# **Stormwater Plan**

# **320 Todd Road Development**

320 Todd Rd NE Puyallup, WA 98371

#### Prepared by

JMJ TEAM 905 Main St Suite 200 Sumner, WA 98390 206.596.2020 Justin Jones, PE



#### **PROJECT ENGINEER'S CERTIFICATION**

I hereby certify that this Stormwater Plan for the 320 Todd Road Development in Puyallup has been prepared by me or under my supervision and meets minimum standards of Washington State Department of Ecology, The City of Puyallup, and normal standards of engineering practice. I hereby acknowledge and agree that the jurisdiction does not and will not assume liability for the sufficiency, suitability, or performance of drainage facilities designed by me.

Justin Jones, PE





#### **TABLE OF CONTENTS**

Project Overview and Maps	1
Existing Conditions Summary	3
Proposed Conditions Summary	3
Summary of Minimum Requirements	4

Appendix A:

**Infiltration Testing Report** 

Appendix B:

**Site Development Plans** 

Appendix C: CSWPPP

Appendix D: WWHM Report

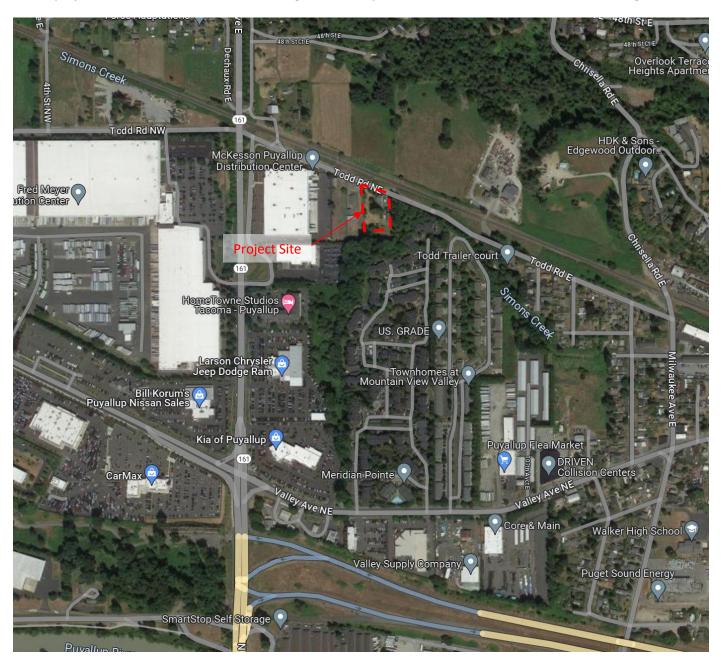
Appendix E:

**Operations & Maintenance Manual** 



#### **PROJECT OVERVIEW AND MAPS**

The 320 Todd Road Development is located in Puyallup, WA along the southern side of Todd Rd NE. The proposed project is on a 65,123 SF residential multi-family lot, RM-20, with a proposed onsite project area of 33,174 SF and offsite project area of 7,997 SF. The surrounding area is comprised of residential and commercial buildings.



The project is a new development project and includes the renovation of an existing two-story residential building with a roof overhang/deck area of 2,745 SF, 168 SF of cement concrete pavement, 11,757 SF of asphalt pavement, and 18,157 SF of landscaping. Additionally, the development will include the construction of a driveway approach and garbage enclosure. The stormwater approach is to fully infiltrate all stormwater onsite using bioretention cells and an underground infiltration gallery.

Half street improvements will be installed, and a ROW dedication will be necessary. The half street improvements will consist of a new cement concrete sidewalk, curb & gutter, asphalt roadway, watermain extension, and stormwater improvements. Stormwater will be captured and conveyed to the existing stormwater system along Todd Rd NE.



#### **EXISTING CONDITIONS SUMMARY**

The Todd Rd Development is a 65,123 SF (1.50 acres) parcel, with a proposed project area of onsite project area of 33,174 SF. The site consists of an existing two-story residential 2,195 SF building, one-story garage, concrete, landscaping, septic drainfield, and wood fence along the perimeter of the property.

The project site is generally flat sloping from east to west; Stormwater that falls within the existing site infiltrates into native soils. There is no existing stormwater conveyance system to the site. The existing project site is approximately 14.3% impervious.

#### PROPOSED CONDITIONS SUMMARY

The Todd Rd Development proposes the conversion of an existing residential building to a 2,745 SF office building (including roof overhangs and decks) with site improvements and half street improvements.

Half street improvements will consist of an 1,879 SF ROW dedication, 212 LF of new curb & gutter, 1,695 SF of new cement concrete sidewalk, 6,140 SF of new asphalt roadway, and a 445 LF watermain extension.

The proposed development will result in 17,170 SF of impervious surface (15,031 SF of New/Replaced and 2,139 SF of Existing) and be 72.9% pervious.

Site improvements include the construction of new asphalt pavement, new cement concrete pavement, and new landscaping. The building will also have utility service connections for sewer, water, power, gas, and communications.

Stormwater from the Todd Rd building will be collected with roof downspouts and conveyed to a proposed infiltration gallery, which will infiltrate 100% of stormwater up to the 100-year storm. Infiltration testing was performed on site to obtain a design infiltration rate for on-site soils in the vicinity of stormwater infiltration systems, see Appendix A.

Runoff from the proposed cement concrete surfaces will sheet flow and infiltrate into native soils onsite.

Bioretention cells will collect and treat the asphalt stormwater runoff; subsequently the runoff in the bioretention cells will be conveyed to the same underground infiltration gallery.

The Todd Rd Development will have 15,031 SF of new and replaced hard surfaces upon project completion, and a total of 33,174 SF of land disturbing activity. The proposed development will result in 17,170 SF of impervious surface (15,031 SF of New/Replaced and 2,139 SF of Existing) and be 27.1% impervious. Since the project exceeds 5,000 SF of new plus replaced hard surfaces, the project is subject to all minimum requirements.

Offsite (Half Street Improvements) runoff is captured with new type 1 catch basins and conveyed to a new type 2 catch basin. The new type 2 catch basin intercepts an existing stormwater line under Todd Rd NE.

See table below for existing and proposed project areas.

Description <sup>a</sup>	Onsite	Offsite	Total
Existing Cond	litions		
Total Project Area <sup>b</sup> (ft²)	33,174-0.762 ac	7,997-0.184 ac	41,171-0.946ac
Existing hard surface (ft²)	8,174-0.188 ac	4,678-0.108 ac	12,852-0.296ac
Existing vegetation area (ft²)	25,000- 0.574ac	3,319-0.076 ac	28,319-0.650ac
Proposed Con	ditions		
Total Project Area <sup>b</sup> (ft²)	33,174-0.762 ac	7,997-0.184 ac	41,171-0.946ac
Amount of new hard surface (ft²)	8,838-0.203 ac	3,304-0.076 ac	12,142-0.279ac
Amount of new pollution generating hard surface (PGHS) <sup>c</sup> (ft²)	8,386-0.193 ac	1,961-0.045 ac	10,347-0.238 ac
Amount of replaced hard surface (ft²)	6,193-0.142 ac	4,678-0.107 ac	10,871-0.249ac
Amount of replaced PGHS <sup>d</sup> (ft²)	3,721-0.085 ac	4,221-0.097 ac	7,942-0.182 ac
Amount of new plus replaced hard surface (ft²)	15,031-0.345ac	7,982-0.183 ac	23,013-0.528ac
Amount of new + replaced PGHS (ft²)	12,107-0.278ac	6,182-0.142 ac	18,289-0.420ac
Amount of existing hard surfaces converted to vegetation (ft²)	1,993-0.046 ac	15-0.001 ac	2,008-0.047 ac
Amount of Land Disturbed (ft²)	33,174-0.762 ac	7,997-0.184 ac	41,171-0.946ac
Vegetation to Lawn/Landscaped (acres)	0.371-16,150 sf	0-0 sf	0.371-16,150 sf
Native Vegetation to Pasture (acres)	0-0 sf	0-0 sf	0-0 sf
Existing hard surface to remain unaltered (ft²)	0-0 ac	0-0 ac	0-0 ac
Existing vegetation area to remain unaltered (ft²)	0-0 ac	0-0 ac	0-0 ac

a.All terms are defined in the 2019 Ecology Manual glossary.

b. The total project area in the existing condition should typically match the total project area in the proposed condition.

c.The "amount of new PGHS" should be part of or all of "amount of new hard surfaces"

d. The "amount of replaced PGHS" should be part of or all of the "amount of replaced hard surfaces".

#### **SUMMARY OF MINIMUM REQUIREMENTS**

The City of Puyallup utilizes the 2019 Department of Ecology Stormwater Manual for Western Washington (manual) for stormwater design. Volume 1 of this manual describes the Minimum Requirements for stormwater management for a New Development site. Using the flow chart below, all minimum requirements apply to the Todd Rd project onsite work.

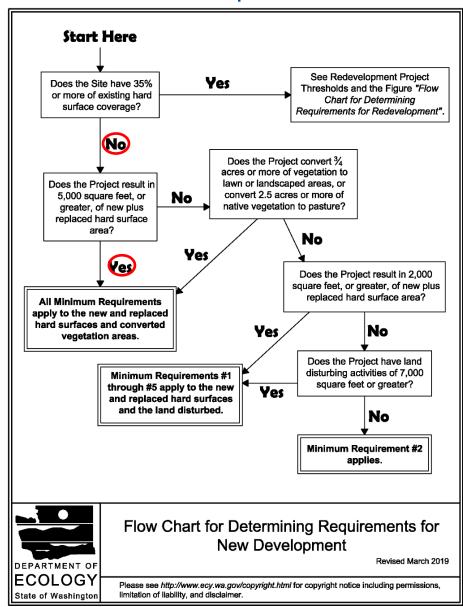


Figure I-3.1: Flow Chart for Determining Requirements for New Development

2019 Stormwater Management Manual for Western Washington

Volume I - Chapter 3 - Page 89

#### MINIMUM REQUIREMENT 1: PREPARATION OF STORMWATER SITE PLANS

Stormwater Site Plan drawings have been prepared per the City of Puyallup development codes and the 2019 DOE Manual, see Appendix B.

#### MINIMUM REQUIREMENT 2: CONSTRUCTION STORMWATER POLLUTION PREVENTION

Temporary Erosion and Sediment Control Plans and a Construction Stormwater Pollution Prevention Plan have been prepared per the City of Puyallup development codes and the 2019 DOE Manual. Construction Stormwater Pollution Prevention measures may include: construction entrance; silt. See Appendix C for CSWPPP.

#### MINIMUM REQUIREMENT 3: SOURCE CONTROL OF POLLUTION

Source control BMPs will be implemented to minimize stormwater contamination and help comply with the Department of Ecology Stormwater Management Manual for Western Washington. BMP's for the project may include:

- Inspect and clean treatment BMPs, conveyance systems, and catch basins as needed, and determine necessary O & M Improvements.
- Clean catch basins when the depth of deposits reaches 60-percent of the sump depth as measured from the bottom of basin to the invert of the lowest pipe into or out of the basin.
- Clean woody debris in a catch basin as frequently as needed to ensure proper operation of the catch basin.

#### MINIMUM REQUIREMENT 4: PRESERVATION OF NATURAL DRAINAGE SYSTEMS AND OUTFALLS

The existing site is comprised of an existing two-story residential building, garage, landscaping, concrete, and a wood fence along the perimeter of the property and is 14.3% impervious. Stormwater currently infiltrates into native soils, and surface flows to the west side of the property. The proposed stormwater runoff will maintain existing drainage patterns and infiltrate onsite.

Offsite drainage consists of catch basins on either half of the road, that connect to an existing stormwater line under the north half of the road. The proposed stormwater runoff will maintain existing drainage patterns and be conveyed to the existing offsite stormwater system.

#### MINIMUM REQUIREMENT 5: ONSITE STORMWATER MANAGEMENT

Minimum Requirement #5 states projects shall utilize either On-Site Stormwater Management BMP's from List #2 or demonstrate compliance with the Low Impact Development (LID) Performance Standard. The LID performance standard requires the site to match predeveloped flows through flow control systems for 8% of the 2-year and 50-year storm events. The Todd Rd project is increasing the amount of impervious surface coverage on-site, and thus would be increasing stormwater flow frequency volumes. List #2 requires the evaluation of BMP's in the order listed to determine the most appropriate stormwater management system for landscaped areas, roofs, and hard surfaces. The stormwater approach is to infiltrate all stormwater runoff onsite, therefore the Todd Rd project is designed to ensure compliance with the LID Performance Standard.

Each BMP requires varying separation between the bottom of the BMP and the seasonal high groundwater level. Therefore, testing of the stormwater infiltration rate and seasonal high groundwater level was conducted. Excavation was conducted to a depth of 5.0-feet. No mottling or groundwater was observed in the test locations. A Pilot Infiltration Test (PIT) was conducted in the west and east sides of the site. The tests recorded infiltration rates

of 0.87 and 0.85 inches per hour, and after applying factors of safety design infiltration rates are 0.39 and 0.38 inches per hour, see Appendix A for Infiltration Report. Groundwater was not encountered during soil inspections.

Three drive-point piezometers (DPPs) were installed by GeoResources to conduct groundwater monitoring for the 320 Todd Rd project site during the wet season. Groundwater levels were manually measured bi-monthly from January 6, 2023 to March 31, 2023, see Appendix E in Appendix A for Soils Report.

The measured seasonal high groundwater level is at elevation 43.0′, approximately 7 to 8 feet below existing grade. All BMP's will have sufficient separation between the bottom of the BMP and seasonal high groundwater level.

Downspout Infiltration and Bioretention Cells will be used to manage stormwater onsite to meet the LID Performance Standard. Runoff from building roof will be collected from the downspout locations and routed through stormwater pipes along the perimeter of the building and connect into the proposed infiltration gallery. Stormwater entering the infiltration gallery will infiltrate 100% up to the 100-year storm event. The infiltration gallery is sized per the design infiltration rate of 0.38 in/hr. Drain Rock with a porosity of 0.33 is the infiltration gallery material. Additionally, 1-foot of separation between the bottom of the infiltration gallery and the seasonal high groundwater level will be maintained.

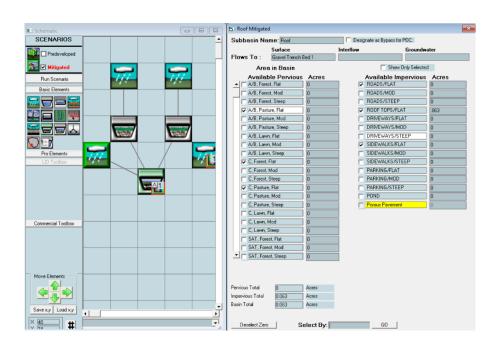
Proposed asphalt pavement runoff will sheetflow to one of two proposed Bioretention Cells to be treated and then conveyed to the same underground infiltration gallery as the roof runoff. Cement concrete walkway runoff will sheetflow onto native soils and infiltrate onsite.

Proposed landscaping will adhere to BMP T5.13 and infiltrate 100% of the stormwater runoff onsite into the native soils below.

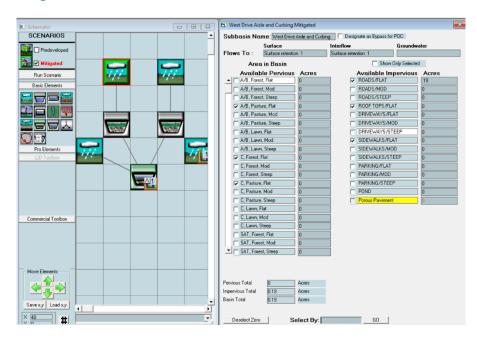
The half street improvements stormwater will be managed with multiple type 1 catch basins, a type 2 catch basins, and stormwater piping. Existing drainage patterns will be maintained.

See Appendix D for full WWHM Report. Results as follows

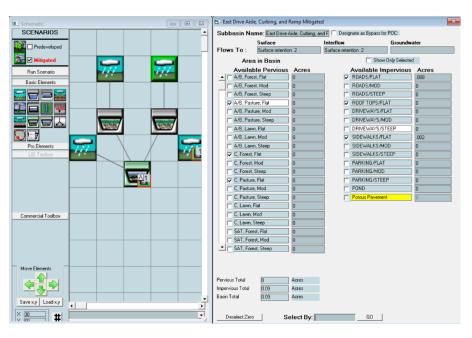
#### **Roof Basin:**



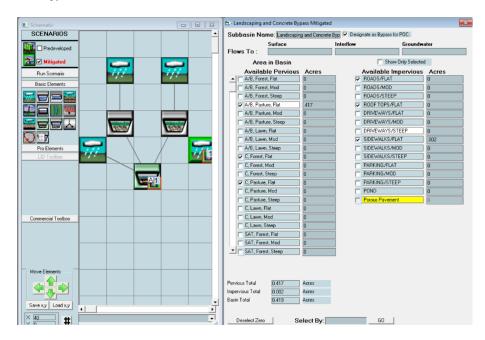
#### West Drive Aisle and Curbing Basin:



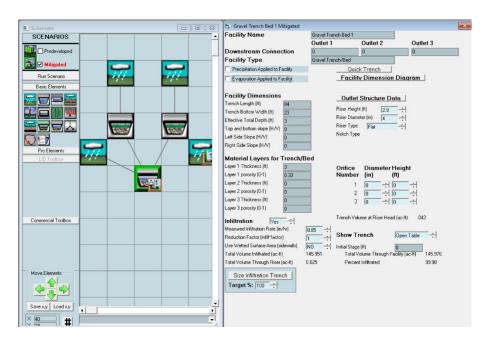
#### East Drive Aisle, Curbing, and Ramp Basin:



#### **Landscaping and Concrete Bypass Basin:**



#### **Infiltration Trench:**



#### **MINIMUM REQUIREMENT 6: WATER QUALITY**

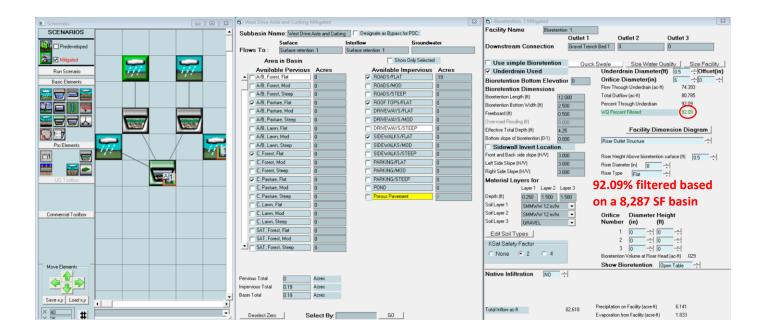
The Department of Ecology Stormwater Management Manual states that any project with a pollution generating threshold discharge area greater than 5,000 SF shall be required to utilize runoff treatment BMPs. The project proposes 11,757 SF of asphalt driveways and is therefore subject to runoff treatment for pollution generating areas. 72 SF of cement concrete walkways and 347 SF of cement concrete curbing will be managed as well.

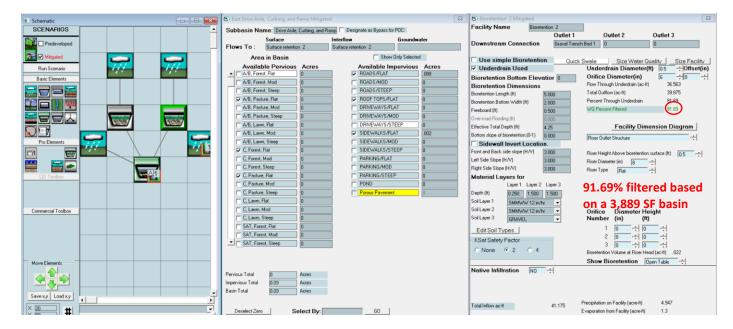
Half-street improvements are not subject to Minimum Requirement #6 since the improvements are road related and do not add more than 5,000 SF of new hard surfaces.

Stormwater runoff from the asphalt parking lot will sheet flow to one of two bioretention cells and be treated before entering the stormwater conveyance system to the underground infiltration gallery, see Appendix D for WWHM modeling.

The bioretention cells have been designed per the 2019 DOE manual and sized using WWHM and the following criteria:

- Treat 91% of runoff
- DOE bioretention soil mix (BSM)
- 3.0-inches per hour infiltration rate for basins less than 8,000 SF
  - Per 2019 DOE manual when using default soil media mix
- 0.5-foot of ponding with 24-hour drawdown
- 6-inches freeboard
- 1.5-foot depth BSM
- 2.0-feet x 5.0-feet and 2.0-feet x 12.0-feet bottom areas will be used for the two bioretention cells
- 3:1 side slopes





Bioretention soil mix to meet 2019 DOE manual "Default Soil Media (BSM)", below:

#### **Default Bioretention Soil Media (BSM)**

Projects which use the following requirements for the bioretention soil media do not have to test the media for it saturated hydraulic conductivity (aka. Infiltration rate). They may assume the rates specified in the subsection titled "Determining Bioretention Soil Mix Infiltration Rate."

#### Mineral Aggregate

Percent Fines: A range of 2 to 4 percent passing the #200 sieve is ideal and fines should not be above 5 percent for a proper functioning specification according to ASTM D422.

#### **Aggregate Gradation**

The aggregate portion of the BSM should be well-graded. According to ASTM D 2487-98 (Classification of Soils for Engineering Purposes (Unified Soil Classification System)), well-graded sand should have the following gradation coefficients:

- Coefficient of Uniformity (Cu = D60/D10) equal to or greater than 4, And
- Coefficient of Curve (Cc = (D30)2/D60 x D10) greater than or equal to 1 and less than or equal to 3.

Table 7.4.1 provides a gradation guideline for the aggregate component of a Bioretention Soil Mix specification in western Washington (Hinman, Robertson, 2007). The sand gradation below is often supplied as a well graded utility or screened. With compost this blend provides enough fines

for adequate water retention, hydraulic conductivity within recommended range (see below), pollutant removal capability, and plant growth characteristics for meeting design guidelines and objectives.

General Guideline for Mineral Aggregate Gradation

Sieve Size	Percent Passing
3/8"	100
#4	95-100
#10	75-90
#40	25-40
#100	4-10
#200	2-5

Where existing soils meet the above aggregate gradation, those soils may be amended rather than importing mineral aggregate.

Compost to Aggregate Ratio, Organic Matter Content, Cation Exchange Capacity:

- Compost to aggregate ratio: 60-65 percent mineral aggregate, 35 40 percent compost by volume.
- Organic matter content: 5 8 percent by weight.
- Cation Exchange Capacity (CEC) must be > 5 milliequivalents/100 g dry soil Note: Soil mixes meeting the above specifications do not have to be tested for CEC. They will readily meet the minimum CEC.

#### Compost

To ensure that the BSM will support healthy plant growth and root development, contribute to biofiltration of pollutants, and not restrict infiltration when used in the proportions cited herein, the following compost standards are required.

- Meets the definition of "composted material" in WAC 173-350-100 and complies with testing parameters and other standards in WAC 173-350-220.
- Produced at a composting facility that is permitted by the jurisdictional health authority. Permitted compost facilities in Washington are included on a list available at http://www.ecy.wa.gov/programs/swfa/organics/soil.html The compost product must originate a minimum of 65 percent by volume from recycled plant waste comprised of "yard debris," "crop residues," and "bulking agents" as those terms are defined in WAC 173-350-100. A maximum of 35 percent by volume of "postconsumer food waste" as defined in WAC 173-350-100 , but not

including biosolids, may be substituted for recycled plant waste.

- Stable (low oxygen use and CO2 generation) and mature (capable of supporting plant growth) by tests shown below. This is critical to plant success in a bioretention soil mixes.
- Moisture content range: no visible free water or dust produced when handling the material.
- Tested in accordance with the U.S. Composting Council "Test Method for the Examination of Compost and Composting" (TMECC), as established in the Composting Council's "Seal of Testing Assurance"

(STA) program. Most Washington compost facilities now use these tests.

• Screened to the following size gradations for Fine Compost when tested in accordance with TMECC test method 02.02-B, Sample Sieving for Aggregate Size Classification."

Fine Compost shall meet the following gradation by dry weight

Minimum percent passing 2" 100%

Minimum percent passing 1" 99%
Minimum percent passing 5/8" 90%
Minimum percent passing 4" 75%

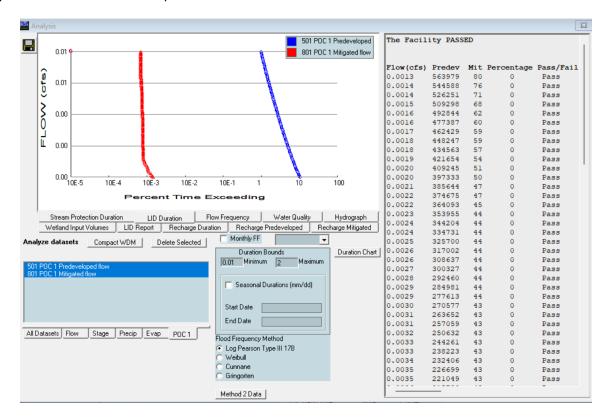
- pH between 6.0 and 8.5 (TMECC 04.11-A). "Physical contaminants" (as defined in WAC 173-350-100) content less that 1% by weight (TMECC 03.08-A) total, not to exceed 0.25 percent film plastic by dry weight.
- Minimum organic matter content of 40% (TMECC 05.07-A "Loss on Ignition)
- Soluble salt content less than 4.0 dS/m (mmhos/cm) (TMECC 04.10-A "Electrical Conductivity, 1:5 Slurry Method, Mass Basis")
- Maturity indicators from a cucumber bioassay (TMECC 05.05-A "Seedling Emergence and Relative Growth) must be greater than 80% for both emergence and vigor")
- Stability of 7 mg CO2-C/g OM/day or below (TMECC 05.08-B "Carbon Dioxide Evolution Rate")
- Carbon to nitrogen ratio (TMECC 05.02A "Carbon to Nitrogen Ratio" which uses 04.01 "Organic Carbon" and 04.02D "Total Nitrogen by Oxidation") of less than 25:1. The C:N ratio may be up to 35:1 for plantings composed entirely of Puget Sound Lowland native species and up to 40:1 for coarse compost to be used as a surface mulch (not in a soil mix).

#### MINIMUM REQUIREMENT 7: FLOW CONTROL

The Todd Rd Development project site uses infiltration to meet the requirement of Minimum Requirement 7 Flow Control.

WWHM modeling was conducted to confirm that predeveloped flows are under the flow duration from 8% of the 2-year peak flow to the full 50-year peak flow. Based on the WWHM LID Duration check, the site meets the LID Performance Standard.

See Appendix D for full WWHM Report. Results are as follows:



Half-street improvements are not subject to Minimum Requirement #7 since the improvements are road related and do not add more than 5,000 SF of new hard surfaces.

#### MINIMUM REQUIREMENT 8: WETLANDS PROTECTION

Any threshold discharge area that discharges stormwater through a conveyance system into a wetland is required to meet the Ecology Manual standards for protecting the wetland. The Todd Rd Development project will not discharge stormwater into a wetland, and thus is not subject to the wetlands protection standards outlined in Minimum Requirement #8.

#### MINIMUM REQUIREMENT 9: OPERATION AND MAINTENANCE

See Appendix E for Operations & Maintenance Manual for all new stormwater BMP's installed with the project.

# **APPENDIX A**

# **Infiltration Testing Report**

## 320 Todd Rd NE

Puyallup, WA

#### **Prepared for**

Catherine & EJ Fernandez 320 Todd Rd NE, Puyallup, WA 98371

### **Prepared by**

JMJ TEAM 905 Main St Suite 200 Sumner, WA 98390 206.596.2020 Justin Jones, PE



#### **PROJECT ENGINEER'S CERTIFICATION**

I hereby certify that this Infiltration Testing Report for Todd RD Development has been prepared by me or under my supervision and meets minimum standards of the Department of Ecology Stormwater Management Manual for Western Washington.

Justin Jones, PE





## **TABLE OF CONTENTS**

Summary	1
Infiltration Test Procedures	3
Findings and Recommendations	4
Test Pit Photo Documentation	6
Appendix A: Data Collection Sheets	7
Appendix B: Pressure Transducer Specification Sheet	8
Appendix C: Department of Ecology PIT Procedure	9
Appendix D: Department of Ecology Factor of Safety Guidelines	12
Appendix E: Soils Report	14



#### **SUMMARY**

This report details the results of infiltration testing for use in the stormwater system design of Todd Road Development located within Puyallup, WA. Two Pilot Infiltration Test (PIT) was conducted on site to determine the onsite stormwater infiltration rate. The test hole was excavated and backfilled by a licensed contractor and the PIT was completed in accordance with the Department of Ecology (ECY) Stormwater Management Manual for Western Washington (Stormwater Manual).

The PIT process evaluates the infiltration within a 12 SF area by first measuring the rate of water required to maintain a constant water elevation of approximately 12-inches in the test pit, and second by measuring the drawdown rate of the water within the test pit. The drawdown is done using a data logger. The test pit is excavated to a depth of 5.0-feet below existing grade and observed for groundwater.

The field data is then analyzed, and a factor of safety applied to determine the stormwater design infiltration rate. Below is a summary of the results.

#### **Test Pit Location**





## **Summary of Results**

Per the PIT, the site soils are suitable for stormwater infiltration. A soil sample was taken from each PIT, the

soil sample has been submitted and is pending results.

on sample has been submitted and is pending results.					
Testing	Test PIT	Results	ECY Threshold		
	Pit Depth	4.0-feet	N/A		
Ground Water	Test Hole 1 Groundwater Level	Ground Water not Observed	N/A		
	Test Hole 2 Groundwater Level	Ground Water not Observed	N/A		
	Infiltration Rate Factor of Safety	0.45	N/A		
		Uncorrected: 0.87 inches per hour			
Infiltration Rate	Test Hole 1 Infiltration Rates	Design: 0.39 Inches per hour	≥ 0.3 inches per hour		
	Test Hole 2 Infiltration Rates	Uncorrected: 0.85 inches per hour	- ≥ 0.3 inches per hour		
		Design: 0.38 inches per hour	per nour		
	Test Hole 1 Lab Analysis	Pending Results	≥ 5.0 milliequivalents CEC/100g		
Water Quality		Pending Results	≥ 1.0%		
	Test Hole 2 Lab Analysis	Pending Results	≥ 5.0 milliequivalents CEC/100g		
		Pending Results	≥ 1.0%		



## **INFILTRATION TEST PROCEDURES**

Below is the process	taken f	for the	e PIT:
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Identify PIT locations based on the site survey of existing buildings and utilities as well as the potential locations of infiltration facilities based on the preliminary site plan.
Obtain public and private utility locates. Prior to the PIT utility locates will be called to ensure there are no utilities present in the PIT locations.
Excavation of PIT holes (approximately 3-feet x 4-feet 4-feet deep). A 3-feet x 4-feet x2-feet tall wood box is inserted into the test hole to ensures that the bottom surface area is exactly 12 SF. The box is backfilled to the top edge to ensure stability and infiltration only through the bottom of the test hole for the duration of the PIT.
A soil sample is collected from the bottom of the hole to test treatment capability. A lab tests the cation exchange rate and organic matter content of soils. Lab results confirm if the soil is suitable for treatment based on Stormwater Manual criteria.
A float system with a water hose connection is set into the center of the test hole. The float system is equipped with a leveling plate, a measuring ruler for visual inspection of water levels and a perforated pipe housing for the data collector.
Using water transfer tanks or hose spigot as available, the test hole is filled to a 12-inch water depth that is maintained. The presoak period ensures that the soils have been fully saturated before conducting the PIT. A 1-hour stabilization test is performed after the presoak period to confirm soil stabilization. If the test yields 4 constant gallon per minute (GPM) readings that are conducted every 15-minutes, the stabilization of the soil is confirmed.
A 1-hour GPM test is conducted per the Stormwater Manual. Using a water meter accurate to the nearest tenth of a gallon, a GPM flow rate is recorded every 15-minutes while the water level is maintained at a 12-inch depth. An infiltration rate (in/hr) can be determined using the GPM flow rate and the 12 SF bottom surface area of the hole.
A drawdown test is performed per Stormwater Manual to determine the drawdown infiltration capability of the soil. A CRS451V (Pressure Transducer) is placed into the test hole and set to take pressure (PSI) readings every 10-minutes. The water source is shutoff, and the pressure transducer will measure water drawdown for a 2-hour period. At the end of the period the sensors are removed from the test hole, the data is collected using a PC interface module and the HydroSci program to communicate with the sensor to retrieve the data.
The wood box and the float system are removed from the test hole.
Over excavate test hole to confirm there is no ground water mounding.
The test pit is then backfilled and restored to prior state of excavation.



#### FINDINGS AND RECOMMENDATIONS

#### **Groundwater Conditions**

The Stormwater Manual specifies minimum separations between the seasonal high groundwater elevation and the bottom of the infiltration facility based on different best management practices (BMP):

Downspout Infiltration: 1-foot
 Permeable Pavement: 1-foot
 Infiltration Facility: 3-foot

With known groundwater conditions for each test hole, there is adequate spacing between groundwater and BMPs. An overflow should be installed with BMP in case of large storm events.

Three drive-point piezometers (DPPs) were installed by GeoResources to conduct groundwater monitoring for the 320 Todd Rd project site during the wet season. Groundwater levels were manually measured bi-monthly from January 6, 2023 to March 31, 2023, see Appendix E for Soils Report.

The measured seasonal high groundwater level is at elevation 43.0', approximately 7 to 8 feet below existing grade. All BMP's will have sufficient separation between the bottom of the BMP and seasonal high groundwater level.

#### Field Measured Infiltration Rate

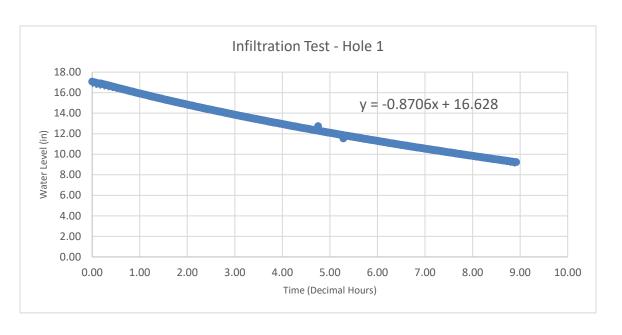
The infiltration rate was collected using two methods in during the PIT. The first method is to measure the gallons per minute flowrate required to maintain a constant water level in the test pit. The average of the flowrate measurements taken over an hour timeframe.

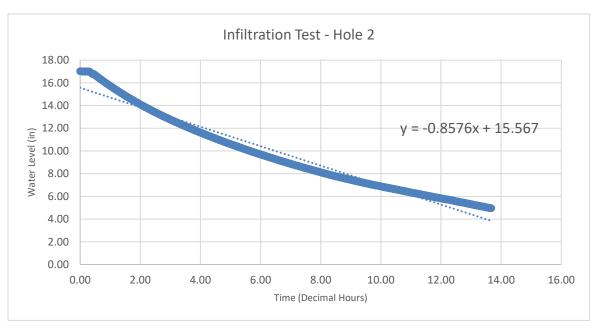
The second method is to measure the drawdown rate of the test pit. Measurements were taken both visually and with a data logger. The average of the drawdown measurements resulted in an infiltration rate of resulted in the following infiltration rates:

Test Hole 1: 0.87 inches per hour

• Test Hole 2: 0.85 inches per hour









#### **Design Infiltration Rate**

Per the Stormwater Manual a minimum design infiltration rate of 0.3 inches per hour is required for onsite infiltration. The design infiltration rate takes the field measured infiltration rate and applies a factor of safety based on three correction factors. The three corrections are based on site variability, test method, and degree of influent control (See Appendix D).

Issue	Partial Correction Factor
Site variability and number of locations tested $CF_V = 0.33 \text{ to } 1.0$ Test Method	
Test Method	
Large-scale PIT	<sup>™</sup> CF <sub>t</sub> = 0.75
Small-scale PIT	□ = 0.50
<ul> <li>Other small-scale (e.g. Double ring, falling head)</li> </ul>	<b>□</b> = 0.40
Grain Size Method	₪ = 0.40
Degree of influent control to prevent siltation and bio-buildup	CF <sub>m</sub> = 0.9

Total Correction Factor,  $CF_T = CF_v \times CF_t \times CF_m$ 

Based on multiple geotechnical reports from nearby projects, soils are known to be consistent in this area. Per the Stormwater Manual, a site variability correction of 1 is used. A correction of 0.5 for the small-scale PIT



and 0.9 for the degree of influent are also used. A total correction factor of 0.45 is applied to the measured infiltration rate yielding a recommended design infiltration rates as follows:

• Test Hole 1: 0.39 inches per hour

• Test Hole 2: 0.38 inches per hour

#### **Treatment Suitability**

Per the Stormwater Manual the soils that stormwater is infiltrated into may be used for treatment of pollution generating surfaces if the soil meets specific requirements. Otherwise, a treatment layer is required to treat pollution generating surfaces. The treatment threshold of the infiltrated soil per the Stormwater Manual is a Cation Exchange Capacity greater than or equal to 5 milliequivalents CEC/100g and a minimum of 1.0% organic content.

