

City of Puyallup Development & Permitting Services ISSUED PERMIT	
Building	Planning
Engineering	Public Works
Fire	Traffic

# SPRINX

## FIRE PROTECTION

EST. 1999

2709 Jahn Ave NW, Suite H2, Gig Harbor WA 98335

Ph. (253) 853-7780 - [www.SprinxFire.com](http://www.SprinxFire.com)

### Hydraulic Calculations

Expires DEC 31, 25	WASHINGTON STATE CERTIFICATE OF COMPETENCY FIRE SPRINKLER SYSTEMS
Joseph G. Faulkner 9491-0699-CEG Level 3 Sprinx Fire Protection, Inc. SPRINFP011LS	
<i>Joseph G. Faulkner</i>	01/18/2025
Signature	Date

SPRINX FIRE PROTECTION INC.  
2709 JAHN AVE NW SUITE H2  
GIG HARBOR, WA 98335  
253-853-7780

Job Name : ETC Building H Area 1  
 Drawing : FP-3.0  
 Location : 2902 E PIONEER PUYALLUP, WA 98372  
 Remote Area : RA#1  
 Contract : 24-093CM  
 Data File : ETC Building H Area 1.WXF

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**HYDRAULIC CALCULATIONS**  
**for**

**JOB NAME** East Town Crossing Building H  
**Location** 2902 E PIONEER PUYALLUP, WA 98372  
**Drawing #** FP-3.0  
**Contract #** 24-093CM  
**Date** 01/06/2025

**DESIGN**

**Remote area #** RA#1  
**Remote area location** UNIT 307 - LIVING ROOM  
**Occupancy classification** RESIDENTIAL NFPA 13R  
**Density** 0.05 - Gpm/SqFt  
**Area of application** 256 - SqFt  
**Coverage/sprinkler** 256 16'X16' - SqFt  
**Type of sprinkler calculated** VIKING VK468 RESIDENTIAL PENDENT K=4.9  
**# Sprinklers calculated** 4  
**In-rack demand** N/A - GPM  
**Hose streams** N/A - GPM  
**Total water required (including hose streams)** 54.1457 - GPM @ 31.2676 - Psi  
**Type of system** WET-CPVC  
**Volume of system (dry or pre-action)** N/A - Gal

**WATER SUPPLY INFORMATION**

**Test date** 4/16/2024  
**Location** 2902 E PIONEER  
**Source of info** CITY OF PUYALLUP WATER DIVISON

**CONTRACTOR INFO** SPRINX FIRE PROTECTION  
**Address** 2709 JAHN AVE. / SUITE H2 / GIG HARBOR  
**Phone #** 253-853-7780  
**Name of designer** ALEXANDER J PARADIS  
**Authority having jurisdiction** CITY OF PUYALLUP  
**NOTES:**

# Water Supply Curve

SPRINX FIRE PROTECTION INC.  
ETC Building H Area 1

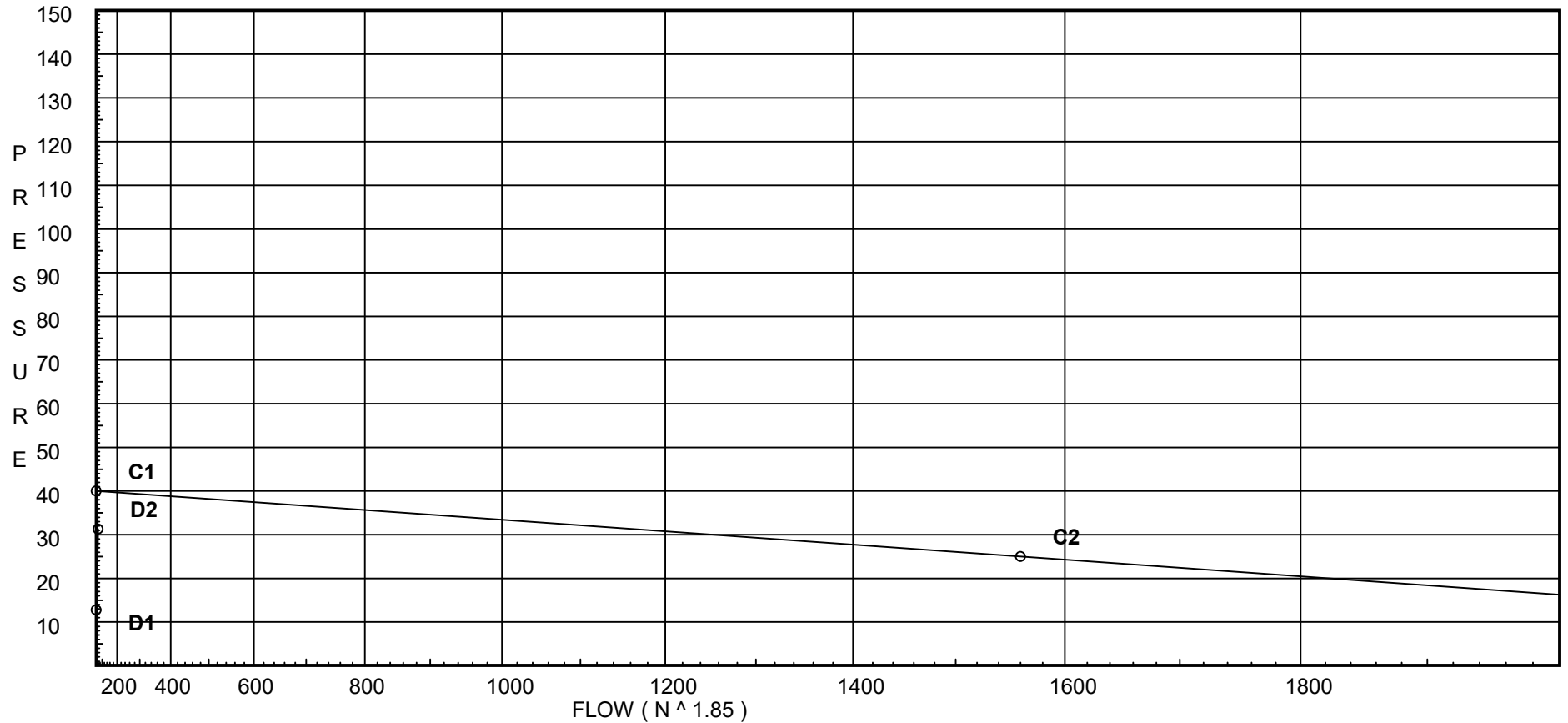
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Date 01/06/2025

### City Water Supply:

C1 - Static Pressure : 40  
C2 - Residual Pressure: 25  
C2 - Residual Flow : 1560

### Demand:

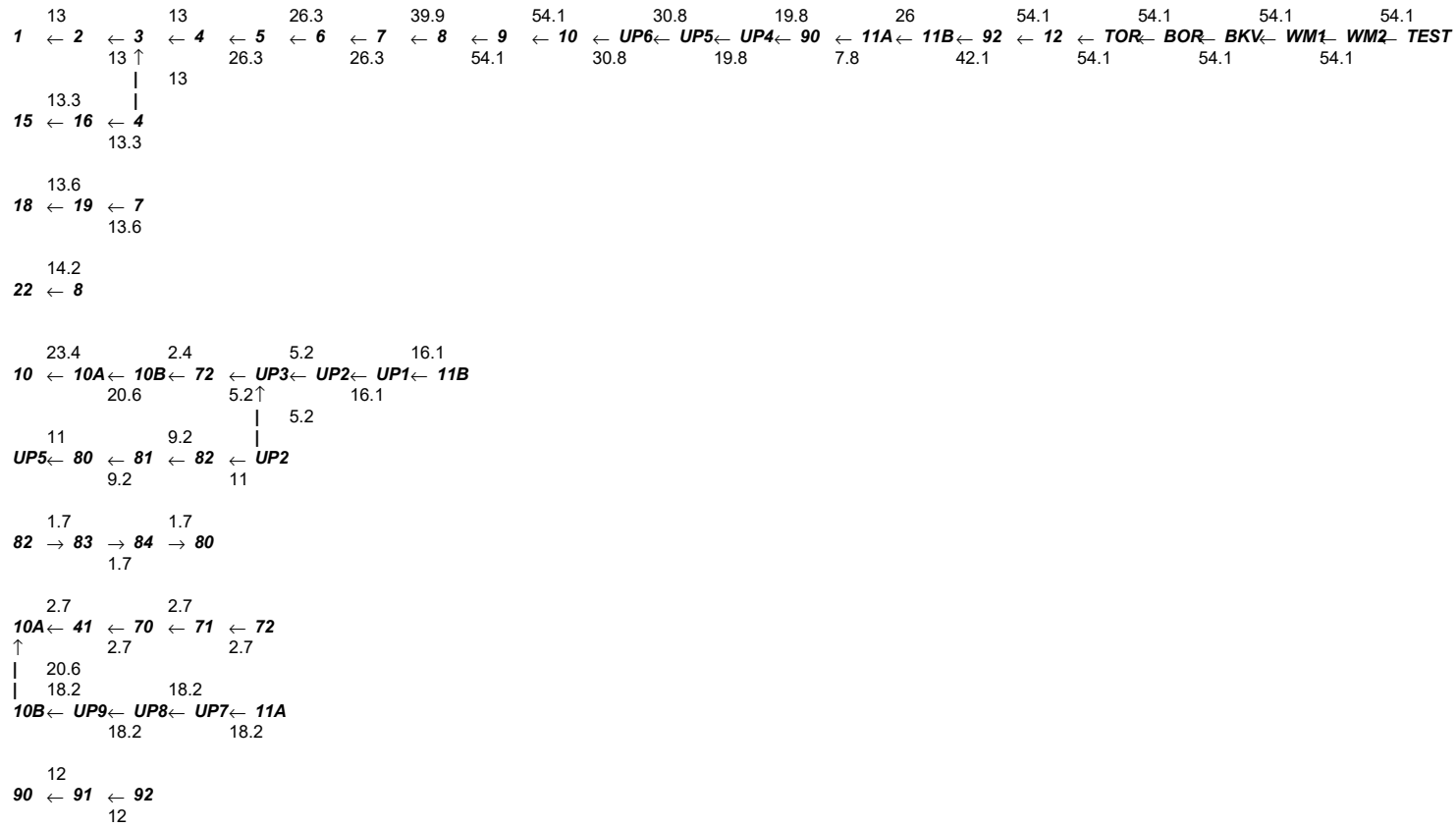
D1 - Elevation : 12.776  
D2 - System Flow : 54.146  
D2 - System Pressure : 31.268  
Hose ( Demand ) : \_\_\_\_\_  
D3 - System Demand : 54.146  
Safety Margin : 8.702



