.
- At the end of the pre-soak period, add water to the pit at a rate that will maintain a 6-12 inch water level above the bottom of the pit over a full hour. The depth should not exceed the pro- posed

maximum depth of water expected in the completed facility.

• Every 15 minutes, record the cumulative volume and instantaneous flow rate in gallons per minute necessary to maintain the water level at the same point (between 6 inches and 1 foot) on the measuring rod. The specific depth should be the same as the maximum designed pond- ing depth (usually 6 – 12 inches).

After one hour, turn off the water and record the rate of infiltration (the drop rate of the standing water) in inches per hour from the measuring rod data, until the pit is empty.

- A self-logging pressure sensor may also be used to determine water depth and drain-down.
- At the conclusion of testing, over-excavate the pit to see if the test water is mounded on shallow restrictive layers or if it has continued to flow deep into the subsurface. The depth of excavation varies depending on soil type and depth to the hydraulic restricting layer, and is determined by the engineer or certified soils professional. The soils professional should judge whether a mounding analysis is necessary.

APPENDIX D

CALCULATED DESIGN INFILTRATION RATE:

Site variability and number of locations tested (CF_v) - The number of locations tested must be capable of producing a picture of the subsurface conditions that fully rep- resents the conditions throughout the proposed location of the infiltration BMP. The partial correction factor used for this issue depends on the level of uncertainty that adverse subsurface conditions may occur. If the range of uncertainty is low - for example, conditions are known to be uniform through previous exploration and site geological factors

- one pilot infiltration test (or grain size analysis location) may be adequate to justify a partial correction factor at the high end of the range.

If the level of uncertainty is high, a partial correction factor near the low end of the range may be appropriate. This might be the case where the site conditions are highly variable due to conditions such as a deposit of ancient landslide debris, or buried stream channels. In these cases, even with many explorations and several pilot infiltration tests (or several grain size test locations), the level of uncertainty may still be high.

A partial correction factor near the low end of the range could be assigned where conditions have a more typical variability, but few explorations and only one pilot infiltration test (or one grain size analysis location) is conducted. That is, the number of explorations and tests conducted do not match the degree of site variability anticipated.

- Uncertainty of test method (CF_t) accounts for uncertainties in the testing methods. For the full scale PIT method, CF_t = 0.75; for the small-scale PIT method, CF_t = 0.50; for smaller-scale infiltration tests such as the double-ring infiltrometer test, CF_t = 0.40; for grain size analysis, CF_t = 0.40. These values are intended to represent the difference in each test's ability to estimate the actual saturated hydraulic conductivity. The assumption is the larger the scale of the test, the more reliable the result.
- Degree of influent control to prevent siltation and bio-buildup (CF_m) Even with a pre-settling basin or a basic treatment BMP for pre-treatment, the soil's initial infiltration rate will gradually decline as more and more stormwater, with some amount of suspended material, passes through the soil profile. The maintenance schedule calls for removing sediment when the BMP is infiltrating at only 90% of its design capacity. Therefore, a correction factor, CF_m, of 0.9 is called for.

Table V-5.1: Correction Factors to be Used With In-Situ Saturated Hydraulic Conductivity Measurements to Estimate Design Rates

Issue	Partial Correction Factor
Site variability and number of locations tested	CF _v = 0.33 to <mark>1.0</mark>
Test Method	
Large-scale PIT	[™] CF _t = 0.75
Small-scale PIT	∞ <mark>= 0.50</mark>
Other small-scale (e.g. Double ring, falling head)	2 = 0.40
Grain Size Method	2 = 0.40
Degree of influent control to prevent siltation and bio-buildup	CF _m <mark>= 0.9</mark>

Total Correction Factor, $CF_T = CF_v \times CF_t \times CF_m$

Total Correction Factor, $CF_T = 1.0 \times 0.5 \times 0.9$

CF_T = 0.45