A soil sample was taken from the PIT, soils samples are still in testing and are pending results.

#### **TEST PIT PHOTO DOCUMENTATION - TEST HOLE 1**



3-feet x 4-feet x 18-inches



Test Pit Pre-soak at 12-inches



1-hour GPM Test





Pressure Transducer Drawdown Test



Over Excavation to observe it Groundwater is Mounding

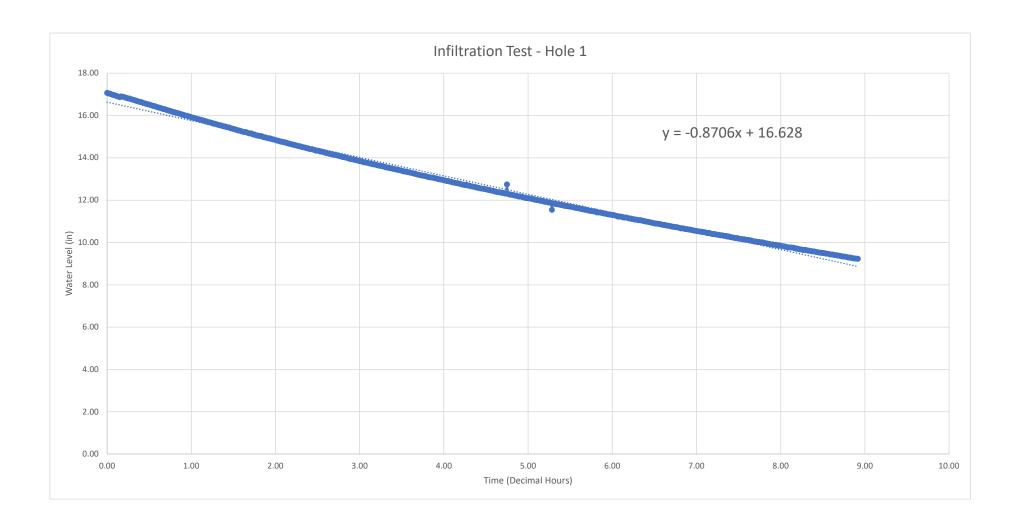


Backfill Test Hole



# **APPENDIX A**





JMJ 02 03/15	5/22	<u> </u>					I	
		Todd Rd Dovolog	ent .					
Project Location: Date of Test:		Todd Rd Developm						
Date of Test	. <del>.</del> 1		3/15/2023					
Test Pit Dim			41	\A(: d+l- (F+).	21	D = = +   (f = + 1).	41	
Test Pit Dim	ensions:	Length (Feet)	4'	Width (Feet):	3	Depth (feet):	4	
B 1			0.55 484 423					
Presoak:			9:55 - AM at 12-11	nch water column				
	<u>l</u>							
Infiltration T	Test:							
		Water Column Mair		12				
		Gallons Per Inch:	7.48					
			Volume				_	Infiltration Rate
		Time(Minutes)	(gallons)		Flow Rate (GPM)	1	Flow (Gallons)	(in/hr)
				Meter Start	Meter End	Flow (Gallons)		
		0						
		15						
		30						
		45						
		60						0.0
			Water Column M	aintained (inches)	12			
Weather Co	ndtions:		Cloudy					
Drawdown 1	Test (Sensor):							
			JMJ 02 (CRS451V					
			Sensors from					
			Campbell					
Sensor Nam	e:		Scientic)					
			,					
Time								
(decimal								
Hours)		Time Stamp	Record #	Reading (PSI)	Level (in)			
0.00	0.0	3:05:00 PM	0		17.07			
0.02	1.0	3:06:00 PM		0.6148627	17.04			
0.03		3:07:00 PM		0.6143792	17.03			
0.05	3.0	3:08:00 PM		0.6133576	17.00			
0.07	4.0	3:09:00 PM	4	0.6126429	16.98			
0.07	1				16.96			
0.10					16.94			
0.10				0.6101094	16.91			
0.12								
0.13					16.89			
0.15					16.87			
0.17								
0.18					16.89			
0.22								
0.23								
0.25					16.80			
0.27					16.80			
0.28								
0.30								
0.32								
0.33								
0.35					16.69			
0.37	22.0	3:27:00 PM	22	0.6014171	16.67			
	23.0	3:28:00 PM	23	0.6006184	16.65			
0.38	23.0				16.61			
0.38 0.40			24	0.6002951	16.64			
	24.0	3:29:00 PM			16.64 16.61			
0.40	24.0 25.0	3:29:00 PM	25	0.5992771	16.61			
0.40 0.42	24.0 25.0 26.0	3:29:00 PM 3:30:00 PM 3:31:00 PM	25 26	0.5992771 0.5982766	16.61			

	0.47	28.0						
		20.0	3:33:00 PM	28	0.5970181	16.55		
	0.48	29.0	3:34:00 PM	29	0.5963655	16.53		
	0.50	30.0	3:35:00 PM	30	0.5959253	16.52		
	0.52	31.0	3:36:00 PM	31	0.5948336	16.49		
	0.53	32.0	3:37:00 PM	32	0.5941705	16.47		
	0.55	33.0	3:38:00 PM	33	0.5933849	16.45		
	0.57	34.0	3:39:00 PM	34	0.5930045	16.44		
	0.58	35.0	3:40:00 PM	35	0.5921196	16.41		
	0.60	36.0	3:41:00 PM	36	0.5912513	16.39		
	0.62	37.0	3:42:00 PM	37	0.5906174	16.37		
	0.63	38.0	3:43:00 PM	38	0.589988	16.35		
	0.65	39.0	3:44:00 PM	39		16.34	+	
					0.5894052			
	0.67	40.0	3:45:00 PM	40	0.588398	16.31		
	0.68	41.0	3:46:00 PM	41	0.5878983	16.30		
	0.70	42.0	3:47:00 PM	42	0.5870169	16.27		
	0.72	43.0	3:48:00 PM	43	0.5864626	16.26		
	0.73	44.0	3:49:00 PM	44	0.5854719	16.23		
	0.75	45.0	3:50:00 PM	45	0.584968	16.22		
	0.77	46.0	3:51:00 PM	46	0.5838918	16.19		
	0.78	47.0	3:52:00 PM	47	0.5833375	16.17		
	0.80	48.0	3:53:00 PM	48	0.5826278	16.15	<u> </u>	
	0.82	49.0	3:54:00 PM	49	0.5819051	16.13	İ	
	0.83	50.0	3:55:00 PM	50	0.5815238	16.12		
<b>-</b>	0.85	51.0	3:56:00 PM	51	0.5808325	16.10		
	0.87	52.0	3:57:00 PM	52	0.5799282	16.08		
	0.88	53.0	3:58:00 PM	53	0.5792771	16.06		
	0.90	54.0	3:59:00 PM	54	0.578376	16.03		
	0.92	55.0	4:00:00 PM	55	0.5778934	16.02		
	0.93	56.0	4:01:00 PM	56	0.5769713	15.99		
	0.95	57.0	4:02:00 PM	57	0.5766121	15.98		
	0.97	58.0		58		15.96		
			4:03:00 PM		0.5757054			
	0.98	59.0	4:04:00 PM	59	0.5750806	15.94		
	1.00	60.0	4:05:00 PM	60	0.5741982	15.92		
	1.02	61.0	4:06:00 PM	61	0.5735646	15.90		
	1.03	62.0	4:07:00 PM	62	0.5729434	15.88		
	1.05	63.0	4:08:00 PM	63	0.5726172	15.87		
	1.07	64.0	4:09:00 PM	64	0.5713918	15.84		
	1.08	65.0	4:10:00 PM	65	0.5710028	15.83		
	1.10	66.0	4:11:00 PM	66	0.5705318	15.82		
	1.12	67.0	4:12:00 PM	67	0.569611	15.79		
	1.13	68.0	4:13:00 PM	68	0.5690674	15.77		
	1.15	69.0	4:14:00 PM	69	0.5684627	15.76		
	1.17	70.0	4:15:00 PM	70		15.73		
<b>-</b>							<del>                                     </del>	
	1.18	71.0	4:16:00 PM	71	0.5669469	15.72		
	1.20	72.0	4:17:00 PM	72	0.5660034	15.69		
L	1.22	73.0	4:18:00 PM	73	0.5655891	15.68	<u> </u>	
	1.23	74.0	4:19:00 PM	74	0.5650941	15.66		<u> </u>
	1.25	75.0	4:20:00 PM	75	0.564332	15.64		
	1.27	76.0	4:21:00 PM	76	0.5630262	15.61		
	1.28	77.0	4:22:00 PM	77	0.5631915	15.61		
	1.30	78.0	4:23:00 PM	78	0.5621863	15.58		
	1.32	79.0	4:24:00 PM	79	0.5614846			
	1.33	80.0	4:25:00 PM	80	0.5608001	15.55		
	1.35	81.0	4:26:00 PM	81	0.5605492	15.54		
	1.37	82.0	4:27:00 PM	82	0.5595577	15.51		
	1.38	83.0	4:28:00 PM	83	0.5588057	15.49	<del> </del>	
	1.40	84.0	4:29:00 PM	84	0.5584829	15.49		
	1.42	85.0	4:30:00 PM	85	0.5576767			
	1.43	86.0	4:31:00 PM	86	0.5570237	15.44	<u> </u>	
	1.45	87.0	4:32:00 PM	87	0.556747	15.43		
	1.47	88.0	4:33:00 PM	88	0.5556393	15.40		
	1.48	89.0	4:34:00 PM	89	0.5549214			
<b>.</b>	1.50	90.0	4:35:00 PM	90	0.5542242	15.36		
	1.52	91.0	4:36:00 PM	91	0.5535494	15.34		
	1.53	92.0	4:37:00 PM	92	0.552975	15.33	i	<u> </u>

						1	
1.55	93.0	4:38:00 PM	93	0.5517957	15.30		
1.57	94.0	4:39:00 PM	94	0.5515959	15.29		
1.58	95.0	4:40:00 PM	95	0.5512913	15.28		
1.60	96.0	4:41:00 PM	96	0.5499135	15.24		
1.62	97.0	4:42:00 PM	97	0.5494438	15.23		
1.63	98.0	4:43:00 PM	98	0.5490008	15.22		
1.65	99.0	4:44:00 PM	99	0.5488402	15.21		
1.67	100.0	4:45:00 PM	100	0.5479615	15.19		
1.68	101.0	4:46:00 PM	101	0.5468689	15.16		
1.70	102.0	4:47:00 PM	102	0.5468307	15.16		
1.72	103.0	4:48:00 PM	103	0.5463324	15.14		
1.73	104.0	4:49:00 PM	104	0.5450302	15.11		
1.75	105.0	4:50:00 PM	105	0.5448695	15.10		
1.77	106.0	4:51:00 PM	106	0.5435811	15.07		
1.78	107.0	4:52:00 PM	107	0.543332	15.06		
1.80	108.0	4:53:00 PM	108	0.5427405	15.04		
1.82	109.0	4:54:00 PM	109	0.5420786	15.03		
1.83	110.0	4:55:00 PM	110	0.5419946	15.02		
1.85	111.0	4:56:00 PM	111	0.5407454	14.99		
1.87	112.0	4:57:00 PM	112	0.5401692	14.97		
1.88	113.0	4:58:00 PM	113	0.5397636	14.96		
1.90	114.0	4:59:00 PM	113	0.5387734	14.93		
1.92	115.0	5:00:00 PM	115	0.5382738	14.92		
1.93	116.0	5:01:00 PM	116	0.5384395	14.93		
1.95	117.0	5:02:00 PM	117	0.5372641	14.89		
1.97	118.0	5:03:00 PM	118	0.536586	14.87		
1.98	119.0	5:04:00 PM	119	0.5359896	14.86		
2.00	120.0	5:05:00 PM	120	0.53537	14.84		
2.02	121.0	5:06:00 PM	121	0.5344813	14.82		
2.03	122.0	5:07:00 PM	122	0.5341182	14.81		
2.05	123.0	5:08:00 PM	123	0.5332245	14.78		
2.07	124.0	5:09:00 PM	124	0.5326889	14.77		
2.08	125.0	5:10:00 PM	125	0.5318959	14.74		
2.10	126.0	5:11:00 PM	126	0.5319012	14.74		
2.12	127.0	5:12:00 PM	127	0.5308706	14.72		
2.13	128.0	5:13:00 PM	128	0.5306203	14.71		
2.15	129.0	5:14:00 PM	129	0.5296948	14.68		
2.17	130.0	5:15:00 PM	130	0.5289809	14.66		
2.18	131.0	5:16:00 PM	131	0.5284132	14.65		
2.20	132.0	5:17:00 PM	132	0.527842	14.63		
2.22	133.0	5:18:00 PM	133	0.5273663	14.62		
2.23	134.0	5:19:00 PM	134	0.5265781	14.60		
2.25	135.0	5:20:00 PM	135	0.5261628	14.59		
2.27	136.0	5:21:00 PM	136	0.5253428	14.56		
2.28	137.0	5:22:00 PM	137	0.5248385	14.55		
2.30	138.0	5:23:00 PM	138	0.5243507	14.54		
2.32	139.0	5:24:00 PM	139	0.5234047	14.51		
2.33	140.0	5:25:00 PM	140	0.5230739	14.50		
2.35	141.0	5:26:00 PM	141	0.5225979	14.49		
2.37	142.0	5:27:00 PM	142	0.5217437	14.46		
2.38	143.0	5:28:00 PM	143	0.5213159	14.45		
2.40	144.0	5:29:00 PM	144	0.5203963	14.43		
2.42	145.0	5:30:00 PM	145	0.5199574	14.41		
2.43	146.0	5:31:00 PM	146	0.5197419	14.41		
2.45	147.0	5:32:00 PM	147	0.5187908	14.38		
2.47	148.0	5:33:00 PM	148	0.5180068	14.36		
2.48	149.0	5:34:00 PM	149	0.5175015	14.35		
2.50	150.0	5:35:00 PM	150	0.5174106	14.34		
2.52	151.0	5:36:00 PM	151	0.5168511	14.33		
2.53	152.0	5:37:00 PM	152	0.5157433	14.30		
2.55	153.0	5:38:00 PM	153	0.5155004	14.29		
2.57	154.0	5:39:00 PM	154	0.5146531	14.27		
2.58	155.0		155	0.5142437	14.27		
2.58		5:40:00 PM					
, , , , , ,	156.0	5:41:00 PM	156	0.5133805	14.23	i l	I
2.62	157.0	5:42:00 PM	157	0.5128037	14.21		

						,	
2.63	158.0	5:43:00 PM	158	0.5122814	14.20		
2.65	159.0	5:44:00 PM	159	0.5115144	14.18		
2.67	160.0	5:45:00 PM	160	0.5113738	14.18		
2.68	161.0	5:46:00 PM	161	0.5105324	14.15		
2.70	162.0	5:47:00 PM	162	0.5101804	14.14		
2.72	163.0	5:48:00 PM	163		14.14		
				0.5099925			
2.73	164.0	5:49:00 PM	164	0.5092018	14.12		
2.75	165.0	5:50:00 PM	165	0.5085192	14.10		
2.77	166.0	5:51:00 PM	166	0.5079156	14.08		
2.78	167.0	5:52:00 PM	167	0.5074483	14.07		
2.80	168.0	5:53:00 PM	168	0.5064862	14.04		
2.82	169.0	5:54:00 PM	169	0.5059146	14.02		
2.83	170.0	5:55:00 PM	170	0.5055254	14.01		
2.85	171.0	5:56:00 PM	171	0.5049577	14.00		
2.87	172.0	5:57:00 PM	172	0.5039244	13.97		
2.88	173.0	5:58:00 PM	173	0.5034221	13.95		
2.90	174.0	5:59:00 PM	174	0.502814	13.94		
2.92	175.0	6:00:00 PM	175	0.5027304	13.94		
2.93	176.0	6:01:00 PM	176	0.5020565	13.92		
2.95	177.0	6:02:00 PM	177	0.5013036	13.90		
2.97	178.0	6:03:00 PM	178	0.5007532	13.88		<del>-  </del>
2.98	179.0	6:04:00 PM	179	0.500052	13.86		
3.00	180.0	6:05:00 PM	180	0.4996347	13.85		
3.02	181.0	6:06:00 PM	181	0.499271	13.84		
3.03	182.0	6:07:00 PM	182	0.4984125	13.82		
3.05	183.0	6:08:00 PM	183	0.4976832	13.80		
3.07	184.0	6:09:00 PM	184	0.4970511	13.78		
3.08	185.0	6:10:00 PM	185	0.4967992	13.77		
	186.0						
3.10		6:11:00 PM	186	0.496339	13.76		
3.12	187.0	6:12:00 PM	187	0.4953722	13.73		
3.13	188.0	6:13:00 PM	188	0.4953351	13.73		
3.15	189.0	6:14:00 PM	189	0.494025	13.69		
3.17	190.0	6:15:00 PM	190	0.4942182	13.70		
3.18	191.0	6:16:00 PM	191	0.4934728	13.68		
3.20	192.0	6:17:00 PM	192	0.4927351	13.66		
3.22	193.0	6:18:00 PM	193	0.4921242	13.64		
3.23	194.0	6:19:00 PM	194	0.4917595	13.63		
3.25	195.0	6:20:00 PM	195	0.491395	13.62		
3.27	196.0	6:21:00 PM	196	0.4907802	13.60		
3.28	197.0	6:22:00 PM	197	0.4902606	13.59		
3.30	198.0	6:23:00 PM	198	0.4893938	13.57		
3.32	199.0	6:24:00 PM	199	0.4886401	13.55		
3.33	200.0	6:25:00 PM	200		13.54		
3.35	201.0	6:26:00 PM	201	0.4877641	13.52		
3.37	202.0	6:27:00 PM	202	0.4873322	13.51		
3.38	203.0	6:28:00 PM	203	0.486859	13.50		
3.40	204.0	6:29:00 PM	204	0.4862999	13.48		
3.42	205.0	6:30:00 PM	205	0.4857687	13.47		
3.43	206.0	6:31:00 PM	206	0.4852299	13.45		
3.45	207.0	6:32:00 PM	207	0.484644	13.43		
3.47	208.0	6:33:00 PM	208	0.4842926	13.42		
3.48	209.0	6:34:00 PM	209	0.483613	13.41		<del></del>
3.50	210.0	6:35:00 PM	210	0.4831619	13.41		<del>-  </del>
3.52	211.0	6:36:00 PM	211	0.4821794	13.37		
3.53	212.0	6:37:00 PM	212	0.4819682	13.36		
3.55	213.0	6:38:00 PM	213	0.4814751	13.35		
3.57	214.0	6:39:00 PM	214	0.4806702	13.32		
3.58	215.0	6:40:00 PM	215	0.4804766	13.32		
3.60	216.0	6:41:00 PM	216	0.4799258	13.30		
3.62	217.0	6:42:00 PM	217	0.4792077	13.28		
							<del>-  </del>
3.63	218.0	6:43:00 PM	218	0.4785481	13.27		
3.65	219.0	6:44:00 PM	219	0.4782073	13.26		
3.67	220.0	6:45:00 PM	220	0.4774906	13.24		
3.68	221.0	6:46:00 PM	221	0.4766157	13.21		
3.70	222.0	6:47:00 PM	222	0.4762415	13.20		
	l.	I					

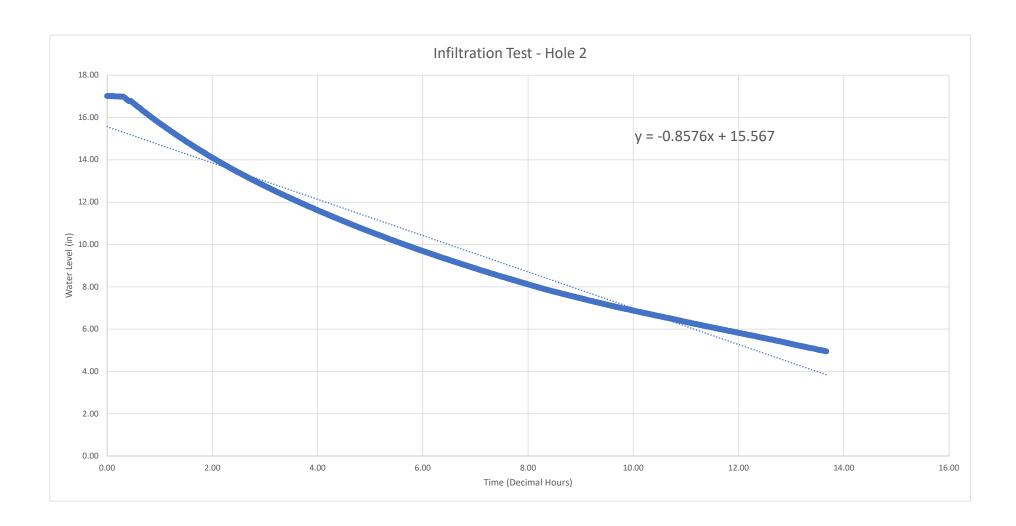
	1	1		ı			
3.72	223.0		223	0.4756183	13.18		
3.73	224.0	6:49:00 PM	224	0.4750919	13.17		
3.75	225.0	6:50:00 PM	225	0.474655	13.16		
3.77	226.0		226	0.4740577	13.14		
3.78		6:52:00 PM	227	0.4739504	13.14		
3.80		6:53:00 PM	228	0.4729107	13.11		-
3.82			229	0.4721898	13.09		-
3.83			230	0.4720053	13.08		
3.85	231.0	6:56:00 PM	231	0.4713734	13.07		
3.87	232.0	6:57:00 PM	232	0.4713112	13.06		
3.88	233.0	6:58:00 PM	233	0.4707035	13.05		
3.90	234.0	6:59:00 PM	234	0.4702266	13.03		
3.92	235.0	7:00:00 PM	235	0.4697167	13.02		
3.93	236.0	7:01:00 PM	236	0.4687088	12.99		
3.95			237	0.4685055	12.99		-
3.97	238.0		238	0.4678922	12.97		
3.98	239.0	7:04:00 PM	239	0.4676406	12.96		
4.00	240.0	7:05:00 PM	240	0.4667491	12.94		
4.02	241.0	7:06:00 PM	241	0.4661983	12.92		
4.03	242.0	7:07:00 PM	242	0.4655441	12.90		
4.05	243.0	7:08:00 PM	243	0.4653235	12.90		
4.07	244.0		244	0.4645744	12.88		
						+	<del>   </del>
4.08			245		12.87		
4.10			246	0.463375	12.84		
4.12	247.0		247	0.4629279	12.83		
4.13	248.0	7:13:00 PM	248	0.4624807	12.82		
4.15	249.0	7:14:00 PM	249	0.4619249	12.80		
4.17	250.0	7:15:00 PM	250	0.4616999	12.80		
4.18		7:16:00 PM	251	0.4609861	12.78		
4.20			252	0.4604497	12.76		
4.22			253	0.4598548	12.75		
4.23			254	0.459208	12.73		
4.25	255.0	7:20:00 PM	255	0.4587872	12.72		
4.27	256.0	7:21:00 PM	256	0.4590833	12.73		
4.28	257.0	7:22:00 PM	257	0.4579127	12.69		
4.30	258.0	7:23:00 PM	258	0.4574784	12.68		
4.32	259.0	7:24:00 PM	259	0.4568346	12.66		
4.33		7:25:00 PM	260	0.4562342	12.65		
4.35			261	0.4558793	12.64		-
4.37	262.0		262		12.62		-
				0.4553724			
4.38	263.0	7:28:00 PM	263	0.4548495	12.61		
4.40		7:29:00 PM	264	0.454033	12.59		
4.42	265.0	7:30:00 PM	265	0.4537116	12.58		
4.43	266.0	7:31:00 PM	266	0.4529433	12.56		
4.45	267.0	7:32:00 PM	267	0.4524295	12.54		
4.47	268.0	7:33:00 PM	268	0.4522238	12.54		
4.48			269	0.4518773	12.53		
4.50			270	0.4513924	12.51	†	<del></del>
4.50	271.0		271	0.4505684	12.49	<del>                                     </del>	<del></del>
4.52			271		12.49		<del>   </del>
				0.4504066			
4.55			273	0.4496302	12.46		
4.57			274	0.4492884	12.45		
4.58		7:40:00 PM	275	0.4488221	12.44		
4.60	276.0		276	0.4480051	12.42		
4.62	277.0	7:42:00 PM	277	0.4474825	12.40		
4.63			278	0.4467733	12.38		
4.65			279	0.4464708			+
4.67			280	0.4463106			<del></del>
4.68			281	0.4454604	12.35		
4.70			282	0.4453031	12.34		
4.72			283	0.4445886	12.32		
4.73	284.0	7:49:00 PM	284	0.4440461	12.31		
4.75	285.0	7:50:00 PM	285	0.4598133	12.75		
4.77	286.0		286	0.4433854	12.29		<del>-  </del>
4.78			287	0.4422977	12.26		<del></del>
7.70	207.0	7.32.00 1101	207	0.7722377	12.20	11	

				Т		1	
4.80	288.0	7:53:00 PM	288		12.25		
4.82	289.0	7:54:00 PM	289	0.4417258	12.24		
4.83	290.0	7:55:00 PM	290	0.4413367	12.23		
4.85	291.0	7:56:00 PM	291	0.4404738	12.21		
4.87	292.0	7:57:00 PM	292	0.4402833	12.20		
4.88	293.0	7:58:00 PM	293	0.4392645	12.18		
4.90	294.0	7:59:00 PM	294	0.4390843	12.17		
4.92	295.0	8:00:00 PM	295	0.4390247	12.17		
4.93	296.0	8:01:00 PM	296	0.4381262	12.14		
4.95	297.0	8:02:00 PM	297	0.4374221	12.13		
4.97	298.0	8:03:00 PM	298	0.4368554	12.11		
4.98	299.0	8:04:00 PM	299	0.4364111	12.10		
5.00	300.0	8:05:00 PM	300	0.4363991	12.10		
5.02	301.0	8:06:00 PM	301	0.4357242	12.08		
5.03	302.0	8:07:00 PM	302	0.4356918	12.08		
5.05	303.0	8:08:00 PM	303	0.4348011	12.05		
5.07	304.0	8:09:00 PM	304	0.4342441	12.04		
5.08	305.0	8:10:00 PM	305	0.4337437	12.02		
5.10		8:11:00 PM	306	0.4331467	12.01		
5.12	307.0	8:12:00 PM	307	0.4325188	11.99		
5.13	308.0	8:13:00 PM	308	0.4326446	11.99		
5.15	309.0	8:14:00 PM	309	0.4316702	11.97		
5.17	310.0	8:15:00 PM	310	0.4315181	11.96		
5.18		8:16:00 PM	310	0.4306561	11.94		
5.20		8:17:00 PM	312	0.4300736	11.92		
5.22	313.0	8:18:00 PM	313	0.4299336	11.92		
5.23	314.0	8:19:00 PM	314	0.4292848	11.90		
5.25	315.0	8:20:00 PM	315	0.4289575	11.89		
5.27	316.0	8:21:00 PM	316	0.4285058	11.88		
5.28		8:22:00 PM	317	0.4163842	11.54		
5.30	318.0	8:23:00 PM	318	0.4272409	11.84		
5.32	319.0	8:24:00 PM	319	0.4268593	11.83		
5.33	320.0	8:25:00 PM	320	0.4261787	11.81		
5.35	321.0	8:26:00 PM	321	0.4260441	11.81		
5.37							
	322.0	8:27:00 PM	322	0.4257566	11.80		
5.38	323.0	8:28:00 PM	323	0.4249824	11.78		
5.40	324.0	8:29:00 PM	324	0.4245381	11.77		
5.42	325.0	8:30:00 PM	325	0.4241344	11.76		
5.43	326.0	8:31:00 PM	326	0.4233149	11.73		
5.45	327.0	8:32:00 PM	327	0.4228588	11.72		
5.47	328.0	8:33:00 PM	328	0.4228771	11.72		
5.48	329.0	8:34:00 PM	329	0.4221428	11.70		
5.50	330.0	8:35:00 PM	330	0.4220134	11.70		
5.52	331.0		331	0.4211294			
5.53	332.0		332	0.4209543	11.67		
5.55		8:38:00 PM	333	0.4203614			
5.57	334.0	8:39:00 PM	334	0.4196712	11.63		
5.58	335.0	8:40:00 PM	335	0.4195567	11.63		
5.60			336		11.61		
5.62		8:42:00 PM	337	0.4185083	11.60		
5.63		8:43:00 PM	338				
5.65	339.0	8:44:00 PM	339		11.59		
5.67	340.0	8:45:00 PM	340	0.4166287	11.55		
5.68	341.0	8:46:00 PM	341	0.4162635	11.54		
5.70		8:47:00 PM	342	0.4159639	11.53		<del>-  </del>
5.72		8:48:00 PM	343	0.4152418			
5.73		8:49:00 PM	344	0.4148639	11.50		
5.75	345.0	8:50:00 PM	345	0.4145225	11.49		
5.77	346.0	8:51:00 PM	346	0.4142239	11.48		
5.78		8:52:00 PM	347	0.4137594	11.47		
5.80		8:53:00 PM	348				
5.82	349.0	8:54:00 PM	349		11.43		
5.83	350.0	8:55:00 PM	350	0.4120906	11.42		
5.85	351.0	8:56:00 PM	351	0.4118601	11.42		
5.87			352		11.40		
5.07	332.0	0.57.00 1 101	332	0.7114033	11.40	l l	

		ı		1	1	,	
5.88			353	0.4109527	11.39		
5.90	354.0	8:59:00 PM	354	0.4103119	11.37		
5.92	355.0	9:00:00 PM	355	0.4100701	11.37		
5.93	356.0	9:01:00 PM	356	0.4093683	11.35		
5.95	357.0	9:02:00 PM	357	0.4088797	11.33		
5.97	358.0		358	0.4086282	11.33		
5.98			359	0.4082363	11.32		
6.00			360	0.4075574	11.30		
6.02	361.0		361	0.4074436			
6.03	362.0	9:07:00 PM	362	0.4066026	11.27		
6.05	363.0	9:08:00 PM	363	0.4060326	11.26		
6.07	364.0	9:09:00 PM	364	0.4049584	11.23		
6.08	365.0	9:10:00 PM	365	0.4050892	11.23		
6.10	366.0	9:11:00 PM	366	0.4050245	11.23		
6.12	367.0		367	0.4043415	11.21		
6.13			368	0.4034517	11.18		
6.15	369.0		369	0.4033616			
6.17	370.0	9:15:00 PM	370	0.403163	11.18		
6.18	371.0	9:16:00 PM	371	0.4025511	11.16		
6.20	372.0	9:17:00 PM	372	0.4015446	11.13		
6.22	373.0	9:18:00 PM	373	0.4017813	11.14		
6.23	374.0		374	0.4008764	11.11		
6.25	374.0		375	0.4007378	11.11	<del>                                     </del>	
						<del>                                     </del>	
6.27	376.0		376	0.3997173	11.08		
6.28	377.0		377	0.3996115	11.08		
6.30	378.0	9:23:00 PM	378	0.3991556	11.06		
6.32	379.0	9:24:00 PM	379	0.3986912	11.05		
6.33	380.0	9:25:00 PM	380	0.398762	11.05		
6.35	381.0	9:26:00 PM	381	0.3978955	11.03		
6.37	382.0		382	0.3974971	11.02		
6.38			383	0.396899			
6.40			384	0.3963188	10.99		
6.42	385.0		385	0.3961894	10.98		
6.43	386.0	9:31:00 PM	386	0.3957344	10.97		
6.45	387.0		387	0.3950145	10.95		
6.47	388.0	9:33:00 PM	388	0.3946161	10.94		
6.48	389.0	9:34:00 PM	389	0.3940708	10.92		
6.50	390.0	9:35:00 PM	390	0.3934942	10.91		
6.52	391.0		391	0.3931231	10.90		
6.53	392.0		392	0.3928045	10.89		
6.55	393.0		393	0.3923118	10.87		
6.57	394.0		394	0.3922051	10.87		
6.58	395.0	9:40:00 PM	395	0.3915047	10.85		
6.60	396.0	9:41:00 PM	396	0.3907251	10.83		
6.62	397.0	9:42:00 PM	397	0.3908065	10.83		
6.63	398.0	9:43:00 PM	398	0.3900802	10.81		
6.65	399.0		399	0.3891978			
6.67	400.0		400	0.3894995			
6.68			400	0.3887725			
6.70			402	0.3882808			
6.72	403.0		403	0.3875159			
6.73	404.0		404	0.3873371	10.74		
6.75	405.0	9:50:00 PM	405	0.3869162	10.73		
6.77	406.0	9:51:00 PM	406	0.3867165	10.72		
6.78	407.0	9:52:00 PM	407	0.3861673	10.70		
6.80			408	0.3855217	10.69		
6.82	409.0		409	0.38482		<del>                                     </del>	
6.83							
	410.0		410				
6.85	411.0		411	0.3844962	10.66		
6.87	412.0	9:57:00 PM	412	0.3837038	10.64		
6.88	413.0	9:58:00 PM	413	0.3836343	10.63		
6.90	414.0	9:59:00 PM	414	0.3830293	10.62		
6.92	415.0		415	0.3827337	10.61		
6.93	416.0		416		10.60		
6.95			417		10.58		+
. 0.95	417.0	10.02:00 PIVI	41/	0.301011/	10.58		