# Flow Diagram

SPRINX FIRE PROTECTION INC.  
ETC Building H Area 1

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# Fittings Used Summary

SPRINX FIRE PROTECTION INC.  
ETC Building H Area 1

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## Fitting Legend

Abbrev.	Name	1/2	3/4	1	1 1/4	1 1/2	2	2 1/2	3	3 1/2	4	5	6	8	10	12	14	16	18	20	24
B	NFPA 13 Butterfly Valve	0	0	0	0	0	6	7	10	0	12	9	10	12	19	21	0	0	0	0	0
E	NFPA 13 90' Standard Elbow	1	2	2	3	4	5	6	7	8	10	12	14	18	22	27	35	40	45	50	61
G	NFPA 13 Gate Valve	0	0	0	0	0	1	1	1	1	2	2	3	4	5	6	7	8	10	11	13
N *	CPVC 90'EI Harvel-Spears		7	7	8	9	11	12	13	0	0	0	0	0	0	0	0	0	0	0	0
O *	CPVC Tee - Branch	3	3	5	6	8	10	12	15	0	0	0	0	0	0	0	0	0	0	0	0
R *	CPVC Coupling Tee - Run	1	1	1	1	1	1	2	2	0	0	0	0	0	0	0	0	0	0	0	0
S	NFPA 13 Swing Check	0	0	5	7	9	11	14	16	19	22	27	32	45	55	65					
T	NFPA 13 90' Flow thru Tee	3	4	5	6	8	10	12	15	17	20	25	30	35	50	60	71	81	91	101	121
Ziw	Wilkins 350AST	Fitting generates a Fixed Loss Based on Flow																			

## Units Summary

Diameter Units                   Inches  
 Length Units                    Feet  
 Flow Units                       US Gallons per Minute  
 Pressure Units                 Pounds per Square Inch

Note: Fitting Legend provides equivalent pipe lengths for fittings types of various diameters. Equivalent lengths shown are standard for actual diameters of Sched 40 pipe and CFactors of 120 except as noted with \*. The fittings marked with a \* show equivalent lengths values supplied by manufacturers based on specific pipe diameters and CFactors and they require no adjustment. All values for fittings not marked with a \* will be adjusted in the calculation for CFactors of other than 120 and diameters other than Sched 40 per NFPA.

# Flow Summary - NFPA

SPRINX FIRE PROTECTION INC.  
ETC Building H Area 1

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## SUPPLY ANALYSIS

<i>Node at Source</i>	<i>Static Pressure</i>	<i>Residual Pressure</i>	<i>Flow</i>	<i>Available Pressure</i>	<i>Total Demand</i>	<i>Required Pressure</i>
TEST	40.0	25	1560.0	39.97	54.15	31.268

## NODE ANALYSIS

<i>Node Tag</i>	<i>Elevation</i>	<i>Node Type</i>	<i>Pressure at Node</i>	<i>Discharge at Node</i>		<i>Notes</i>
1	106.5	4.9	7.04	13.0	0.05	256
2	107.0		7.05			
3	107.0		7.53			
4	107.0		7.63			
5	107.0		7.7			
6	107.0		7.95			
7	107.0		7.96			
8	107.0		8.03			
9	107.0		8.15			
10	107.0		8.46			
UP6	107.0		8.56			
UP5	96.75		13.09			
UP4	86.5		17.61			
90	86.5		17.89			
11A	86.5		17.9			
11B	86.5		18.04			
92	86.5		18.45			
12	86.5		18.84			
TOR	86.5		20.12			
BOR	80.0		23.66			
BKV	77.0		31.25			
WM1	77.0		31.26			
WM2	77.0		31.27			
TEST	77.0		31.27			
15	106.5	4.9	7.35	13.29	0.05	256
16	107.0		7.31			
18	106.5	4.9	7.72	13.62	0.05	256
19	107.0		7.75			
22	105.5	4.9	8.45	14.24	0.05	256
10A	107.0		8.8			
10B	107.0		8.85			
72	107.0		8.85			
UP3	107.0		8.88			
UP2	96.75		13.32			
UP1	86.5		17.82			
80	96.75		13.19			
81	96.75		13.2			
82	96.75		13.21			
83	96.75		13.21			
84	96.75		13.2			
41	107.0		8.81			
70	107.0		8.82			

# Flow Summary - NFPA

SPRINX FIRE PROTECTION INC.  
ETC Building H Area 1

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## *NODE ANALYSIS (cont.)*

<i>Node Tag</i>	<i>Elevation</i>	<i>Node Type</i>	<i>Pressure at Node</i>	<i>Discharge at Node</i>	<i>Notes</i>
71	107.0		8.84		
UP9	107.0		8.89		
UP8	96.75		13.36		
UP7	86.5		17.87		
91	86.5		18.18		

# Final Calculations : Hazen-Williams

SPRINX FIRE PROTECTION INC.  
ETC Building H Area 1

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Date 01/06/2025

Node1 to Node2	Elev1 Elev2	K Fact	Qa Qt	Nom Act	Fitting or Eqiv	Len	Pipe Ftngs Total	CFact Pf/Ft	Pt Pe Pf	*****	Notes	*****
1 to 2	106.500 107	4.90	13.00 13.0	1 1.101	N	7.0	0.500 7.000 7.500	150 0.0307	7.040 -0.217 0.230		Vel = 4.38	
2 to 3	107 107		0.0 13.0	1 1.101	O	5.0	10.500 5.000 15.500	150 0.0307	7.053 0.0 0.476		Vel = 4.38	
3 to 4	107 107		0.0 13.0	1.25 1.394	R	1.0	9.640 1.000 10.640	150 0.0097	7.529 0.0 0.103		Vel = 2.73	
4 to 5	107 107		13.29 26.29	1.25 1.394	R	1.0	1.000 1.000 2.000	150 0.0360	7.632 0.0 0.072		Vel = 5.53	
5 to 6	107 107		0.0 26.29	1.25 1.394	R	1.0	5.750 1.000 6.750	150 0.0357	7.704 0.0 0.241		Vel = 5.53	
6 to 7	107 107		0.0 26.29	2 2.003	R	1.0	1.170 1.000 2.170	150 0.0060	7.945 0.0 0.013		Vel = 2.68	
7 to 8	107 107		13.61 39.9	2 2.003	R	1.0	4.670 1.000 5.670	150 0.0134	7.958 0.0 0.076		Vel = 4.06	
8 to 9	107 107		14.25 54.15	2 2.003	2R	2.0	2.830 2.000 4.830	150 0.0232	8.034 0.0 0.112		Vel = 5.51	
9 to 10	107 107		0.0 54.15	2 2.003	O	10.0	3.580 10.000 13.580	150 0.0233	8.146 0.0 0.316		Vel = 5.51	
10 to UP6	107 107		-23.37 30.78	2 2.003	N	11.0	1.170 11.000 12.170	150 0.0082	8.462 0.0 0.100		Vel = 3.13	
UP6 to UP5	107 96.750		0.0 30.78	2 2.003	R	1.0	10.250 1.000 11.250	150 0.0083	8.562 4.439 0.093		Vel = 3.13	
UP5 to UP4	96.750 86.500		-10.99 19.79	2 2.003	N	11.0	10.250 11.000 21.250	150 0.0036	13.094 4.439 0.077		Vel = 2.01	
UP4 to 90	86.500 86.500		0.0 19.79	2 2.003	2O 9R	20.0 9.0	49.670 29.000 78.670	150 0.0036	17.610 0.0 0.285		Vel = 2.01	
90 to 11A	86.500 86.500		-12.00 7.79	2 2.003	2R	2.0	11.580 2.000 13.580	150 0.0006	17.895 0.0 0.008		Vel = 0.79	
11A to 11B	86.500 86.500		18.22 26.01	2 2.003	R O	1.0 10.0	11.250 11.000 22.250	150 0.0060	17.903 0.0 0.134		Vel = 2.65	
11B to 92	86.500 86.500		16.14 42.15	2 2.003	5R	5.0	23.500 5.000 28.500	150 0.0146	18.037 0.0 0.417		Vel = 4.29	



# Final Calculations : Hazen-Williams

SPRINX FIRE PROTECTION INC.  
ETC Building H Area 1

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Node1 to Node2	Elev1 Elev2	K Fact	Qa Qt	Nom Act	Fitting or Eqiv	Len	Pipe Ftngs Total	CFact Pf/Ft	Pt Pe Pf	*****	Notes	*****
92 to 12	86.500 86.500		12.00 54.15	2 2.003	O	10.0	6.420 10.000 16.420	150 0.0233	18.454 0.0 0.383			Vel = 5.51
12 to TOR	86.500 86.500		0.0 54.15	2 2.003	3R 3N	3.0 33.0	19.010 36.000 55.010	150 0.0233	18.837 0.0 1.281			Vel = 5.51
TOR to BOR	86.500 80		0.0 54.15	2 2.203	B S	8.183 15.003	9.500 23.186 32.686	120 0.0222	20.118 2.815 0.725			Vel = 4.56
BOR to BKV	80 77		0.0 54.15	6 6.16	T 3E Ziw	43.037 60.252 0.0	72.080 103.289 175.369	140 0.0001	23.658 7.577 0.019		** Fixed Loss = 6.278	Vel = 0.58
BKV to WM1	77 77		0.0 54.15	6 6.16	T G	43.037 4.304	40.000 47.341 87.341	140 0.0001	31.254 0.0 0.010			Vel = 0.58
WM1 to WM2	77 77		0.0 54.15	8 8.27	T	55.354	75.000 55.354 130.354	140 0	31.264 0.0 0.004			Vel = 0.32
WM2 to TEST	77 77		0.0 54.15	8 8.27			4.000 4.000	140 0	31.268 0.0 0.0			Vel = 0.32
TEST			0.0 54.15						31.268		K Factor = 9.68	
15 to 16	106.500 107	4.90	13.29 13.29	1 1.101	O	5.0	0.500 5.000 5.500	150 0.0320	7.354 -0.217 0.176			Vel = 4.48
16 to 4	107 107		0.0 13.29	1 1.101	O	5.0	5.000 5.000 10.000	150 0.0319	7.313 0.0 0.319			Vel = 4.48
4			0.0 13.29						7.632		K Factor = 4.81	
18 to 19	106.500 107	4.90	13.62 13.62	1 1.101	N	7.0	0.500 7.000 7.500	150 0.0335	7.721 -0.217 0.251			Vel = 4.59
19 to 7	107 107		0.0 13.62	1 1.101	O	5.0	1.100 5.000 6.100	150 0.0333	7.755 0.0 0.203			Vel = 4.59
7			0.0 13.62						7.958		K Factor = 4.83	
22 to 8	105.500 107	4.90	14.24 14.24	1 1.101	O	5.0	1.500 5.000 6.500	150 0.0365	8.447 -0.650 0.237			Vel = 4.80
8			0.0 14.24						8.034		K Factor = 5.02	
10 to 10A	107 107		23.37 23.37	2 2.003	9R O	9.0 10.0	49.670 19.000 68.670	150 0.0049	8.462 0.0 0.338			Vel = 2.38