	1			ı		T	
6.97	418.0	10:03:00 PM	418	0.3812735	10.57		
6.98	419.0	10:04:00 PM	419	0.3808888	10.56		
7.00	420.0	10:05:00 PM	420	0.3803261	10.54		
7.02	421.0	10:06:00 PM	421	0.37999	10.53		
7.03	422.0	10:07:00 PM	422	0.379525	10.52		
7.05	423.0	10:08:00 PM	423	0.3791612	10.51		
7.07	424.0	10:09:00 PM	424	0.3788717	10.50		
7.08		10:10:00 PM	425	0.3785872	10.49		
7.10		10:11:00 PM	426	0.3780693	10.48		
7.12	427.0	10:12:00 PM	427	0.3775157	10.46		
7.13	428.0	10:13:00 PM	428	0.3765889	10.44		
7.15	429.0	10:14:00 PM	429	0.3771551	10.45		
7.17	430.0	10:15:00 PM	430	0.3759286	10.42		
7.18	431.0	10:16:00 PM	431	0.3753921	10.41		
7.20		10:17:00 PM	432	0.3748997	10.39		
7.20							
	433.0	10:18:00 PM	433	0.3752069	10.40		
7.23	434.0	10:19:00 PM	434	0.3743168	10.38		
7.25	435.0	10:20:00 PM	435	0.3740495	10.37		
7.27	436.0	10:21:00 PM	436	0.3739115	10.36		
7.28	437.0	10:22:00 PM	437	0.3730409	10.34		
7.30	438.0	10:23:00 PM	438	0.3730856	10.34		
7.32	439.0	10:24:00 PM	439	0.3725324	10.33		
7.32		10:25:00 PM	440	0.3718792	10.33		
7.35		10:25:00 PM	440	0.3719645	10.31	<del> </del>	<del>-</del>
7.37	442.0	10:27:00 PM	442	0.3709205	10.28		
7.38		10:28:00 PM	443	0.3709977	10.28		
7.40	444.0	10:29:00 PM	444	0.3700362	10.26		
7.42	445.0	10:30:00 PM	445	0.3697953	10.25		
7.43	446.0	10:31:00 PM	446	0.3692849	10.24		
7.45	447.0	10:32:00 PM	447	0.3687208	10.22		
7.47	448.0	10:33:00 PM	448	0.3680923	10.20		
7.48		10:34:00 PM	449	0.3682602	10.21		
7.50		10:35:00 PM	450	0.3672431	10.18		
7.52	451.0	10:36:00 PM	451	0.3671553	10.18		
7.53		10:37:00 PM	452	0.3667587	10.17		
7.55	453.0	10:38:00 PM	453	0.3663796	10.16		
7.57	454.0	10:39:00 PM	454	0.3661635	10.15		
7.58	455.0	10:40:00 PM	455	0.3653865	10.13		
7.60	456.0	10:41:00 PM	456	0.3653121	10.13		
7.62	457.0	10:42:00 PM	457	0.3650196	10.12		
7.63	458.0	10:43:00 PM	458	0.3641022	10.09		
7.65	459.0	10:44:00 PM	459	0.364122	10.09		
7.67		10:45:00 PM	460		10.06		
7.68		10:46:00 PM	461	0.3626614			
7.70	462.0	10:47:00 PM	462	0.3623884	10.05		
7.72	463.0	10:48:00 PM	463	0.3618577	10.03		
7.73	464.0	10:49:00 PM	464	0.3616126	10.02		
7.75	465.0	10:50:00 PM	465	0.3615493	10.02		
7.77	466.0	10:51:00 PM	466	0.3606695	10.00		
7.78		10:52:00 PM	467	0.3609027	10.00	+	
7.78		10:53:00 PM	468	0.3596428	9.97		
7.80							
		10:54:00 PM	469	0.3597279			
7.83		10:55:00 PM	470	0.3592831	9.96		
7.85		10:56:00 PM	471	0.3586352	9.94		
7.87	472.0	10:57:00 PM	472	0.3583514	9.93		
7.88	473.0	10:58:00 PM	473	0.3576606	9.91		
7.90	474.0	10:59:00 PM	474	0.3573305	9.91		
7.92		11:00:00 PM	475	0.3569244	9.89		
7.93		11:01:00 PM	476	0.3567483	9.89		
							-
7.95	477.0	11:02:00 PM	477	0.3565202	9.88		
7.97		11:03:00 PM	478				
7.98		11:04:00 PM	479	0.3556866	9.86		
8.00	480.0	11:05:00 PM	480	0.3551398	9.84		
8.02	481.0	11:06:00 PM	481	0.3547916	9.83		
8.03	482.0	11:07:00 PM	482	0.3541431	9.82		
						L	

		l I				
		-			5.15	
				Factor of Safety:	0.45	
			Average	Infiltration Rate:	0.87	
			A.,	Infiltration Data	0.07	
8.92	535.0	12:00:00 AM	535	0.3328936	9.23	
8.90	534.0	11:59:00 PM	534	0.3331816		
8.88	533.0	11:58:00 PM	533	0.333342	9.24	
8.87	532.0	11:57:00 PM	532	0.3336633		
8.83 8.85	530.0	11:55:00 PM 11:56:00 PM	530	0.334726	9.28	
8.82 8.83	529.0 530.0	11:54:00 PM 11:55:00 PM	529 530	0.3352662 0.334726	9.29 9.28	
8.80	528.0	11:53:00 PM	528	0.3350894		
8.78	527.0	11:52:00 PM	527	0.3361159		
8.77	526.0	11:51:00 PM	526	0.336421	9.33	
8.75	525.0	11:50:00 PM	525	0.3366016		
8.73	524.0	11:49:00 PM	524	0.3371136	9.34	
8.72	523.0	11:48:00 PM	523	0.3376943	9.36	
8.70	522.0	11:47:00 PM	522	0.3379867	9.37	
8.68	521.0	11:46:00 PM	520	0.3383609	9.39	
8.65 8.67	519.0 520.0	11:44:00 PM 11:45:00 PM	519 520	0.3393098 0.3388627	9.41 9.39	
8.63	518.0	11:43:00 PM	518	0.3394211	9.41	
8.62	517.0	11:42:00 PM	517	0.3402545	9.43	
8.60	516.0	11:41:00 PM	516	0.3403109	9.43	
8.58	515.0	11:40:00 PM	515	0.3405904	9.44	
8.57	514.0	11:39:00 PM	514	0.3413677	9.46	
8.55	513.0	11:38:00 PM	513	0.3417095	9.47	
8.53	512.0	11:37:00 PM	512	0.3419479	9.48	
8.52	511.0	11:36:00 PM	510	0.3427011	9.50	
8.50	510.0	11:35:00 PM	510	0.3426367	9.50	
8.47 8.48	508.0 509.0	11:33:00 PM 11:34:00 PM	508 509	0.3433304 0.3433363	9.52 9.52	
8.45	507.0	11:32:00 PM	507	0.34374	9.53	
8.43	506.0	11:31:00 PM	506	0.3445507	9.55	
8.42	505.0	11:30:00 PM	505	0.3444213	9.55	
8.40	504.0	11:29:00 PM	504	0.3453229	9.57	
8.38	503.0	11:28:00 PM	503	0.3456394	9.58	
8.37	502.0	11:27:00 PM	502	0.3459623	9.59	
8.35	501.0	11:26:00 PM	501	0.3463698	9.60	
8.32	500.0	11:24:00 PM	500	0.3470287	9.62	
8.30 8.32	498.0 499.0	11:23:00 PM 11:24:00 PM	498 499	0.3479398 0.3470287	9.64 9.62	
8.28	497.0	11:22:00 PM	497	0.3481885	9.65	
8.27	496.0	11:21:00 PM	496	0.348048	9.65	
8.25	495.0	11:20:00 PM	495	0.3489193	9.67	
8.23	494.0	11:19:00 PM	494	0.3490596	9.68	
8.22	493.0	11:18:00 PM	493	0.3493306	9.68	
8.20	492.0	11:17:00 PM	492	0.3502798	9.71	
8.18	491.0	11:16:00 PM	491	0.3500417	9.70	
8.17	490.0	11:15:00 PM	489	0.3517121	9.73	
8.13	488.0 489.0	11:13:00 PM 11:14:00 PM	488 489	0.3519594 0.3517121	9.76 9.75	
8.12 8.13	487.0	11:12:00 PM	487	0.3522007	9.76	
8.10	486.0	11:11:00 PM	486	0.3524059	9.77	
8.08	485.0	11:10:00 PM	485	0.3525001	9.77	
8.07	484.0	11:09:00 PM	484	0.3532099	9.79	
8.05	483.0	11:08:00 PM	483	0.3541102	9.82	



IMI 01 02 /11	5/22		<u> </u>	<u> </u>			I	
JMJ 01 03/15		Todd Pd Douglass	l				<del>                                     </del>	
Project Loca		Todd Rd Developm						
Date of Test	; 		3/15/2023					
Toot Dit Die	onsions:	Longth (Foot)	4'	\A/;d+b /F/\	21	Donth /f/	41	
Test Pit Dim	ensions:	Length (Feet)	4	Width (Feet):	3	Depth (feet):	<del>'1</del>	
Drococky			0.4E AN4 at 12 :	nch water calures				
Presoak:			9:45 - AIVI at 12-11	nch water column I				
Infiltration T	est:			10				
		Water Column Mair		12				
		Gallons Per Inch:	7.48					
			Volume				_ , ,_ , ,	Infiltration Rate
		Time(Minutes)	(gallons)		Flow Rate (GPM)		Flow (Gallons)	(in/hr)
				Meter Start	Meter End	Flow (Gallons)		
		0						
		15						
		30						
		45						
		60						0.0
			Water Column M	aintained (inches)	12			
Weather Co	ndtions:		Cloudy					
Drawdown 1	Test (Sensor):							
			JMJ 01 (CRS451V					
			Sensors from					
			Campbell					
Sensor Nam	e:		Scientic)					
	<u> </u>		,					
Time								
(decimal	Readings							
Hours)	(min)	Time Stamp	Record #	Reading (PSI)	Level (in)			
0.00	0.0	2:47:00 PM	47	0.6138949	17.02			
0.02	1.0	2:48:00 PM	48	0.6139137	17.02			
0.02	2.0	2:49:00 PM		0.6138233	17.02			
0.05	3.0	2:50:00 PM	50		17.01			
0.03	4.0	2:51:00 PM	51	0.6136847	17.01			
0.07	5.0	2:52:00 PM			17.01			
			52	0.6136202				
0.10					17.01			
0.12	7.0				17.01			
0.13	8.0							
0.15	9.0				17.00			
0.17	10.0							
0.18					17.00			
0.20					17.00			
0.22	13.0				17.00			
0.23					16.99			
0.25	15.0				16.99			
0.27	16.0				16.99			
0.28	17.0				16.99			
0.30					16.99			
0.32	19.0							
0.33	20.0				16.94			
0.35			68	0.6099396				
0.37	22.0	3:09:00 PM	69	0.6085999	16.87			
0.38	23.0	3:10:00 PM	70	0.6072317	16.83			
0.40	24.0	3:11:00 PM	71	0.6059656	16.80			
0.42	25.0				16.77			
0.43	26.0							
0.45	27.0	3:14:00 PM			16.78			
	28.0				16.74			
0.47		. J.1J.UU FIVI	. /3	0.004033/	10.74		Ī	i

	1	1		1			
0.48		3:16:00 PM	76	0.6028686	16.71		
0.50	30.0	3:17:00 PM	77	0.6016765	16.68		
0.52	31.0	3:18:00 PM	78	0.6003692	16.64		
0.53	32.0	3:19:00 PM	79	0.5993606	16.61		
0.55	33.0	3:20:00 PM	80	0.5979576	16.58		
0.57	34.0	3:21:00 PM	81	0.5968477	16.54		
0.58			82	0.5956032	16.51		
0.60			83	0.5944473	16.48		
0.62	37.0	3:24:00 PM	84	0.5934092	16.45		
0.63	38.0	3:25:00 PM	85	0.5921558	16.41		
0.65	39.0	3:26:00 PM	86	0.5909004	16.38		
0.67	40.0	3:27:00 PM	87	0.5895347	16.34		
0.68	41.0	3:28:00 PM	88	0.5882849	16.31		
0.70	42.0	3:29:00 PM	89	0.587389	16.28		
0.72		3:30:00 PM	90	0.5861614	16.25		
0.73			91	0.5849614	16.22		
0.75		3:32:00 PM	92	0.5840887	16.19		
0.77	46.0	3:33:00 PM	93	0.5826423	16.15		
0.78	47.0	3:34:00 PM	94	0.5815355	16.12		
0.80	48.0	3:35:00 PM	95	0.5805561	16.09		
0.82	49.0	3:36:00 PM	96	0.5794017	16.06		
0.83	50.0	3:37:00 PM	97	0.5781374	16.03		
0.85		3:38:00 PM	98		16.00		
				0.5771498			
0.87	52.0	3:39:00 PM	99	0.576111	15.97		
0.88		3:40:00 PM	100	0.5752172	15.95		
0.90	54.0	3:41:00 PM	101	0.5738214	15.91		
0.92	55.0	3:42:00 PM	102	0.5727864	15.88		
0.93	56.0	3:43:00 PM	103	0.5715603	15.84		
0.95	57.0	3:44:00 PM	104	0.5704766	15.81		
0.97	58.0	3:45:00 PM	105	0.5694889	15.79		
0.98			106	0.5683067	15.75		
			107		15.73		
1.00		3:47:00 PM		0.567291			
1.02	61.0	3:48:00 PM	108	0.5661273	15.69		
1.03	62.0	3:49:00 PM	109	0.5651829	15.67		
1.05	63.0	3:50:00 PM	110	0.5641884	15.64		
1.07	64.0	3:51:00 PM	111	0.5629238	15.60		
1.08	65.0	3:52:00 PM	112	0.5619357	15.58		
1.10	66.0	3:53:00 PM	113	0.5608607	15.55		
1.12	67.0	3:54:00 PM	114	0.5598859	15.52		
1.13		3:55:00 PM	115	0.5587642	15.49		
		3:56:00 PM					
1.15	69.0		116	0.5578076	15.46		
1.17	70.0	3:57:00 PM	117	0.5567368	15.43		
1.18	71.0	3:58:00 PM	118	0.5557813	15.41		
1.20	72.0	3:59:00 PM	119	0.5545589	15.37		
1.22	73.0	4:00:00 PM	120	0.5537387	15.35		
1.23	74.0	4:01:00 PM	121	0.5527689	15.32		
1.25			122	0.5515224	15.29		
1.27	76.0	4:03:00 PM	123	0.5506927	15.27		
1.28			124	0.5495603	15.23		+
				0.5484399			+
1.30			125				
1.32	79.0		126	0.5475421	15.18		
1.33		4:07:00 PM	127	0.5464627	15.15		
1.35		4:08:00 PM	128	0.5453817	15.12		
1.37	82.0	4:09:00 PM	129	0.5445515	15.09		
1.38	83.0	4:10:00 PM	130	0.5433772	15.06		
1.40	84.0	4:11:00 PM	131	0.5425327	15.04		
1.42			132	0.5415183			
1.42			133	0.5405626			
						<u> </u>	
1.45			134	0.5395008			
1.47	88.0		135	0.5386769			
1.48			136	0.5373784			
1.50	90.0	4:17:00 PM	137	0.5364618	14.87		
1.52	91.0	4:18:00 PM	138	0.5354849	14.84		
1.53		4:19:00 PM	139	0.5344545	14.82		
1.55			140			+	
1.55	55.0	1.20.001101	140	0.5550515	17.73		

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1.57	94.0	4:21:00 PM	141	0.532706	14.77		
1.58	95.0	4:22:00 PM	142	0.5317665	14.74		
1.60	96.0	4:23:00 PM	143	0.5307212	14.71		
1.62	97.0	4:24:00 PM	144	0.5298718	14.69		<del></del>
1.63	98.0	4:25:00 PM	145	0.528906	14.66		
1.65	99.0	4:26:00 PM	146	0.5279417	14.63		
1.67	100.0	4:27:00 PM	147	0.5270448	14.61		
1.68	101.0	4:28:00 PM	148	0.5259753	14.58		
1.70	102.0	4:29:00 PM	149	0.5248329	14.55		
1.72	103.0	4:30:00 PM	150	0.5242014	14.53		<del></del>
1.73	104.0	4:31:00 PM	151	0.523153	14.50		
1.75	105.0	4:32:00 PM	152	0.5223269	14.48		
1.77	106.0	4:33:00 PM	153	0.5213259	14.45		
1.78	107.0	4:34:00 PM	154	0.5203286	14.42		
1.80	108.0	4:35:00 PM	155	0.5196723	14.41		
1.82	109.0	4:36:00 PM	156	0.5185503	14.37		<del></del>
							-
1.83	110.0	4:37:00 PM	157	0.5179019	14.36		
1.85	111.0	4:38:00 PM	158	0.5169567	14.33		
1.87	112.0	4:39:00 PM	159	0.5159566	14.30		
1.88	113.0	4:40:00 PM	160	0.5149618	14.27		
1.90	114.0	4:41:00 PM	161	0.5139663	14.25		
1.92	115.0	4:42:00 PM	162	0.5131132	14.22		<del></del>
1.93	116.0	4:43:00 PM	163	0.5121055	14.20		
1.95	117.0	4:44:00 PM	164	0.5111621	14.17		
1.97	118.0	4:45:00 PM	165	0.5103054	14.15		
1.98	119.0	4:46:00 PM	166	0.509398	14.12		
2.00	120.0	4:47:00 PM	167	0.5086018	14.10		
2.02	121.0	4:48:00 PM	168	0.5076022	14.07		
							-
2.03	122.0	4:49:00 PM	169	0.5069062	14.05		
2.05	123.0	4:50:00 PM	170	0.5059137	14.02		
2.07	124.0	4:51:00 PM	171	0.505071	14.00		
2.08	125.0	4:52:00 PM	172	0.5042806	13.98		
2.10	126.0	4:53:00 PM	173	0.5034274	13.96		
2.12	127.0	4:54:00 PM	174	0.5024111	13.93		<del></del>
							+
2.13	128.0	4:55:00 PM	175	0.5017368	13.91		
2.15	129.0	4:56:00 PM	176	0.5007994	13.88		
2.17	130.0	4:57:00 PM	177	0.4998519	13.86		
2.18	131.0	4:58:00 PM	178	0.4990126	13.83		
2.20	132.0	4:59:00 PM	179	0.4982367	13.81		
2.22	133.0	5:00:00 PM	180	0.4973976	13.79		<del></del>
2.23	134.0	5:01:00 PM	181	0.4965979	13.77		
2.25	135.0	5:02:00 PM	182	0.4956314	13.74		
2.27	136.0	5:03:00 PM	183	0.49486	13.72		
2.28	137.0	5:04:00 PM	184	0.4941613	13.70		
2.30	138.0	5:05:00 PM	185	0.4932607	13.67		
2.32	139.0	5:06:00 PM	186		13.65		
2.33	140.0	5:07:00 PM	187	0.4913437	13.62		
2.35	141.0	5:08:00 PM	188	0.4908319	13.61		
2.37	142.0	5:09:00 PM	189	0.4898734	13.58		
2.38	143.0	5:10:00 PM	190	0.4890663	13.56		
2.40	144.0	5:11:00 PM	191	0.4880845	13.53		
2.42	145.0	5:12:00 PM	192	0.4873962	13.51		
2.43	146.0	5:12:00 PM	193	0.4867199	13.49		
2.45	147.0	5:14:00 PM	194		13.46	<del>                                     </del>	
2.47	148.0	5:15:00 PM	195	0.4848653	13.44		
2.48	149.0	5:16:00 PM	196	0.4840568	13.42		
2.50	150.0	5:17:00 PM	197	0.4834069	13.40		
2.52	151.0	5:18:00 PM	198		13.38		
2.53	152.0	5:19:00 PM	199	0.4816568	13.35		
2.55	153.0	5:20:00 PM	200	0.4809865	13.33		
2.57	154.0	5:21:00 PM	201	0.480343	13.32		
2.58	155.0	5:22:00 PM	202	0.4793691	13.29		
2.60	156.0	5:23:00 PM	203	0.4787618	13.27		
2.62	157.0	5:24:00 PM	204	0.4779957	13.25		
2.63	158.0		205		13.23		
2.03	136.0	3.23.00 2101	205	0.4771409	15.23		

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2.65	159.0	5:26:00 PM	206	0.476334	13.20	
2.67	160.0	5:27:00 PM	207	0.4755825	13.18	
2.68	161.0	5:28:00 PM	208	0.4746859	13.16	
2.70	162.0	5:29:00 PM	209	0.4739624	13.14	
2.72	163.0	5:30:00 PM	210	0.4732182	13.12	
2.73	164.0	5:31:00 PM	211	0.4723836	13.09	
2.75	165.0	5:32:00 PM	212	0.4713183	13.06	
2.77	166.0	5:33:00 PM	213	0.4709212	13.05	
2.78	167.0	5:34:00 PM	214	0.4701534	13.03	
2.80	168.0	5:35:00 PM	215	0.4692768	13.01	
2.82	169.0	5:36:00 PM	216	0.4686942	12.99	
2.83	170.0	5:37:00 PM	217	0.46774	12.97	
2.85	171.0	5:38:00 PM	218	0.4669708	12.94	
2.87	172.0	5:39:00 PM	219	0.4663706	12.93	
2.88	173.0	5:40:00 PM	220	0.4655534	12.91	
2.90	174.0	5:41:00 PM	221	0.4649832	12.89	
2.92	175.0	5:42:00 PM	222	0.4640834	12.86	
2.93	176.0	5:43:00 PM	223	0.4633295	12.84	
2.95	177.0	5:44:00 PM	224	0.4625263	12.82	
2.97	178.0	5:45:00 PM	225	0.462071	12.81	
2.98	179.0	5:46:00 PM	226	0.4611074	12.78	
3.00	180.0	5:47:00 PM	227	0.4603954	12.76	
3.02	181.0	5:48:00 PM	228	0.4596648	12.74	
3.03	182.0	5:49:00 PM	229	0.4590178	12.72	
3.05	183.0	5:50:00 PM	230	0.4579962	12.70	
3.07	184.0	5:51:00 PM	231	0.4574017	12.68	
3.08	185.0	5:52:00 PM	232	0.4567198	12.66	
3.10	186.0	5:53:00 PM	233	0.4559443	12.64	
3.12	187.0	5:54:00 PM	234	0.4552072	12.62	
3.13	188.0	5:55:00 PM	235	0.4543852	12.60	
3.15	189.0	5:56:00 PM	236	0.4536676		
3.17	190.0		237		12.56	
		5:57:00 PM		0.4530433		
3.18	191.0	5:58:00 PM	238	0.4523938	12.54	
3.20	192.0	5:59:00 PM	239	0.4516217	12.52	
3.22	193.0	6:00:00 PM	240	0.4509042	12.50	
3.23	194.0	6:01:00 PM	241	0.4501046	12.48	
3.25	195.0	6:02:00 PM	242	0.4493408	12.46	
3.27	196.0	6:03:00 PM	243	0.4487663	12.44	
3.28	197.0	6:04:00 PM	244	0.4481133	12.42	
3.30	198.0	6:05:00 PM	245	0.4472297	12.40	
3.32	199.0	6:06:00 PM	246	0.4466785	12.38	
3.33	200.0	6:07:00 PM	247	0.446042	12.36	
3.35			248		12.34	
3.37	202.0		249	0.4446959	12.33	
3.38	203.0	6:10:00 PM	250	0.4437504		
3.40	204.0	6:11:00 PM	251	0.4430337	12.28	
3.42	205.0	6:12:00 PM	252	0.4425249	12.27	
3.43	206.0	6:13:00 PM	253	0.4417984	12.25	
3.45	207.0	6:14:00 PM	254	0.4410664	12.23	
3.47	208.0	6:15:00 PM	255	0.4404542	12.21	-
3.48		6:16:00 PM	256			
3.50		6:17:00 PM	257	0.4389174		
3.52	211.0	6:18:00 PM	258			
3.53	212.0	6:19:00 PM	259	0.4376729	12.13	
3.55	213.0	6:20:00 PM	260	0.4370528	12.12	
3.57	214.0	6:21:00 PM	261	0.4363786	12.10	
3.58	215.0	6:22:00 PM	262	0.435578		
3.60		6:23:00 PM	263	0.4350446		
3.62	217.0	6:24:00 PM	264	0.4341744		
3.63	218.0	6:25:00 PM	265	0.4336565	12.02	
3.65	219.0	6:26:00 PM	266	0.4329698	12.00	
3.67	220.0	6:27:00 PM	267	0.4322543	11.98	
3.68	221.0	6:28:00 PM	268	0.4315143	11.96	
3.70	222.0	6:29:00 PM	269	0.4309178	11.95	
3.72	223.0		270			
3.72	223.0	0.30.00 FIVI	2/0	0.4503034	11.93	

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3.73	224.0	6:31:00 PM	271	0.4296393	11.91		
3.75	225.0	6:32:00 PM	272	0.4289357	11.89		
3.77	226.0	6:33:00 PM	273	0.4281855	11.87		
3.78	227.0	6:34:00 PM	274	0.4277325	11.86		
3.80	228.0	6:35:00 PM	275	0.4268539	11.83		
3.82	229.0	6:36:00 PM	276	0.4262902	11.82		
3.83		6:37:00 PM	277	0.4256231	11.80		
3.85		6:38:00 PM	278	0.4249681	11.78		
3.87	232.0	6:39:00 PM	279	0.4243424	11.76		
3.88	233.0	6:40:00 PM	280	0.4237059	11.75		
3.90	234.0	6:41:00 PM	281	0.4230243	11.73		
3.92	235.0	6:42:00 PM	282	0.4222762	11.71		
3.93	236.0	6:43:00 PM	283	0.4217376	11.69		
3.95	237.0	6:44:00 PM	284	0.420995	11.67		
3.97	238.0	6:45:00 PM	285	0.4202533	11.65		
3.98	239.0	6:46:00 PM	286	0.4195064	11.63		
4.00	240.0	6:47:00 PM	287	0.4190864	11.62		
4.02	241.0	6:48:00 PM	288	0.41845	11.60		
4.03	242.0	6:49:00 PM	289	0.4177613	11.58		
4.05	243.0	6:50:00 PM	290	0.4170712	11.56		
4.07	244.0	6:51:00 PM	291	0.4164875	11.55		
4.08	245.0	6:52:00 PM	292	0.415774	11.53		
4.10		6:53:00 PM	293	0.4152345	11.51	<del>                                     </del>	
4.10	246.0						
		6:54:00 PM	294	0.4146182	11.49		
4.13	248.0	6:55:00 PM	295	0.4139433	11.47		
4.15	249.0	6:56:00 PM	296	0.4134012	11.46		
4.17	250.0	6:57:00 PM	297	0.4127483	11.44		
4.18	251.0	6:58:00 PM	298	0.412238	11.43		
4.20	252.0	6:59:00 PM	299	0.4113494	11.40		
4.22	253.0	7:00:00 PM	300	0.4107655	11.39		
4.23		7:01:00 PM	301	0.4100648	11.37		
4.25	255.0	7:02:00 PM	302	0.4095483	11.35		
4.27	256.0	7:03:00 PM	303	0.4088717	11.33		
4.28	257.0	7:04:00 PM	304	0.40831	11.32		
4.30	258.0	7:05:00 PM	305	0.4076103	11.30		
4.32	259.0	7:06:00 PM	306	0.4069979	11.28		
4.33	260.0	7:07:00 PM	307	0.4064675	11.27		
4.35	261.0	7:08:00 PM	308	0.4058159	11.25		
4.37	262.0	7:09:00 PM	309	0.4052145	11.23		
4.38	263.0	7:10:00 PM	310	0.4046304	11.22		
4.40	264.0	7:11:00 PM	311	0.4038675	11.20		
4.42	265.0	7:12:00 PM	312	0.4030887	11.17		
4.43	266.0	7:13:00 PM	313	0.4027538	11.16		
4.45	267.0	7:14:00 PM	314	0.4021398	11.15		
4.47	268.0	7:15:00 PM	315	0.4013925	11.13		
4.48	269.0	7:16:00 PM	316	0.4007931	11.11		
4.50	270.0	7:17:00 PM	317	0.4002134	11.09		
4.52	271.0	7:18:00 PM	318		11.08		
4.52	271.0	7:19:00 PM	318		11.06		
4.55		7:20:00 PM	320				
4.57	274.0	7:21:00 PM	321	0.3977389	11.03		
4.58		7:22:00 PM	322	0.3972622	11.01		
4.60	276.0	7:23:00 PM	323	0.3965082	10.99		
4.62	277.0	7:24:00 PM	324	0.3958451	10.97		
4.63	278.0	7:25:00 PM	325	0.3954873	10.96		
4.65		7:26:00 PM	326	0.3948646			
4.67	280.0	7:27:00 PM	327	0.3941381	10.93		
4.68						+	
		7:28:00 PM	328				
4.70		7:29:00 PM	329	0.3930239	10.89		
4.72	283.0	7:30:00 PM	330	0.3924027	10.88		
4.73	284.0	7:31:00 PM	331	0.3917203	10.86		
4.75	285.0	7:32:00 PM	332	0.3911826	10.84		
4.77	286.0	7:33:00 PM	333	0.3904842	10.82		
4.78	287.0	7:34:00 PM	334		10.81		
4.80		7:35:00 PM	335		10.79		
	2ŏŏ.U	7.55:UU PIVI	335	0.5693/01	10.79	i l	

4.82	289.0	7:36:00 PM	336	0.3888079	10.78		
4.83	290.0	7:37:00 PM	337	0.3880244	10.76		
4.85	291.0	7:38:00 PM	338	0.3876562	10.75		
4.87	292.0	7:39:00 PM	339	0.3869135	10.73		
4.88	293.0	7:40:00 PM	340	0.386407	10.71		
4.90	294.0	7:41:00 PM	341	0.385884	10.70		
4.92	295.0	7:42:00 PM	342	0.3853933	10.68		
4.93	296.0	7:43:00 PM	343	0.3847068	10.66		
4.95	297.0	7:44:00 PM	344	0.3841428	10.65		
4.97	298.0	7:45:00 PM	345	0.3836304	10.63		
4.98	299.0	7:46:00 PM	346	0.3830567	10.62		
5.00	300.0	7:47:00 PM	347	0.3823491	10.60		
5.02			348				
	301.0	7:48:00 PM		0.3819116	10.59		
5.03	302.0	7:49:00 PM	349	0.3812596	10.57		
5.05	303.0	7:50:00 PM	350	0.3806176	10.55		
5.07	304.0	7:51:00 PM	351	0.3800986	10.54		
5.08	305.0	7:52:00 PM	352	0.3794895	10.52		
5.10	306.0	7:53:00 PM	353	0.378943	10.50		
5.12	307.0	7:54:00 PM	354	0.3783875	10.49		
5.13	308.0	7:55:00 PM	355	0.3779738	10.48		
5.15	309.0	7:56:00 PM	356	0.3773686	10.46		
5.17	310.0	7:57:00 PM	357	0.3766908	10.44		
5.18	311.0	7:58:00 PM	358	0.3761404	10.43		
5.20	312.0	7:59:00 PM	359	0.3757232	10.42		
5.22	313.0	8:00:00 PM	360	0.3750913	10.40		
5.23	314.0	8:01:00 PM	361	0.3745391	10.38		
5.25	315.0	8:02:00 PM	362	0.3739198	10.37		
5.27	316.0	8:03:00 PM	363	0.3734775	10.35		
5.28			364				<del>   </del>
	317.0	8:04:00 PM		0.3726285	10.33		
5.30	318.0	8:05:00 PM	365	0.3721547	10.32		
5.32	319.0	8:06:00 PM	366	0.3714828	10.30		
5.33	320.0	8:07:00 PM	367	0.3712516	10.29		
5.35	321.0	8:08:00 PM	368	0.3705567	10.27		
5.37	322.0	8:09:00 PM	369	0.3699436	10.25		
5.38	323.0	8:10:00 PM	370	0.3692336	10.24		
5.40	324.0	8:11:00 PM	371	0.3688316	10.22		
	325.0	8:12:00 PM	371		10.22		
5.42				0.3683915			
5.43	326.0	8:13:00 PM	373	0.3678633	10.20		
5.45	327.0	8:14:00 PM	374	0.3672081	10.18		
5.47	328.0	8:15:00 PM	375	0.3666074	10.16		
5.48	329.0	8:16:00 PM	376	0.3661046	10.15		
5.50	330.0	8:17:00 PM	377	0.3654379	10.13		
5.52	331.0		378	0.3648874	10.11		
5.53	332.0	8:19:00 PM	379	0.3644522	10.10		
5.55	333.0	8:20:00 PM	380	0.3638973	10.09		
5.57	334.0	8:21:00 PM	381	0.3632666	10.07		
5.58	335.0	8:22:00 PM	382	0.3628179	10.06		
5.60	336.0	8:23:00 PM	383	0.3622772	10.04		
5.62	337.0	8:24:00 PM	384	0.3617661	10.03		
5.63	338.0	8:25:00 PM	385	0.3611802	10.01		
5.65	339.0	8:26:00 PM	386	0.3606049	10.00		
5.67	340.0	8:27:00 PM	387	0.3600149	9.98		
5.68	341.0	8:28:00 PM	388	0.359555	9.97		+
5.70						<del> </del>	<del></del>
	342.0	8:29:00 PM	389	0.359046	9.95		
5.72	343.0	8:30:00 PM	390	0.3583884	9.93		
5.73	344.0	8:31:00 PM	391	0.3579948	9.92		
5.75	345.0	8:32:00 PM	392	0.357685	9.92		
5.77	346.0	8:33:00 PM	393	0.3569876	9.90		
5.78	347.0	8:34:00 PM	394	0.3563657	9.88		
5.80	348.0	8:35:00 PM	395	0.3557646	9.86		<del></del>
5.82	349.0	8:36:00 PM	396	0.3553344	9.85		<del>-  </del>
5.83	350.0	8:37:00 PM	397	0.3548241	9.84		
5.85	351.0	8:38:00 PM	398	0.3542756	9.82		
5.87	352.0	8:39:00 PM	399	0.3536789	9.80		
5.88	353.0	8:40:00 PM	400	0.3529287	9.78		

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5.90	354.0	8:41:00 PM	401	0.3527308	9.78		
5.92	355.0	8:42:00 PM	402	0.3522555	9.76		
5.93	356.0	8:43:00 PM	403	0.3515829	9.75		
5.95	357.0	8:44:00 PM	404	0.3511348	9.73		
5.97	358.0	8:45:00 PM	405	0.3505864	9.72		
5.98	359.0	8:46:00 PM	406	0.3501766	9.71		
6.00	360.0	8:47:00 PM	407	0.3495872	9.69		
6.02	361.0	8:48:00 PM	408	0.3489751	9.67		
6.03	362.0	8:49:00 PM	409	0.3485341	9.66		
6.05	363.0	8:50:00 PM	410	0.348086	9.65		
6.07	364.0	8:51:00 PM	411	0.3476068	9.64		
6.08	365.0	8:52:00 PM	412	0.3468601	9.61		
6.10	366.0	8:53:00 PM	413	0.346528	9.61		
6.12	367.0	8:54:00 PM	414	0.3459253	9.59		
6.13	368.0	8:55:00 PM	415	0.3455652	9.58		
6.15	369.0	8:56:00 PM	416	0.3450215	9.56		
6.17	370.0	8:57:00 PM	417	0.3444068	9.55		
6.18	371.0	8:58:00 PM	418	0.343888	9.53		
6.20	372.0	8:59:00 PM	419	0.3435142	9.52		
6.22	373.0	9:00:00 PM	420	0.3429617	9.51		
6.23	374.0	9:01:00 PM	421	0.3424506	9.49		
6.25	375.0	9:02:00 PM	422	0.3417067	9.47	+	
						+	<del></del>
6.27	376.0	9:03:00 PM	423	0.3415975	9.47		
6.28	377.0	9:04:00 PM	424	0.3407967	9.45		
6.30	378.0	9:05:00 PM	425	0.3404202	9.44		
6.32	379.0	9:06:00 PM	426	0.3398587	9.42		
6.33	380.0	9:07:00 PM	427	0.3393693	9.41		
6.35	381.0	9:08:00 PM	428	0.3387113	9.39		
6.37	382.0	9:09:00 PM	429	0.3385239	9.38		
6.38	383.0	9:10:00 PM	430	0.3377045	9.36		
6.40		9:11:00 PM	431	0.337216	9.35		
6.42	385.0	9:12:00 PM	432	0.3368336	9.34		
6.43	386.0	9:13:00 PM	433	0.3365165	9.33		
6.45	387.0	9:14:00 PM	434	0.3357499	9.31		
6.47	388.0	9:15:00 PM	435	0.3355028	9.30		
6.48	389.0	9:16:00 PM	436	0.3347953	9.28		
6.50	390.0	9:17:00 PM	437	0.33433	9.27		
6.52	391.0	9:18:00 PM	438	0.3339249	9.26		
6.53	392.0	9:19:00 PM	439	0.3331754	9.24		
6.55	393.0	9:20:00 PM	440	0.3328319	9.23		
6.57	394.0	9:21:00 PM	441	0.3323514	9.21		
6.58	395.0	9:22:00 PM	442	0.331957	9.20		
6.60	396.0	9:23:00 PM	443	0.3313985	9.19		
6.62	397.0	9:24:00 PM	444	0.3308695	9.17		
6.63	398.0	9:25:00 PM	445	0.3304327	9.16		
6.65	399.0	9:26:00 PM	446	0.32994	9.15		
6.67	400.0	9:27:00 PM	447	0.3293374	9.13		
6.68	401.0	9:28:00 PM	448	0.3290542	9.12		
6.70		9:29:00 PM	449	0.3284717	9.11		
6.72	403.0	9:30:00 PM	450	0.3279082	9.09		
6.73	404.0	9:31:00 PM	451	0.3275704	9.08		
6.75	405.0	9:32:00 PM	452	0.3269824	9.06		
6.77	406.0	9:33:00 PM	453	0.3265906	9.05		
						+	<del></del>
6.78		9:34:00 PM	454	0.3261551	9.04		
6.80	408.0	9:35:00 PM	455	0.325501	9.02		
6.82	409.0	9:36:00 PM	456	0.3251712	9.01		
6.83	410.0	9:37:00 PM	457	0.3246202	9.00		
6.85	411.0	9:38:00 PM	458	0.3241235	8.98		
6.87	412.0	9:39:00 PM	459	0.3236007	8.97		
6.88	413.0	9:40:00 PM	460	0.3233609	8.96		
			460				<del></del>
6.90	414.0	9:41:00 PM		0.3226585	8.94		
6.92	415.0	9:42:00 PM	462	0.3220744	8.93		
6.93	416.0	9:43:00 PM	463	0.3218187	8.92		
6.95	417.0	9:44:00 PM	464	0.321153	8.90	T	
6.97	418.0	9:45:00 PM	465	0.3209304	8.90		
,							

6.98	419.0		466	0.3201574	8.87	
7.00	420.0	9:47:00 PM	467	0.3199719	8.87	
7.02	421.0	9:48:00 PM	468	0.3193471	8.85	
7.03	422.0	9:49:00 PM	469	0.3189234	8.84	
7.05	423.0	9:50:00 PM	470	0.3183325	8.82	
7.07	424.0	9:51:00 PM	471	0.3179225	8.81	
7.08	425.0	9:52:00 PM	472	0.31732668	8.79	
7.10	426.0	9:53:00 PM	473	0.3169887	8.79	
7.12	427.0	9:54:00 PM	474	0.3166049	8.78	
7.13	428.0	9:55:00 PM	475	0.3160063	8.76	
7.15	429.0	9:56:00 PM	476	0.3156134	8.75	
7.17	430.0	9:57:00 PM	477	0.3150926	8.73	
7.18	431.0	9:58:00 PM	478	0.3145929	8.72	
7.20	432.0	9:59:00 PM	479	0.3142574	8.71	
7.22	433.0	10:00:00 PM	480	0.3137705	8.70	
7.23	434.0		481	0.3132855	8.68	
-		10:01:00 PM				
7.25	435.0	10:02:00 PM	482	0.3127896	8.67	
7.27	436.0	10:03:00 PM	483	0.3123173	8.66	
7.28	437.0	10:04:00 PM	484	0.3118723	8.65	
7.30	438.0	10:05:00 PM	485	0.3113218	8.63	!
7.32	439.0	10:06:00 PM	486	0.3109029	8.62	
7.33	440.0	10:07:00 PM	487	0.310556	8.61	
7.35	441.0	10:08:00 PM	488	0.3102688	8.60	
7.37	442.0	10:09:00 PM	489	0.3097191	8.59	
7.38	443.0	10:10:00 PM	490	0.3091728	8.57	
7.40	444.0	10:11:00 PM	491	0.3086664	8.56	
7.40	445.0				8.55	
		10:12:00 PM	492	0.3082929		
7.43	446.0	10:13:00 PM	493	0.3078355	8.53	
7.45	447.0	10:14:00 PM	494	0.3072872	8.52	
7.47	448.0	10:15:00 PM	495	0.306905	8.51	
7.48	449.0	10:16:00 PM	496	0.306535	8.50	
7.50	450.0	10:17:00 PM	497	0.3059694	8.48	!
7.52	451.0	10:18:00 PM	498	0.3055866	8.47	
7.53	452.0	10:19:00 PM	499	0.3050818	8.46	
7.55	453.0	10:20:00 PM	500	0.3047073	8.45	
7.57	454.0	10:21:00 PM	501	0.3043042	8.44	-
7.58	455.0	10:22:00 PM	502	0.3038845	8.42	
7.60	456.0	10:23:00 PM	503	0.3033504	8.41	
7.62						
	457.0	10:24:00 PM	504	0.3028854	8.40	
7.63	458.0	10:25:00 PM	505	0.302429	8.38	
7.65	459.0	10:26:00 PM	506	0.3021383	8.38	
7.67	460.0	10:27:00 PM	507	0.3016852	8.36	
7.68	461.0	10:28:00 PM	508	0.3011046	8.35	
7.70	462.0	10:29:00 PM	509	0.3006677	8.33	
7.72	463.0	10:30:00 PM	510	0.3002995	8.32	
7.73	464.0	10:31:00 PM	511	0.2999159	8.31	
7.75	465.0	10:32:00 PM	512	0.2994536	8.30	
7.77	466.0	10:33:00 PM	513	0.2988558	8.28	
7.78	467.0	10:34:00 PM	514	0.2985285	8.28	<del></del>
7.78	468.0	10:35:00 PM	515	0.2980798	8.26	
7.80	468.0		516		8.25	
		10:36:00 PM		0.2977571		
7.83	470.0	10:37:00 PM	517	0.2971527	8.24	
7.85	471.0	10:38:00 PM	518	0.2966553	8.22	
7.87	472.0	10:39:00 PM	519	0.2962384	8.21	
7.88	473.0	10:40:00 PM	520	0.295904	8.20	
7.90	474.0	10:41:00 PM	521	0.2954712	8.19	
7.92	475.0	10:42:00 PM	522	0.2949799	8.18	
7.93	476.0	10:43:00 PM	523	0.2945293	8.16	
7.95	477.0	10:44:00 PM	524	0.2942546	8.16	
7.97	478.0	10:45:00 PM	525	0.2936298	8.14	<del></del>
7.98	478.0	10:46:00 PM	526	0.2932622	8.13	
8.00	480.0	10:47:00 PM	527	0.2927607	8.12	
8.02	481.0	10:48:00 PM	528	0.2923438	8.10	
8.03	482.0	10:49:00 PM	529	0.2919472	8.09	
8.05	483.0	10:50:00 PM	530	0.2914852	8.08	

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8.07	484.0	10:51:00 PM	531	0.2910667	8.07		
8.08	485.0	10:52:00 PM	532	0.2905825	8.05		
8.10	486.0	10:53:00 PM	533	0.290187	8.04		
8.12	487.0	10:54:00 PM	534	0.2898004	8.03		
8.13	488.0	10:55:00 PM	535	0.2893795	8.02		
8.15		10:56:00 PM	536	0.288977	8.01		
8.17	490.0	10:57:00 PM	537	0.2884958	8.00		
8.18		10:58:00 PM	538	0.2880446			
8.20	492.0	10:59:00 PM	539	0.2876054	7.97		
8.22	493.0	11:00:00 PM	540	0.2871532	7.96		
8.23	494.0	11:01:00 PM	541	0.2865692	7.94		
8.25	495.0	11:02:00 PM	542	0.2863439	7.94		
8.27	496.0	11:03:00 PM	543	0.285934	7.93		
8.28	497.0	11:04:00 PM	544	0.2853926	7.91		
8.30		11:05:00 PM	545	0.2850575	7.90		
8.32	499.0	11:06:00 PM	546	0.2845982	7.89		
8.33	500.0	11:07:00 PM	547	0.2841134	7.88		
8.35	501.0	11:08:00 PM	548	0.2838154	7.87		
8.37	502.0	11:09:00 PM	549	0.2833345	7.85		
8.38	503.0	11:10:00 PM	550	0.2829339	7.84		
8.40		11:11:00 PM	551	0.2823529	7.83		
8.42	505.0	11:12:00 PM	552	0.2820951	7.82		
8.43		11:13:00 PM	553	0.2817876	7.81		
8.45	507.0	11:14:00 PM	554	0.2812302	7.80		
8.47	508.0	11:15:00 PM	555	0.2809139	7.79		
8.48	509.0	11:16:00 PM	556	0.2804275	7.77		
8.50	510.0	11:17:00 PM	557	0.2801899	7.77		
8.52	511.0	11:18:00 PM	558	0.2798247	7.76		
8.53	512.0	11:19:00 PM	559	0.2795561	7.75		
8.55		11:20:00 PM	560	0.2791081	7.74		
8.57		11:21:00 PM	561	0.2787391	7.73		
8.58		11:22:00 PM	562	0.2783832	7.72		
8.60	516.0	11:23:00 PM	563	0.2780272	7.71		
8.62	517.0	11:24:00 PM	564	0.2776232	7.70		
8.63	518.0	11:25:00 PM	565	0.2771862	7.68		
8.65	519.0	11:26:00 PM	566	0.2767598	7.67		
8.67	520.0	11:27:00 PM	567	0.2764525	7.66		
		11:28:00 PM					+
8.68			568	0.2760223	7.65		
8.70		11:29:00 PM	569	0.2757339	7.64		
8.72	523.0	11:30:00 PM	570	0.2753151	7.63		
8.73	524.0	11:31:00 PM	571	0.2749712	7.62		
8.75	525.0	11:32:00 PM	572	0.2745787	7.61		
8.77	526.0	11:33:00 PM	573	0.2741412	7.60		
8.78		11:34:00 PM	574	0.2739182	7.59		
8.80		11:35:00 PM	575	0.2733957	7.58		
8.82	529.0	11:36:00 PM	576		7.57		
8.83		11:37:00 PM	577	0.2727462	7.56		
8.85		11:38:00 PM	578	0.2724059	7.55		
8.87	532.0	11:39:00 PM	579	0.2718234	7.53		
8.88	533.0	11:40:00 PM	580	0.2716563	7.53		
8.90	534.0	11:41:00 PM	581	0.2713009	7.52		
8.92	535.0	11:42:00 PM	582	0.2707418			
8.93		11:43:00 PM	583	0.2705838			
8.95		11:44:00 PM	584	0.2701097	7.49		
8.97	538.0	11:45:00 PM	585	0.2696346	7.47		
8.98		11:46:00 PM	586	0.2694211	7.47		
9.00	540.0	11:47:00 PM	587	0.2689682	7.46		
9.02	541.0	11:48:00 PM	588	0.2684885	7.44		
9.03	542.0	11:49:00 PM	589	0.2682942	7.44		
9.05	543.0	11:50:00 PM	590	0.267786			
9.07	544.0	11:51:00 PM	591	0.2675043	7.42		
9.08		11:52:00 PM	592	0.2671519	7.41		
9.10		11:53:00 PM	593	0.266704	7.39		
9.12	547.0	11:54:00 PM	594	0.266351	7.38		
9.13	548.0	11:55:00 PM	595	0.2659157	7.37		
		L. L					