# Final Calculations : Hazen-Williams

SPRINX FIRE PROTECTION INC.  
ETC Building H Area 1

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Node1 to Node2	Elev1 Elev2	K Fact	Qa Qt	Nom Act	Fitting or Eqiv	Len	Pipe Ftngs Total	CFact Pf/Ft	Pt Pe Pf	*****	Notes	*****
10A to 10B	107 107		-2.73 20.64	2 2.003	2R	2.0	11.580 2.000 13.580	150 0.0040	8.800 0.0 0.054			Vel = 2.10
10B to 72	107 107		-18.21 2.43	2 2.003	2R	2.0	11.170 2.000 13.170	150 0.0001	8.854 0.0 0.001			Vel = 0.25
72 to UP3	107 107		2.73 5.16	2 2.003	8R 2O N	8.0 20.0 11.0	50.830 39.000 89.830	150 0.0003	8.855 0.0 0.027			Vel = 0.53
UP3 to UP2	107 96.750		0.0 5.16	2 2.003	R	1.0	10.250 1.000 11.250	150 0.0003	8.882 4.439 0.003			Vel = 0.53
UP2 to UP1	96.750 86.500		10.98 16.14	2 2.003	N	11.0	10.250 11.000 21.250	150 0.0025	13.324 4.439 0.053			Vel = 1.64
UP1 to 11B	86.500 86.500		0.0 16.14	2 2.003	8R 3O	8.0 30.0	50.830 38.000 88.830	150 0.0025	17.816 0.0 0.221			Vel = 1.64
11B			0.0 16.14						18.037			K Factor = 3.80
UP5 to 80	96.750 96.750		10.99 10.99	2 2.003	2O 9R	20.0 9.0	50.830 29.000 79.830	150 0.0012	13.094 0.0 0.097			Vel = 1.12
80 to 81	96.750 96.750		-1.75 9.24	2 2.003	2R	2.0	11.580 2.000 13.580	150 0.0009	13.191 0.0 0.012			Vel = 0.94
81 to 82	96.750 96.750		0.0 9.24	2 2.003	2R	2.0	11.250 2.000 13.250	150 0.0009	13.203 0.0 0.012			Vel = 0.94
82 to UP2	96.750 96.750		1.75 10.99	2 2.003	8R 2O N	8.0 20.0 11.0	51.000 39.000 90.000	150 0.0012	13.215 0.0 0.109			Vel = 1.12
UP2			0.0 10.99						13.324			K Factor = 3.01
82 to 83	96.750 96.750		-1.75 -1.75	1.25 1.394	4R O	4.0 6.0	23.500 10.000 33.500	150 -0.0002	13.215 0.0 -0.008			Vel = 0.37
83 to 84	96.750 96.750		0.0 -1.75	1.25 1.394	4R O	4.0 6.0	22.830 10.000 32.830	150 -0.0002	13.207 0.0 -0.008			Vel = 0.37
84 to 80	96.750 96.750		0.0 -1.75	1.25 1.394	4R O	4.0 6.0	23.500 10.000 33.500	150 -0.0002	13.199 0.0 -0.008			Vel = 0.37
80			0.0 -1.75						13.191			K Factor = -0.48
10A to 41	107 107		2.73 2.73	1.25 1.394	4R	4.0	19.000 4.000 23.000	150 0.0006	8.800 0.0 0.013			Vel = 0.57

# Final Calculations : Hazen-Williams

SPRINX FIRE PROTECTION INC.  
ETC Building H Area 1

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Date 01/06/2025

Node1 to Node2	Elev1 Elev2	K Fact	Qa Qt	Nom Act	Fitting or Eqiv	Len	Pipe Ftngs Total	CFact Pf/Ft	Pt Pe Pf	*****	Notes	*****
41 to 70	107 107		0.0 2.73	1.25 1.394	O	6.0	4.500 6.000 10.500	150 0.0006	8.813 0.0 0.006		Vel = 0.57	
70 to 71	107 107		0.0 2.73	1.25 1.394	4R O	4.0 6.0	22.830 10.000 32.830	150 0.0005	8.819 0.0 0.017		Vel = 0.57	
71 to 72	107 107		0.0 2.73	1.25 1.394	4R O	4.0 6.0	23.500 10.000 33.500	150 0.0006	8.836 0.0 0.019		Vel = 0.57	
72			0.0 2.73						8.855		K Factor = 0.92	
10B to UP9	107 107		18.21 18.21	2 2.003	N	11.0	0.670 11.000 11.670	150 0.0031	8.854 0.0 0.036		Vel = 1.85	
UP9 to UP8	107 96.750		0.0 18.21	2 2.003	R	1.0	10.250 1.000 11.250	150 0.0031	8.890 4.439 0.035		Vel = 1.85	
UP8 to UP7	96.750 86.500		0.0 18.21	2 2.003	N	11.0	10.250 11.000 21.250	150 0.0031	13.364 4.439 0.066		Vel = 1.85	
UP7 to 11A	86.500 86.500		0.0 18.21	2 2.003	O	10.0	1.000 10.000 11.000	150 0.0031	17.869 0.0 0.034		Vel = 1.85	
11A			0.0 18.21						17.903		K Factor = 4.30	
90 to 91	86.500 86.500		12.00 12.0	1.25 1.394	4R O	4.0 6.0	24.000 10.000 34.000	150 0.0084	17.895 0.0 0.284		Vel = 2.52	
91 to 92	86.500 86.500		0.0 12.0	1.25 1.394	4R O	4.0 6.0	22.830 10.000 32.830	150 0.0084	18.179 0.0 0.275		Vel = 2.52	
92			0.0 12.00						18.454		K Factor = 2.79	

# SPRINX

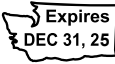
## FIRE PROTECTION

EST. 1999

2709 Jahn Ave NW, Suite H2, Gig Harbor WA 98335

Ph. (253) 853-7780— [www.SprinxFire.com](http://www.SprinxFire.com)

### Hydraulic Calculations

 Expires DEC 31, 25	<b>WASHINGTON STATE CERTIFICATE OF COMPETENCY FIRE SPRINKLER SYSTEMS</b>
Joseph G. Faulkner 9491-0699-CEG Level 3 Sprinx Fire Protection, Inc. SPRINF011LS	
<i>Joseph G. Faulkner</i> Signature	01/18/2025 Date

SPRINX FIRE PROTECTION INC.  
2709 JAHN AVE NW SUITE H2  
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Job Name	: ETC Building H Area 2
Drawing	: FP-3.0
Location	: 2902 E PIONEER PUYALLUP, WA 98372
Remote Area	: RA#2
Contract	: 24-093CM
Data File	: ETC Building H Area 2.WXF

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**HYDRAULIC CALCULATIONS**  
*for*

**JOB NAME** East Town Crossing Building H  
**Location** 2902 E PIONEER PUYALLUP, WA 98372  
**Drawing #** FP-3.0  
**Contract #** 24-093CM  
**Date** 01/06/2025

**DESIGN**

**Remote area #** RA#2  
**Remote area location** UNIT 307 - BEDROOM  
**Occupancy classification** RESIDENTIAL NFPA 13R  
**Density** 0.05 - Gpm/SqFt  
**Area of application** 324 - SqFt  
**Coverage/sprinkler** 324 - SqFt  
**Type of sprinkler calculated** VIKING VK468 RESIDENTIAL PENDENT K=4.9  
**# Sprinklers calculated** 1  
**In-rack demand** N/A - GPM  
**Hose streams** N/A - GPM  
**Total water required (including hose streams)** 17.0024 - GPM @ 33.3682 - Psi  
**Type of system** WET-CPVC  
**Volume of system (dry or pre-action)** N/A - Gal

**WATER SUPPLY INFORMATION**

**Test date** 4/16/2024  
**Location** 2902 E PIONEER  
**Source of info** SPRINX FIRE PROTECTION

**CONTRACTOR INFO** SPRINX FIRE PROTECTION  
**Address** 2709 JAHN AVE. / SUITE H2 / GIG HARBOR  
**Phone #** 253-853-7780  
**Name of designer** ALEXANDER J PARADIS  
**Authority having jurisdiction** CITY OF PUYALLUP  
**NOTES:**

# Water Supply Curve

SPRINX FIRE PROTECTION INC.  
ETC Building H Area 2

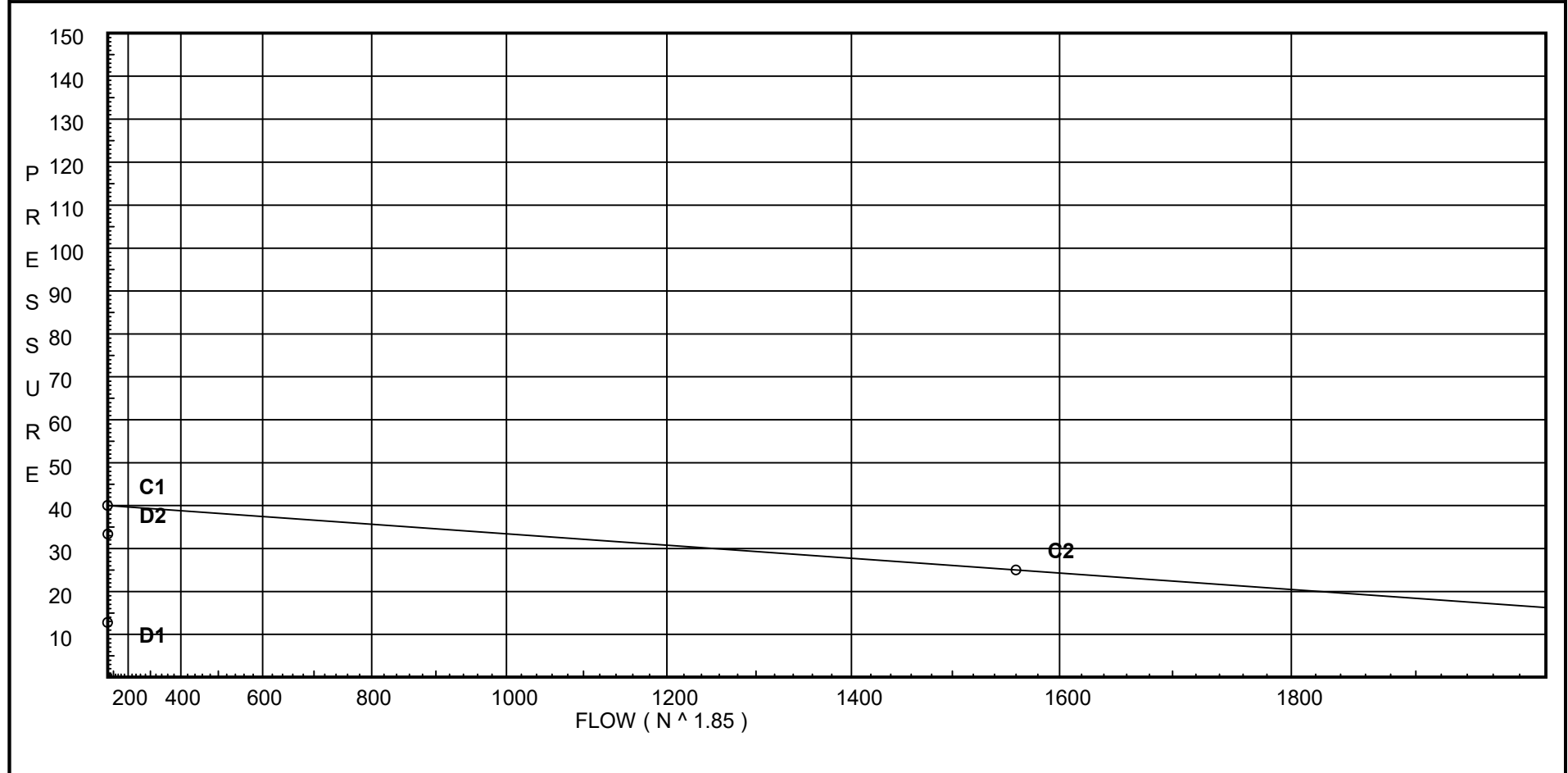
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Date 01/06/2025

### City Water Supply:

C1 - Static Pressure : 40  
C2 - Residual Pressure: 25  
C2 - Residual Flow : 1560

### Demand:

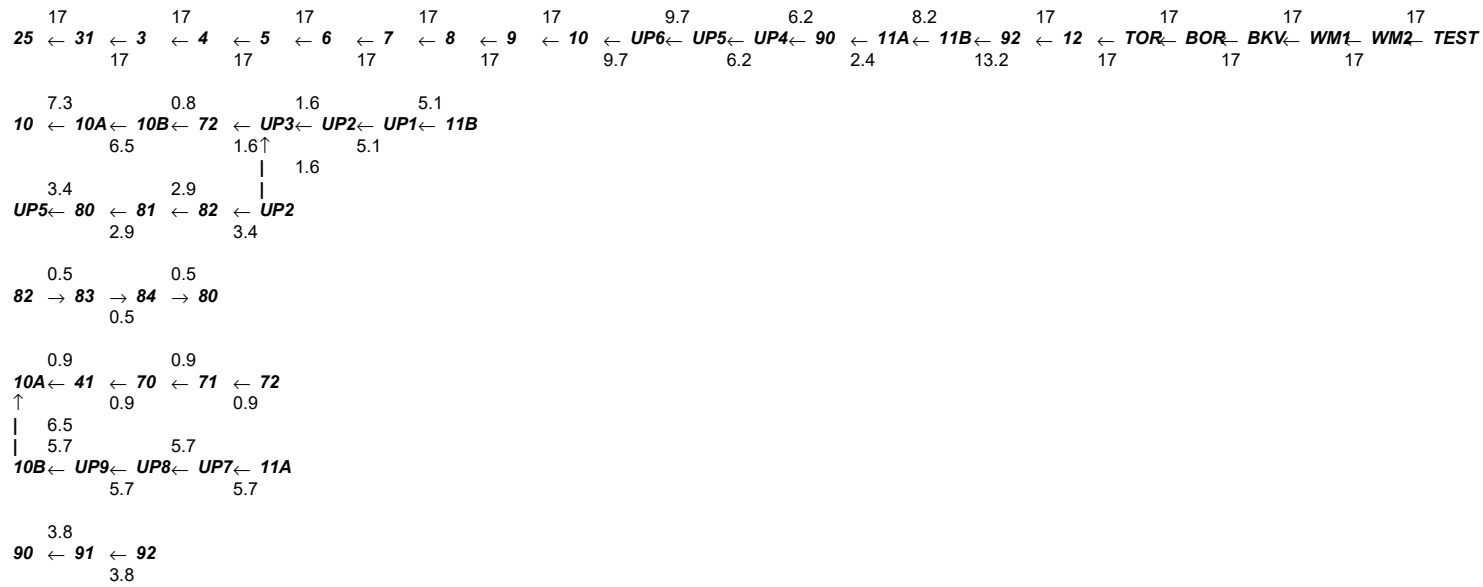
D1 - Elevation : 12.776  
D2 - System Flow : 17.002  
D2 - System Pressure : 33.368  
Hose ( Demand ) : \_\_\_\_\_  
D3 - System Demand : 17.002  
Safety Margin : 6.628



# Flow Diagram

SPRINX FIRE PROTECTION INC.  
ETC Building H Area 2

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# Fittings Used Summary

SPRINX FIRE PROTECTION INC.  
ETC Building H Area 2

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## Fitting Legend

Abbrev.	Name	1/2	3/4	1	1 1/4	1 1/2	2	2 1/2	3	3 1/2	4	5	6	8	10	12	14	16	18	20	24
B	NFPA 13 Butterfly Valve	0	0	0	0	0	6	7	10	0	12	9	10	12	19	21	0	0	0	0	0
E	NFPA 13 90' Standard Elbow	1	2	2	3	4	5	6	7	8	10	12	14	18	22	27	35	40	45	50	61
G	NFPA 13 Gate Valve	0	0	0	0	0	1	1	1	1	2	2	3	4	5	6	7	8	10	11	13
N *	CPVC 90'EI Harvel-Spears		7	7	8	9	11	12	13	0	0	0	0	0	0	0	0	0	0	0	0
O *	CPVC Tee - Branch	3	3	5	6	8	10	12	15	0	0	0	0	0	0	0	0	0	0	0	0
R *	CPVC Coupling Tee - Run	1	1	1	1	1	1	2	2	0	0	0	0	0	0	0	0	0	0	0	0
S	NFPA 13 Swing Check	0	0	5	7	9	11	14	16	19	22	27	32	45	55	65					
T	NFPA 13 90' Flow thru Tee	3	4	5	6	8	10	12	15	17	20	25	30	35	50	60	71	81	91	101	121
Ziw	Wilkins 350AST	Fitting generates a Fixed Loss Based on Flow																			

## Units Summary

Diameter Units                   Inches  
Length Units                       Feet  
Flow Units                         US Gallons per Minute  
Pressure Units                   Pounds per Square Inch

Note: Fitting Legend provides equivalent pipe lengths for fittings types of various diameters. Equivalent lengths shown are standard for actual diameters of Sched 40 pipe and CFactors of 120 except as noted with \*. The fittings marked with a \* show equivalent lengths values supplied by manufacturers based on specific pipe diameters and CFactors and they require no adjustment. All values for fittings not marked with a \* will be adjusted in the calculation for CFactors of other than 120 and diameters other than Sched 40 per NFPA.



# Flow Summary - NFPA

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## SUPPLY ANALYSIS

<i>Node at Source</i>	<i>Static Pressure</i>	<i>Residual Pressure</i>	<i>Flow</i>	<i>Available Pressure</i>	<i>Total Demand</i>	<i>Required Pressure</i>
TEST	40.0	25	1560.0	39.996	17.0	33.368

## NODE ANALYSIS

<i>Node Tag</i>	<i>Elevation</i>	<i>Node Type</i>	<i>Pressure at Node</i>	<i>Discharge at Node</i>	<i>Notes</i>
25	106.5	4.9	12.04	17.0	0.05 324
31	107.0		12.1		
3	107.0		12.81		
4	107.0		12.98		
5	107.0		13.01		
6	107.0		13.12		
7	107.0		13.12		
8	107.0		13.14		
9	107.0		13.15		
10	107.0		13.19		
UP6	107.0		13.2		
UP5	96.75		17.65		
UP4	86.5		22.1		
90	86.5		22.13		
11A	86.5		22.13		
11B	86.5		22.15		
92	86.5		22.2		
12	86.5		22.24		
TOR	86.5		22.39		
BOR	80.0		25.29		
BKV	77.0		33.37		
WM1	77.0		33.37		
WM2	77.0		33.37		
TEST	77.0		33.37		
10A	107.0		13.23		
10B	107.0		13.23		
72	107.0		13.23		
UP3	107.0		13.24		
UP2	96.75		17.68		
UP1	86.5		22.12		
80	96.75		17.66		
81	96.75		17.66		
82	96.75		17.66		
83	96.75		17.66		
84	96.75		17.66		
41	107.0		13.23		
70	107.0		13.23		
71	107.0		13.23		
UP9	107.0		13.24		
UP8	96.75		17.68		
UP7	86.5		22.13		
91	86.5		22.16		

# Flow Summary - NFPA

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## *NODE ANALYSIS (cont.)*

<i>Node Tag</i>	<i>Elevation</i>	<i>Node Type</i>	<i>Pressure at Node</i>	<i>Discharge at Node</i>	<i>Notes</i>
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# Final Calculations : Hazen-Williams

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Node1 to Node2	Elev1 Elev2	K Fact	Qa Qt	Nom Act	Fitting or Eqiv	Len	Pipe Ftngs Total	CFact Pf/Ft	Pt Pe Pf	*****	Notes	*****
25 to 31	106.500 107	4.90	17.00 17.0	1 1.101	O	5.0	0.500 5.000 5.500	150 0.0505	12.040 -0.217 0.278		Vel = 5.73	
31 to 3	107 107		0.0 17.0	1 1.101	N R	7.0 1.0	6.000 8.000 14.000	150 0.0504	12.101 0.0 0.705		Vel = 5.73	
3 to 4	107 107		0.0 17.0	1.25 1.394	R	1.0	9.640 1.000 10.640	150 0.0160	12.806 0.0 0.170		Vel = 3.57	
4 to 5	107 107		0.0 17.0	1.25 1.394	R	1.0	1.000 1.000 2.000	150 0.0160	12.976 0.0 0.032		Vel = 3.57	
5 to 6	107 107		0.0 17.0	1.25 1.394	R	1.0	5.750 1.000 6.750	150 0.0160	13.008 0.0 0.108		Vel = 3.57	
6 to 7	107 107		0.0 17.0	2 2.003	R	1.0	1.170 1.000 2.170	150 0.0028	13.116 0.0 0.006		Vel = 1.73	
7 to 8	107 107		0.0 17.0	2 2.003	R	1.0	4.670 1.000 5.670	150 0.0026	13.122 0.0 0.015		Vel = 1.73	
8 to 9	107 107		0.0 17.0	2 2.003	2R	2.0	2.830 2.000 4.830	150 0.0027	13.137 0.0 0.013		Vel = 1.73	
9 to 10	107 107		0.0 17.0	2 2.003	O	10.0	3.580 10.000 13.580	150 0.0027	13.150 0.0 0.037		Vel = 1.73	
10 to UP6	107 107		-7.34 9.66	2 2.003	N	11.0	1.170 11.000 12.170	150 0.0010	13.187 0.0 0.012		Vel = 0.98	
UP6 to UP5	107 96.750		0.0 9.66	2 2.003	R	1.0	10.250 1.000 11.250	150 0.0010	13.199 4.439 0.011		Vel = 0.98	
UP5 to UP4	96.750 86.500		-3.45 6.21	2 2.003	N	11.0	10.250 11.000 21.250	150 0.0004	17.649 4.439 0.009		Vel = 0.63	
UP4 to 90	86.500 86.500		0.0 6.21	2 2.003	2O 9R	20.0 9.0	49.670 29.000 78.670	150 0.0004	22.097 0.0 0.034		Vel = 0.63	
90 to 11A	86.500 86.500		-3.76 2.45	2 2.003	2R	2.0	11.580 2.000 13.580	150 0.0001	22.131 0.0 0.001		Vel = 0.25	
11A to 11B	86.500 86.500		5.72 8.17	2 2.003	R O	1.0 10.0	11.250 11.000 22.250	150 0.0007	22.132 0.0 0.016		Vel = 0.83	
11B to 92	86.500 86.500		5.06 13.23	2 2.003	5R	5.0	23.500 5.000 28.500	150 0.0017	22.148 0.0 0.048		Vel = 1.35	