9.15 S89.0 115:800 PM 598 0.2648579 7.35 9.7 9.7 9.7 9.7 9.7 9.7 9.7 9.7 9.7 9.7							1	
9.18   9.18   9.18   11.58.00 PM   998   0.2648574   7.34   9.27   9.27   9.52.0   11.58.00 PM   99   0.2648574   7.33   9.27   9.27   9.53.0   12.00.00 AM   600   0.2641849   7.32   9.28   9.29   9.554.0   12.00.00 AM   600   0.2625908   7.31   9.29   9.554.0   12.00.00 AM   602   0.2625908   7.31   9.29   9.29   9.556.0   12.00.00 AM   602   0.2625902   7.28   9.37   9.38   9.57   12.00.00 AM   604   0.2625902   7.28   9.39   9.30   9.58.0   12.00.00 AM   604   0.2625902   7.28   9.30	9.15	549.0		596		7.36		
9.20   552.0   11.59.00 PM   599   0.2645844   7.33   9.21   9.21   5.53.0   12.00 OAM   601   0.2637908   7.31   9.21   9.23   5.54.0   12.01.00 AM   601   0.2637908   7.31   9.27   9.25   5.55.0   12.02.00 AM   602   0.2636454   7.31   9.27   9.28   5.55.0   12.03.00 AM   603   0.2629656   7.29   9.28   5.57.0   12.03.00 AM   603   0.2629656   7.29   9.30   5.58.0   12.03.00 AM   605   0.2629282   7.27   9.30   9.30   5.58.0   12.03.00 AM   605   0.2622382   7.27   9.33   5.50.0   12.07.00 AM   606   0.2622382   7.27   9.33   5.50.0   12.07.00 AM   607   0.2617341   7.26   9.33   5.50.0   12.07.00 AM   607   0.2617341   7.26   9.33   5.50.0   12.07.00 AM   607   0.2617341   7.24   9.37   5.50.0   12.07.00 AM   607   0.2610367   7.24   9.38   5.53.0   12.10.00 AM   608   0.261057   7.24   9.38   5.53.0   12.10.00 AM   601   0.2603680   7.23   9.40   5.54.0   12.11.00 AM   611   0.260137   7.21   9.43   5.56.0   12.11.00 AM   613   0.2594338   7.19   9.44   5.56.0   12.11.00 AM   613   0.2594338   7.19   9.47   5.56.0   12.11.00 AM   614   0.2591348   7.17   9.47   5.58.0   12.13.00 AM   615   0.2586742   7.17   9.47   5.58.0   12.13.00 AM   615   0.2586742   7.17   9.47   5.59   7.10   12.00 AM   617   0.2581647   7.16   9.57   7.18   9.50   5.70   12.17.00 AM   617   0.2581647   7.16   9.57   7.14   9.55   5.70   12.17.00 AM   617   0.2581647   7.16   9.57   7.14   9.55   5.70   12.17.00 AM   618   0.257378   7.13   9.50   5.70   12.17.00 AM   619   0.257378   7.14   9.50   9.50   5.70   12.00 AM   619   0.257378   7.13   9.50   5.70   12.17.00 AM   619   0.257378   7.14   9.50   9.50   5.70   9.50   9.50   9.50   9.50   9.50   9.50   9.50   9.50   9.5								
9.22   553.0   12.00.00 AM   600   0.2641549   7.32   9.25   555.0   12.02.00 AM   602   0.263546   7.31   9.25   555.0   12.02.00 AM   602   0.263546   7.31   9.27   555.0   12.03.00 AM   602   0.263546   7.31   9.27   7.28   9.28   557.0   12.03.00 AM   604   0.262560   7.28   9.28   557.0   12.03.00 AM   606   0.262580   7.28   9.29   7.28   9.30   558.0   12.05.00 AM   606   0.262582   7.27   9.31   9.32   555.0   12.05.00 AM   606   0.2620318   7.26   9.33   556.0   12.05.00 AM   608   0.2620318   7.26   9.33   556.0   12.05.00 AM   608   0.2620318   7.26   9.33   556.0   12.05.00 AM   608   0.2611405   7.24   9.33   556.0   12.05.00 AM   608   0.2611405   7.24   9.33   556.0   12.05.00 AM   608   0.261037   7.21   9.34   556.0   12.15.00 AM   610   0.2605808   7.23   9.34   556.0   12.15.00 AM   611   0.2605808   7.23   9.34   556.0   12.15.00 AM   612   0.2597816   7.20   9.34   556.0   12.15.00 AM   612   0.2597816   7.20   9.34   556.0   12.15.00 AM   613   0.2593489   7.18   9.34   556.0   12.15.00 AM   614   0.259489   7.18   9.34   556.0   12.15.00 AM   615   0.2597816   7.27   9.35   9.30   7.30   9.30   7	9.18	551.0	11:58:00 PM	598	0.2648574	7.34		
9.22   554.0   12:01:00 AM   601   0.2837908   7.31   9.27   556.0   12:03:00 AM   602   0.2855445   7.31   9.27   556.0   12:03:00 AM   603   0.2629656   7.29   9.38   557.0   12:04:00 AM   603   0.2629656   7.29   9.38   557.0   12:05:00 AM   605   0.2622282   7.27   9.39   9.30   558.0   12:05:00 AM   606   0.2622382   7.27   9.31   560.0   12:07:00 AM   607   0.2617341   7.26   9.33   560.0   12:07:00 AM   607   0.2617341   7.26   9.37   561.0   12:08:00 AM   608   0.261105   7.24   9.37   561.0   12:09:00 AM   609   0.2610267   7.24   9.37   562.0   12:09:00 AM   609   0.2610267   7.24   9.38   563.0   12:10:00 AM   611   0.266808   7.23   9.34   563.0   12:10:00 AM   611   0.266808   7.23   9.34   563.0   12:10:00 AM   612   0.259736   7.20   9.34   565.0   12:10:00 AM   613   0.259736   7.20   9.34   565.0   12:10:00 AM   613   0.259736   7.20   9.34   565.0   12:10:00 AM   614   0.259139   7.19   9.34   565.0   12:10:00 AM   614   0.259139   7.19   9.34   565.0   12:10:00 AM   615   0.2587342   7.17   9.34   565.0   12:10:00 AM   615   0.2587342   7.17   9.35   567.0   12:10:00 AM   616   0.2588147   7.16   9.35   57.0   12:10:00 AM   617   0.2581647   7.16   9.35   57.0   12:10:00 AM   617   0.2581647   7.16   9.35   57.0   12:10:00 AM   617   0.2581647   7.16   9.35   57.0   12:10:00 AM   618   0.257730   7.14   9.35   57.0   12:10:00 AM   619   0.2572378   7.13   9.35   57.0   12:10:00 AM   619   0.2572378   7.13   9.35   57.0   12:10:00 AM   621   0.259388   7.12   9.35   57.0   12:10:00 AM   621   0.259388   7.12   9.35   57.0   12:20:00 AM   622   0.259388   7.12   9.35   57.0   12:20:00 AM   623   0.259388   7.12   9.35   57.0   12:20:00 AM   623   0.259388   7.12   9.35   57.0   12:20:00 AM   623   0.259388   7.12   9.35   57.0   12:20:00 AM   624   0.25977   7.00   9.35   9.35   57.0   12:20:00 AM   624   0.25977   7.00   9.35   9.35   9.35				599	0.2645844			
9.25   5.55.0   12.02.03.0 AM   602   0.263545   7.31   9.27   5.55.0   12.02.03.0 AM   603   0.262502   7.28   9.28   5.55.0   12.04.00.0 AM   604   0.262602   7.28   9.29   5.55.0   12.04.00.0 AM   606   0.262602   7.28   9.20   5.55.0   12.04.00.0 AM   606   0.262602   7.28   9.21   5.55.0   12.04.00.0 AM   606   0.26203   7.26   9.22   5.55.0   12.04.00.0 AM   606   0.26203   7.26   9.23   5.56.0   12.04.00.0 AM   606   0.26203   7.26   9.24   5.55.0   12.04.00.0 AM   607   0.2611405   7.26   9.25   9.25   5.50.0   12.04.00.0 AM   608   0.2611405   7.24   9.26   9.27   7.24   9.27   9.28   5.56.0   12.03.0 AM   608   0.2611405   7.24   9.28   5.56.0   12.10.0 AM   611   0.260603   7.22   9.29   9.20   5.56.0   12.11.00.0 AM   611   0.260603   7.22   9.24   5.56.0   12.11.00.0 AM   612   0.259343   7.29   9.24   5.56.0   12.11.00.0 AM   613   0.259343   7.29   9.25   5.56.0   12.11.00.0 AM   614   0.259343   7.29   9.26   5.57.0   12.11.00.0 AM   614   0.259343   7.29   9.27   9.28   5.57.0   12.11.00.0 AM   616   0.258481   7.21   9.28   5.57.0   12.11.00.0 AM   616   0.258481   7.21   9.29   5.57.0   12.11.00.0 AM   618   0.2573205   7.14   9.29   5.57.0   12.12.00.0 AM   618   0.2573205   7.14   9.29   5.57.0   12.12.00.0 AM   618   0.2573205   7.14   9.29   5.57.0   12.12.00.0 AM   620   0.2569388   7.12   9.20   5.57.0   12.22.00.0 AM   620   0.2569388   7.12   9.21   9.22   5.57.0   12.22.00.0 AM   620   0.2569388   7.12   9.22   5.57.0   12.22.00.0 AM   620   0.2569388   7.12   9.23   5.57.0   12.22.00.0 AM   620   0.2569388   7.12   9.24   5.58.0   12.22.00.0 AM   620   0.2569388   7.12   9.25   5.57.0   12.22.00.0 AM   620   0.2569388   7.12   9.26   5.57.0   12.22.00.0 AM   620   0.2569388   7.12   9.27   5.58.0   12.23.00.0 AM   620   0.2569388   7.00   9.28   5.59.0   12.23.00.0 AM   620   0.2569388   7.00   9.29   5.59.0   12.23.00.0 AM   620   0.2569388   7.00   9.20   5.59.0   12.23.00.0 AM   620   0.2569388   7.00   9.21   5.59.0   12.23.00.0 AM   620   0.2569388   7.00   9.22   5.59.0   12.2	9.22	553.0	12:00:00 AM	600	0.2641949	7.32		
9.27   SS6.0   12:03:00.AM   603   0.2629656   7.29   9.28   SS7.0   12:05:00.AM   605   0.2622281   7.27   9.30   SS8.0   12:05:00.AM   605   0.2622282   7.27   9.31   SS8.0   12:05:00.AM   606   0.2622282   7.27   9.33   SS6.0   12:07:00.AM   607   0.2617341   7.26   9.33   SS6.0   12:07:00.AM   607   0.2617341   7.26   9.33   SS6.0   12:09:00.AM   608   0.2610267   7.24   9.37   SS6.0   12:09:00.AM   609   0.2610267   7.24   9.37   SS6.0   12:09:00.AM   609   0.2610267   7.24   9.37   SS6.0   12:10.00.AM   610   0.266080   7.23   9.34   SS6.0   12:11:00.AM   611   0.260327   7.21   9.34   SS6.0   12:11:00.AM   611   0.260327   7.21   9.34   SS6.0   12:11:00.AM   612   0.2597816   7.20   9.34   SS6.0   12:11:00.AM   613   0.2597816   7.20   9.34   SS6.0   12:13:00.AM   613   0.2597818   7.29   9.34   SS6.0   12:13:00.AM   614   0.2597818   7.29   9.34   SS6.0   12:15:00.AM   615   0.2597817   7.17   9.34   SS6.0   12:15:00.AM   615   0.25978742   7.17   9.34   SS6.0   12:15:00.AM   616   0.25978742   7.17   9.35   9.37   0.2597818   7.19   9.37   0.2598818   7.19   9.37   0.2598818   7.19   9.37   0.2598818   7.19   9.37   0.2598818   7.19   9.37   0.2598818   7.19   9.37   0.2598818   7.19   9.37   0.2598818   7.19   9.37   0.2598818   7.19   9.37   0.2598818   7.19   9.39   0.25700   12:1700.AM   617   0.258818   7.17   1.2599.0   9.39   0.25700   12:1200.AM   618   0.257700   7.11   9.39   9.39   0.25700   12:1200.AM   619   0.2572078   7.11   9.39   9.39   0.25700   12:1200.AM   619   0.2572078   7.11   9.39   0.25700   0.25200.AM   620   0.2559868   7.12	9.23	554.0	12:01:00 AM	601	0.2637908	7.31		
9.28   557.0   12.04.00 AM   604   0.26.0602   7.28	9.25	555.0	12:02:00 AM	602	0.2635445	7.31		
9.30	9.27	556.0	12:03:00 AM	603	0.2629656	7.29		
9.32   S59.0   12.06.00 AM   606   0.2620318   7.26     9.38   S50.0   12.09.00 AM   608   0.2611405   7.24     9.39   S51.0   12.09.00 AM   608   0.2611405   7.24     9.39   S52.0   12.09.00 AM   609   0.2610567   7.24     9.39   S53.0   12.100.00 AM   610   0.2600608   7.23     9.30   S53.0   12.100.00 AM   611   0.2600608   7.23     9.40   S55.0   12.110.00 AM   611   0.250137   7.21     9.42   S55.0   12.110.00 AM   612   0.2591316   7.20     9.43   S56.0   12.110.00 AM   613   0.2591316   7.20     9.44   S56.0   12.110.00 AM   614   0.2591399   7.18     9.45   S66.0   12.110.00 AM   614   0.2591399   7.18     9.47   S66.0   12.110.00 AM   615   0.258742   7.17     9.48   S66.0   12.110.00 AM   615   0.258742   7.17     9.49   S57.0   12.110.00 AM   617   0.2581847   7.16     9.50   S71.0   12.18.00 AM   617   0.2581847   7.16     9.51   S71.0   12.18.00 AM   618   0.2577306   7.14     9.52   S71.0   12.18.00 AM   619   0.2577378   7.13     9.53   S72.0   12.12.00 AM   620   0.2589381   7.11     9.54   S73.0   12.20.00 AM   620   0.2593881   7.11     9.55   S73.0   12.20.00 AM   621   0.2559380   7.12     9.56   S75.0   12.22.00 AM   622   0.259381   7.11     9.56   S75.0   12.22.00 AM   623   0.259380   7.12     9.57   S74.0   12.12.00 AM   621   0.2553341   7.11     9.58   S78.0   12.20.00 AM   622   0.259381   7.11     9.59   S75.0   12.23.00 AM   623   0.259380   7.00     9.60   S76.0   12.23.00 AM   624   0.255772   7.00     9.61   S78.0   12.23.00 AM   624   0.255772   7.00     9.62   S78.0   12.23.00 AM   627   0.259341   7.00     9.63   S78.0   12.23.00 AM   627   0.259341   7.00     9.64   S78.0   12.23.00 AM   627   0.259341   7.00     9.67   S80.0   12.24.00 AM   627   0.2593419   7.00     9.69   S79.0   12.250.00 AM   627   0.2593419   7.00     9.70   S80.0   12.23.00 AM   630   0.2593419   7.00     9.71   S80.0   12.23.00 AM   630   0.2593419   7.00     9.72   S80.0   12.23.00 AM   630   0.2593419   7.00     9.73   S80.0   12.23.00 AM   630   0.2593419   7.00     9.74   S80.0   12.24.00 AM   64	9.28	557.0	12:04:00 AM	604	0.2626902	7.28		
9.33   SOO. 12.07.00 AM   GO7   0.261741   7.26   9.37   SEO. 12.08.00 AM   GO8   0.2611405   7.24   9.37   SEO. 12.08.00 AM   GO8   0.2610267   7.24   9.38   SS.30   12.11.00 AM   G10   0.2600267   7.24   9.40   SS40   12.11.00 AM   G11   0.260137   7.21   9.41   SS6.0   12.11.00 AM   G11   0.250137   7.21   9.42   SS6.0   12.11.00 AM   G11   0.250137   7.21   9.43   SS6.0   12.11.00 AM   G12   0.2597816   7.20   9.44   SS6.0   12.11.00 AM   G13   0.2594336   7.19   9.45   SS6.0   12.11.50 AM   G14   0.2591436   7.19   9.47   SS6.0   12.11.50 AM   G14   0.2591436   7.19   9.48   SS0.0   12.11.50 AM   G15   0.258742   7.17   9.48   SS0.0   12.11.50 AM   G16   0.258481   7.17   9.49   SS6.0   12.11.50 AM   G17   0.2581647   7.16   9.50   S70.0   12.17.00 AM   G17   0.2581647   7.16   9.51   S71.0   12.18.00 AM   G18   0.2577306   7.14   9.52   S71.0   12.18.00 AM   G19   0.2577306   7.14   9.53   S72.0   12.19.00 AM   G19   0.2577376   7.13   9.55   S73.0   12.200 AM   G20   0.2569386   7.12   9.57   S74.0   12.21.00 AM   G21   0.2569386   7.12   9.58   S75.0   12.22.00 AM   G21   0.2569386   7.11   9.59   S77.0   12.23.00 AM   G21   0.2569386   7.11   9.50   S77.0   12.23.00 AM   G23   0.2559304   7.09   9.61   S77.0   12.23.00 AM   G23   0.2559304   7.09   9.62   S77.0   12.24.00 AM   G24   0.255772   7.09   9.63   S78.0   12.22.00 AM   G26   0.2559347   7.09   9.64   S78.0   12.22.00 AM   G26   0.2559347   7.09   9.65   S78.0   12.22.00 AM   G26   0.2559347   7.00   9.67   S78.0   12.22.00 AM   G27   0.254568   7.05   9.68   S81.0   1.22.00 AM   G27   0.254568   7.05   9.69   S78.0   12.23.00 AM   G27   0.254568   7.05   9.69   S78.0   12.23.00 AM   G28   0.2559377   7.09   9.61   S78.0   12.23.00 AM   G28   0.2559372   7.09   9.62   S77.0   12.24.00 AM   G28   0.2559374   7.00   9.63   S78.0   12.250.00 AM   G28   0.253841   7.00   9.64   S78.0   12.250.00 AM   G28   0.2559374   7.00   9.65   S78.0   12.250.00 AM   G29   0.253841   7.00   9.67   S83.0   12.6000 AM   G28   0.2559375   7.05   9.68   S81.0   12	9.30	558.0	12:05:00 AM	605	0.2622282	7.27		
9.35   S51.0   12.09.00 AM   608   0.2611405   7.24   9.37   S52.0   12.09.00 AM   609   0.2610267   7.24   9.38   S63.0   12.10.00 AM   610   0.260808   7.23   9.40   S64.0   12.11.00 AM   611   0.260377   7.21   9.41   S65.0   12.12.00 AM   612   0.2597365   7.20   9.43   S65.0   12.13.00 AM   613   0.2594369   7.19   9.45   S65.0   12.13.00 AM   613   0.2594369   7.19   9.47   S68.0   12.15.00 AM   614   0.2591399   7.19   9.48   S65.0   12.15.00 AM   615   0.2587742   7.17   9.49   S68.0   12.15.00 AM   615   0.2587742   7.17   9.50   S70.0   12.17.00 AM   617   0.258147   7.16   9.51   S71.0   12.18.00 AM   618   0.2577306   7.14   9.52   S71.0   12.18.00 AM   618   0.2577306   7.14   9.53   S72.0   12.19.00 AM   619   0.2577378   7.13   9.55   S73.0   12.20.00 AM   620   0.2593881   7.11   9.56   S70.0   12.19.00 AM   621   0.259382   7.11   9.57   S74.0   12.19.00 AM   621   0.259382   7.11   9.58   S73.0   12.20.00 AM   621   0.259388   7.12   9.59   S70.0   12.19.00 AM   621   0.259388   7.12   9.59   S70.0   12.21.00 AM   621   0.259388   7.12   9.50   S70.0   12.21.00 AM   621   0.259388   7.12   9.51   S75.0   12.22.00 AM   622   0.259304   7.09   9.52   S76.0   12.22.00 AM   623   0.259300   7.09   9.53   S75.0   12.22.00 AM   624   0.259772   7.09   9.60   S76.0   12.22.00 AM   624   0.259772   7.09   9.61   S76.0   12.22.00 AM   625   0.259347   7.00   9.62   S78.0   12.22.00 AM   626   0.259347   7.00   9.63   S78.0   12.22.00 AM   626   0.259347   7.00   9.64   S80.0   12.270.00 AM   627   0.259368   7.04   9.67   S80.0   12.270.00 AM   628   0.259367   7.00   9.68   S81.0   12.290.00 AM   626   0.259367   7.00   9.78   S80.0   12.290.00 AM   627   0.259367   7.00   9.79   S80.0   12.390.00 AM   628   0.259367   7.00   9.79   S80.0   12.390.00 AM   629   0.259367   7.00   9.79   S80.0   12.390.00 AM   630   0.259367   7.00   9.79   S80.0   12.390.00 AM   630   0.259367   6.99   9.89   S90.0   12.490.00 AM   640   0.249375   6.99   9.89   S90.0   12.490.00 AM   640   0.249375   6.99   9.89   S90	9.32	559.0	12:06:00 AM	606	0.2620318	7.26		
9.37 S20.0 12.09.00 AM 669 0.2610267 7.24 9.38 S53.0 12.11.00 AM 610 0.260137 7.21 9.40 S54.0 12.11.00 AM 611 0.260137 7.21 9.41 S56.0 12.12.00 AM 611 0.260137 7.21 9.42 S55.0 12.12.00 AM 612 0.2597816 7.20 9.43 S66.0 12.12.00 AM 613 0.259436 7.19 9.45 S67.0 12.14.00 AM 614 0.3591499 7.18 9.47 S68.0 12.15.00 AM 615 0.259436 7.17 9.48 S69.0 12.15.00 AM 615 0.259436 7.17 9.48 S69.0 12.15.00 AM 616 0.259436 7.17 9.49 S69.0 12.10.00 AM 617 0.2591499 7.18 9.50 S70.0 12.17.00 AM 617 0.2591497 7.16 9.51 S71.0 12.18.00 AM 618 0.2597376 7.16 9.52 S71.0 12.18.00 AM 619 0.259368 7.12 9.53 S72.0 12.19.00 AM 619 0.259368 7.12 9.55 S73.0 12.200 AM 620 0.2569368 7.12 9.57 S74.0 12.21.00 AM 621 0.2569368 7.12 9.58 S75.0 12.22.00 AM 621 0.2569368 7.11 9.58 S75.0 12.22.00 AM 622 0.2569341 7.11 9.58 S75.0 12.22.00 AM 623 0.2559377 7.09 9.60 S77.0 12.24.00 AM 623 0.255937 7.09 9.61 S77.0 12.24.00 AM 623 0.2559304 7.09 9.62 S77.0 12.24.00 AM 623 0.2559304 7.09 9.63 S78.0 12.22.00 AM 625 0.255347 7.08 9.65 S78.0 12.22.00 AM 626 0.255972 7.09 9.65 S78.0 12.22.00 AM 626 0.2559347 7.08 9.65 S78.0 12.22.00 AM 626 0.2559347 7.08 9.65 S78.0 12.22.00 AM 627 0.254949 7.09 9.69 S78.0 12.2500 AM 626 0.2559349 7.09 9.69 S78.0 12.2500 AM 627 0.254969 7.09 9.69 S78.0 12.2500 AM 627 0.254969 7.09 9.79 S80.0 12.2500 AM 628 0.254969 7.09 9.79 S80.0 12.2500 AM 629 0.253899 7.02 9.79 S80.0 12.2500 AM 629 0.253899 7.02 9.79 S80.0 12.2500 AM 629 0.253899 7.09 9.70	9.33	560.0	12:07:00 AM	607	0.2617341	7.26		
9.38   S63.0   12:10:00 AM   610   0.2606806   7.23   9.40   S64.0   12:11:00 AM   611   0.260137   7.21   9.42   S65.0   12:12:00 AM   612   0.2691316   7.20   9.43   S66.0   12:13:00 AM   613   0.2594316   7.19   9.44   S68.0   12:13:00 AM   614   0.2591499   7.18   9.47   S68.0   12:13:00 AM   615   0.259742   7.17   9.48   S69.0   12:14:00 AM   616   0.259742   7.17   9.59   S70.0   12:14:00 AM   617   0.258167   7.16   9.50   S70.0   12:17:00 AM   618   0.259742   7.17   9.50   S70.0   12:17:00 AM   618   0.259730   7.14   9.51   S71.0   12:18:00 AM   619   0.257730   7.14   9.52   S71.0   12:18:00 AM   620   0.257730   7.13   9.55   S73.0   12:20:00 AM   620   0.257936   7.14   9.55   S73.0   12:20:00 AM   621   0.256342   7.11   9.56   S75.0   12:22:00 AM   622   0.256342   7.11   9.57   S74.0   12:22:00 AM   622   0.256341   7.11   9.58   S77.0   12:23:00 AM   622   0.256341   7.11   9.60   S76.0   12:23:00 AM   622   0.255347   7.09   9.61   S78.0   12:25:00 AM   624   0.255772   7.09   9.62   S77.0   12:25:00 AM   624   0.255772   7.09   9.63   S78.0   12:25:00 AM   625   0.253347   7.08   9.65   S78.0   12:25:00 AM   626   0.255347   7.08   9.66   S61.0   12:23:00 AM   627   0.254516   7.06   9.67   S80.0   12:27:00 AM   627   0.254516   7.05   9.68   S61.0   12:28:00 AM   628   0.253347   7.08   9.79   S82.0   12:28:00 AM   629   0.253347   7.08   9.70   S82.0   12:28:00 AM   627   0.254516   7.06   9.71   S83.0   12:28:00 AM   628   0.2545199   7.00   9.72   S83.0   12:23:00 AM   629   0.253347   7.00   9.73   S84.0   12:33:00 AM   630   0.2543199   7.00   9.74   S83.0   12:33:00 AM   630   0.2543199   7.00   9.75   S83.0   12:33:00 AM   630   0.2543199   7.00   9.77   S83.0   12:33:00 AM   630   0.2533199   7.00   9.78   S84.0   12:34:00 AM   630   0.2533199   7.00   9.79   S85.0   12:35:00 AM   630   0.2533199   7.00   9.79   S85.0   12:35:00 AM   630   0.2533199   7.00   9.79   S86.0   12:33:00 AM   630   0.2533199   6.99   9.80   S88.0   12:33:00 AM   630   0.2533199   6.99   9.81   S88.0   12:	9.35	561.0	12:08:00 AM	608	0.2611405	7.24		
9.40	9.37	562.0	12:09:00 AM	609	0.2610267	7.24		
9.42   565.0   12:12:00 AM   612   0.2597816   7.20   9.45   565.0   12:13:00 AM   613   0.2594336   7.19   9.45   567.0   12:14:00 AM   614   0.2591499   7.18   9.47   568.0   12:15:00 AM   614   0.2591499   7.18   9.47   568.0   12:15:00 AM   615   0.259742   7.17   9.50   570.0   12:17:00 AM   616   0.259149   7.16   9.50   570.0   12:17:00 AM   617   0.2591467   7.16   9.50   570.0   12:17:00 AM   618   0.259736   7.14   1.2590   7.14   9.55   571.0   12:18:00 AM   618   0.2577306   7.14   1.25914   7.15   9.52   571.0   12:19:00 AM   619   0.257278   7.13   9.55   573.0   12:21:00 AM   620   0.259368   7.12   9.57   574.0   12:21:00 AM   621   0.259368   7.12   9.57   574.0   12:21:00 AM   621   0.2563441   7.11   9.56   575.0   12:22:00 AM   622   0.2563441   7.11   9.56   576.0   12:23:00 AM   623   0.2559004   7.09   9.62   577.0   12:24:00 AM   624   0.255777   7.09   9.63   578.0   12:23:00 AM   625   0.2559004   7.09   9.65   579.0   12:25:00 AM   625   0.2559377   7.08   9.65   579.0   12:25:00 AM   626   0.2583116   7.06   9.65   579.0   12:27:00 AM   627   0.2553147   7.08   9.65   579.0   12:27:00 AM   627   0.2545063   7.05   9.66   581.0   12:28:00 AM   628   0.2541068   7.04   9.75   582.0   12:28:00 AM   627   0.2545063   7.05   9.66   581.0   12:28:00 AM   628   0.2541068   7.04   9.75   583.0   12:28:00 AM   629   0.2541068   7.04   9.75   583.0   12:28:00 AM   629   0.2541068   7.04   9.75   583.0   12:28:00 AM   629   0.2541069   7.00   9.75   585.0   12:38:00 AM   630   0.2531099   7.00   9.75   585.0   12:38:00 AM   630   0.2531099   7.00   9.75   585.0   12:38:0	9.38	563.0	12:10:00 AM	610	0.2606808	7.23		
9.42   565.0   12:12:00 AM   612   0.2597816   7.20   9.45   565.0   12:13:00 AM   613   0.2594336   7.19   9.45   567.0   12:14:00 AM   614   0.2591499   7.18   9.47   568.0   12:15:00 AM   614   0.2591499   7.18   9.47   568.0   12:15:00 AM   615   0.259742   7.17   9.50   570.0   12:17:00 AM   616   0.259149   7.16   9.50   570.0   12:17:00 AM   617   0.2591467   7.16   9.50   570.0   12:17:00 AM   618   0.259736   7.14   1.2590   7.14   9.55   571.0   12:18:00 AM   618   0.2577306   7.14   1.25914   7.15   9.52   571.0   12:19:00 AM   619   0.257278   7.13   9.55   573.0   12:21:00 AM   620   0.259368   7.12   9.57   574.0   12:21:00 AM   621   0.259368   7.12   9.57   574.0   12:21:00 AM   621   0.2563441   7.11   9.56   575.0   12:22:00 AM   622   0.2563441   7.11   9.56   576.0   12:23:00 AM   623   0.2559004   7.09   9.62   577.0   12:24:00 AM   624   0.255777   7.09   9.63   578.0   12:23:00 AM   625   0.2559004   7.09   9.65   579.0   12:25:00 AM   625   0.2559377   7.08   9.65   579.0   12:25:00 AM   626   0.2583116   7.06   9.65   579.0   12:27:00 AM   627   0.2553147   7.08   9.65   579.0   12:27:00 AM   627   0.2545063   7.05   9.66   581.0   12:28:00 AM   628   0.2541068   7.04   9.75   582.0   12:28:00 AM   627   0.2545063   7.05   9.66   581.0   12:28:00 AM   628   0.2541068   7.04   9.75   583.0   12:28:00 AM   629   0.2541068   7.04   9.75   583.0   12:28:00 AM   629   0.2541068   7.04   9.75   583.0   12:28:00 AM   629   0.2541069   7.00   9.75   585.0   12:38:00 AM   630   0.2531099   7.00   9.75   585.0   12:38:00 AM   630   0.2531099   7.00   9.75   585.0   12:38:0	9.40	564.0	12:11:00 AM	611	0.260137	7.21		
9.48   566.0   12:13:00 AM   613   0.2594336   7.19   9.45   567.0   12:14:00 AM   614   0.2594336   7.19   9.47   568.0   12:15:00 AM   615   0.2587742   7.17   9.48   569.0   12:15:00 AM   615   0.2587742   7.17   9.48   569.0   12:15:00 AM   615   0.2581647   7.16   9.55   7.10   12:13:00 AM   617   0.2581647   7.16   9.52   571.0   12:13:00 AM   618   0.2577306   7.14   9.55   571.0   12:13:00 AM   618   0.2577306   7.14   9.55   571.0   12:19:00 AM   619   0.2573796   7.14   9.55   573.0   12:20:00 AM   620   0.259588   7.12   9.55   573.0   12:20:00 AM   621   0.2587388   7.12   9.55   573.0   12:20:00 AM   622   0.256341   7.11   9.58   575.0   12:22:00 AM   622   0.256341   7.11   9.58   575.0   12:22:00 AM   622   0.256341   7.11   9.56   577.0   12:24:00 AM   622   0.256341   7.11   9.56   577.0   12:24:00 AM   624   0.255772   7.09   9.63   578.0   12:25:00 AM   624   0.255772   7.09   9.63   578.0   12:25:00 AM   624   0.255772   7.09   9.63   578.0   12:25:00 AM   626   0.2553347   7.08   9.67   580.0   12:27:00 AM   626   0.2543166   7.06   9.67   580.0   12:27:00 AM   627   0.2545063   7.05   9.68   581.0   12:2800 AM   628   0.2543166   7.04   9.70   582.0   12:2800 AM   628   0.2533161   7.06   9.70   582.0   12:2800 AM   628   0.2533161   7.04   9.70   588.0   12:2300 AM   630   0.2533199   7.02   9.73   584.0   12:13:00 AM   631   0.2533003   7.02   9.75   585.0   12:3300 AM   633   0.2533103   7.02   9.77   586.0   12:3300 AM   633   0.2533171   7.00   9.78   585.0   12:3300 AM   633   0.253171   7.00   9.78   585.0   12:3300 AM   633   0.253171   7.00   9.79   586.0   12:3300 AM   633   0.253171   7.00   9.79   586.0   12:3300 AM   633   0.253171   7.00   9.79   586.0   12:3300 AM   633   0.253073   6.98   9.88   593.0   12:3500 AM   634   0.2500555   6.94   9.95   597.0   12:4400 AM   644   0.249350   6.91   9.95   597.0   12:4400 AM								
9.45   567.0   12:14:00 AM   614   0.2591499   7.18								
9.47 568.0 12:15:00 AM 615 0.258742 7.17 9.48 569.0 12:16:00 AM 616 0.255481 7.17 9.50 570.0 12:17:00 AM 617 0.2581647 7.16 9.51 571.0 12:18:00 AM 618 0.2577306 7.14 9.52 571.0 12:18:00 AM 619 0.2572978 7.13 9.53 572.0 12:19:00 AM 619 0.2572978 7.13 9.55 573.0 12:200 AM 620 0.2569368 7.12 9.57 574.0 12:20 AM 620 0.2569368 7.12 9.58 575.0 12:220 AM 620 0.2569368 7.11 9.58 575.0 12:220 AM 621 0.2565182 7.11 9.58 575.0 12:220 AM 622 0.256341 7.11 9.59 575.0 12:220 AM 622 0.256341 7.11 9.60 576.0 12:2300 AM 622 0.2559004 7.09 9.61 577.0 12:2400 AM 624 0.255772 7.09 9.63 578.0 12:2500 AM 626 0.2559347 7.08 9.65 578.0 12:2500 AM 626 0.2559347 7.08 9.66 578.0 12:2500 AM 626 0.2559347 7.08 9.67 580.0 12:2700 AM 627 0.2545063 7.05 9.67 580.0 12:2700 AM 628 0.2559304 7.00 9.68 581.0 12:2500 AM 628 0.2541268 7.04 9.70 582.0 12:2800 AM 628 0.2541268 7.04 9.71 583.0 12:2800 AM 628 0.2541268 7.04 9.72 583.0 12:2800 AM 628 0.2541268 7.04 9.73 584.0 12:2800 AM 630 0.2534199 7.02 9.75 585.0 12:2300 AM 631 0.253003 7.02 9.77 585.0 12:3200 AM 632 0.253999 7.02 9.78 585.0 12:3200 AM 633 0.253117 7.00 9.79 585.0 12:3300 AM 633 0.253117 7.00 9.79 585.0 12:3300 AM 633 0.253177 6.99 9.89 588 588 0.12:3300 AM 633 0.253177 6.99 9.89 588 589 0.12:3300 AM 634 0.2532513 6.99 9.89 589 0.12:3400 AM 644 0.249128 6.91 9.99 599 0.99 0.99 0.99 0.99 0.99 0.99 0								
9.48								
9.50   5700   12:17:00 AM   617   0.2581647   7.16     9.52   571.0   12:18:00 AM   618   0.257306   7.14     9.53   572.0   12:19:00 AM   619   0.257278   7.13     9.55   573.0   12:20:00 AM   620   0.2569368   7.12     9.57   574.0   12:21:00 AM   620   0.2569382   7.11     9.58   575.0   12:22:00 AM   622   0.256312   7.11     9.59   575.0   12:22:00 AM   622   0.256341   7.11     9.60   576.0   12:23:00 AM   622   0.256341   7.11     9.60   576.0   12:23:00 AM   622   0.255972   7.09     9.62   577.0   12:24:00 AM   624   0.255772   7.09     9.63   578.0   12:25:00 AM   626   0.255772   7.08     9.65   578.0   12:25:00 AM   626   0.255347   7.08     9.67   580.0   12:27:00 AM   627   0.2545063   7.05     9.67   580.0   12:27:00 AM   628   0.254168   7.04     9.70   582.0   12:28:00 AM   629   0.253816   7.04     9.71   582.0   12:29:00 AM   629   0.253816   7.04     9.72   583.0   12:30:00 AM   631   0.2532003   7.02     9.73   584.0   12:31:00 AM   631   0.2532003   7.02     9.75   585.0   12:33:00 AM   632   0.253173   7.00     9.77   586.0   12:33:00 AM   633   0.253173   7.00     9.78   587.0   12:33:00 AM   633   0.2525173   7.00     9.79   588.0   12:33:00 AM   633   0.2525173   7.00     9.70   9.71   9.72   9.72   9.72   9.72   9.73   9.74   9.75   9.7								
9.52 571.0 12:18:00 AM 618 0.257306 7.14 9.53 572.0 12:19:00 AM 619 0.2573978 7.13 9.55 573.0 12:20:00 AM 620 0.256388 7.12 9.57 574.0 12:21:00 AM 621 0.256388 7.12 9.58 575.0 12:22:00 AM 621 0.256382 7.11 9.58 575.0 12:22:00 AM 622 0.2563441 7.11 9.58 575.0 12:23:00 AM 623 0.2559004 7.09 9.60 576.0 12:23:00 AM 623 0.2559004 7.09 9.61 577.0 12:24:00 AM 624 0.255772 7.09 9.62 577.0 12:24:00 AM 624 0.255772 7.09 9.63 578.0 12:25:00 AM 625 0.253347 7.08 9.65 579.0 12:25:00 AM 626 0.2548116 7.06 9.67 580.0 12:27:00 AM 627 0.254503 7.05 9.68 581.0 12:28:00 AM 628 0.2541288 7.04 9.70 582.0 12:29:00 AM 629 0.258816 7.04 9.72 583.0 12:30:00 AM 630 0.2534199 7.02 9.73 584.0 12:31:00 AM 631 0.253003 7.02 9.75 585.0 12:33:00 AM 632 0.2530795 7.02 9.77 586.0 12:33:00 AM 631 0.252503 7.02 9.78 587.0 12:33:00 AM 633 0.2525171 7.00 9.79 586.0 12:33:00 AM 631 0.252503 7.02 9.77 586.0 12:33:00 AM 631 0.252503 7.02 9.78 587.0 12:34:00 AM 631 0.252503 7.02 9.79 586.0 12:33:00 AM 632 0.2530795 7.02 9.79 586.0 12:33:00 AM 633 0.2525171 7.00 9.80 588.0 12:35:00 AM 634 0.2525613 6.99 9.80 588.0 12:35:00 AM 635 0.2519194 6.98 9.81 589.0 12:35:00 AM 636 0.251673 6.98 9.82 589.0 12:35:00 AM 637 0.251539 6.97 9.83 591.0 12:33:00 AM 639 0.2508717 6.95 9.85 591.0 12:33:00 AM 639 0.2508715 6.95 9.86 591.0 12:33:00 AM 639 0.2508717 6.95 9.99 595.0 12:43:00 AM 644 0.2502653 6.99 9.90 594.0 12:44:00 AM 644 0.2502653 6.99 9.91 596.0 12:43:00 AM 649 0.250955 6.94 9.90 594.0 12:44:00 AM 640 0.250955 6.94 9.90 594.0 12:44:00 AM 641 0.2504846 6.88 10.00 600.0 12:47:00 AM 647 0.248155 6.88 10.00 600.0 12:47:00 AM 649 0.2477337 6.85 10.01 600.0 12:48:00 AM 649 0.2477337 6.85 10.01 600.0 12:48:00 AM 649 0.2477337 6.85 10.01 600.0 12:48:00 AM 649 0.247752 6.87 10.01 600.0 12:48:00 AM 649 0.247753 6.88 10.00 600.0 12:48:00 AM 649 0.247753 6.88 10.								
9.53								
9.55   573.0   1.2:2:00 AM   620   0.2569368   7.12   9.57   574.0   12:2:00 AM   621   0.2565182   7.11   9.58   575.0   12:2:200 AM   622   0.2563441   7.11   9.60   576.0   12:2:300 AM   623   0.2559004   7.09   9.60   576.0   12:2:300 AM   624   0.255772   7.09   9.61   577.0   12:2:400 AM   624   0.255772   7.09   9.63   578.0   12:2:500 AM   625   0.2553447   7.08   9.65   579.0   12:2:600 AM   626   0.2558116   7.06   9.67   580.0   12:27:00 AM   627   0.2545663   7.05   9.68   581.0   12:28:00 AM   628   0.2541268   7.04   9.70   582.0   12:29:00 AM   629   0.2538816   7.04   9.71   582.0   12:29:00 AM   630   0.2541268   7.04   9.72   583.0   12:300 AM   630   0.2541269   7.02   9.73   584.0   12:31:00 AM   631   0.253003   7.02   9.74   584.0   12:31:00 AM   631   0.253003   7.02   9.75   586.0   12:32:00 AM   632   0.2530795   7.02   9.77   586.0   12:33:00 AM   633   0.252613   6.99   9.80   588.0   12:33:00 AM   634   0.2522613   6.99   9.80   588.0   12:33:00 AM   636   0.251673   6.98   9.81   589.0   12:33:00 AM   636   0.251673   6.98   9.83   590.0   12:37:00 AM   637   0.2513539   6.97   9.87   592.0   12:38:00 AM   638   0.251673   6.98   9.88   591.0   12:38:00 AM   638   0.251673   6.98   9.89   594.0   12:38:00 AM   639   0.250653   6.95   9.80   594.0   12:38:00 AM   630   0.251673   6.98   9.81   591.0   12:38:00 AM   630   0.251859   6.97   9.87   592.0   12:38:00 AM   638   0.2508717   6.95   9.88   593.0   12:38:00 AM   639   0.250653   6.95   9.99   594.0   12:38:00 AM   640   0.249328   6.97   9.99   595.0   12:42:00 AM   641   0.250148   6.99   9.99   595.0   12:42:00 AM   642   0.249725   6.92   9.99   595.0   12:42:00 AM   643   0.2493508   6.91   9.99   599.0   12:43:00 AM   644   0.2491928   6.91   9.99   599.0   12:43:00 AM   645   0.2493508   6.91   9.99   599.0   12:43:00 AM   646   0.2493508   6.91   9.99   599.0   12:43:00 AM   647   0.248329   6.90   9.99   599.0   12:43:00 AM   648   0.2493508   6.91   10.00   600.0   12:47:00 AM   647   0.248350   6.91   10.01   600.0								
9.57   5740   12:21:00 AM   621   0.2565182   7.11   9.58   575.0   12:22:00 AM   622   0.2563441   7.11   9.60   576.0   12:23:00 AM   623   0.2559004   7.09   9.62   577.0   12:24:00 AM   624   0.255772   7.09   9.62   577.0   12:24:00 AM   624   0.255772   7.09   9.62   577.0   12:24:00 AM   625   0.255347   7.08   9.65   579.0   12:26:00 AM   626   0.2548116   7.06   9.65   579.0   12:26:00 AM   626   0.2548116   7.06   9.67   580.0   12:27:00 AM   627   0.2545063   7.05   9.67   580.0   12:27:00 AM   628   0.2541268   7.04   9.70   582.0   12:29:00 AM   628   0.2541268   7.04   9.70   582.0   12:29:00 AM   630   0.2534199   7.02   9.73   584.0   12:31:00 AM   631   0.2532003   7.02   9.73   584.0   12:31:00 AM   631   0.2532003   7.02   9.75   585.0   12:32:00 AM   632   0.2534199   7.02   9.77   586.0   12:33:00 AM   633   0.2525171   7.00   9.78   587.0   12:33:00 AM   633   0.2525171   7.00   9.78   587.0   12:33:00 AM   633   0.2525171   7.00   9.78   587.0   12:33:00 AM   635   0.2519194   6.98   9.82   589.0   12:35:00 AM   636   0.251673   6.98   9.83   590.0   12:37:00 AM   637   0.251673   6.98   9.83   590.0   12:38:00 AM   638   0.2508717   6.95   9.87   592.0   12:38:00 AM   639   0.2508517   6.95   9.97   9.97   592.0   12:38:00 AM   634   0.252613   6.99   9.97   9.97   592.0   12:38:00 AM   636   0.251673   6.98   9.97   9.97   592.0   12:38:00 AM   638   0.2508717   6.95   9.97   9.97   9.90								
9.58 575.0 12:22:00 AM 622 0.2563441 7.11 9.60 576.0 12:23:00 AM 623 0.2559004 7.09 9.62 577.0 12:24:00 AM 624 0.255772 7.09 9.63 578.0 12:25:00 AM 625 0.2553347 7.08 9.63 578.0 12:25:00 AM 625 0.2553347 7.08 9.65 579.0 12:26:00 AM 626 0.2548116 7.06 9.67 580.0 12:27:00 AM 627 0.2545063 7.05 9.68 581.0 12:28:00 AM 628 0.2541268 7.04 9.70 582.0 12:29:00 AM 629 0.253816 7.04 9.71 582.0 12:29:00 AM 629 0.253816 7.04 9.72 583.0 12:30:00 AM 630 0.2534199 7.02 9.73 584.0 12:31:00 AM 631 0.2532003 7.02 9.75 585.0 12:33:00 AM 632 0.2532199 7.02 9.77 586.0 12:33:00 AM 632 0.253219 7.02 9.78 587.0 12:34:00 AM 634 0.2522613 6.99 9.80 588.0 12:33:00 AM 635 0.2519194 6.98 9.82 589.0 12:35:00 AM 636 0.251673 6.98 9.83 589.0 12:33:00 AM 636 0.251673 6.98 9.84 589.0 12:38:00 AM 636 0.251673 6.98 9.85 591.0 12:38:00 AM 638 0.2508717 6.95 9.87 592.0 12:39:00 AM 639 0.2508517 6.95 9.88 593.0 12:38:00 AM 639 0.2508517 6.95 9.89 594.0 12:38:00 AM 639 0.2508517 6.95 9.80 588.0 12:38:00 AM 639 0.2508717 6.95 9.81 599.0 12:38:00 AM 639 0.2508515 6.95 9.82 589.0 12:38:00 AM 639 0.2508517 6.95 9.85 591.0 12:38:00 AM 639 0.2508517 6.95 9.87 592.0 12:38:00 AM 639 0.2508518 6.97 9.99 594.0 12:40.00 AM 640 0.2502955 6.94 9.90 594.0 12:40.00 AM 641 0.2501408 6.93 9.91 594.0 12:40.00 AM 642 0.249725 6.92 9.93 595.0 12:43:00 AM 643 0.249725 6.92 9.93 595.0 12:43:00 AM 644 0.2491928 6.91 9.95 597.0 12:44:00 AM 644 0.2491928 6.91 10.00 600.0 12:47:00 AM 649 0.2493508 6.91 10.01 600.0 12:47:00 AM 649 0.2493508 6.91 10.02 601.0 12:48:00 AM 643 0.249755 6.85 10.03 602.0 12:48:00 AM 649 0.2493508 6.91 10.03 602.0 12:48:00 AM 649 0.2493508 6.91 10.04 605.0 12:48:00 AM 649 0.2493508 6.91 10.05 603.0 12:49:00 AM 649 0.2493508 6.91 10.06 603.0 12:49:00 AM 649 0.2493508 6.91 10.07 604.0 12:48:00 AM 649 0.2493508 6.81 10.00 600.0 12:49:00 AM 664 0.2483446 6.88 10.00 600.0 12:49:00 AM 664 0.2483446 6.88 10.00 600.0 12:49:00 AM 664 0.2483446 6.88 10.00 600.0 12:49:00 AM 665 0.2485029 6.99 10.10 600.0 12:49:00 AM 667 0.248329 6.99 10.11 600.0 12:500 AM 659 0								
9.60								
9.62   577.0   12:24:00 AM   624   0.255772   7.09     9.63   578.0   12:25:00 AM   625   0.2553347   7.08     9.65   579.0   12:25:00 AM   626   0.2548116   7.06     9.67   580.0   12:27:00 AM   627   0.2545063   7.05     9.68   581.0   12:28:00 AM   628   0.2541268   7.04     9.70   582.0   12:29:00 AM   629   0.258816   7.04     9.71   582.0   12:39:00 AM   630   0.2538199   7.02     9.72   583.0   12:30:00 AM   630   0.2534199   7.02     9.75   585.0   12:32:00 AM   632   0.2530795   7.02     9.76   585.0   12:33:00 AM   633   0.2525073   7.00     9.77   586.0   12:33:00 AM   633   0.2525171   7.00     9.78   587.0   12:34:00 AM   634   0.2522613   6.99     9.80   588.0   12:35:00 AM   635   0.2519194   6.98     9.81   589.0   12:36:00 AM   636   0.251373   6.98     9.82   589.0   12:36:00 AM   637   0.2513539   6.97     9.85   591.0   12:38:00 AM   638   0.2508717   6.95     9.85   591.0   12:38:00 AM   638   0.2508717   6.95     9.86   593.0   12:40:00 AM   640   0.2502553   6.94     9.90   594.0   12:41:00 AM   641   0.2501408   6.93     9.90   595.0   12:42:00 AM   641   0.2501408   6.93     9.90   594.0   12:41:00 AM   641   0.2501408   6.93     9.90   595.0   12:42:00 AM   642   0.249725   6.92     9.91   595.0   12:42:00 AM   643   0.2493508   6.91     9.92   595.0   12:43:00 AM   644   0.2491228   6.91     9.93   596.0   12:43:00 AM   648   0.249725   6.92     9.93   596.0   12:43:00 AM   648   0.249725   6.92     9.93   596.0   12:43:00 AM   648   0.249725   6.95     9.93   596.0   12:43:00 AM   648   0.249725   6.95     9.93   596.0   12:43:00 AM   648   0.249725   6.95     9.93   596.0   12:43:00 AM   649   0.2493508   6.91     9.91   597.0   12:44:00 AM   646   0.2493508   6.91     9.92   595.0   12:44:00 AM   649   0.2493508   6.91     9.93   596.0   12:44:00 AM   649   0.2493508   6.91     10.00   600.0   12:44:00 AM   649   0.2493508   6.91     10.01   600.0   12:44:00 AM   649   0.2493508   6.91     10.02   601.0   12:50.00 AM   659   0.2466466   6.83     10.03   602.0   12:50.00 AM   659								
9.63   578.0   12:25:00 AM   625   0.2553347   7.08   9.65   579.0   12:26:00 AM   626   0.2548116   7.06   9.67   580.0   12:27:00 AM   627   0.2545063   7.05   9.68   581.0   12:28:00 AM   628   0.2541268   7.04   9.70   582.0   12:29:00 AM   629   0.253816   7.04   9.70   582.0   12:39:00 AM   630   0.2534199   7.02   9.73   584.0   12:31:00 AM   631   0.253303   7.02   9.75   585.0   12:32:00 AM   632   0.253303   7.02   9.75   585.0   12:32:00 AM   633   0.2530795   7.02   9.77   586.0   12:33:00 AM   633   0.2530795   7.02   9.78   587.0   12:34:00 AM   634   0.2522613   6.99   9.80   588.0   12:35:00 AM   635   0.2519194   6.98   9.82   589.0   12:35:00 AM   636   0.251673   6.98   9.83   590.0   12:37:00 AM   637   0.2516539   6.97   9.85   591.0   12:38:00 AM   639   0.2506553   6.95   9.85   591.0   12:38:00 AM   630   0.2506553   6.95   9.88   593.0   12:35:00 AM   630   0.2506553   6.95   9.98   599.0   12:38:00 AM   630   0.2506553   6.95   9.99   9.90   594.0   12:41:00 AM   640   0.2502955   6.94   9.99   9.90   594.0   12:41:00 AM   641   0.2501408   6.93   9.90   9.90   12:41:00 AM   642   0.249725   6.92   9.93   595.0   12:42:00 AM   643   0.249928   6.91   9.97   598.0   12:45:00 AM   643   0.249928   6.91   9.97   598.0   12:45:00 AM   644   0.249128   6.91   9.97   598.0   12:45:00 AM   645   0.248329   6.90   9.98   599.0   12:45:00 AM   646   0.248346   6.68   6.88   10.00   600.0   12:47:00 AM   646   0.248346   6.68   6.91   9.98   599.0   12:45:00 AM   647   0.248346   6.68   6.81   10.00   600.0   12:47:00 AM   647   0.2487676   6.86   6.81   10.00   600.0   12:47:00 AM   647   0.2487676   6.86   6.81   10.00   600.0   12:47:00 AM   649   0.2477672   6.85   6.81   10.00   600.0   12:47:00 AM   649   0.2477672   6.85   6.81   10.00   600.0   12:50.00 AM   659   0.2466465   6.81   10.00   600.0   12:50.00 AM								
9.65 579.0 12:26:00 AM 626 0.2548116 7.06 9.67 580.0 12:27:00 AM 627 0.2545063 7.05 9.68 581.0 12:28:00 AM 628 0.2541268 7.04 9.70 582.0 12:28:00 AM 629 0.253816 7.04 9.70 582.0 12:28:00 AM 630 0.2534199 7.02 9.73 584.0 12:31:00 AM 631 0.2532003 7.02 9.73 584.0 12:31:00 AM 631 0.2532003 7.02 9.75 585.0 12:32:00 AM 632 0.2530795 7.02 9.77 586.0 12:33:00 AM 633 0.255171 7.00 9.77 586.0 12:33:00 AM 633 0.255171 7.00 9.78 587.0 12:34:00 AM 634 0.2522613 6.99 9.78 587.0 12:35:00 AM 635 0.255171 7.00 9.88 587.0 12:35:00 AM 635 0.255171 6.98 9.80 588.0 12:35:00 AM 636 0.251673 6.98 9.99 9.80 588.0 12:35:00 AM 636 0.251673 6.98 9.99 9.83 590.0 12:35:00 AM 636 0.251673 6.98 9.99 9.85 591.0 12:38:00 AM 638 0.2508717 6.95 9.85 591.0 12:38:00 AM 638 0.2508717 6.95 9.988 591.0 12:38:00 AM 639 0.2506553 6.95 9.99 9.90 594.0 12:40:00 AM 641 0.2502955 6.94 9.90 594.0 12:41:00 AM 641 0.2501408 6.93 9.99 9.99 595.0 12:42:00 AM 642 0.249725 6.92 9.99 595.0 12:42:00 AM 644 0.249128 6.91 9.99 595.0 12:43:00 AM 645 0.2488329 6.90 9.99 595.0 12:43:00 AM 645 0.2488329 6.90 9.99 595.0 12:43:00 AM 645 0.24893508 6.91 9.99 597.0 12:44:00 AM 644 0.249128 6.91 9.99 595.0 12:45:00 AM 645 0.24893508 6.91 9.99 597.0 12:45:00 AM 646 0.2483446 6.88 10.00 600.0 12:4700 AM 649 0.2493508 6.91 9.99 597.0 12:45:00 AM 646 0.2483446 6.88 10.00 600.0 12:4700 AM 647 0.2481155 6.88 10.00 600.0 12:4700 AM 649 0.2483367 6.86 10.00 600.0 12:4700 AM 649 0.2483367 6.86 10.00 600.0 12:4700 AM 649 0.2483466 6.88 10.00 600.0 12:45:00 AM 650 0.24863664 6.88 10.00 600.0 12:45:00 AM 651 0.2486465 6.84 10.00 600.0 12:45:00 AM 651 0.2486465 6.84 10.00 600.0 12:45:00 AM 651 0.2486465 6.84 10.00 600.0 12:50.00 AM 655 0.2486566 6.81 10.10 6								
9.67   580.0   12:27:00 AM   627   0.2545063   7.05   9.88   581.0   12:28:00 AM   628   0.2541268   7.04   9.70   582.0   12:29:00 AM   629   0.2538816   7.04   9.72   583.0   12:30:00 AM   630   0.2534199   7.02   9.73   584.0   12:31:00 AM   631   0.2532003   7.02   9.73   584.0   12:31:00 AM   631   0.2532003   7.02   9.77   586.0   12:32:00 AM   632   0.2530795   7.02   9.77   586.0   12:33:00 AM   633   0.2525171   7.00   9.78   587.0   12:34:00 AM   634   0.2522613   6.99   9.80   588.0   12:35:00 AM   635   0.2519194   6.96   9.82   589.0   12:36:00 AM   636   0.251673   6.98   9.82   589.0   12:36:00 AM   637   0.2513539   6.97   9.93   595.0   12:39:00 AM   638   0.2508717   6.95   9.87   592.0   12:39:00 AM   638   0.2508717   6.95   9.87   9.98   592.0   12:39:00 AM   638   0.2508573   6.95   9.98   9.99   9.90								
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9.88         593.0         12:40:00 AM         640         0.2502955         6.94           9.90         594.0         12:41:00 AM         641         0.2501408         6.93           9.92         595.0         12:42:00 AM         642         0.249725         6.92           9.93         596.0         12:43:00 AM         643         0.2493508         6.91           9.95         597.0         12:44:00 AM         644         0.249128         6.91           9.97         598.0         12:45:00 AM         645         0.248329         6.90           9.98         599.0         12:46:00 AM         646         0.2483446         6.88           10.00         600.0         12:47:00 AM         647         0.2481155         6.88           10.02         601.0         12:48:00 AM         648         0.2477672         6.87           10.03         602.0         12:49:00 AM         649         0.2473367         6.86           10.05         603.0         12:50:00 AM         650         0.2469757         6.85           10.07         604.0         12:51:00 AM         651         0.2466465         6.84           10.10         606.0         12:53:00 AM							ł — — — — — — — — — — — — — — — — — — —	
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9.92       595.0       12:42:00 AM       642       0.249725       6.92         9.93       596.0       12:43:00 AM       643       0.2493508       6.91         9.95       597.0       12:44:00 AM       644       0.2491928       6.91         9.97       598.0       12:45:00 AM       645       0.2488329       6.90         9.98       599.0       12:46:00 AM       646       0.2483446       6.88         10.00       600.0       12:47:00 AM       647       0.2481155       6.88         10.02       601.0       12:48:00 AM       648       0.2477672       6.87         10.03       602.0       12:49:00 AM       649       0.2473367       6.86         10.05       603.0       12:50:00 AM       650       0.2469757       6.85         10.07       604.0       12:51:00 AM       651       0.2466465       6.84         10.08       605.0       12:52:00 AM       652       0.2464564       6.83         10.10       606.0       12:53:00 AM       653       0.2460556       6.82         10.12       607.0       12:54:00 AM       654       0.2457658       6.81         10.13       608.0       12:								
9.93       596.0       12:43:00 AM       643       0.2493508       6.91         9.95       597.0       12:44:00 AM       644       0.2491928       6.91         9.97       598.0       12:45:00 AM       645       0.248329       6.90         9.98       599.0       12:46:00 AM       646       0.2483446       6.88         10.00       600.0       12:47:00 AM       647       0.2481155       6.88         10.02       601.0       12:48:00 AM       648       0.2477672       6.87         10.03       602.0       12:49:00 AM       649       0.2473367       6.86         10.05       603.0       12:50:00 AM       650       0.2469757       6.85         10.07       604.0       12:51:00 AM       651       0.2466465       6.84         10.08       605.0       12:52:00 AM       652       0.2464564       6.83         10.10       606.0       12:53:00 AM       653       0.2460556       6.82         10.12       607.0       12:54:00 AM       654       0.2457658       6.81         10.13       608.0       12:55:00 AM       655       0.2455626       6.81         10.15       609.0       12								
9.95       597.0       12:44:00 AM       644       0.2491928       6.91         9.97       598.0       12:45:00 AM       645       0.2488329       6.90         9.98       599.0       12:46:00 AM       646       0.2483446       6.88         10.00       600.0       12:47:00 AM       647       0.2481155       6.88         10.02       601.0       12:48:00 AM       648       0.2477672       6.87         10.03       602.0       12:49:00 AM       649       0.2473367       6.86         10.05       603.0       12:50:00 AM       650       0.2469757       6.85         10.07       604.0       12:51:00 AM       651       0.2466465       6.84         10.08       605.0       12:52:00 AM       652       0.2464564       6.83         10.10       606.0       12:53:00 AM       653       0.2460556       6.82         10.12       607.0       12:54:00 AM       654       0.2457658       6.81         10.13       608.0       12:55:00 AM       655       0.2457658       6.81         10.15       609.0       12:56:00 AM       656       0.2450209       6.79         10.18       611.0								
9.97         598.0         12:45:00 AM         645         0.2488329         6.90           9.98         599.0         12:46:00 AM         646         0.2483446         6.88           10.00         600.0         12:47:00 AM         647         0.2481155         6.88           10.02         601.0         12:48:00 AM         648         0.2477672         6.87           10.03         602.0         12:49:00 AM         649         0.2473367         6.86           10.05         603.0         12:50:00 AM         650         0.2469757         6.85           10.07         604.0         12:51:00 AM         651         0.2466465         6.84           10.08         605.0         12:52:00 AM         652         0.2464564         6.83           10.10         606.0         12:53:00 AM         653         0.2460556         6.82           10.12         607.0         12:54:00 AM         654         0.2457658         6.81           10.13         608.0         12:55:00 AM         655         0.2455626         6.81           10.15         609.0         12:56:00 AM         656         0.24450209         6.79           10.18         611.0         12:55:00 A								
9.98       599.0       12:46:00 AM       646       0.2483446       6.88         10.00       600.0       12:47:00 AM       647       0.2481155       6.88         10.02       601.0       12:48:00 AM       648       0.2477672       6.87         10.03       602.0       12:49:00 AM       649       0.2473367       6.86         10.05       603.0       12:50:00 AM       650       0.2469757       6.85         10.07       604.0       12:51:00 AM       651       0.2466465       6.84         10.08       605.0       12:52:00 AM       652       0.2464564       6.83         10.10       606.0       12:53:00 AM       653       0.2460556       6.82         10.12       607.0       12:54:00 AM       654       0.2457658       6.81         10.13       608.0       12:55:00 AM       655       0.2455626       6.81         10.15       609.0       12:56:00 AM       656       0.2450209       6.79         10.17       610.0       12:57:00 AM       657       0.244832       6.79         10.18       611.0       12:58:00 AM       658       0.2443352       6.77         10.20       612.0 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>								
10.00       600.0       12:47:00 AM       647       0.2481155       6.88         10.02       601.0       12:48:00 AM       648       0.2477672       6.87         10.03       602.0       12:49:00 AM       649       0.2473367       6.86         10.05       603.0       12:50:00 AM       650       0.2469757       6.85         10.07       604.0       12:51:00 AM       651       0.2466465       6.84         10.08       605.0       12:52:00 AM       652       0.2464564       6.83         10.10       606.0       12:53:00 AM       653       0.2460556       6.82         10.12       607.0       12:54:00 AM       654       0.2457658       6.81         10.13       608.0       12:55:00 AM       655       0.2455626       6.81         10.15       609.0       12:56:00 AM       656       0.2450209       6.79         10.17       610.0       12:57:00 AM       658       0.2443352       6.77         10.20       612.0       12:59:00 AM       659       0.2441674       6.77								
10.02       601.0       12:48:00 AM       648       0.2477672       6.87         10.03       602.0       12:49:00 AM       649       0.2473367       6.86         10.05       603.0       12:50:00 AM       650       0.2469757       6.85         10.07       604.0       12:51:00 AM       651       0.2466465       6.84         10.08       605.0       12:52:00 AM       652       0.2464564       6.83         10.10       606.0       12:53:00 AM       653       0.2460556       6.82         10.12       607.0       12:54:00 AM       654       0.2457658       6.81         10.13       608.0       12:55:00 AM       655       0.2455626       6.81         10.15       609.0       12:56:00 AM       656       0.2450209       6.79         10.17       610.0       12:57:00 AM       657       0.244832       6.79         10.18       611.0       12:58:00 AM       658       0.2443352       6.77         10.20       612.0       12:59:00 AM       659       0.2441674       6.77								
10.03       602.0       12:49:00 AM       649       0.2473367       6.86         10.05       603.0       12:50:00 AM       650       0.2469757       6.85         10.07       604.0       12:51:00 AM       651       0.2466465       6.84         10.08       605.0       12:52:00 AM       652       0.2464564       6.83         10.10       606.0       12:53:00 AM       653       0.2460556       6.82         10.12       607.0       12:54:00 AM       654       0.2457658       6.81         10.13       608.0       12:55:00 AM       655       0.2455626       6.81         10.15       609.0       12:56:00 AM       656       0.2450209       6.79         10.17       610.0       12:57:00 AM       657       0.244832       6.79         10.18       611.0       12:58:00 AM       658       0.2443352       6.77         10.20       612.0       12:59:00 AM       659       0.2441674       6.77								
10.05       603.0       12:50:00 AM       650       0.2469757       6.85         10.07       604.0       12:51:00 AM       651       0.2466465       6.84         10.08       605.0       12:52:00 AM       652       0.2464564       6.83         10.10       606.0       12:53:00 AM       653       0.2460556       6.82         10.12       607.0       12:54:00 AM       654       0.2457658       6.81         10.13       608.0       12:55:00 AM       655       0.2455626       6.81         10.15       609.0       12:56:00 AM       656       0.2450209       6.79         10.17       610.0       12:57:00 AM       657       0.244832       6.79         10.18       611.0       12:58:00 AM       658       0.2443352       6.77         10.20       612.0       12:59:00 AM       659       0.2441674       6.77					0.2477672			
10.07       604.0       12:51:00 AM       651       0.2466465       6.84         10.08       605.0       12:52:00 AM       652       0.2464564       6.83         10.10       606.0       12:53:00 AM       653       0.2460556       6.82         10.12       607.0       12:54:00 AM       654       0.2457658       6.81         10.13       608.0       12:55:00 AM       655       0.2455626       6.81         10.15       609.0       12:56:00 AM       656       0.2450209       6.79         10.17       610.0       12:57:00 AM       657       0.244832       6.79         10.18       611.0       12:58:00 AM       658       0.2443352       6.77         10.20       612.0       12:59:00 AM       659       0.2441674       6.77								
10.08       605.0       12:52:00 AM       652       0.2464564       6.83         10.10       606.0       12:53:00 AM       653       0.2460556       6.82         10.12       607.0       12:54:00 AM       654       0.2457658       6.81         10.13       608.0       12:55:00 AM       655       0.2455626       6.81         10.15       609.0       12:56:00 AM       656       0.2450209       6.79         10.17       610.0       12:57:00 AM       657       0.244832       6.79         10.18       611.0       12:58:00 AM       658       0.2443352       6.77         10.20       612.0       12:59:00 AM       659       0.2441674       6.77								
10.10     606.0     12:53:00 AM     653     0.2460556     6.82       10.12     607.0     12:54:00 AM     654     0.2457658     6.81       10.13     608.0     12:55:00 AM     655     0.2455626     6.81       10.15     609.0     12:56:00 AM     656     0.2450209     6.79       10.17     610.0     12:57:00 AM     657     0.244832     6.79       10.18     611.0     12:58:00 AM     658     0.2443352     6.77       10.20     612.0     12:59:00 AM     659     0.2441674     6.77								
10.12     607.0     12:54:00 AM     654     0.2457658     6.81       10.13     608.0     12:55:00 AM     655     0.2455626     6.81       10.15     609.0     12:56:00 AM     656     0.2450209     6.79       10.17     610.0     12:57:00 AM     657     0.244832     6.79       10.18     611.0     12:58:00 AM     658     0.2443352     6.77       10.20     612.0     12:59:00 AM     659     0.2441674     6.77								
10.13     608.0     12:55:00 AM     655     0.2455626     6.81       10.15     609.0     12:56:00 AM     656     0.2450209     6.79       10.17     610.0     12:57:00 AM     657     0.244832     6.79       10.18     611.0     12:58:00 AM     658     0.2443352     6.77       10.20     612.0     12:59:00 AM     659     0.2441674     6.77		606.0	12:53:00 AM		0.2460556			
10.15     609.0     12:56:00 AM     656     0.2450209     6.79       10.17     610.0     12:57:00 AM     657     0.244832     6.79       10.18     611.0     12:58:00 AM     658     0.2443352     6.77       10.20     612.0     12:59:00 AM     659     0.2441674     6.77	10.12	607.0		654	0.2457658	6.81		
10.17     610.0     12:57:00 AM     657     0.244832     6.79       10.18     611.0     12:58:00 AM     658     0.2443352     6.77       10.20     612.0     12:59:00 AM     659     0.2441674     6.77	10.13	608.0	12:55:00 AM	655	0.2455626	6.81		
10.18     611.0     12:58:00 AM     658     0.2443352     6.77       10.20     612.0     12:59:00 AM     659     0.2441674     6.77		609.0	12:56:00 AM	656	0.2450209	6.79		
10.20 612.0 12:59:00 AM 659 0.2441674 6.77	10.17	610.0	12:57:00 AM	657	0.244832	6.79		
	10.18	611.0	12:58:00 AM	658	0.2443352	6.77		
10.22 613.0 1:00:00 AM 660 0.2438309 6.76	10.20	612.0	12:59:00 AM	659	0.2441674	6.77		
	10.22	613.0	1:00:00 AM	660	0.2438309	6.76		

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10.23	614.0	1:01:00 AM	661	0.2433557	6.75		
10.25	615.0	1:02:00 AM	662	0.2432244	6.74		
10.27	616.0	1:03:00 AM	663	0.2428895	6.73		!
10.28	617.0	1:04:00 AM	664	0.2424634	6.72		
10.30	618.0	1:05:00 AM	665	0.242226	6.71		
10.32	619.0	1:06:00 AM	666	0.24213	6.71		
10.33	620.0	1:07:00 AM	667	0.2415085	6.69		-
10.35	621.0	1:08:00 AM	668	0.2413204	6.69		
10.37	622.0	1:09:00 AM	669	0.2411366	6.68		
10.37	623.0	1:10:00 AM	670	0.2406868	6.67		
10.40	624.0	1:11:00 AM	671	0.2403203	6.66		
10.42	625.0	1:12:00 AM	672	0.2399281	6.65		
10.43	626.0	1:13:00 AM	673	0.2394554	6.64		
10.45	627.0	1:14:00 AM	674	0.2394218	6.64		
10.47	628.0	1:15:00 AM	675	0.2391005	6.63		
10.48	629.0	1:16:00 AM	676	0.2386801	6.62		
10.50	630.0	1:17:00 AM	677	0.2385307	6.61		
10.52	631.0	1:18:00 AM	678	0.238242	6.60		
10.53	632.0	1:19:00 AM	679	0.2378317	6.59		
10.55	633.0	1:20:00 AM	680	0.23752	6.58		
10.57	634.0	1:21:00 AM	681	0.2372568	6.58		
10.58	635.0	1:22:00 AM	682	0.2367324	6.56		
10.60	636.0	1:23:00 AM	683	0.2365582	6.56		
10.62	637.0	1:24:00 AM	684	0.2361709	6.55		
10.63	638.0	1:25:00 AM	685	0.2359665	6.54		
		1:26:00 AM					
10.65	639.0		686	0.2357119	6.53		
10.67	640.0	1:27:00 AM	687	0.2353159	6.52		
10.68	641.0	1:28:00 AM	688	0.2349618	6.51		
10.70	642.0	1:29:00 AM	689	0.2347174	6.51		
10.72	643.0	1:30:00 AM	690	0.2342418	6.49		
10.73	644.0	1:31:00 AM	691	0.2341276	6.49		
10.75	645.0	1:32:00 AM	692	0.233656	6.48		
10.77	646.0	1:33:00 AM	693	0.2334084	6.47		
10.78	647.0	1:34:00 AM	694	0.2330576	6.46		
10.80	648.0	1:35:00 AM	695	0.2327521	6.45		
10.82	649.0	1:36:00 AM	696	0.2322982	6.44		
10.83	650.0	1:37:00 AM	697	0.2321964	6.44		
10.85	651.0	1:38:00 AM	698	0.2315463	6.42		
10.87	652.0	1:39:00 AM	699	0.2312906	6.41		
10.88	653.0	1:40:00 AM	700	0.2311036			
10.88	654.0	1:41:00 AM	700		6.40		
				0.2308283			
10.92	655.0	1:42:00 AM	702	0.2303913	6.39		
10.93	656.0	1:43:00 AM	703		6.38		
10.95	657.0	1:44:00 AM	704	0.2296918	6.37		
10.97	658.0	1:45:00 AM	705	0.2291716			
10.98	659.0	1:46:00 AM	706	0.2291427	6.35		
11.00	660.0	1:47:00 AM	707	0.2287972	6.34		
11.02	661.0	1:48:00 AM	708	0.2283093	6.33		
11.03	662.0	1:49:00 AM	709	0.2281099	6.32		
11.05	663.0	1:50:00 AM	710	0.2277659	6.31		
11.07	664.0	1:51:00 AM	711	0.2275424	6.31		
11.08	665.0	1:52:00 AM	712	0.2271643	6.30		
11.10	666.0	1:53:00 AM	713	0.226747	6.29		
11.12	667.0	1:54:00 AM	714		6.28		
11.13	668.0	1:55:00 AM	715		6.27		
11.15	669.0	1:56:00 AM	715	0.2257873	6.26		
11.15	670.0	1:57:00 AM	716	0.2257873	6.25		
11.18	671.0	1:58:00 AM	718		6.25		
11.20		1:59:00 AM	719		6.24		
11.22	673.0	2:00:00 AM	720	0.2245898	6.23		
11.23	674.0	2:01:00 AM	721	0.2243778	6.22		
11.25	675.0	2:02:00 AM	722	0.2239155	6.21		
11.27	676.0	2:03:00 AM	723	0.2238094	6.20		
11.28	677.0	2:04:00 AM	724	0.2233901	6.19		
11.30	678.0	2:05:00 AM	725	0.2231255	6.19		
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11.32	679.0	2:06:00 AM	726				
11.33	680.0	2:07:00 AM	727	0.2224415	6.17		
11.35	681.0	2:08:00 AM	728	0.2218914	6.15		
11.37	682.0	2:09:00 AM	729	0.2218229	6.15		
11.38	683.0	2:10:00 AM	730	0.2212987	6.13		
11.40	684.0	2:11:00 AM	731	0.2211595	6.13		
11.42	685.0	2:12:00 AM	732	0.220771	6.12		
11.43	686.0	2:13:00 AM	733	0.2205335	6.11		
11.45	687.0	2:14:00 AM	734	0.2202411	6.11		
11.47	688.0	2:15:00 AM	735	0.2199863	6.10		
11.48	689.0	2:16:00 AM	736	0.2196768	6.09		
11.50	690.0	2:17:00 AM	737	0.2192997	6.08		
11.52	691.0	2:18:00 AM	738	0.2191253	6.07		
11.53	692.0	2:19:00 AM	739	0.21875	6.06		
11.55	693.0	2:20:00 AM	740	0.2184979	6.06		<del> </del>
11.57	694.0	2:21:00 AM	741	0.2181474	6.05		
11.58	695.0	2:22:00 AM	742	0.2177172	6.04		
11.60	696.0	2:23:00 AM	743	0.2175665	6.03		
11.62	697.0	2:24:00 AM	744	0.217322	6.02		
11.63	698.0	2:25:00 AM	745	0.2168784	6.01		
11.65	699.0	2:26:00 AM	746	0.2165503	6.00		
11.67	700.0	2:27:00 AM	747	0.2163334	6.00		
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11.68	701.0	2:28:00 AM	748	0.2160437	5.99		<u> </u>
11.70	702.0	2:29:00 AM	749	0.2155117	5.97		
11.72	703.0	2:30:00 AM	750	0.2153101	5.97		
11.73	704.0	2:31:00 AM	751	0.2151149	5.96		
11.75	705.0	2:32:00 AM	752	0.2147408	5.95		
11.77	706.0	2:33:00 AM	753	0.2144705	5.95		
11.78	707.0	2:34:00 AM	754	0.2140915	5.93		
11.80	707.0	2:35:00 AM	755	0.213584	5.92		
11.82	709.0	2:36:00 AM	756	0.213325	5.91		
11.83	710.0	2:37:00 AM	757	0.2131992	5.91		
11.85	711.0	2:38:00 AM	758	0.2129974	5.90		
11.87	712.0	2:39:00 AM	759	0.2126255	5.89		
11.88	713.0	2:40:00 AM	760	0.2123617	5.89		
11.90	714.0	2:41:00 AM	761	0.2120121	5.88		
11.92	715.0	2:42:00 AM	762	0.2116331	5.87		
11.93	716.0	2:43:00 AM	763	0.211447	5.86		
11.95	717.0	2:44:00 AM	764	0.2110848	5.85		
11.97	718.0	2:45:00 AM	765	0.2107854	5.84		
11.98	719.0	2:46:00 AM	766	0.2104446	5.83		
12.00	720.0	2:47:00 AM	767	0.2101597	5.83		
12.02	721.0	2:48:00 AM	768	0.2097838	5.82		
12.03	722.0	2:49:00 AM	769	0.2094871	5.81		
12.05	723.0	2:50:00 AM	770	0.2093	5.80		
12.07	724.0	2:51:00 AM	771	0.2088682	5.79		+
12.07	724.0		771		5.78		<del></del>
		2:52:00 AM		0.2084447			<del></del>
12.10	726.0	2:53:00 AM	773	0.2083865	5.78		
12.12	727.0	2:54:00 AM	774	0.2079379	5.76		
12.13	728.0	2:55:00 AM	775	0.2078394			
12.15	729.0	2:56:00 AM	776	0.2073376	5.75		
12.17	730.0	2:57:00 AM	777	0.2073809	5.75		
12.18	731.0	2:58:00 AM	778	0.2067196			
12.10	731.0	2:59:00 AM	778		5.72		
							<del></del>
12.22	733.0	3:00:00 AM	780	0.2061854	5.72		
12.23	734.0	3:01:00 AM	781	0.2059976			
12.25	735.0	3:02:00 AM	782	0.205719	5.70		
12.27	736.0	3:03:00 AM	783	0.2053176	5.69		
12.28	737.0	3:04:00 AM	784	0.2051308	5.69		
12.30	738.0	3:05:00 AM	785	0.2049534	5.68		
12.32	739.0	3:06:00 AM	786	0.2045095	5.67	-	
12.32	740.0	3:07:00 AM	787	0.2042739			<del></del>
							<del></del>
12.35	741.0	3:08:00 AM	788	0.2038753	5.65		
12.37	742.0	3:09:00 AM	789	0.2034201	5.64		
12.38	743.0	3:10:00 AM	790	0.2031928	5.63		

						Г	
12.40	744.0	3:11:00 AM	791	0.2029659	5.63		
12.42	745.0	3:12:00 AM	792	0.2024055	5.61		
12.43	746.0	3:13:00 AM	793	0.2023484	5.61		
12.45	747.0	3:14:00 AM	794	0.2017809	5.59		
12.47	748.0	3:15:00 AM	795	0.201733	5.59		
12.48	749.0	3:16:00 AM	796	0.2011694	5.58		
12.50	750.0	3:17:00 AM	797	0.2008379	5.57		
12.52	751.0	3:18:00 AM	798	0.2005912	5.56		
12.53	752.0	3:19:00 AM	799	0.2002134	5.55		
12.55	753.0	3:20:00 AM	800	0.199972	5.54		
12.57	754.0	3:21:00 AM	801	0.1996798	5.54		
12.58	754.0	3:22:00 AM	802	0.1993177	5.53		
12.60	756.0	3:23:00 AM	803	0.1990687	5.52		
12.62	757.0	3:24:00 AM	804	0.1987474	5.51		
12.63	758.0	3:25:00 AM	805	0.198751	5.51		
12.65	759.0	3:26:00 AM	806	0.1981454	5.49		
12.67	760.0	3:27:00 AM	807	0.1978096	5.48		
12.68	761.0	3:28:00 AM	808	0.1976218	5.48		
12.70	762.0	3:29:00 AM	809	0.1972546	5.47		
12.72	763.0	3:30:00 AM	810	0.1969735	5.46		
12.73	764.0	3:31:00 AM	811	0.1965597	5.45		
12.75	765.0	3:32:00 AM	812	0.1963765	5.44		
12.77	766.0	3:33:00 AM	813	0.1960853	5.44		
12.78	767.0	3:34:00 AM	814	0.1957227	5.43		
12.80	768.0	3:35:00 AM	815	0.195296	5.41		
12.82	769.0	3:36:00 AM	816	0.1952702	5.41		
12.83	770.0	3:37:00 AM	817	0.1946333	5.40		
12.85	771.0	3:38:00 AM	818	0.1944285	5.39		
12.87	771.0	3:39:00 AM	819	0.1939748	5.38		<del>     </del>
12.88	772.0		820		5.37		
		3:40:00 AM		0.1937036			
12.90	774.0	3:41:00 AM	821	0.193235	5.36		
12.92	775.0	3:42:00 AM	822	0.193021	5.35		
12.93	776.0	3:43:00 AM	823	0.192614	5.34		
12.95	777.0	3:44:00 AM	824	0.1923282	5.33		
12.97	778.0	3:45:00 AM	825	0.1920118	5.32		
12.98	779.0	3:46:00 AM	826	0.1916044	5.31		
13.00	780.0	3:47:00 AM	827	0.1913645	5.30		
13.02	781.0	3:48:00 AM	828	0.1909942	5.29		
13.03	782.0	3:49:00 AM	829	0.1904634	5.28		
13.05	783.0	3:50:00 AM	830	0.1902112	5.27		
13.07	784.0	3:51:00 AM	831	0.1899803	5.27		
13.08	785.0	3:52:00 AM	832	0.1896005	5.26		
13.10	786.0	3:53:00 AM	833	0.1890518	5.24		
13.12	787.0	3:54:00 AM	834	0.1890419	5.24		
13.13	788.0	3:55:00 AM	835	0.1885242	5.23		
13.15	789.0	3:56:00 AM	836	0.1882483	5.23		<del>-  </del>
13.17	790.0	3:57:00 AM	837	0.1880348	5.21		
13.17	790.0	+	838		5.21		
	791.0 792.0	3:58:00 AM		0.1876725			
13.20		3:59:00 AM	839	0.1872986	5.19		
13.22	793.0	4:00:00 AM	840	0.1871082	5.19		
13.23	794.0	4:01:00 AM	841	0.1867086	5.18		
13.25	795.0	4:02:00 AM	842	0.1863241	5.16		
13.27	796.0	4:03:00 AM	843	0.1861088	5.16		
13.28	797.0	4:04:00 AM	844	0.1857601	5.15		
13.30	798.0	4:05:00 AM	845	0.185582	5.14		
13.32	799.0	4:06:00 AM	846	0.1851991	5.13		
13.33	800.0	4:07:00 AM	847	0.1848724	5.12		
13.35	801.0	4:08:00 AM	848	0.1845708	5.12		
13.37	802.0	4:09:00 AM	849	0.184144	5.10		
13.38	803.0	4:10:00 AM	850	0.1839373	5.10		
13.40	804.0	4:11:00 AM	851	0.1837896	5.09		
13.42	805.0	4:12:00 AM	852	0.1836488	5.09		
13.42	806.0	4:13:00 AM	853	0.1832347	5.08		
13.45	807.0	4:14:00 AM	853	0.1832347	5.07		
13.45	808.0						<del></del>
13.4/	808.0	4:15:00 AM	855	0.1823733	5.06		

13.48	809.0	4:16:00 AM	856	0.1821455	5.05		
13.50	810.0	4:17:00 AM	857	0.1818089	5.04		
13.52	811.0	4:18:00 AM	858	0.1812184	5.02		
13.53	812.0	4:19:00 AM	859	0.180979	5.02		
13.55	813.0	4:20:00 AM	860	0.1807313	5.01		
13.57	814.0	4:21:00 AM	861	0.1804284	5.00		
13.58	815.0	4:22:00 AM	862	0.1803585	5.00		
13.60	816.0	4:23:00 AM	863	0.1799616	4.99		
13.62	817.0	4:24:00 AM	864	0.179759	4.98		
13.63	818.0	4:25:00 AM	865	0.179339	4.97		
13.65	819.0	4:26:00 AM	866	0.1789101	4.96		
13.67	820.0	4:27:00 AM	867	0.1786771	4.95		
			<u>Average</u>	<b>Infiltration Rate:</b>	0.85		
		`					
		`		Factor of Safety:	0.45		
		`					
					Infiltration Rate of	f 0.38 in/hr Used for Si	zing of System

## **APPENDIX B**







Stainless-Steel Vented Stand-Alone Pressure Transducer



# Pressure Transducer Combined with a Recorder

High resolution and accuracy

#### Overview

The CRS451V consists of a submersible water-level and water-temperature sensor with its own time clock and memory to store the collected data—in a compact stainless-steel case. This data logging capability frees users to place the sensor in remote sites and let it collect data for long periods. HydroSci software is included and elegantly supports test setup, data

retrieval, and data display. Long battery life and rugged construction mean you can trust the CRS451V to collect important data. Low cost and ease of use make it a good choice in a variety of applications. The CRS456V is the same as this, but with a titanium case.

### **Benefits and Features**

- Sensors and data-collection features in one instrument case
- Rugged stainless-steel case protects piezoresistive sensor
- Quality construction ensures product reliability
- > Fully temperature-compensated

- Fast scan rate
- Large data-storage capacity
- ) Long battery life
- Easy-to-use software

### **Detailed Description**

The CRS451V has several pressure range options.

HydroSci software is available for download. This software simplifies the process of configuring the CRS451V. Users can

configure the CRS451V to monitor surface water, ground water, or a standard pump test.

HydroSci software will display the data in tabular or graphical formats.

### **Specifications**

Venting Vented

Measurement Time

< 1.0 s



## **APPENDIX C**

### **INFILTRATION TEST**

The Washington State Department of Ecology Stormwater Manual provides testing procedures and best practices, which are described below.

- Testing should occur between December 1 and April 1.
- The horizontal and vertical locations of the PIT shall be surveyed by a licensed land surveyor and accurately shown on the design drawings.
- Excavate the test pit to the estimated elevation of the proposed infiltration into the native soil. Note that for some proposed BMPs, such as and <u>BMP T5.15: Per-meable Pavements</u>, this will be below the proposed finished grade. If the native soils will have to meet a minimum subgrade compaction requirement (for example, the road subgrade if using <u>BMP T5.15: Permeable Pavements</u>), compact the native soil to that requirement prior to testing. Lay back the slopes sufficiently to avoid caving and erosion during the test. Altern- atively, consider shoring the sides of the test pit.
- The horizontal surface area of the bottom of the test pit should be approximately 100 square feet. Document the size and geometry of the test pit.
- Install a vertical measuring rod (long enough to measure the ponded water depth, minimum 5- ft. long) marked in half-inch increments in the center of the pit bottom.
- Use a rigid 6-inch diameter pipe with a splash plate on the bottom to convey water to the test pit and reduce side-wall erosion or excessive disturbance of the test pit bottom. Excessive erosion and bottom disturbance will result in clogging of the infiltration receptor and yield lower than actual infiltration rates.
- Add water to the pit at a rate that will maintain a water level between 6 and 12 inches above the bottom of the pit. A rotameter can be used to measure the flow rate into the pit.

The depth should not exceed the proposed maximum depth of water expected in the completed BMP. For infiltration BMPs serving large drainage areas, designs with multiple feet of standing water can have infiltration tests with greater than 1 foot of standing water.

- Every 15-30 min, record the cumulative volume and instantaneous flow rate in gallons per minute necessary to maintain the water level at the same point on the measuring rod.
- Keep adding water to the pit until one hour after the flow rate into the pit has stabilized (constant flow rate; a goal of 5% or less variation in the total flow) while maintaining the same pond water level. The total of the pre-soak time plus one hour after the flow rate has stabilized should be no less than 6 hours.
- After the flow rate has stabilized for at least one hour, turn off the water and record the rate of infiltration (the drop rate of the standing water) in inches per hour from the measuring rod data, until the pit is empty. Consider running this falling head phase of the test several times to estimate the



dependency of the infiltration rate with head.

At the conclusion of testing, over-excavate the pit to see if the test water is mounded on shallow
restrictive layers or if it has continued to flow deep into the subsurface. The depth of excavation varies
depending on soil type and depth to the hydraulic restricting layer, and is determined by the
engineer or certified soils professional. Mounding is an indication that a mounding analysis is
necessary.

### DATA ANALYSIS

Calculate and record the initial K<sub>sat</sub> rate in inches per hour in 30 minutes or one-hour increments until one hour after the flow has stabilized.

Use statistical/trend analysis to obtain the hourly flow rate when the flow stabilizes. This would be the lowest hourly flow rate. *Example:* 

The area of the bottom of the test pit is 8.5-ft. by 11.5-ft. (97.75 sq. ft.).

Water flow rate was measured and recorded at intervals ranging from 15 to 30 minutes throughout the test. Between 400 minutes and 1,000 minutes the flow rate stabilized between 10 and 12.5 gal- lons per minute or 600 to 750 gallons per hour, or 80.2 to  $100\,\mathrm{ft}^3$  per hour. Dividing this rate by the surface area gives an initial  $K_{sat}$  of 9.8 to 12.3 inches per hour.

## K<sub>sat</sub> Determination Option 2: Small Scale Pilot Infiltration Test (PIT)

A small-scale PIT can be substituted for <u>Ksat Determination Option 1: Large Scale Pilot Infiltration</u> <u>Test (PIT)</u> in any of the following instances:

- The drainage area to the infiltration BMP is less than 1 acre.
- The testing is for <u>BMP T7.30: Bioretention</u> or <u>BMP T5.15: Permeable Pavements</u> that either serve small drainage areas and/or are widely dispersed throughout a project site.
- The site has a high infiltration rate (>4 in/hr), making a large scale PIT difficult, and the site geo-technical investigation suggests uniform subsurface characteristics.

### INFILTRATION TEST

Use the same procedures described above in <u>Ksat Determination Option 1: Large Scale Pilot Infiltra-tion Test</u> (PIT), with the following changes:

- The horizontal surface area of the bottom of the test pit should be 12 to 32 square feet. It may be circular or rectangular. Document the size and geometry of the test pit.
- The rigid pipe with a splash plate used to convey water to the pit may be a 3-inch diameter pipe for



pits on the smaller end of the recommended surface area, or a 4-inch pipe for pits on the larger end of the recommended surface area.

- Pre-soak period: Add water to the pit so that there is standing water for at least 6 hours. Maintain the pre-soak water level at least 12 inches above the bottom of the pit.
- At the end of the pre-soak period, add water to the pit at a rate that will maintain a 6-12 inch water level above the bottom of the pit over a full hour. The depth should not exceed the pro- posed maximum depth of water expected in the completed facility.
- Every 15 minutes, record the cumulative volume and instantaneous flow rate in gallons per minute necessary to maintain the water level at the same point (between 6 inches and 1 foot) on the measuring rod. The specific depth should be the same as the maximum designed pond-ing depth (usually 6 12 inches).

After one hour, turn off the water and record the rate of infiltration (the drop rate of the standing water) in inches per hour from the measuring rod data, until the pit is empty.

- A self-logging pressure sensor may also be used to determine water depth and drain-down.
- At the conclusion of testing, over-excavate the pit to see if the test water is mounded on shallow
  restrictive layers or if it has continued to flow deep into the subsurface. The depth of excavation varies
  depending on soil type and depth to the hydraulic restricting layer, and is determined by the
  engineer or certified soils professional. The soils professional should judge whether a mounding
  analysis is necessary.



## **APPENDIX D**

### **CALCULATED DESIGN INFILTRATION RATE:**

Site variability and number of locations tested ( $CF_V$ ) - The number of locations tested must be capable of producing a picture of the subsurface conditions that fully rep- resents the conditions throughout the proposed location of the infiltration BMP. The partial correction factor used for this issue depends on the level of uncertainty that adverse subsurface conditions may occur. If the range of uncertainty is low - for example, conditions are known to be uniform through previous exploration and site geological factors

- one pilot infiltration test (or grain size analysis location) may be adequate to justify a partial correction factor at the high end of the range.

If the level of uncertainty is high, a partial correction factor near the low end of the range may be appropriate. This might be the case where the site conditions are highly variable due to conditions such as a deposit of ancient landslide debris, or buried stream channels. In these cases, even with many explorations and several pilot infiltration tests (or several grain size test locations), the level of uncertainty may still be high.

A partial correction factor near the low end of the range could be assigned where conditions have a more typical variability, but few explorations and only one pilot infiltration test (or one grain size analysis location) is conducted. That is, the number of explorations and tests conducted do not match the degree of site variability anticipated.

- Uncertainty of test method (CF<sub>t</sub>) accounts for uncertainties in the testing methods. For the full scale PIT method, CF<sub>t</sub> = 0.75; for the small-scale PIT method, CF<sub>t</sub> = 0.50; for smaller-scale infiltration tests such as the double-ring infiltrometer test, CF<sub>t</sub> = 0.40; for grain size analysis, CF<sub>t</sub> = 0.40. These values are intended to represent the difference in each test's ability to estimate the actual saturated hydraulic conductivity. The assumption is the larger the scale of the test, the more reliable the result.
- Degree of influent control to prevent siltation and bio-buildup (CF<sub>m</sub>) Even with a pre-settling basin or a
  basic treatment BMP for pre-treatment, the soil's initial infiltration rate will gradually decline as more and
  more stormwater, with some amount of suspended material, passes through the soil profile. The
  maintenance schedule calls for removing sediment when the BMP is infiltrating at only 90% of its design
  capacity. Therefore, a correction factor, CF<sub>m</sub>, of 0.9 is called for.



Table V-5.1: Correction Factors to be Used With In-Situ Saturated Hydraulic Conductivity Measurements to Estimate Design Rates

Issue	Partial Correction Factor					
Site variability and number of locations tested	CF <sub>V</sub> = 0.33 to <mark>1.0</mark>					
Test Method						
Large-scale PIT	<sup>2</sup> CF <sub>t</sub> = 0.75					
Small-scale PIT	<b>= 0.50</b>					
<ul> <li>Other small-scale (e.g. Double ring, falling head)</li> </ul>	<b>2</b> = 0.40					
Grain Size Method	□ = 0.40					
Degree of influent control to prevent siltation and bio-buildup	CF <sub>m</sub> = 0.9					

Total Correction Factor,  $CF_T = CF_V \times CF_t \times CF_m$ 

Total Correction Factor,  $CF_T = 1.0 \times 0.5 \times 0.9$ 

**CF<sub>T</sub> = 0.45** 



# **APPENDIX B**







CRS451V

Stainless-Steel Vented Stand-Alone Pressure Transducer



# Pressure Transducer Combined with a Recorder

High resolution and accuracy

#### Overview

The CRS451V consists of a submersible water-level and water-temperature sensor with its own time clock and memory to store the collected data—in a compact stainless-steel case. This data logging capability frees users to place the sensor in remote sites and let it collect data for long periods. HydroSci software is included and elegantly supports test setup, data

retrieval, and data display. Long battery life and rugged construction mean you can trust the CRS451V to collect important data. Low cost and ease of use make it a good choice in a variety of applications. The CRS456V is the same as this, but with a titanium case.

### **Benefits and Features**

- > Sensors and data-collection features in one instrument case
- Rugged stainless-steel case protects piezoresistive sensor
- Quality construction ensures product reliability
- > Fully temperature-compensated

- Fast scan rate
- Large data-storage capacity
- ) Long battery life
- > Easy-to-use software

### **Detailed Description**

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configure the CRS451V to monitor surface water, ground water, or a standard pump test.

HydroSci software will display the data in tabular or graphical formats.

< 1.0 s

### **Specifications**

Venting Vented

Measurement Time



## **APPENDIX C**

### **INFILTRATION TEST**

The Washington State Department of Ecology Stormwater Manual provides testing procedures and best practices, which are described below.

- Testing should occur between December 1 and April 1.
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- Excavate the test pit to the estimated elevation of the proposed infiltration into the native soil. Note that for some proposed BMPs, such as and <u>BMP T5.15: Per-meable Pavements</u>, this will be below the proposed finished grade. If the native soils will have to meet a minimum subgrade compaction requirement (for example, the road subgrade if using <u>BMP T5.15: Permeable Pavements</u>), compact the native soil to that requirement prior to testing. Lay back the slopes sufficiently to avoid caving and erosion during the test. Altern- atively, consider shoring the sides of the test pit.
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- Add water to the pit at a rate that will maintain a water level between 6 and 12 inches above the bottom of the pit. A rotameter can be used to measure the flow rate into the pit.

The depth should not exceed the proposed maximum depth of water expected in the completed BMP. For infiltration BMPs serving large drainage areas, designs with multiple feet of standing water can have infiltration tests with greater than 1 foot of standing water.

- Every 15-30 min, record the cumulative volume and instantaneous flow rate in gallons per minute necessary to maintain the water level at the same point on the measuring rod.
- Keep adding water to the pit until one hour after the flow rate into the pit has stabilized (constant flow rate; a goal of 5% or less variation in the total flow) while maintaining the same pond water level. The total of the pre-soak time plus one hour after the flow rate has stabilized should be no less than 6 hours.
- After the flow rate has stabilized for at least one hour, turn off the water and record the rate of infiltration (the drop rate of the standing water) in inches per hour from the measuring rod data, until the pit is empty. Consider running this falling head phase of the test several times to estimate the



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At the conclusion of testing, over-excavate the pit to see if the test water is mounded on shallow
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depending on soil type and depth to the hydraulic restricting layer, and is determined by the
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### DATA ANALYSIS

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A small-scale PIT can be substituted for <u>Ksat Determination Option 1: Large Scale Pilot Infiltration</u> <u>Test (PIT)</u> in any of the following instances:

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- The testing is for <u>BMP T7.30: Bioretention</u> or <u>BMP T5.15: Permeable Pavements</u> that either serve small drainage areas and/or are widely dispersed throughout a project site.
- The site has a high infiltration rate (>4 in/hr), making a large scale PIT difficult, and the site geo-technical investigation suggests uniform subsurface characteristics.

### INFILTRATION TEST

Use the same procedures described above in <u>Ksat Determination Option 1: Large Scale Pilot Infiltra-tion Test</u> (PIT), with the following changes:

- The horizontal surface area of the bottom of the test pit should be 12 to 32 square feet. It may be circular or rectangular. Document the size and geometry of the test pit.
- The rigid pipe with a splash plate used to convey water to the pit may be a 3-inch diameter pipe for



pits on the smaller end of the recommended surface area, or a 4-inch pipe for pits on the larger end of the recommended surface area.

- Pre-soak period: Add water to the pit so that there is standing water for at least 6 hours. Maintain the pre-soak water level at least 12 inches above the bottom of the pit.
- At the end of the pre-soak period, add water to the pit at a rate that will maintain a 6-12 inch water level above the bottom of the pit over a full hour. The depth should not exceed the pro- posed maximum depth of water expected in the completed facility.
- Every 15 minutes, record the cumulative volume and instantaneous flow rate in gallons per minute necessary to maintain the water level at the same point (between 6 inches and 1 foot) on the measuring rod. The specific depth should be the same as the maximum designed pond-ing depth (usually 6 12 inches).

After one hour, turn off the water and record the rate of infiltration (the drop rate of the standing water) in inches per hour from the measuring rod data, until the pit is empty.

- A self-logging pressure sensor may also be used to determine water depth and drain-down.
- At the conclusion of testing, over-excavate the pit to see if the test water is mounded on shallow
  restrictive layers or if it has continued to flow deep into the subsurface. The depth of excavation varies
  depending on soil type and depth to the hydraulic restricting layer, and is determined by the
  engineer or certified soils professional. The soils professional should judge whether a mounding
  analysis is necessary.



## **APPENDIX D**

### **CALCULATED DESIGN INFILTRATION RATE:**

Site variability and number of locations tested ( $CF_V$ ) - The number of locations tested must be capable of producing a picture of the subsurface conditions that fully rep- resents the conditions throughout the proposed location of the infiltration BMP. The partial correction factor used for this issue depends on the level of uncertainty that adverse subsurface conditions may occur. If the range of uncertainty is low - for example, conditions are known to be uniform through previous exploration and site geological factors

- one pilot infiltration test (or grain size analysis location) may be adequate to justify a partial correction factor at the high end of the range.

If the level of uncertainty is high, a partial correction factor near the low end of the range may be appropriate. This might be the case where the site conditions are highly variable due to conditions such as a deposit of ancient landslide debris, or buried stream channels. In these cases, even with many explorations and several pilot infiltration tests (or several grain size test locations), the level of uncertainty may still be high.

A partial correction factor near the low end of the range could be assigned where conditions have a more typical variability, but few explorations and only one pilot infiltration test (or one grain size analysis location) is conducted. That is, the number of explorations and tests conducted do not match the degree of site variability anticipated.

- Uncertainty of test method (CF<sub>t</sub>) accounts for uncertainties in the testing methods. For the full scale PIT method, CF<sub>t</sub> = 0.75; for the small-scale PIT method, CF<sub>t</sub> = 0.50; for smaller-scale infiltration tests such as the double-ring infiltrometer test, CF<sub>t</sub> = 0.40; for grain size analysis, CF<sub>t</sub> = 0.40. These values are intended to represent the difference in each test's ability to estimate the actual saturated hydraulic conductivity. The assumption is the larger the scale of the test, the more reliable the result.
- Degree of influent control to prevent siltation and bio-buildup (CF<sub>m</sub>) Even with a pre-settling basin or a
  basic treatment BMP for pre-treatment, the soil's initial infiltration rate will gradually decline as more and
  more stormwater, with some amount of suspended material, passes through the soil profile. The
  maintenance schedule calls for removing sediment when the BMP is infiltrating at only 90% of its design
  capacity. Therefore, a correction factor, CF<sub>m</sub>, of 0.9 is called for.



Table V-5.1: Correction Factors to be Used With In-Situ Saturated Hydraulic Conductivity Measurements to Estimate Design Rates

Issue	Partial Correction Factor			
Site variability and number of locations tested	CF <sub>V</sub> = 0.33 to 1.0			
Test Method				
Large-scale PIT	© CF <sub>t</sub> = 0.75			
Small-scale PIT	<b>□</b> = 0.50			
<ul> <li>Other small-scale (e.g. Double ring, falling head)</li> </ul>	<b>2</b> = 0.40			
Grain Size Method	₃ = 0.40			
Degree of influent control to prevent siltation and bio-buildup	CF <sub>m</sub> = 0.9			

Total Correction Factor,  $CF_T = CF_V \times CF_t \times CF_m$ 

Total Correction Factor,  $CF_T = 1.0 \times 0.5 \times 0.9$ 

**CF<sub>T</sub> = 0.45** 



# **APPENDIX E**



April 6, 2023

Advanced Underground Utilities PO Box 309 Sumner, Washington 98390

Attn: E.J. Fernandez

(253) 988-2449 ej@auuinc.com

> Soils Report Addendum: Groundwater Monitoring Proposed Contractor's Yard 320 Todd Road NE

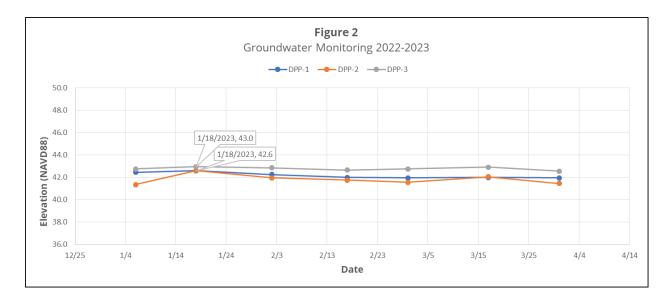
Puyallup, Washington PN: 0420222005

Doc ID: AdvancedUndergroundUtilities.ToddRdNE.SRa

This *Soils Report Addendum* summarizes our seasonal groundwater monitoring for the proposed contractor's yard to be constructed at 320 Todd Road NE in Puyallup, Washington. We prepared a *Soils Report* for the site dated January 4, 2023. To satisfy the groundwater monitoring requirements of the *2019 Stormwater Management Manual for Western Washington* (SWMMWW), we recorded groundwater levels periodically during the 2022-2023 winter wet season.