# Final Calculations : Hazen-Williams

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Node1 to Node2	Elev1 Elev2	K Fact	Qa Qt	Nom Act	Fitting or Eqiv	Len	Pipe Ftngs Total	CFact Pf/Ft	Pt Pe Pf	*****	Notes	*****
92 to 12	86.500 86.500		3.77 17.0	2 2.003	O	10.0	6.420 10.000 16.420	150 0.0027	22.196 0.0 0.045			Vel = 1.73
12 to TOR	86.500 86.500		0.0 17.0	2 2.003	3R 3N	3.0 33.0	19.010 36.000 55.010	150 0.0027	22.241 0.0 0.151			Vel = 1.73
TOR to BOR	86.500 80		0.0 17.0	2 2.203	B S	8.183 15.003	9.500 23.186 32.686	120 0.0026	22.392 2.815 0.085			Vel = 1.43
BOR to BKV	80 77		0.0 17.0	6 6.16	T 3E Zw	43.037 60.252 0.0	72.080 103.289 175.369	140 0	25.292 8.073 0.002		** Fixed Loss = 6.773	Vel = 0.18
BKV to WM1	77 77		0.0 17.0	6 6.16	T G	43.037 4.304	40.000 47.341 87.341	140 0	33.367 0.0 0.001			Vel = 0.18
WM1 to WM2	77 77		0.0 17.0	8 8.27	T	55.354	75.000 55.354 130.354	140 0	33.368 0.0 0.0			Vel = 0.10
WM2 to TEST	77 77		0.0 17.0	8 8.27			4.000 4.000	140 0	33.368 0.0 0.0			Vel = 0.10
TEST			0.0 17.00						33.368		K Factor = 2.94	
10 to 10A	107 107		7.34 7.34	2 2.003	9R O	9.0 10.0	49.670 19.000 68.670	150 0.0006	13.187 0.0 0.040			Vel = 0.75
10A to 10B	107 107		-0.86 6.48	2 2.003	2R	2.0	11.580 2.000 13.580	150 0.0004	13.227 0.0 0.006			Vel = 0.66
10B to 72	107 107		-5.72 0.76	2 2.003	2R	2.0	11.170 2.000 13.170	150 0	13.233 0.0 0.0			Vel = 0.08
72 to UP3	107 107		0.86 1.62	2 2.003	8R 2O N	8.0 20.0 11.0	50.830 39.000 89.830	150 0	13.233 0.0 0.003			Vel = 0.16
UP3 to UP2	107 96.750		0.0 1.62	2 2.003	R	1.0	10.250 1.000 11.250	150 0.0001	13.236 4.439 0.001			Vel = 0.16
UP2 to UP1	96.750 86.500		3.45 5.07	2 2.003	N	11.0	10.250 11.000 21.250	150 0.0003	17.676 4.439 0.007			Vel = 0.52
UP1 to 11B	86.500 86.500		0.0 5.07	2 2.003	8R 3O	8.0 30.0	50.830 38.000 88.830	150 0.0003	22.122 0.0 0.026			Vel = 0.52
11B			0.0 5.07						22.148		K Factor = 1.08	
UP5 to 80	96.750 96.750		3.45 3.45	2 2.003	2O 9R	20.0 9.0	50.830 29.000 79.830	150 0.0001	17.649 0.0 0.011			Vel = 0.35

# Final Calculations : Hazen-Williams

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Node1 to Node2	Elev1 Elev2	K Fact	Qa Qt	Nom Act	Fitting or Eqiv	Len	Pipe Ftngs Total	CFact Pf/Ft	Pt Pe Pf	*****	Notes	*****
80 to 81	96.750 96.750		-0.55 2.9	2 2.003	2R	2.0	11.580 2.000 13.580	150 0.0001	17.660 0.0 0.002			Vel = 0.30
81 to 82	96.750 96.750		0.0 2.9	2 2.003	2R	2.0	11.250 2.000 13.250	150 0.0001	17.662 0.0 0.001			Vel = 0.30
82 to UP2	96.750 96.750		0.55 3.45	2 2.003	8R 2O N	8.0 20.0 11.0	51.000 39.000 90.000	150 0.0001	17.663 0.0 0.013			Vel = 0.35
UP2			0.0 3.45						17.676			K Factor = 0.82
82 to 83	96.750 96.750		-0.55 -0.55	1.25 1.394	4R O	4.0 6.0	23.500 10.000 33.500	150 0	17.663 0.0 -0.001			Vel = 0.12
83 to 84	96.750 96.750		0.0 -0.55	1.25 1.394	4R O	4.0 6.0	22.830 10.000 32.830	150 0	17.662 0.0 0.0			Vel = 0.12
84 to 80	96.750 96.750		0.0 -0.55	1.25 1.394	4R O	4.0 6.0	23.500 10.000 33.500	150 -0.0001	17.662 0.0 -0.002			Vel = 0.12
80			0.0 -0.55						17.660			K Factor = -0.13
10A to 41	107 107		0.86 0.86	1.25 1.394	4R	4.0	19.000 4.000 23.000	150 0	13.227 0.0 0.001			Vel = 0.18
41 to 70	107 107		0.0 0.86	1.25 1.394	O	6.0	4.500 6.000 10.500	150 0.0001	13.228 0.0 0.001			Vel = 0.18
70 to 71	107 107		0.0 0.86	1.25 1.394	4R O	4.0 6.0	22.830 10.000 32.830	150 0.0001	13.229 0.0 0.002			Vel = 0.18
71 to 72	107 107		0.0 0.86	1.25 1.394	4R O	4.0 6.0	23.500 10.000 33.500	150 0.0001	13.231 0.0 0.002			Vel = 0.18
72			0.0 0.86						13.233			K Factor = 0.24
10B to UP9	107 107		5.72 5.72	2 2.003	N	11.0	0.670 11.000 11.670	150 0.0004	13.233 0.0 0.005			Vel = 0.58
UP9 to UP8	107 96.750		0.0 5.72	2 2.003	R	1.0	10.250 1.000 11.250	150 0.0004	13.238 4.439 0.004			Vel = 0.58
UP8 to UP7	96.750 86.500		0.0 5.72	2 2.003	N	11.0	10.250 11.000 21.250	150 0.0004	17.681 4.439 0.008			Vel = 0.58
UP7 to 11A	86.500 86.500		0.0 5.72	2 2.003	O	10.0	1.000 10.000 11.000	150 0.0004	22.128 0.0 0.004			Vel = 0.58

# Final Calculations : Hazen-Williams

SPRINX FIRE PROTECTION INC.  
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Node1 to Node2	Elev1 Elev2	K Fact	Qa Qt	Nom Act	Fitting or Eqiv	Len	Pipe Ftngs Total	CFact Pf/Ft	Pt Pe Pf	*****	Notes	*****
11A			0.0 5.72						22.132		K Factor = 1.22	
90 to 91	86.500 86.500		3.77	1.25 1.394	4R O	4.0 6.0	24.000 10.000 34.000	150 0.0010	22.131 0.0 0.033		Vel = 0.79	
91 to 92	86.500 86.500		0.0 3.77	1.25 1.394	4R O	4.0 6.0	22.830 10.000 32.830	150 0.0010	22.164 0.0 0.032		Vel = 0.79	
92			0.0 3.77						22.196		K Factor = 0.80	

# SPRINX

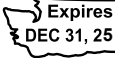

## FIRE PROTECTION

EST. 1999

2709 Jahn Ave NW, Suite H2, Gig Harbor WA 98335

Ph. (253) 853-7780- [www.SprinxFire.com](http://www.SprinxFire.com)

### Hydraulic Calculations

 Expires DEC 31, 25	<b>WASHINGTON STATE CERTIFICATE OF COMPETENCY FIRE SPRINKLER SYSTEMS</b>
Joseph G. Faulkner 9491-0699-CEG Level 3 Sprinx Fire Protection, Inc. SPRINF011LS	
 Signature	01/18/2025 Date

SPRINX FIRE PROTECTION INC.  
2709 JAHN AVE NW SUITE H2  
GIG HARBOR, WA 98335  
253-853-7780

Job Name : ETC Building H Area 3  
Drawing : FP-3.0  
Location : 2902 E PIONEER PUYALLUP, WA 98372  
Remote Area : RA#3  
Contract : 24-093CM  
Data File : ETC Building H Area 3.WXF

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**HYDRAULIC CALCULATIONS**  
**for**

**JOB NAME** East Town Crossing Building H  
**Location** 2902 E PIONEER PUYALLUP, WA 98372  
**Drawing #** FP-3.0  
**Contract #** 24-093CM  
**Date** 01/06/2025

**DESIGN**

**Remote area #** RA#3  
**Remote area location** STAIRWELL  
**Occupancy classification** LIGHT HAZARD  
**Density** 0.10 - Gpm/SqFt  
**Area of application** 273 - SqFt  
**Coverage/sprinkler** 4 HEADS - SqFt  
**Type of sprinkler calculated** VIKING VK178 QR CHROME DRY HORIZONTAL SIDEWALL  
**# Sprinklers calculated** 4  
**In-rack demand** N/A - GPM  
**Hose streams** N/A - GPM  
**Total water required (including hose streams)** 62.9317 - GPM @ 32.9567 - Psi  
**Type of system** WET-CPVC  
**Volume of system (dry or pre-action)** N/A - Gal

**WATER SUPPLY INFORMATION**

**Test date** 4/16/2024  
**Location** 2902 E PIONEER  
**Source of info** CITY OF PUYALLUP WATER DIVISON

**CONTRACTOR INFO** SPRINX FIRE PROTECTION  
**Address** 2709 JAHN AVE. / SUITE H2 / GIG HARBOR  
**Phone #** 253-853-7780  
**Name of designer** ALEXANDER J PARADIS  
**Authority having jurisdiction** CITY OF PUYALLUP  
**NOTES:**