Three drive-point piezometers (DPPs) were installed by GeoResources at select locations across the site on December 13, 2022 to depths of approximately 10 feet below the existing ground surface. The locations of the DPPs are shown on the Site & Exploration Map, Figure 1. At the time of installation, no groundwater seepage was observed. Groundwater readings for the DPPs were manually measured on a bi-monthly basis from January 6, 2023 to March 31, 2023.

Based on our wet season monitoring, it appears that seasonal high groundwater occurs at about Elevation 42.6 to 43.0 feet (NAVD 88) at the locations monitored. These levels were recorded on January 18, 2023. Based on our measurements, it appears that seasonal high groundwater occurs within about 7 to 8 feet of the ground surface across the site. Figure 2, below, summarizes the groundwater levels recorded as part of our groundwater monitoring program during our monitoring period.



#### **LIMITATIONS**

We have prepared this report for use by Advanced Underground Utilities and other members of the design team, for use in the design of a portion of this project. The data used in preparing this report and this report should be provided to prospective contractors for their bidding or estimating purposes only. Our report, conclusions and interpretations are based on our subsurface explorations, data from others and limited site reconnaissance, and should not be construed as a warranty of the subsurface conditions.

Variations in subsurface conditions are possible between the explorations and may also occur with time. A contingency for unanticipated conditions should be included in the budget and schedule. Sufficient monitoring, testing and consultation should be provided by our firm during construction to confirm that the conditions encountered are consistent with those indicated by the explorations, to provide recommendations for design changes should the conditions revealed during the work differ from those anticipated, and to evaluate whether earthwork and foundation installation activities comply with contract plans and specifications.

If there are any changes in the loads, grades, locations, configurations or type of facilities to be constructed, the conclusions and recommendations presented in this report may not be fully applicable. If such changes are made, we should be given the opportunity to review our recommendations and provide written modifications or verifications, as appropriate.





We have appreciated working for you on this project. Please do not hesitate to call at your earliest convenience if you have any questions or comments.

Respectfully submitted, GeoResources, LLC

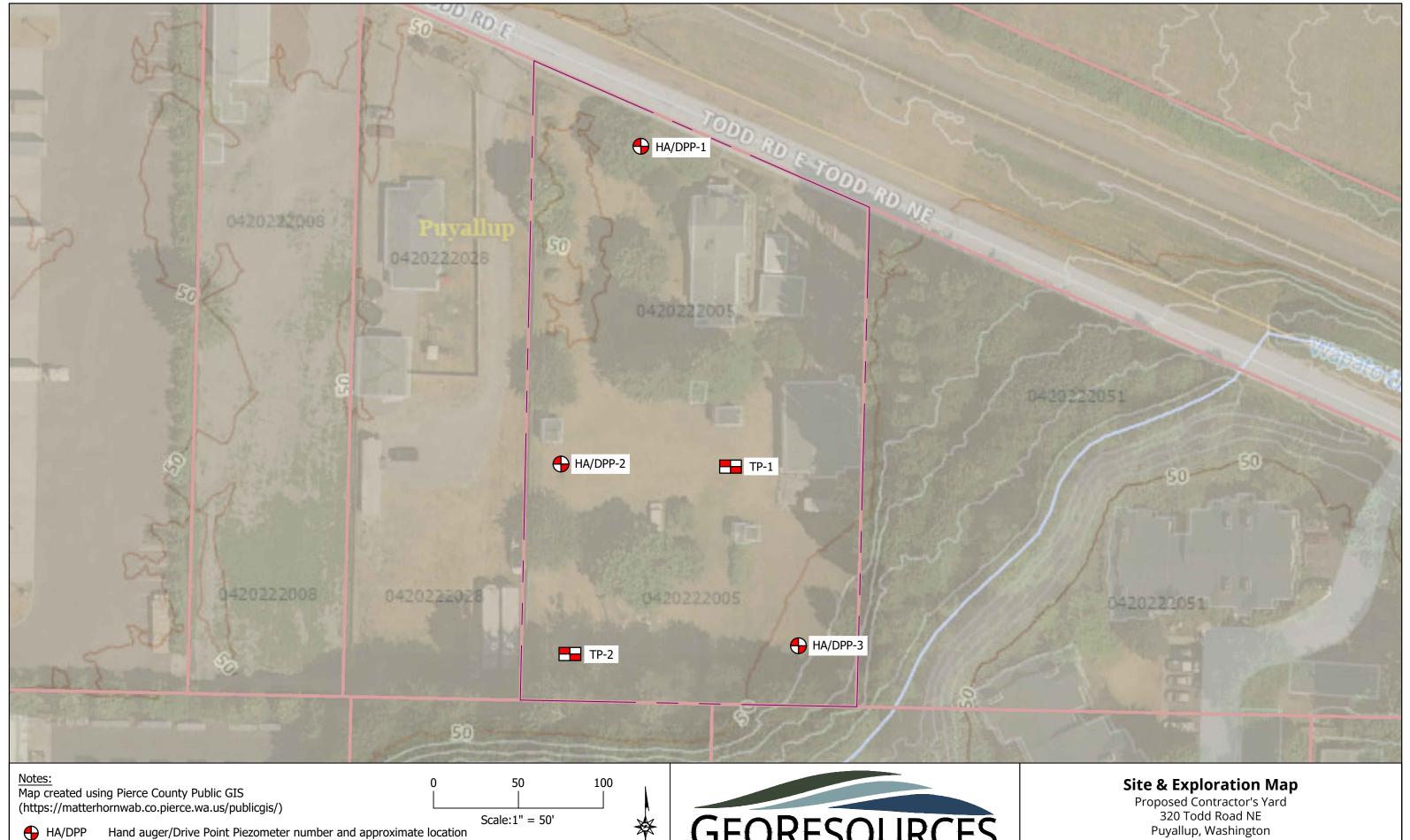


Jordan L. Kovash, LG Project Geologist Eric W. Heller, PE, LG Senior Geotechnical Engineer

JLK:EWH/jlk

Doc ID: AdvancedUndergroundUtilities.ToddRdNE.SRa Attachments: Figure 1 – Site & Exploration Plan





TP

Test pit number and approximate location

This is not a survey.



Puyallup, Washington PN: 0420222005

DocID: AdvanceUndergroundUtilities.ToddRdNE

Figure 1

## **APPENDIX B**

## **ARCHITECT**

MSGS ARCHITECTS
510 CAPITOL WAY SOUTH
OLYMPIA, WA 98501
(360) 943-6774, EXT. 112
CONTACT: GARNER MILLER

## **CIVIL ENGINEER**

JMJ TEAM
905 MAIN STREET
SUITE 200
SUMNER, WA 98390
(206) 596-2020
CONTACT: JUSTIN JONES, PE

## SURVEYOR

CONTOUR ENGINEERING LLC 4706 97TH STREET NW, SUITE 100 GIG HARBOR, WA 98335

(253) 857-5454 CONTACT: STEPHEN H. WOODS, PLS

### **SITE INFORMATION:**

SITE ADDRESS 320 TODD RD NE, PUYALLUP, WA 98371

TAX PARCEL NUMBER: 0420222005

ZONING: RM-20

TOTAL PROJECT AREA: 1.50 AC

## **VERTICAL DATUM:**

BASE:

HELD STATION TACO AS PUBLISHED ON WASHINGTON STATE REFERENCE NETWORK WEBSITE (HTTP://WSRN3.ORG/) (2018)

ELEVATION: 341.348' (NAVD88)

SITE #1: CE 500, A SET HUB AND TACK ON THE NORTH SIDE OF TODD ROAD NORTHEAST, 8.8' EAST OF STORM DRAINAGE MANHOLE AS SHOWN HEREON.

ELEVATION: 50.2' (NAVD88)

SITE #2: CE 505, A SET HUB AND TACK IN THE BACK OF YARD OF THE SITE AS SHOWN HEREON.

ELEVATION: 51.35' (NAVD88)

SITE AREA: 65,123 SQ FT (1.495 ACRES)

### HORIZONTAL DATUM:

THE NORTH AMERICAN DATUM OF 1983/2011 (NAD 83/2011 EPOCH 2010.00) GRID COORDINATES WERE FOUND TO BE 690850.70 / 1194622.67 AT AN "X" IN A 2.5" BRASS DISK.

### **SERVICE PROVIDERS:**

WATER: CITY OF PUYALLUP

SEWER: ON—SITE SEPTIC

POWER: PUGET SOUND ENERGY

GAS: PUGET SOUND ENERGY

**VICINITY MAP** 



320 Todd Rd NE, Puyallup, WA 98371



## SHEET INDEX

Sheet #	Sheet Name	
C1-001	Cover Sheet	
C1-002	General Notes	
C1-003	General Notes	
C1-004	General Notes	
C1-101	Existing Site Plan	
C1-201	Alignment Control Plan	
C1-301	Zone Transition Buffer Plan	
C1-401	Fire Turning Movement	
C2-101	TESC Plan	
C2-201	TESC Details	
C2-301	Demolition Plan	
C3-101	Proposed Site Plan	
C3-201	Hardscape Details	
C3-202	Hardscape Details	
C3-301	Grading Plan	
C3-302	Grading Plan	
C4-101	Composite Utility Plan	
C4-201	Storm Details	
C4-202	Storm Details	
C4-203	Storm Details	
C5-101	Water Details	
C5-102	Water Details	
C6-101	Channelization & Signage Plan	
C6-102	Channelization & Signage Details	
C7-101	Frontage Improvement Plan & Profile	
C7-201	Frontage Site Triangle	
C7-301	Frontage Storm Plan & Profile	
C7-401	Frontage Water Plan & Profile	
C7-402	Frontage Water Plan & Profile	
C7-501	Frontage Details	
C8-101	Traffic Control Plan	
L1	Buffer Planting Plan	
L2	Landscape Details & Notes	

## PROJECT DISTURBED AREA

Description <sup>a</sup>	Onsite	Offsite	Total
Existing Con	ditions		
Total Project Area <sup>b</sup> (ft²)	33,174-0.762 ac	7,997-0.184 ac	41,171-0.946ac
Existing hard surface (ft²)	8,174-0.188 ac	4,678-0.108 ac	12,852-0.296ac
Existing vegetation area (ft²)	25,000- 0.574ac	3,319-0.076 ac	28,319-0.650ac
Proposed Cor	ditions		
Total Project Area <sup>b</sup> (ft²)	33,174-0.762 ac	7,997-0.184 ac	41,171-0.946ac
Amount of new hard surface (ft²)	8,838-0.203 ac	3,304-0.076 ac	12,142-0.279ac
Amount of new pollution generating hard surface (PGHS) <sup>c</sup> (ft²)	8,386-0.193 ac	1,961-0.045 ac	10,347-0.238 ac
Amount of replaced hard surface (ft²)	6,193-0.142 ac	4,678-0.107 ac	10,871-0.249ac
Amount of replaced PGHS <sup>d</sup> (ft²)	3,721-0.085 ac	4,221-0.097 ac	7,942-0.182 ac
Amount of new plus replaced hard surface (ft²)	15,031-0.345ac	7,982-0.183 ac	23,013-0.528ac
Amount of new + replaced PGHS (ft²)	12,107-0.278ac	6,182-0.142 ac	18,289-0.420ac
Amount of existing hard surfaces converted to vegetation (ft²)	1,993-0.046 ac	15-0.001 ac	2,008-0.047 ac
Amount of Land Disturbed (ft²)	33,174-0.762 ac	7,997-0.184 ac	41,171-0.946ac
Vegetation to Lawn/Landscaped (acres)	0.371-16,150 sf	0-0 sf	0.371-16,150 st
Native Vegetation to Pasture (acres)	0-0 sf	0-0 sf	0-0 sf
Existing hard surface to remain unaltered (ft²)	0-0 ac	0-0 ac	0-0 ac
Existing vegetation area to remain unaltered (ft²)	0-0 ac	0-0 ac	0-0 ac

## APPROVED

CITY OF PUYALLUP
DEVELOPMENT ENGINEERING

DATE \_\_\_\_

NOTE: THIS APPROVAL IS VOID
AFTER 180 DAYS FROM APPROVAL
DATE.
THE CITY WILL NOT BE
RESPONSIBLE FOR ERRORS
AND/OR OMISSIONS ON THESE
PLANS.
FIELD CONDITIONS MAY DICTATE
CHANGES TO THESE PLANS AS
DETERMINED BY THE
DEVELOPMENT ENGINEERING

CALL TWO BUSINESS DAYS
BEFORE YOU DIG
1-800-424-5555

UTILITIES UNDERGROUND LOCATION CENTER

Owner/Developer:

EJ Fernandez PO Box 309 Sumner, WA 98390

Architect:

Garner Miller msgs Carve Architects 510 Capitol Way South Olympia, WA 98501



Justin Jones, PE PO Box 2066 Sumner, WA 98390 (206) 596-2020

Project:

320 Todd Road Development

ONE INCH AT FULL SCALE. IF NOT, SCALE ACCORDINGLY

Civil Construction Permit



06-02-25

REV	DATE	DESCRIPTION

Cover Sheet

 PROJ. NO:
 1611-001

 DATE:
 June 02, 2025

 DRAWN BY:
 DESIGN BY:

C1-001

E. Kearney

WG. \_\_\_\_\_1\_ OF \_\_\_31\_\_\_

### **GENERAL PLAN NOTES**

- 1. All work in City right—of—way requires a permit from the City of Puyallup. Prior to any work commencing, the general contractor shall arrange for a preconstruction meeting at the Development Services Center to be attended by all contractors that will perform work shown on the approved engineering plans, representatives from all applicable utility companies, the project owner and appropriate city staff. Contact Engineering Services at (253-841-5568) to schedule the meeting. The contractor is responsible to have their own set of approved plans at the meeting.
- 2. After completion of all items shown on these plans and before acceptance of the project the contractor shall obtain a "punch list"prepared by the City's inspector detailing remaining items of work to be completed. All items of work shown on these plans shall be completed to the satisfaction of the City prior to acceptance of the water system and provision of sanitary sewer service.
- 3. All materials and workmanship shall conform to the Standard Specifications for Road, Bridge, and Municipal Construction (hereinafter referred to as the "Standard Specifications"), Washington State Department of Transportation and American Public Works Association, Washington State Chapter, latest edition, unless superseded or amended by the City of Puyallup City Standards for Public Works Engineering and Construction (hereinafter referred to as the "City Standards").
- 4. A copy of these approved plans and applicable city developer specifications and details shall be on site during construction.
- 5. Any revision made to these plans must be reviewed and approved by the developer's engineer and the City prior to any implementation in the field. The City shall not be responsible for any errors and/or omissions on these plans.
- 6. The contractor shall have all utilities verified on the ground prior to any construction. Call (811) at least two working days in advance. The owner and his/her engineer shall be contacted immediately if a conflict exists.
- 7. Any structure and/or obstruction that requires removal or relocation relating to this project shall be done so at the developer's expense.
- 8. Locations of existing utilities are approximate. It shall be the contractor's responsibility to determine the true elevations and locations of hidden utilities. All visible items shall be the engineer's responsibility.
- 9. The contractor shall install, replace, or relocate all signs, as shown on the plans or as affected by construction, per City Standards.
- 10. Power, street light, cable, and telephone lines shall be in a trench located within a 10-foot utility easement adjacent to public right—of—way. Right—of—way crossings shall have a minimum horizontal separation from other utilities (sewer, water, and storm) of 5 feet.
- 11. All construction surveying for extensions of public facilities shall be done under the direction of a Washington State licensed land surveyor or a Washington State licensed professional civil
- 12. During construction, all public streets adjacent to this project shall be kept clean of all material deposits resulting from on-site construction, and existing structures shall be protected as directed by the City.
- 13. Certified record drawings are required prior to project acceptance.
- 14. A NPDES Stormwater General Permit may be required by the Department of Ecology for this project. For information contact the Department of Ecology, Southwest Region Office as (360) 407-6300.
- 15. Any disturbance or damage to Critical Areas and associated buffers, or significant trees designated for preservation and protection shall be mitigated in accordance with a Mitigation Plan reviewed and approved by the City's Planning Division. Preparation and implementation of the Mitigation Plan shall be at the developer's expense.

### STORMWATER NOTES

- 1. All work in City right—of—way requires a permit from the City of Puyallup. Prior to any work commencing, the general contractor shall arrange for a preconstruction meeting at the Development Services Center to be attended by all contractors that will perform work shown on the engineering plans, representatives from all applicable Utility Companies, the project owner and appropriate City staff. Contact Engineering Services to schedule the meeting (253) 841-5568. The contractor is responsible to have their own approved set of plans at the meeting.
- 2. After completion of all items shown on these plans and before acceptance of the project, the contractor shall obtain a "punch list" prepared by the City's inspector detailing remaining items of work to be completed. All items of work shown on these plans shall be completed to the satisfaction of the City prior to acceptance of the water system and provision of sanitary
- 3. All materials and workmanship shall conform to the Standard Specifications for Road. Bridge, and Municipal Construction (hereinafter referred to as the "Standard Specifications"), Washington State Department of Transportation and American Public Works Association, Washington State Chapter, latest edition, unless superseded or amended by the City of Puyallup City Standards for Public Works Engineering and Construction (hereinafter referred to as the "City Standards").
- 4. A copy of these approved plans and applicable city developer specifications and details shall be on site during construction.
- 5. Any revisions made to these plans must be reviewed and approved by the developer's engineer and the Engineering Services Staff prior to any implementation in the field. The City shall not be responsible for any errors and/or omissions on these plans.
- 6. The contractor shall have all utilities verified on the ground prior to any construction. Call (811) at least two working days in advance. The owner and his/her engineer shall be contacted immediately if a conflict exists.
- 7. Any structure and/or obstruction which require removal or relocation relating to this project, shall be done so at the developer's expense.
- 8. During construction, all existing and newly installed drainage structures shall be protected from sediments.
- 9. All storm manholes shall conform to City Standard Detail No. 02.01.01. Flow control manhole/oil water separator shall conform to City Standard Detail No. 02.01.06 and 02.01.07.
- 10. Manhole ring and cover shall conform to City Standard Detail 06.01.02.
- 11. Catch basins Type I shall conform to City Standard Detail No.02.01.02 and 02.01.03 and shall be used only for depths less than 5 feet from top of the grate to the invert of the storm pipe.
- 12. Catch basins Type II shall conform to City Standard Detail No.02.01.04 and shall be used for depths greater than 5 feet from top of the grate to the invert of the storm pipe.
- 13. Cast iron or ductile iron frame and grate shall conform to City Standard Detail No.02.01.05. Grate shall be marked with "drains to stream". Solid catch basin lids (square unless noted as round) shall conform to WSDOT Standard Plan B-30.20-04 (Olympic Foundry No. SM60 or equal). Vaned grates shall conform to WSDOT Standard Plan B-30.30-03 (Olympic Foundry
- 14. Stormwater pipe shall be only PVC, concrete, ductile iron, or dual walled Polypropylene pipe. a. The use of any other type shall be reviewed and approved by the
- Engineering Services Staff prior to installation. b. PVC pipe shall be per ASTM D3034, SDR 35 for pipe size 15-inch and smaller and F679 for pipe sizes 18 to 27 inch. Minimum cover on PVC
- pipe shall be 3.0 feet. c. Concrete pipe shall conform to the WSDOT Standard Specifications for concrete underdrain pipe. Minimum cover on concrete pipe shall not less
- than 3.0 feet. d. Ductile iron pipe shall be Class 50, conforming to AWWA C151. Minimum cover on ductile iron pipe shall be 1.0 foot.
- e.Polypropylene Pipe (PP) shall be dual walled, have a smooth interior and exterior corrugations and meet WSDOT 9-05.24(1). 12-inch through 30-inch pipe shall meet or exceed ASTM F2736 and AASHTO M330, Type S, or Type D. 36-inch through 60-inch pipe shall meet or exceed ASTM F2881 and AASHTO M330, Type S, or Type D. Testing shall be per ASTM F1417. Minimum cover over Polypropylene pipe shall be 3-feet.
- 15. Trenching, bedding, and backfill for pipe shall conform to City Standard Detail No. 06.01.01.
- 16. Storm pipe shall be a minimum of 10 feet away from building foundations and/or roof lines.
- 17. All storm drain mains shall be tested and inspected for acceptance as outlined in Section 406 of the City of Puyallup Sanitary Sewer System
- 18. All temporary sedimentation and erosion control measures, and protective measures for critical areas and significant trees shall be installed prior to initiating any construction activities.

## **SANITARY SEWER NOTES**

- 1. All work in City right—of—way requires a permit from the City of Puyallup. Prior to any work commencing, the general contractor shall arrange for a preconstruction meeting at the Development Services Center to be attended by all contractors that will perform work shown on the engineering plans, representatives from all applicable Utility Companies, the project owner and appropriate City staff. Contact Engineering Services to schedule the meeting (253) 841-5568. The contractor is responsible to have their own approved set of plans at the meeting.
- 2. After completion of all items shown on these plans and before acceptance of the project, the contractor shall obtain a "punch list" prepared by the City's inspector detailing remaining items of work to be completed. All items of work shown on these plans shall be completed to the satisfaction of the City prior to acceptance of the sewer system and provision of sanitary sewer
- 3. All materials and workmanship shall conform to the Standard Specifications for Road, Bridge, and Municipal Construction (hereinafter referred to as the "Standard Specifications"), Washington State Department of Transportation and American Public Works Association, Washington State Chapter, latest edition, unless superseded or amended by the City of Puyallup City Standards for Public Works Engineering and Construction (hereinafter referred to as the "City Standards").
- 4. A copy of these approved plans and applicable city developer specifications and details shall be on site during construction.
- 5. Any revisions made to these plans must be reviewed and approved by the developer's engineer and the Engineering Services Staff prior to any implementation in the field. The City shall not be responsible for any errors and/or omissions on these plans.
- 6. The contractor shall have all utilities verified on the ground prior to any construction. Call (811) at least two working days in advance. The owner and his/her engineer shall be contacted immediately if a conflict exists.
- 7. Any structure and/or obstruction which require removal or relocation relating to this project shall be done so at the developer's expense.
- 8. Minimum grade on all 4 inch residential side sewers shall be 2 percent and 6 inch commercial side sewers shall be 1 percent; maximum shall be 8 percent. All side sewers shall be 6 inches within City right-of-way.
- 9. Side sewers shall be installed in accordance with City Standard Nos. 04.03.01, 04.03.02, 04.03.03 and 04.03.04. Side sewer installation work shall be done in accordance with the Washington Industrial Safety and Health Act (WISHA).
- 10. All sewer pipe shall be PVC, Polypropylene, or Ductile Iron. PVC sewer pipe shall conform to ASTM D-3034, SDR35 for pipe sizes 15-inch and smaller and ASTM F679 for pipe sizes 18- to 27-inch, ductile iron pipe shall be Class 51 or greater, lined with Protecto 401TM epoxy lining or equivalent, unless otherwise noted. 12-inch through 30-inch Polypropylene Pipe (PP) shall be dual walled, have a smooth interior and exterior corrugations and meet WSDOT 9-05.24(2). It shall meet or exceed ASTM F2764. 36-inch through 60-inch PP pipe shall be triple walled and meet WSDOT 9-05.24(2). It shall meet or exceed ASTM F2764. PP shall have a minimum pipe stiffness of 46 pii when tested in accordance with ASTM D2412. Testing shall be per ASTM F1417. Trenching, bedding, and backfill shall be in accordance with City Standard No. 06.01.01. Minimum cover on PVC and PP pipe shall be 3.0 feet. Minimum cover on ductile iron pipe shall be 1.0 foot.
- 11. Sanitary sewer manhole frames and covers shall conform to City Standard
- 12. Sanitary sewer manholes shall conform to City Standard Nos. 04.01.01, 04.01.02, 04.01.03 and 04.01.04. All manholes shall be channeled for future lines as specified on these plans. Manhole steps and ladder shall conform to Standard No. 06.01.03.
- 13. Sanitary sewer pipe and side sewers shall be 10 feet away from building foundations and/or roof lines with the exception of side sewers that provide service to a single-family residence. At the discretion of the review engineer, a Licensed Professional Engineer will be required to stamp the design to account for depth or proximity to foundation, steep slopes, or other factors.
- 14. No side sewers shall be connected to any house or building until all manholes are adjusted to the finished grade of the completed asphalt roadway and the asphalt patch and seal around the ring are accepted.
- 15. For commercial developments in which sources of grease and/or oils may be introduced to the City sanitary sewer system, a City approved grease interceptor shall be installed downstream from the source.
- 16. Once sewer and all other utility construction is completed, all sanitary sewer mains and side sewers shall be tested per Section 406 of the City

- 1. All work in City right—of—way requires a permit from the City of Puyallup. Prior to any work commencing, the general contractor shall arrange for a preconstruction meeting at the Development Services Center to be attended by all contractors that will perform work shown on the approved engineering plans, representatives from all applicable utility companies, the project owner and appropriate city staff. Contact Engineering Services at (253-841-5568) to schedule the meeting. The contractor is responsible to have their own set of approved plans at the meeting.
- 2. After completion of all items shown on these plans and before acceptance of the project the contractor shall obtain a "punch list" prepared by the City's inspector detailing remaining items of work to be completed. All items of work shown on these plans shall be completed to the satisfaction of the City prior to acceptance of the water system and provision of sanitary sewer service.
- 3. All materials and workmanship shall conform to the Standard Specifications for Road, Bridge, and Municipal Construction (hereinafter referred to as the "Standard Specifications"), Washington State Department of Transportation and American Public Works Association, Washington State Chapter, latest edition, unless superseded or amended by the City of Puyallup City Standards for Public Works Engineering and Construction (hereinafter referred to as the "City Standards"), or as directed by Fruitland Mutual Water Company (FMWC), Valley Water (VW), or Tacoma City Water (TCW) is the purveyor.
- 4. A copy of these approved plans and applicable city developer specifications and details shall be on site during construction.
- 5. Any revision made to these plans must be reviewed and approved by the developer's engineer and the Engineering Services Staff, and the FMWC, VW, or TCW when served by that purveyor, prior to any implementation in the field. The City shall not be responsible for any errors and/or omissions on these plans.
- 6. The contractor shall have all utilities verified on the ground prior to any construction. Call (811) at least two working days in advance. The owner and his/her engineer shall be contacted immediately if a conflict exists.
- 7. All limits of clearing and areas of vegetation preservation as prescribed on the plans shall be clearly flagged in the field and observed during construction.
- 8. All required sedimentation and erosion control facilities must be constructed and in operation prior to any land clearing and/or other construction to ensure that sediment laden water does not enter the natural drainage system. The contractor shall schedule an inspection of the erosion control facilities PRIOR to any land clearing and/or other construction. All erosion and sediment facilities shall be maintained in a satisfactory condition as determined by the City, until such time that clearing and/or construction is completed and the potential for on—site erosion has passed. The implementation, maintenance, replacement, and additions to the erosion and sedimentation control systems shall be the responsibility of the permittee.
- 9. The erosion and sedimentation control system facilities depicted on these plans are intended to be minimum requirements to meet anticipated site conditions. As construction progresses and unexpected or seasonal conditions dictate, facilities will be necessary to ensure complete situation control on the site. During the course of construction, it shall be the obligation and responsibility of the permittee to address any new conditions that may be created by his activities and to provide additional facilities, over and above the minimum requirements, as may be needed to protect adjacent properties, sensitive areas, natural water courses, and/or storm drainage systems.
- 10. Approval of these plans is for grading, temporary drainage, erosion, and sedimentation control only. It does not constitute an approval of permanent storm drainage design, size or location of pipes, restrictors, channels, or
- 11. Any disturbed area which has been stripped of vegetation and where no further work is anticipated for a period of 30 days or more, must be immediately stabilized with mulching, grass planting, or other approved erosion control treatment applicable to the time of year in question. Grass seeding alone will be acceptable only during the months of April through September inclusive. Seeding may proceed outside the specified time period whenever it is in the interest of the permittee but must be augmented with mulching, netting, or other treatment approved by the City.
- 12. In case erosion or sedimentation occurs to adjacent properties, all construction work within the development that will further aggravate the situation must cease, and the owner/contractor will immediately commence restoration methods. Restoration activity will continue until such time as the affected property owner is satisfied.
- 13. No temporary or permanent stockpiling of materials or equipment shall occur within critical areas or associated buffers, or the critical root zone for vegetation proposed for retention.

**GRADING, EROSION, AND** SEDIMENT CONTROL PLAN NOTES

> EJ Fernandez PO Box 309 Sumner, WA 98390

Owner/Developer:

Architect:

Garner Miller msgs Carve Architects 510 Capitol Way South Olympia, WA 98501



(206) 596-2020

320 Todd Road Development

ONE INCH AT FULL SCALE. IF NOT, SCALE ACCORDINGLY

**Civil Construction Permit** 



06-02-25

REV	DATE	DESCRIPTION

RAWN BY:

SHEET NUMBER.

CITY OF PUYALLUP DEVELOPMENT ENGINEERING

**APPROVED** 

**NOTE:** THIS APPROVAL IS VOID AFTER 180 DAYS FROM APPROVAL THE CITY WILL NOT BE RESPONSIBLE FOR ERRORS AND/OR OMISSIONS ON THESE FIELD CONDITIONS MAY DICTATE

CHANGES TO THESE PLANS AS DETERMINED BY THE DEVELOPMENT ENGINEERING MANAGER.

CALL TWO BUSINESS DAYS BEFORE YOU DIG -800-424-5555

UTILITIES UNDERGROUND LOCATION CENTER

C1-002

**General Notes** 

1611-001

June 02, 2025

DESIGN BY:

J. Jones

\_\_\_\_\_2 OF \_\_\_\_31

E. Kearney

### **WATER NOTES**

- 1. All work in City right—of—way requires a permit from the City of Puyallup. Prior to any work commencing, the general contractor shall arrange for a preconstruction meeting at the Development Services Center to be attended by all contractors that will perform work shown on the engineering plans, representatives from all applicable Utility Companies, the project owner and appropriate City staff. Contact Engineering Services to schedule the meeting (253) 841—5568. The contractor is responsible to have their own approved set of plans at the meeting.
- 2. After completion of all items shown on these plans and before acceptance of the project, the contractor shall obtain a "punch list" prepared by the City's inspector detailing remaining items of work to be completed. All items of work shown on these plans shall be completed to the satisfaction of the City prior to acceptance of the water system and provision of sanitary sewer service.
- All materials and workmanship shall conform to the Standard Specifications for Road, Bridge, and Municipal Construction (hereinafter referred to as the "Standard Specifications"). Washington State Department of Transportation and American Public Works Association, Washington State Chapter, latest edition, unless superseded or amended by the City of Puyallup City Standards for Public Works Engineering and Construction (hereinafter referred to as the "City Standards"), or as directed by Fruitland Mutual Water Company (FMWC), Valley Water (VW), or Tacoma City Water (TCW) is the purveyor.
- 4. A copy of these approved plans and applicable city developer specifications and details shall be on site during construction.
- 5. Any revisions made to these plans must be reviewed and approved by the developer's engineer, the Engineering Services Staff, and the FMWC, VW or TCW when served by that purveyor, prior to any implementation in the field. The City shall not be responsible for any errors and/or omissions on these plans.
- 6. The contractor shall have all utilities verified on the ground prior to any construction. Call (811) at least two working days in advance. The owner and his/her engineer shall be contacted immediately if a conflict exists.
- 7. Any structure and/or obstruction which requires removal or relocation relating to this project shall be done so at the developer's expense.
- 8. Bacteriological (Coliform and Iron Bacteria) test samples will be taken by the City (or FMWC, VW or TCW when served by that purveyor) and paid for by the contractor, except for Capital Improvement Projects (CIP) which shall be paid for by the City.
- 9. Water mains shall have a minimum cover of 36 inches from paved final grade in improved right—of—way and improved easements, and a minimum of 48 inches in unimproved right-of- way and unimproved easements.
- 10. Pipe for water mains shall be ductile iron conforming to Section 7—09 of the Standard Specifications, Class 52 with tyton or approved equal joints. Pipe shall be cement lined in accordance with A.S.A. Specification A 21.4-1964.
- 11. Connections to existing water mains typically shall be wet taps through a tapping tee and tapping valve and shall be made by a city approved contractor. The tapping sleeve shall be Romac SST all stainless steel tapping sleeve or approved equal. A two-piece epoxy coated or ductile iron tapping sleeve may be used on ductile iron pipe, when the tap is smaller than the water main size i.e. 6—inch tap on 8—inch pipe. The City (or FMWC, VW or TCW when served by that purveyor) shall approve the time and location for these connections.
- 12. All water mains and appurtenances shall be hydrostatically tested at 200 psi in accordance with Standard Specification 7-09.3(23). Pressure testing shall not be performed until satisfactory purity samples have been received, except when new water mains are installed independently from the water system piping.
- 13. Fire hydrants shall be installed in accordance with City Standard Detail 03.05.01 and as directed by the City of Puyallup Fire Code Official.
- 14. Valve marker posts shall be installed where valve boxes are hidden from view or in unpaved areas. The installation shall be in accordance with City Standard Detail
- 15. Resilient seated wedge gate valves shall be used for 10-inch mains and smaller.
- 16. Pipe fitting for water mains shall be ductile iron and shall be mechanical joint conforming to AWWA Specification C111-72.
- 17. Water main pipe and service connections shall be a minimum of 10 feet away from building foundations and/or roof lines.
- 18. Where a water main crosses the Northwest Gas pipeline, the water line shall be cased with PVC pipe a minimum of 10 feet beyond each side of the gas line easement. Contact Williams Northwest Pipeline before the crossing is made.
- 19. Trenching, bedding, and backfill for water mains shall be installed in accordance with City Standard Detail 06.01.01.
- 20. All commercial and industrial developments, irrigation systems, and multi-family water service connections shall be protected by a double check valve assembly or a reduced pressure backflow assembly as directed by the City (or FMWC, VW or TCW when served by that purveyor) conforming to City Standard Details 03.04.01, 03.04.02, and
- 21. Any lead joint fitting disturbed during construction shall be replaced with a mechanical joint fitting at the contractor's expense.
- 22. When hydraulic fire flow modeling is required for a project, the City will issue a permit. The hydraulic modeling criteria is based on the projected 2030 water demand, while maintaining a minimum system pressure of 20 pounds per square inch and a maximum velocity of 10 feet per second.
- 23. When using a fire hydrant for non-firefighting purposes, a city hydrant meter must be used. Coordinate the acquisition of the hydrant meter with the City's Utility Billing Division at Puyallup City Hall. A city approved backflow protection assembly shall be installed by the person requesting use of a fire hydrant. The assembly shall be accompanied by a current backflow assembly test report. The test report shall be available at the site for the duration of the hydrant use.
- 24. Should a break occur on any City water main, the Contractor shall follow the City's adopted "Water Main Break Procedure" issued to them at the Pre-Construction Meeting and notify those connected to the system in the impacted area as outlined in the

- 25. Water Main Repairs (References: AWWA C651-14 and WSDOT Standard Specification Section 7-09) (Note: A planned water main repair shall be approved by the City Inspector and/or Water Division Supervisor prior to commencing work.)
- a. Repair without depressurization Small leaks shall be repaired using repair bands while maintaining positive pressure in the water main. Valves surrounding the leak will be partially shut by the City Water Department to reduce the flow and pressure to the area. Blowoffs and hydrants in the reduced pressure area may be opened as needed to further reduce the pressure. The water main trench shall be over-excavated to allow water in the trench to be pumped out and maintained below the level of the water main. The repair shall be completed with the water main pressure remaining positive. After the repair is made, the system shall be fully pressurized and a visual leak inspection will be completed. The water main in the affected area shall be flushed to achieve three pipe volumes pulled from the pipe (distance measured from valve opened for flushing to the exit hydrant or blowoff).
- b. <u>Repair/cut—in with depressurization</u> Trench shall be over excavated and dewatered below the water main. Flush water from pipe from each direction until it runs clear. Immediately prior to installation of a new pipe section for repair or cut in tee, all new fittings and pipe spools shall be swabbed with a five percent (5%) chlorine solution (minimum). The interior of the existing pipe shall be swabbed with a five percent (5%) chlorine solution at least 6 feet in each direction from exposed cut ends. The water main in the affected area shall be flushed to achieve three pipe volumes pulled from the pipe (distance measured from the valve opened for flushing to the exit hydrant or blowoff). Customers shall be notified after the water main is flushed and repairs have been completed, as outlined in the "Water Main Break Procedure."
- 26. New Water Main Installation:
  - a. Each new water main section shall be delivered, stacked and stored onsite with ends plugged. The plugs shall remain in the pipe until each particular section is installed. National Sanitation Foundation (NSF) approved sixty-five percent (65%) calcium hypochlorite shall be added to the upstream end of each pipe section, and at each hydrant tee in the amount given in the table below (or per approved manufacturer specifications). The minimum amount of calcium hypochlorite added should be sufficient to achieve a 50 mg/L concentration within the impacted area.