# Water Supply Curve

SPRINX FIRE PROTECTION INC.  
ETC Building H Area 3

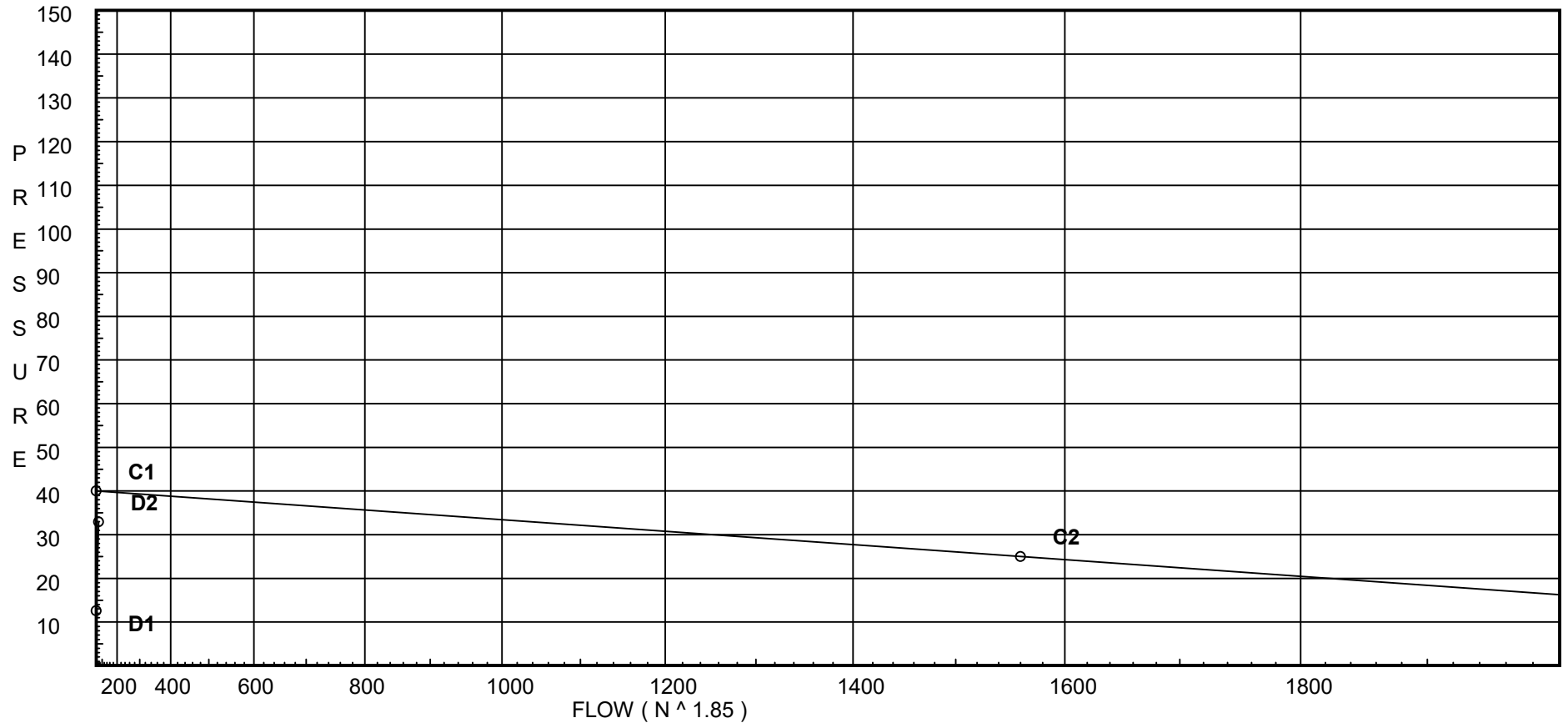
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## City Water Supply:

C1 - Static Pressure : 40  
C2 - Residual Pressure: 25  
C2 - Residual Flow : 1560

## Demand:

D1 - Elevation : 12.560  
D2 - System Flow : 62.932  
D2 - System Pressure : 32.957  
Hose ( Demand ) : \_\_\_\_\_  
D3 - System Demand : 62.932  
Safety Margin : 7.004



# Flow Diagram

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$30 \leftarrow 31 \leftarrow 3 \leftarrow 4 \leftarrow 5 \leftarrow 6 \leftarrow 7 \leftarrow 8 \leftarrow 9 \leftarrow 10 \leftarrow UP6 \leftarrow UP5 \leftarrow UP4 \leftarrow 90 \leftarrow 11A \leftarrow 11B \leftarrow 92 \leftarrow 12 \leftarrow TOR \leftarrow BOR \leftarrow BKV \leftarrow WM1 \leftarrow WM2 \leftarrow TEST$   
 14.8 14.8 14.8 30.1 46.4 29.6 20 30.1 62.9 62.9 62.9 62.9  
 14.8 14.8 30.1 30.1 29.6 20 6.1 49 62.9 62.9 62.9

16.5  
 $40 \leftarrow 41$

15.3  
 $50 \leftarrow 6$

16.3  
 $60 \leftarrow 9$

$10 \leftarrow 10A \leftarrow 10B \leftarrow 72 \leftarrow UP3 \leftarrow UP2 \leftarrow UP1 \leftarrow 11B$   
 16.8 2.6 9.3 19  
 26.6 9.3↑ 19  
 9.6 8.1 9.3  
 $UP5 \leftarrow 80 \leftarrow 81 \leftarrow 82 \leftarrow UP2$   
 8.1 8.1 9.6

$82 \rightarrow 83 \rightarrow 84 \rightarrow 80$   
 1.5 1.5  
 1.5

$10A \rightarrow 41 \leftarrow 70 \leftarrow 71 \leftarrow 72$   
 ↑ 9.8 6.7 6.7  
 | 26.6  
 | 24 24  
 $10B \leftarrow UP9 \leftarrow UP8 \leftarrow UP7 \leftarrow 11A$   
 24 24

$90 \leftarrow 91 \leftarrow 92$   
 13.9  
 13.9

# Fittings Used Summary

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## Fitting Legend

Abbrev.	Name	1/2	3/4	1	1 1/4	1 1/2	2	2 1/2	3	3 1/2	4	5	6	8	10	12	14	16	18	20	24
B	NFPA 13 Butterfly Valve	0	0	0	0	0	6	7	10	0	12	9	10	12	19	21	0	0	0	0	0
E	NFPA 13 90' Standard Elbow	1	2	2	3	4	5	6	7	8	10	12	14	18	22	27	35	40	45	50	61
G	NFPA 13 Gate Valve	0	0	0	0	0	1	1	1	1	2	2	3	4	5	6	7	8	10	11	13
N *	CPVC 90'EI Harvel-Spears		7	7	8	9	11	12	13	0	0	0	0	0	0	0	0	0	0	0	0
O *	CPVC Tee - Branch	3	3	5	6	8	10	12	15	0	0	0	0	0	0	0	0	0	0	0	0
R *	CPVC Coupling Tee - Run	1	1	1	1	1	1	2	2	0	0	0	0	0	0	0	0	0	0	0	0
S	NFPA 13 Swing Check	0	0	5	7	9	11	14	16	19	22	27	32	45	55	65					
T	NFPA 13 90' Flow thru Tee	3	4	5	6	8	10	12	15	17	20	25	30	35	50	60	71	81	91	101	121
Ziw	Wilkins 350AST	Fitting generates a Fixed Loss Based on Flow																			

## Units Summary

Diameter Units                      Inches  
 Length Units                         Feet  
 Flow Units                            US Gallons per Minute  
 Pressure Units                       Pounds per Square Inch

Note: Fitting Legend provides equivalent pipe lengths for fittings types of various diameters. Equivalent lengths shown are standard for actual diameters of Sched 40 pipe and CFactors of 120 except as noted with \*. The fittings marked with a \* show equivalent lengths values supplied by manufacturers based on specific pipe diameters and CFactors and they require no adjustment. All values for fittings not marked with a \* will be adjusted in the calculation for CFactors of other than 120 and diameters other than Sched 40 per NFPA.

# Flow Summary - NFPA

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ETC Building H Area 3

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## SUPPLY ANALYSIS

<i>Node at Source</i>	<i>Static Pressure</i>	<i>Residual Pressure</i>	<i>Flow</i>	<i>Available Pressure</i>	<i>Total Demand</i>	<i>Required Pressure</i>
TEST	40.0	25	1560.0	39.96	62.93	32.957

## NODE ANALYSIS

<i>Node Tag</i>	<i>Elevation</i>	<i>Node Type</i>	<i>Pressure at Node</i>	<i>Discharge at Node</i>		<i>Notes</i>
30	106.0	5.6	7.0	14.82	0.1	140
31	107.0		8.2			
3	107.0		8.75			
4	107.0		8.88			
5	107.0		8.9			
6	107.0		8.99			
7	107.0		9.01			
8	107.0		9.05			
9	107.0		9.09			
10	107.0		9.33			
UP6	107.0		9.42			
UP5	96.75		13.94			
UP4	86.5		18.46			
90	86.5		18.75			
11A	86.5		18.76			
11B	86.5		18.93			
92	86.5		19.48			
12	86.5		19.99			
TOR	86.5		21.68			
BOR	80.0		25.45			
BKV	77.0		32.94			
WM1	77.0		32.95			
WM2	77.0		32.96			
TEST	77.0		32.96			
40	106.0	5.6	8.73	16.55	0.1	98
50	106.0	5.6	7.44	15.27	0.1	140
60	106.0	5.6	8.47	16.3	0.1	98
10A	107.0		9.51			
10B	107.0		9.59			
72	107.0		9.59			
UP3	107.0		9.67			
UP2	96.75		14.12			
UP1	86.5		18.63			
80	96.75		14.02			
81	96.75		14.03			
82	96.75		14.04			
83	96.75		14.03			
84	96.75		14.03			
41	107.0		9.37			
70	107.0		9.4			
71	107.0		9.5			
UP9	107.0		9.65			

# Flow Summary - NFPA

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## *NODE ANALYSIS (cont.)*

<i>Node Tag</i>	<i>Elevation</i>	<i>Node Type</i>	<i>Pressure at Node</i>	<i>Discharge at Node</i>	<i>Notes</i>
UP8	96.75		14.15		
UP7	86.5		18.7		
91	86.5		19.12		

# Final Calculations : Hazen-Williams

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Node1 to Node2	Elev1 Elev2	K Fact	Qa Qt	Nom Act	Fitting or Eqiv	Len	Pipe Ftngs Total	CFact Pf/Ft	Pt Pe Pf	*****	Notes	*****
30 to 31	106 107	5.60	14.82	1	4N R	28.0 1.0	12.920 29.000 41.920	150	7.000 -0.433 1.637			
										Vel =	4.99	
31 to 3	107 107		0.0	1	N R	7.0 1.0	5.920 8.000 13.920	150	8.204 0.0 0.544			
										Vel =	4.99	
3 to 4	107 107		0.0	1.25	R	1.0	9.640 1.000 10.640	150	8.748 0.0 0.132			
										Vel =	3.12	
4 to 5	107 107		0.0	1.25	R	1.0	1.000 1.000 2.000	150	8.880 0.0 0.024			
										Vel =	3.12	
5 to 6	107 107		0.0	1.25	R	1.0	5.750 1.000 6.750	150	8.904 0.0 0.084			
										Vel =	3.12	
6 to 7	107 107		15.27	2	R	1.0	1.170 1.000 2.170	150	8.988 0.0 0.017			
										Vel =	3.06	
7 to 8	107 107		0.0	2	R	1.0	4.670 1.000 5.670	150	9.005 0.0 0.045			
										Vel =	3.06	
8 to 9	107 107		0.0	2	2R	2.0	2.830 2.000 4.830	150	9.050 0.0 0.038			
										Vel =	3.06	
9 to 10	107 107		16.30	2	O	10.0	3.580 10.000 13.580	150	9.088 0.0 0.237			
										Vel =	4.72	
10 to UP6	107 107		-16.77	2	N	11.0	1.170 11.000 12.170	150	9.325 0.0 0.093			
										Vel =	3.02	
UP6 to UP5	107 96.750		0.0	2	R	1.0	10.250 1.000 11.250	150	9.418 4.439 0.086			
										Vel =	3.02	
UP5 to UP4	96.750 86.500		-9.63	2	N	11.0	10.250 11.000 21.250	150	13.943 4.439 0.079			
										Vel =	2.04	
UP4 to 90	86.500 86.500		0.0	2	2O 9R	20.0 9.0	49.670 29.000 78.670	150	18.461 0.0 0.290			
										Vel =	2.04	
90 to 11A	86.500 86.500		-13.88	2	2R	2.0	11.580 2.000 13.580	150	18.751 0.0 0.005			
										Vel =	0.62	
11A to 11B	86.500 86.500		23.98	2	R O	1.0 10.0	11.250 11.000 22.250	150	18.756 0.0 0.175			
										Vel =	3.06	
11B to 92	86.500 86.500		18.96	2	5R	5.0	23.500 5.000 28.500	150	18.931 0.0 0.553			
										Vel =	4.99	

# Final Calculations : Hazen-Williams

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Node1 to Node2	Elev1 Elev2	K Fact	Qa Qt	Nom Act	Fitting or Eqiv	Len	Pipe Ftngs Total	CFact Pf/Ft	Pt Pe Pf	*****	Notes	*****
92 to 12	86.500 86.500		13.88 62.93	2 2.003	O	10.0	6.420 10.000 16.420	150 0.0308	19.484 0.0 0.506			Vel = 6.41
12 to TOR	86.500 86.500		0.0 62.93	2 2.003	3R 3N	3.0 33.0	19.010 36.000 55.010	150 0.0308	19.990 0.0 1.692			Vel = 6.41
TOR to BOR	86.500 80		0.0 62.93	2 2.203	B S	8.183 15.003	9.500 23.186 32.686	120 0.0292	21.682 2.815 0.956			Vel = 5.30
BOR to BKV	80 77		0.0 62.93	6 6.16	T 3E Ziw	43.037 60.252 0.0	72.080 103.289 175.369	140 0.0001	25.453 7.460 0.026		** Fixed Loss = 6.161	Vel = 0.68
BKV to WM1	77 77		0.0 62.93	6 6.16	T G	43.037 4.304	40.000 47.341 87.341	140 0.0001	32.939 0.0 0.013			Vel = 0.68
WM1 to WM2	77 77		0.0 62.93	8 8.27	T	55.354	75.000 55.354 130.354	140 0	32.952 0.0 0.004			Vel = 0.38
WM2 to TEST	77 77		0.0 62.93	8 8.27			4.000 4.000	140 0.0002	32.956 0.0 0.001			Vel = 0.38
TEST			0.0 62.93						32.957		K Factor = 10.96	
40 to 41	106 107	5.60	16.55 16.55	1 1.101	2N O	14.0 5.0	3.500 19.000 22.500	150 0.0479	8.730 -0.433 1.077			Vel = 5.58
41			0.0 16.55						9.374		K Factor = 5.41	
50 to 6	106 107	5.60	15.27 15.27	1 1.101	4N 2R O	28.0 2.0 5.0	13.080 35.000 48.080	150 0.0413	7.435 -0.433 1.986			Vel = 5.15
6			0.0 15.27						8.988		K Factor = 5.09	
60 to 9	106 107	5.60	16.30 16.3	1 1.101	2N O	14.0 5.0	3.500 19.000 22.500	150 0.0466	8.472 -0.433 1.049			Vel = 5.49
9			0.0 16.30						9.088		K Factor = 5.41	
10 to 10A	107 107		16.76 16.76	2 2.003	9R O	9.0 10.0	49.670 19.000 68.670	150 0.0027	9.325 0.0 0.183			Vel = 1.71
10A to 10B	107 107		9.84 26.6	2 2.003	2R	2.0	11.580 2.000 13.580	150 0.0063	9.508 0.0 0.085			Vel = 2.71
10B to 72	107 107		-23.99 2.61	2 2.003	2R	2.0	11.170 2.000 13.170	150 0.0001	9.593 0.0 0.001			Vel = 0.27

# Final Calculations : Hazen-Williams

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Node1 to Node2	Elev1 Elev2	K Fact	Qa Qt	Nom Act	Fitting or Eqiv	Len	Pipe Ftngs Total	CFact Pf/Ft	Pt Pe Pf	*****	Notes	*****
72 to UP3	107 107		6.71 9.32	2 2.003	8R 2O N	8.0 20.0 11.0	50.830 39.000 89.830	150 0.0009	9.594 0.0 0.081		Vel = 0.95	
UP3 to UP2	107 96.750		0.0 9.32	2 2.003	R	1.0	10.250 1.000 11.250	150 0.0009	9.675 4.439 0.010		Vel = 0.95	
UP2 to UP1	96.750 86.500		9.64 18.96	2 2.003	N	11.0	10.250 11.000 21.250	150 0.0033	14.124 4.439 0.071		Vel = 1.93	
UP1 to 11B	86.500 86.500		0.0 18.96	2 2.003	8R 3O	8.0 30.0	50.830 38.000 88.830	150 0.0033	18.634 0.0 0.297		Vel = 1.93	
11B			0.0 18.96						18.931		K Factor = 4.36	
UP5 to 80	96.750 96.750		9.64 9.64	2 2.003	2O 9R	20.0 9.0	50.830 29.000 79.830	150 0.0010	13.943 0.0 0.077		Vel = 0.98	
80 to 81	96.750 96.750		-1.54 8.1	2 2.003	2R	2.0	11.580 2.000 13.580	150 0.0007	14.020 0.0 0.009		Vel = 0.82	
81 to 82	96.750 96.750		0.0 8.1	2 2.003	2R	2.0	11.250 2.000 13.250	150 0.0007	14.029 0.0 0.009		Vel = 0.82	
82 to UP2	96.750 96.750		1.54 9.64	2 2.003	8R 2O N	8.0 20.0 11.0	51.000 39.000 90.000	150 0.0010	14.038 0.0 0.086		Vel = 0.98	
UP2			0.0 9.64						14.124		K Factor = 2.57	
82 to 83	96.750 96.750		-1.53 -1.53	1.25 1.394	4R O	4.0 6.0	23.500 10.000 33.500	150 -0.0002	14.038 0.0 -0.006		Vel = 0.32	
83 to 84	96.750 96.750		0.0 -1.53	1.25 1.394	4R O	4.0 6.0	22.830 10.000 32.830	150 -0.0002	14.032 0.0 -0.006		Vel = 0.32	
84 to 80	96.750 96.750		0.0 -1.53	1.25 1.394	4R O	4.0 6.0	23.500 10.000 33.500	150 -0.0002	14.026 0.0 -0.006		Vel = 0.32	
80			0.0 -1.53						14.020		K Factor = -0.41	
10A to 41	107 107		-9.84 -9.84	1.25 1.394	4R	4.0	19.000 4.000 23.000	150 -0.0058	9.508 0.0 -0.134		Vel = 2.07	
41 to 70	107 107		16.55 6.71	1.25 1.394	O	6.0	4.500 6.000 10.500	150 0.0029	9.374 0.0 0.030		Vel = 1.41	
70 to 71	107 107		0.0 6.71	1.25 1.394	4R O	4.0 6.0	22.830 10.000 32.830	150 0.0029	9.404 0.0 0.094		Vel = 1.41	



# Final Calculations : Hazen-Williams

SPRINX FIRE PROTECTION INC.  
ETC Building H Area 3

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Node1 to Node2	Elev1 Elev2	K Fact	Qa Qt	Nom Act	Fitting or Eqiv	Len	Pipe Ftngs Total	CFact Pf/Ft	Pt Pe Pf	*****	Notes	*****
71 to 72	107 107		0.0 6.71	1.25 1.394	4R O	4.0 6.0	23.500 10.000 33.500	150 0.0029	9.498 0.0 0.096		Vel = 1.41	
72			0.0 6.71						9.594		K Factor = 2.17	
10B to UP9	107 107		23.99 23.99	2 2.003	N	11.0	0.670 11.000 11.670	150 0.0051	9.593 0.0 0.060		Vel = 2.44	
UP9 to UP8	107 96.750		0.0 23.99	2 2.003	R	1.0	10.250 1.000 11.250	150 0.0052	9.653 4.439 0.059		Vel = 2.44	
UP8 to UP7	96.750 86.500		0.0 23.99	2 2.003	N	11.0	10.250 11.000 21.250	150 0.0052	14.151 4.439 0.110		Vel = 2.44	
UP7 to 11A	86.500 86.500		0.0 23.99	2 2.003	O	10.0	1.000 10.000 11.000	150 0.0051	18.700 0.0 0.056		Vel = 2.44	
11A			0.0 23.99						18.756		K Factor = 5.54	
90 to 91	86.500 86.500		13.88 13.88	1.25 1.394	4R O	4.0 6.0	24.000 10.000 34.000	150 0.0110	18.751 0.0 0.373		Vel = 2.92	
91 to 92	86.500 86.500		0.0 13.88	1.25 1.394	4R O	4.0 6.0	22.830 10.000 32.830	150 0.0110	19.124 0.0 0.360		Vel = 2.92	
92			0.0 13.88						19.484		K Factor = 3.14	



## MEMORANDUM

TO: BRIAN JOHNSON, WATER SYSTEM  
SPECIALIST  
FROM: KERRI SIDEBOTTOM, P.E.  
DATE: APRIL 16, 2024  
SUBJECT: EAST TOWN CROSSING ADDITIONAL  
FIRE FLOW AVAILABILITY  
CITY OF PUYALLUP, PIERCE COUNTY,  
WASHINGTON  
G&O #21415.19

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Per your request, I have analyzed the available fire flow at the proposed East Town Crossing development, in the central part of the City's water service area. Fire flow at this location was previously analyzed in a memo from Gray & Osborne, dated February 14, 2024. The Developer has proposed a Revised Water Piping Plan for the site, which has been analyzed in this memo. The setup of the hydraulic model and the assumptions used to determine the static pressure and available fire flow are noted as follows.

- The available fire flows and pressures are measured at 14 nodes, corresponding to the proposed hydrants within the development, as shown in the attached figure.
- Water system demands are based on projected 2038 demands and reservoirs are depleted of fire suppression and equalizing storage, as established in the *2019 Water System Plan (WSP)*, approved by the Department of Health (DOH). The City's water model was updated in 2021 to reflect additional system improvements since the WSP was developed.
- All pump stations are idle, and the Salmon Springs source is operating at 1,100 gallons per minute (gpm).

The development is located in Zone 1, which is supplied by Maplewood Springs and the 15<sup>th</sup> Avenue SE Reservoirs. The system was modeled as-is, with the proposed piping indicated on the attached figure. The model was run for two different scenarios, all of which include new 8-inch piping. The new piping for Scenario 1 includes the Phase 1 piping shown on the attached figure in pink. Scenario 2 includes additional piping for Phase 2 of the development is shown in orange on the attached figure.



The available pressure under 2038 peak hour demands at the hydrants is included in Table 1.

**TABLE 1**

**Peak Hour Pressure**

<b>Node</b>	<b>Hydrant</b>	<b>Elevation, feet</b>	<b>Peak Hour Pressure, psi</b>
J2238	J	71	41
J2240	L	72	41
J2242	M	72	40
J2244	N	76	39
J2246	H	76	39
J2248	I	76	41
J2250	F	73	40
J2252	D	69	42
J2254	C	67	43
J2256	B	66	43
J2258	A	66	43
J2260	E	72	41
J2274	G	75	39
J2276	K	71	41

The peak hour pressures within the development are essentially the same under either of the proposed scenarios, and the looping does not appreciably impact the pressures.

**SCENARIO 1**

Scenario 1 includes the piping planned for Phase 1, shown in pink on the attached figure. The piping includes 8-inch mains, mostly dead-ends, extending from the existing 8-inch main running from north to south through the site, as well as a connection to the 16-inch main on Shaw Road, to the west. Part of the existing 8-inch main will be replaced during construction of the development.

Available fire flow was modeled at 12 of the proposed hydrants in the development; Hydrants A through L. The hydrants are located on 8-inch pipes throughout the development, many of which are dead-ends. The results of this modeling are included in Table 2. The modeled fire flow is available at any hydrant individually, but not simultaneously.



**TABLE 2**  
**Modeled Fire Flow Availability, Scenario 1**

<b>Node</b>	<b>Hydrant</b>	<b>Available Fire Flow, gpm</b>	<b>Residual Pressure at Available Fire Flow, psi</b>	<b>Minimum System Pressure at Available Fire Flow, psi</b>
J2238	J	2,140 <sup>(1)</sup>	25	25
J2240	L	1,560 <sup>(1)</sup>	23	23
J2246	H	1,560 <sup>(1)</sup>	22	22
J2248	I	2,580 <sup>(1)</sup>	23	23
J2250	F	1,560 <sup>(1)</sup>	25	25
J2252	D	2,170 <sup>(1)</sup>	28	28
J2254	C	1,920 <sup>(1)</sup>	29	28
J2256	B	2,230 <sup>(1)</sup>	26	26
J2258	A	1,560 <sup>(1)</sup>	28	28
J2260	E	1,560 <sup>(1)</sup>	23	23
J2274	G	1,560 <sup>(1)</sup>	25	25
J2276	K	1,560 <sup>(1)</sup>	27	27

(1) Limited by maximum system-wide velocity of 10 feet per second.

Fire flow to all of the hydrants is limited by the 10-fps maximum velocity through the existing and proposed 8-inch pipes in this scenario.

## **SCENARIO 2**

Scenario 2 includes the piping indicated for Phases 1 and 2, shown in pink and orange on the attached figure. The piping includes 8-inch pipes extending from the existing 8-inch main running from north to south through the site, a connection to the existing 16-inch main on Shaw Road to the west, and improved looping as compared with Scenario 1.

Available fire flow was measured at the 14 proposed hydrants in the development; Hydrants A through N. The hydrants are located on 8-inch pipes throughout the development. The results of this modeling are included in Table. The modeled fire flow is available at any hydrant individually, but not simultaneously.



**TABLE 3**  
**Modeled Fire Flow Availability, Scenario 2**

<b>Node</b>	<b>Hydrant</b>	<b>Available Fire Flow, gpm</b>	<b>Residual Pressure at Available Fire Flow, psi</b>	<b>Minimum System Pressure at Available Fire Flow, psi</b>
J2238	J	2,430 <sup>(1)</sup>	25	25
J2240	L	2,340 <sup>(1)</sup>	21	21
J2242	M	2,320 <sup>(2)</sup>	20	20
J2244	N	2,120 <sup>(2)</sup>	20	20
J2246	H	2,330 <sup>(1)</sup>	20	20
J2248	I	2,540 <sup>(1)</sup>	24	24
J2250	F	1,560 <sup>(1)</sup>	26	26
J2252	D	2,230 <sup>(1)</sup>	28	28
J2254	C	1,980 <sup>(1)</sup>	29	28
J2256	B	2,340 <sup>(1)</sup>	26	26
J2258	A	1,560 <sup>(1)</sup>	38	38
J2260	E	1,560 <sup>(1)</sup>	23	23
J2274	G	1,980 <sup>(1)</sup>	25	25
J2276	K	2,040 <sup>(1)</sup>	25	25

(1) Limited by maximum system-wide velocity of 10 fps.

(2) Limited by minimum system-wide pressure of 20 psi at all service locations.

Fire flow to the hydrants is limited by the 10-fps maximum velocity through the existing and proposed 8-inch pipes.

It should be noted that the dead-end 8-inch mains within the proposed site can only provide 1,560 gpm, due to the City's 10-fps velocity limitation considered for the fire flow analysis. Therefore, if 1,500 gpm is required at the hydrant, located on a dead-end main, there is essentially no additional flow available for the sprinkler system supplied by the same dead-end main. This impacts Hydrants A, E, and F in both scenarios, and additionally Hydrants G and H in Scenario 1 only.

The Department of Health and City Standards for water distribution systems are to meet the peak hourly demand of the system while providing a minimum pressure of 30 psi, system-wide. Under peak daily demand with a fire flow, the system is designed to maintain a minimum pressure of 20 psi, system-wide. Although the peak hourly demand pressure may currently be higher than these standards, the Developer must recognize that

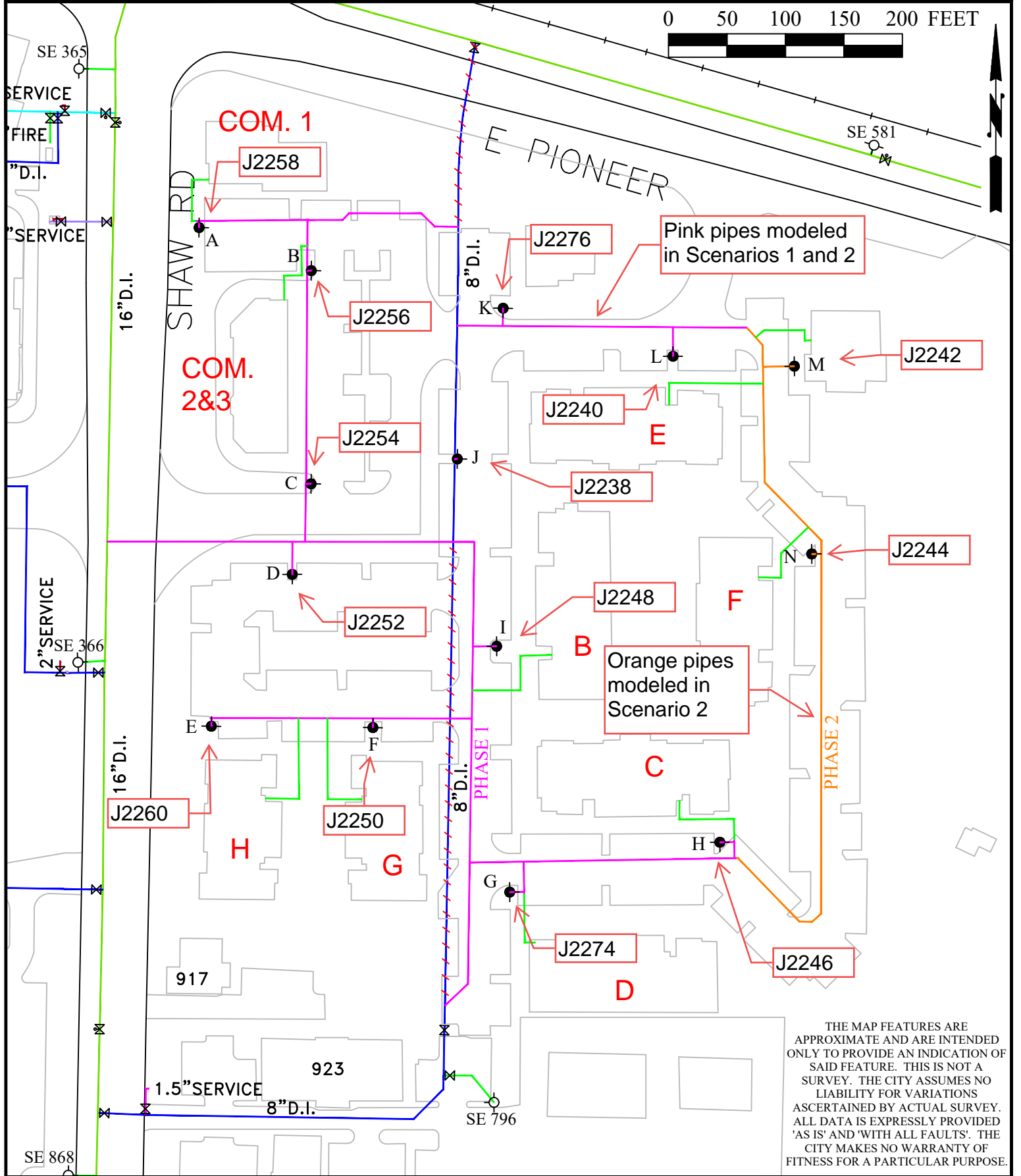


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the City may not provide pressure higher than 30 psi in the future. The flows and pressures determined in this memo are based on the approximate hydrant elevation at ground level. The Developer may design their sprinkler system for whatever pressure they wish, however they must recognize and be responsible for conditions when the pressure may be less than currently exists.

KS/sr

0 50 100 150 200 FEET



THE MAP FEATURES ARE APPROXIMATE AND ARE INTENDED ONLY TO PROVIDE AN INDICATION OF SAID FEATURE. THIS IS NOT A SURVEY. THE CITY ASSUMES NO LIABILITY FOR VARIATIONS ASCERTAINED BY ACTUAL SURVEY. ALL DATA IS EXPRESSLY PROVIDED 'AS IS' AND 'WITH ALL FAULTS'. THE CITY MAKES NO WARRANTY OF FITNESS FOR A PARTICULAR PURPOSE.



CITY OF PUYALLUP  
PUBLIC WORKS  
WATER DIVISION

# HYDRAULIC MODEL FOR EAST TOWN CROSSING

SCALE AS SHOWN

04/10/2024

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PG104/MODEL EAST TOWN CROSSING