	Pipe Volume	5-gram	Hypochlori	te Granules	Maximum
Pipe Diameter	per 18 feet	tablets per	Ounces per	Teaspoons	Fill Rate
(Inches)	(gal)	pipe section	500 feet	per 18 feet	(gpm)_
4	35	1	1.7	0.2	40
6	53	1	3.8	0.4	90
8	70	2	6.7	0.7	150
12	106	4	15.1	1.4	350
16	141	6	27	2.5	600

- b. New water mains shall be filled using an approved backflow prevention assembly. The water main shall be filled from the lower elevation end so that as the water main is filled, the chorine is contacted, dissolved and spread relatively uniform through the length of the new water main. The fill rate shall be minimized so that the velocity of the water is less than 1 ft/sec (see table above). Successful pressure test and bacteriological tests shall be completed and provided to the City prior to any new mater main connection to the existing water system.
- c. The chlorinated water will be allowed to remain in contact with the new water main system for 24 to 72 hours. After 24 hours, water may be added to the water main for the purposes of pressure testing. The water in the main used for pressure testing must remain in the water main until pressure test is completed. If necessary, liquid chlorine shall be injected into the water main with fill water to maintain a concentration in the water main above 50 mg/L. Under no circumstance shall "super" chlorinated water be allowed to sit within a new water main for more than 5 days.
- d. Pressure testing includes testing against new valves and hydrants. Each valve shall be tested by closing each in turn and reducing the pressure beyond the valve. The pressure on the back side of the valve should not be eliminated. Care must be taken that, during this process, positive pressure remains throughout the system being tested at all times. All hydrant foot valves shall be open during pressure testing so that the pressure test is against the hydrant valve. Pressure testing will not be allowed against any existing valves.
- e. After successful pressure testing, the water main shall be thoroughly flushed to remove all "super" chlorinated water from the new water main. Flushing of new or extended water mains shall be conducted per WSDOT Specification 7-09.3(24)A with a minimum velocity developed within the pipe while flushing of 2.5 feet per second (fps). All flushed water shall be dechlorinated prior to disposal. The Contractor shall be responsible for disposal of all chlorinated water flushed from mains. The City shall approve the disposal method prior to implementation in the field. The Contractor shall utilize on— site disposal methods, if available. Disposal of flush water to the sanitary sewer system shall not be allowed without written permission from the Water Pollution Control Plant (WPCP) Supervisor. Any planned discharge to a stormwater system shall be dechlorinated to a concentration of 0.1 ppm or less, pH adjusted (if necessary) to be between 6.5 and 8.5, and volumetrically and velocity controlled to prevent any resuspension of sediments. The City will require independent testing throughout the water discharge process to ensure compliance of these standards are met.
- f. Samples for bacteriological analysis shall be collected after flushing and again 24 hours after the first set of samples.
- g. All closure/final connection fittings shall be sprayed clean and then swabbed with a five percent (5%) chlorine solution immediately prior to installation per AWWA Standard C651. Additional samples for bacteriological analysis shall be collected from the immediate vicinity of the new or replaced water main and analyzed after the final connections are made. If necessary, additional flushing shall be conducted and additional samples shall be collected until satisfactory results are obtained.

## **SANITARY SEWER TESTING REQUIREMENTS**

Gravity sanitary sewer cleaning and testing requirements shall be as outlined in WSDOT Section 7-17.3(2). Sanitary sewer cleaning and testing shall be completed to the satisfaction of the Office of the City Engineer and/or Public Works Department prior to final acceptance. After completion of all project utility work (sewer, water, storm, etc.) and associated utility trench backfill and compaction, sewer lines shall be cleaned and tested by the Contractor prior to final project acceptance, as outlined in Section 406.1 through 406.4. At the end of the Maintenance and Warranty Period, the City will perform a final CCTV inspection per 406.4 to verify that the work performed conforms to City Standards prior to bond release.

### 1.1. <u>Cleaning</u>

Physical connection to the existing City sewer system shall not be allowed until all pipes have been thoroughly cleaned by jetting and/or pigging to remove any solids or construction debris that may have entered the pipe.

The Contractor shall arrange to have the water accumulated during construction and sanitary system cleaning operations removed from the sewer system by a Vactor truck. Water from the new sewer extension shall not be permitted to enter the existing City system until final project approval. Sediment or debris introduced to existing City sewers as a result of any construction activity shall be removed immediately by the Contractor in conformance with WSDOT Section 7-17.

#### 1.2. <u>Deflection Testing</u>

Gravity sanitary sewers shall be tested for deflection prior to visual inspection. Thermoplastic pipe shall be tested for deflection not less than 30 days after the trench backfill and compaction has been completed. Deflection testing shall be conducted by pulling a mandrel (rigid or adjustable) with a diameter not less than 95 percent of the normal diameter of the pipe being tested. Mandrel testing shall be conducted in conformance with WSDOT Section 7-17.3(2)G.

#### 1.3. <u>Leakage Testing</u>

All new gravity sanitary sewer mains and the right-of-way laterals shall be subject to a low-pressure air test per WSDOT Section 7-17.3(2)F. Low pressure air testing shall be conducted after backfilling is completed and the backfill material has been compacted in conformance with the approved plans. Conforming compaction shall be verified by nuclear gauge testing and/or proof rolling at the discretion of Engineering staff. The City Engineer or designee shall observe all testing to verify satisfactory completion. The City Engineer or designee may require that air test pressure be maintained at 4.0 psig with no drop for 15 minutes for a passing leakage test where groundwater pressure is deemed negligible, or at the City Engineer's or designee's discretion.

The Contractor shall furnish all necessary equipment and personnel for conducting the pressure test. The Contractor shall provide certification from a certified/accredited laboratory that testing equipment is accurate. All equipment and personnel shall be subject to approval by the City Engineer or designee.

If any portion of the sanitary system fails to meet the testing requirements, the Contractor shall determine, at their own expense, the source of leakage and shall repair or replace all defective materials or workmanship. The completed pipe installation shall meet the minimum testing requirements before being considered acceptable.

### 1.4. <u>Television Inspection</u>

All new gravity sanitary sewer extensions shall be visually inspected in conformance with WSDOT Section 7-17.3(2)H, following satisfactory trench compaction testing, flushing, low pressure air testing, and deflection testing. All manholes shall be channeled and grade rings set in place prior to sewer video inspection.

The remote camera used in sewer visual inspection shall be one specifically designed for such an application, with the ability to rotate the camera 180 degrees and lighting suitable to allow a clear picture of the entire periphery of the pipe. The camera shall proceed through the pipe at a sufficiently slow velocity to allow adequate inspection of all pipe All sewer lateral fittings and joints and suspect pipe joints shall be closely inspected by rotating the camera as needed to provide a clear

The Contractor shall introduce water to the new sewer system immediately prior to the visual inspection by adding water to the upstream manhole until water is seen flowing in the lowest manhole. Video inspection of the line shall begin when flow in the lowest manhole has stopped. A 1—Inch sewer ball shall be attached to the front of the camera to provide a basis for estimating the depth of the ponding within the sewer pipe.

<u>Television Inspection Acceptance Criteria:</u>

- 1.4.1. Any ponding within a pipe shall be less than one—half inch (1/2) in
- 1.4.2. The total accumulated ponding length, regardless of depth, from manhole to manhole shall be less than ten (10) percent of the total length from manhole to manhole.

Any sewer pipe that exceeds either of the above acceptance criteria will be rejected and require repair and/or replacement by the Contractor.

The Contractor shall bear all costs for the correction of any deficiencies found during TV inspection, including the costs for additional TV inspection and leakage testing needed to verify the deficiencies were corrected. All components of the video and recording equipment shall be sufficient to provide picture quality to the satisfaction of the City Engineer or designee.

Upon completion of the video inspection, the digital video, of common format, and written inspection report shall be submitted to the City for review. At a minimum, the inspection report shall contain the following information:

-Size, length, and material type of the sewer main.

-Location of all lateral connections.

-Estimated depth and location of all ponding over 1/4 inch in depth

-Manhole numbers that correspond to the approved plans

-Street name and/or location of sewer main

Owner/Developer:

EJ Fernandez PO Box 309 Sumner, WA 98390

Architect:

Garner Miller msgs Carve Architects 510 Capitol Way South Olympia, WA 98501



Justin Jones, PE PO Box 2066 Sumner, WA 98390 (206) 596-2020

320 Todd Road Development

ONE INCH AT FULL SCALE. IF NOT, SCALE ACCORDINGLY

**Civil Construction Permit** 



REV DATE DESCRIPTION

06-02-25

1611-001

C1-003

June 02, 2025

DESIGN BY:

J. Jones

DRAWN BY:

**General Notes** 

**NOTE:** THIS APPROVAL IS VOID AFTER 180 DAYS FROM APPROVAL THE CITY WILL NOT BE RESPONSIBLE FOR ERRORS AND/OR OMISSIONS ON THESE FIELD CONDITIONS MAY DICTATE CHANGES TO THESE PLANS AS DETERMINED BY THE

**APPROVED** 

CITY OF PUYALLUP

DEVELOPMENT ENGINEERING

DATE

MANAGER.

SHEET NUMBER.

E. Kearney

CALL TWO BUSINESS DAYS BEFORE YOU DIG

DEVELOPMENT ENGINEERING

-800-424-5555 UTILITIES UNDERGROUND LOCATION CENTER

## **TESTING AND INSPECTION**

Stormwater system cleaning and testing requirements shall be as outlined in WSDOT Section 7-17.3(2) and the standards herein. Stormwater system cleaning and testing shall be completed to the satisfaction of the City Engineer, or designee, prior to final acceptance. After completion of all project utility work (sewer, water, storm, etc.) and associated utility trench backfill and compaction, stormwater lines shall be cleaned and tested by the Contractor prior to final project acceptance, as outlined in Section 209.1 through 209.4. At the end of the maintenance and warranty period, the developer/contractor is required to clean and flush the lines as outlined in the standards herein. Other testing may be required at the end of the maintenance and warranty period, as determined by the City Engineer.

#### 209.1 Cleaning/Flushing

The Contractor shall arrange to have all water and debris accumulated during construction removed from the system. Stormwater cleaning operations shall consist of jetting all stormwater lines, both main lines and laterals. Jetting lines shall never result in pushing sediment or debris downstream and all sediment, debris and water shall be removed from the stormwater system by a vactor truck. Sediment or debris introduced to the City's stormwater system because of construction activity shall be removed immediately by the Contractor in conformance with WSDOT Section 7-04.

#### 209.2 Deflection Testing

Stormwater pipes shall be tested for deflection prior to visual inspection. Thermoplastic pipe shall be tested for deflection not less than 30 days after the trench backfill and compaction has been completed. Deflection testing shall be conducted by pulling a mandrel (rigid or adjustable) with a diameter not less than 95 percent of the normal diameter of the pipe being tested. Mandrel testing shall be conducted in conformance with WSDOT Section 7-17.3(2)G.

### 209.3 Pressure Testing

- All new stormwater pipes shall be subject to a low-pressure air test per WSDOT Section 7-17.3(2)F. Pressure testing shall be in accordance with the following, unless otherwise determined by the City Engineer, or designee.
- 1. Low pressure air testing shall be conducted after backfilling is completed. Backfill material shall be compacted in accordance with the approved plans.
- 2. Conforming compaction shall be verified by nuclear gauge testing and/or proof rolling. The City Engineer, or designee, shall observe all testing to verify satisfactory completion.
- 3. The Contractor shall furnish all necessary equipment and personnel for conducting the pressure test. The Contractor shall provide certification from certified/accredited laboratory that testing equipment is accurate. All equipment and personnel shall be subject to approval.
- 4. The Contractor shall conduct a preliminary pressure test prior to City observation, any portions of the system that fail the preliminary test should be remedied prior to City observation.
- 5. If any portion of the stormwater system fails to meet the testing requirements, the Contractor shall determine, at their own expense, the source of leakage and shall repair or replace all defective materials or workmanship. The completed pipe installation shall meet the minimum testing requirements before being considered acceptable.

### 209.4 Television Inspection

- All new stormwater pipes shall be visually inspected in conformance with WSDOT Section 7-17.3(2)H, following satisfactory trench compaction testing, flushing, low pressure air testing, and deflection testing. All manholes and catch basins shall be watertight with grade rings set in place prior to stormwater video inspection. The remote camera used in stormwater visual inspection shall be one specifically designed for such an application, with the ability to rotate the camera 180 degrees and lighting suitable to allow a clear high-quality picture of the entire periphery of the pipe. The camera shall proceed through the pipe at an appropriate velocity to allow adequate inspection of all pipe joints. All pipe joints shall be closely inspected by rotating the camera as needed to provide a clear view. The Contractor shall introduce water, with dye, to the stormwater system immediately prior to the visual inspection. The water shall be added to the upstream manhole until water is seen flowing in the downstream manhole. An incremented 1—inch sewer ball shall be attached to the front of the camera to provide a basis for estimating the depth of the ponding within the stormwater
- All new stormwater pipes shall be inspected by television camera with the City Engineer, or designee, present. Video and inspection reports shall be submitted to the City and include the following:
- 1. An electronic report of the inspection and copy of the inspection video in electronic form on a flash drive.
- 2. Video shall be labeled with the date and time, street name or location, upstream/ downstream structure, pipe size, pipe length and pipe material type.
- 3. Location and depths of all ponding 1/4" or greater.
- 4. Location of deflections, deformation, or structural defects.
- 5. One file should be submitted with all stormwater pipe runs for the project. One-by-one submittals will not be accepted.
- 6. Video or inspection reports failing to meet criteria 1—5 above will not be reviewed and will be returned to the contractor/developer.

#### 209.5 Acceptance Criteria

- All new storm pipe installed (public and private) shall be tested, in accordance with Section 209, and video shall be reviewed and approved by the City Engineer, or designee, prior to the placement of curb and gutter or pavement. Unless determined otherwise by the City Engineer, or designee, all repairs identified shall be completed as follows:
- 1. Any ponding within a pipe shall be less than one—half inch (1/2) in depth.
- 2. The total accumulated ponding length, regardless of depth, from manhole to manhole shall be less than ten (10) percent of the total length from manhole to manhole.
- 3. The use of couplers is prohibited.
- 4. If a pipe needs to be cut into for the repair, the storm pipe run shall be removed and reinstalled from the nearest bell to the nearest catch basin.
- 5. If removal and replacement of any section of storm pipe is required to make a repair, the entire length of mainline shall be required to be retested after repairs
- 6. A new video shall be required after the required repairs have been completed, in accordance with Section 209.4.
- Any stormwater pipe that exceeds any of the above acceptance criteria will be rejected and require repair and/or replacement by the Contractor.
- The Contractor shall bear all costs for the correction of any deficiencies found during TV inspection, including the costs for additional TV inspection and pressure testing needed to verify that the deficiencies were corrected. All components of the video and recording equipment shall be sufficient to provide picture quality to the satisfaction of the City Engineer, or designee.

Owner/Developer:

EJ Fernandez PO Box 309 Sumner, WA 98390

Architect:

Garner Miller msgs Carve Architects 510 Capitol Way South Olympia, WA 98501



Justin Jones, PE PO Box 2066 Sumner, WA 98390 (206) 596-2020

320 Todd Road Development

ONE INCH AT FULL SCALE. IF NOT, SCALE ACCORDINGLY

Civil Construction Permit



REV	DATE	DESCRIPTION

**General Notes** 

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AND/OR OMISSIONS ON THESE FIELD CONDITIONS MAY DICTATE CHANGES TO THESE PLANS AS DETERMINED BY THE DEVELOPMENT ENGINEERING MANAGER.

**APPROVED** 

CITY OF PUYALLUP DEVELOPMENT ENGINEERING

DATE

E. Kearney

SHEET NUMBER.

C1-004

1611-001

June 02, 2025

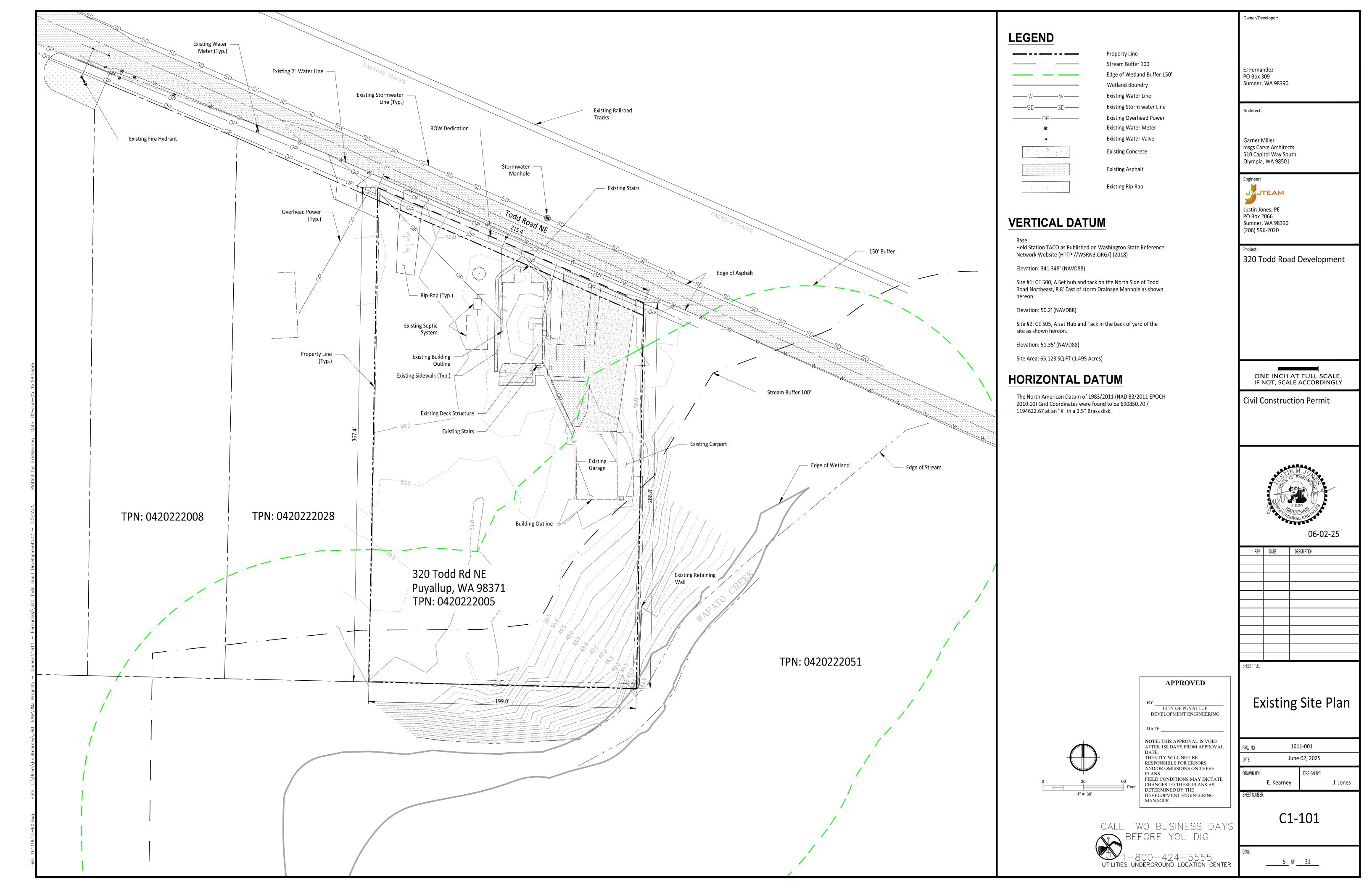
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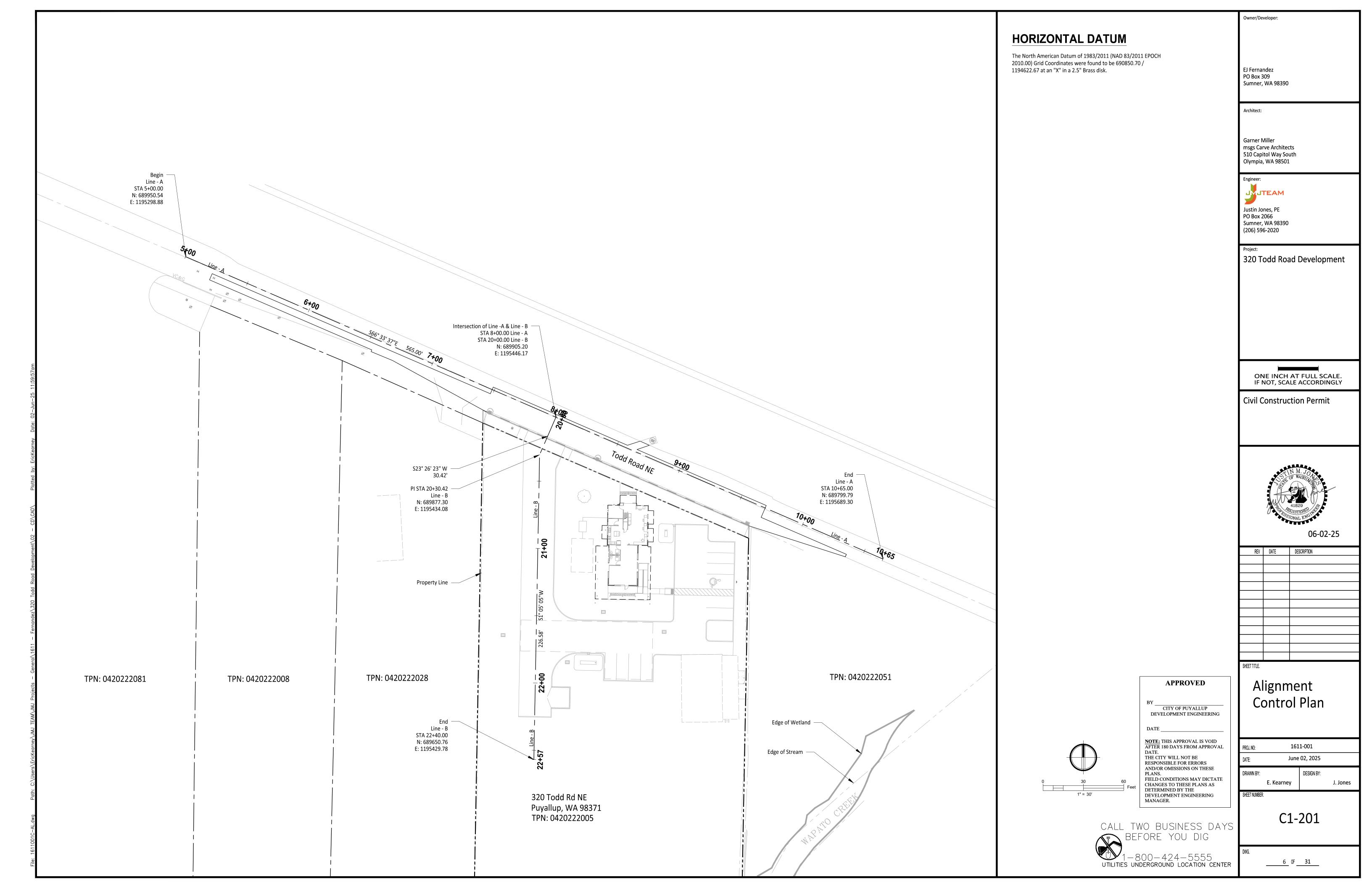
J. Jones

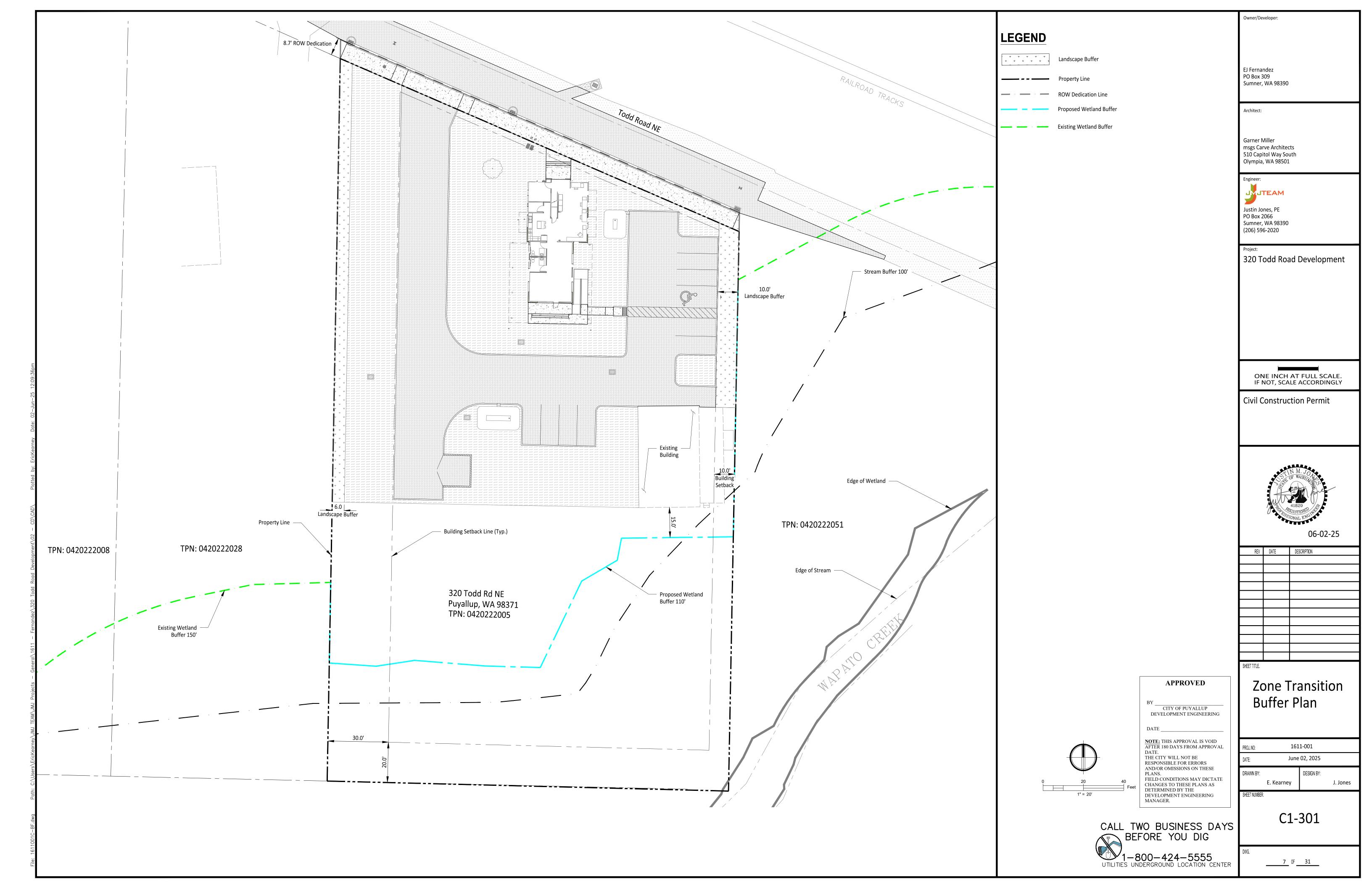
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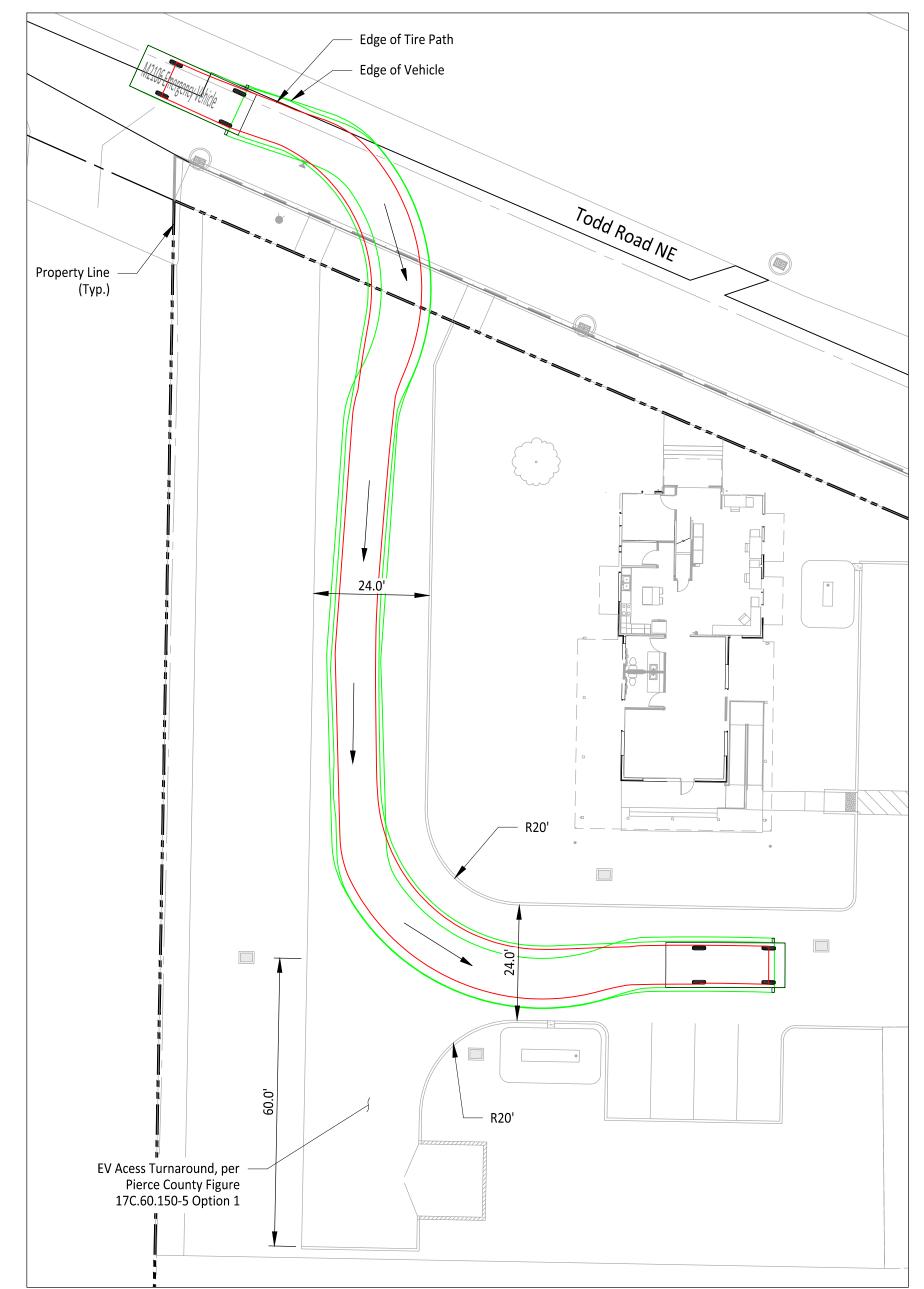
BEFORE YOU DIG UTILITIES UNDERGROUND LOCATION CENTER

CALL TWO BUSINESS DAYS











## **TURNING MOVEMENT NOTES:**

Turning movements based upon M2106 Emergency Vehicle and information provided by Central Pierce Fire Department.

Owner/Developer:

EJ Fernandez PO Box 309 Sumner, WA 98390

Architect:

Garner Miller msgs Carve Architects 510 Capitol Way South Olympia, WA 98501



Justin Jones, PE PO Box 2066 Sumner, WA 98390 (206) 596-2020

320 Todd Road Development

ONE INCH AT FULL SCALE. IF NOT, SCALE ACCORDINGLY

Civil Construction Permit



06-02-25

REV	DATE	DESCRIPTION

APPROVED

FIRE HYDRANT/FDC LOCATION/ACCESS APPROVED

NOTE: THIS APPROVAL IS VOID AFTER 180 DAYS FROM APPROVAL

AFTER 180 DAYS FROM APPROVAL DATE.
THE CITY WILL NOT BE
RESPONSIBLE FOR ERRORS
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PLANS.
FIELD CONDITIONS MAY DICTATE
CHANGES TO THESE PLANS AS
DETERMINED BY THE FIRE CODE
OFFICIAL.

CALL TWO BUSINESS DAYS

BEFORE YOU DIG

1-800-424-5555

UTILITIES UNDERGROUND LOCATION CENTER

BY \_\_\_\_\_CITY OF PUYALLUP FIRE CODE OFFICIAL

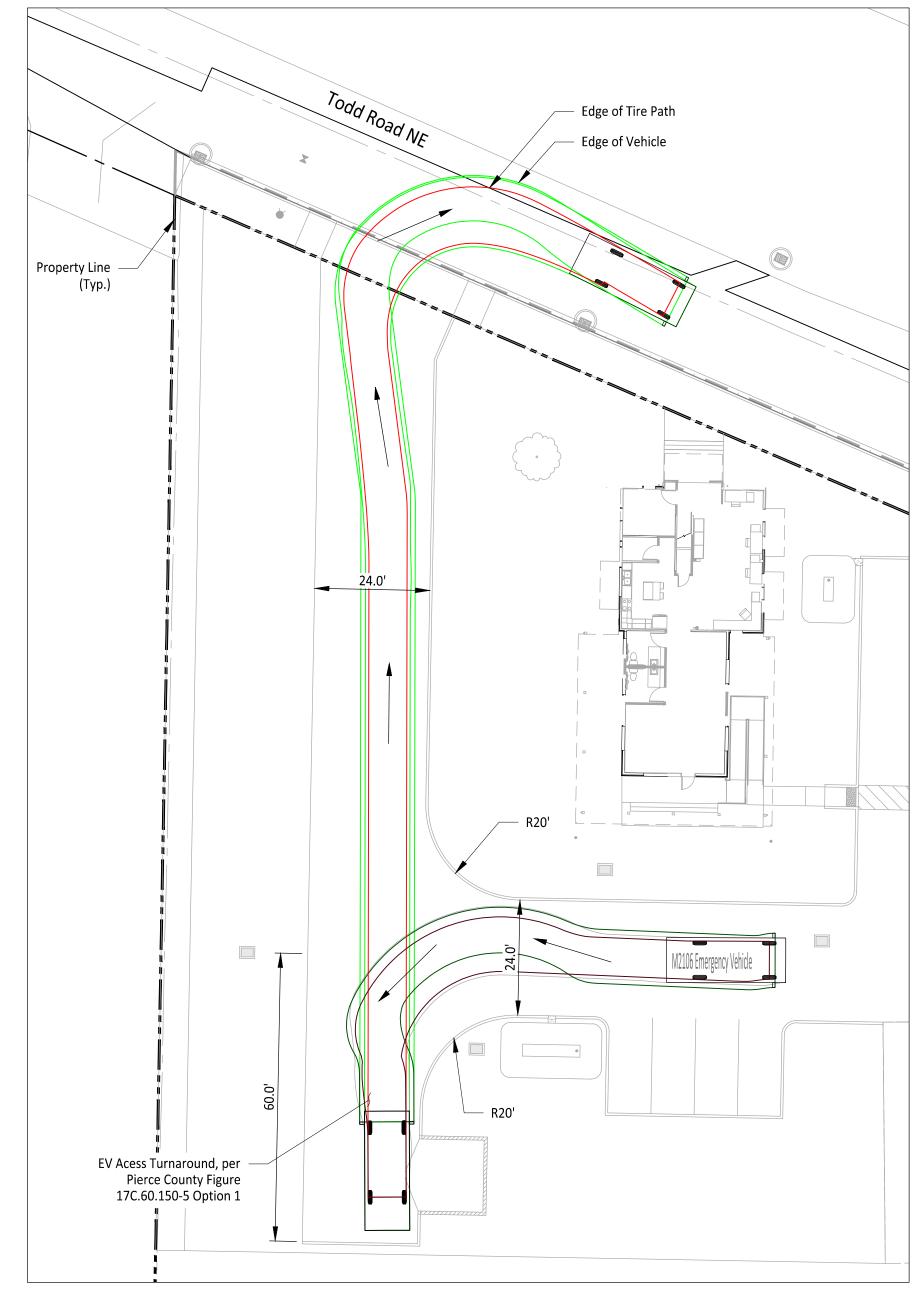
Fire Turning Movement BY \_\_\_\_\_\_\_
CITY OF PUYALLUP
DEVELOPMENT ENGINEERING

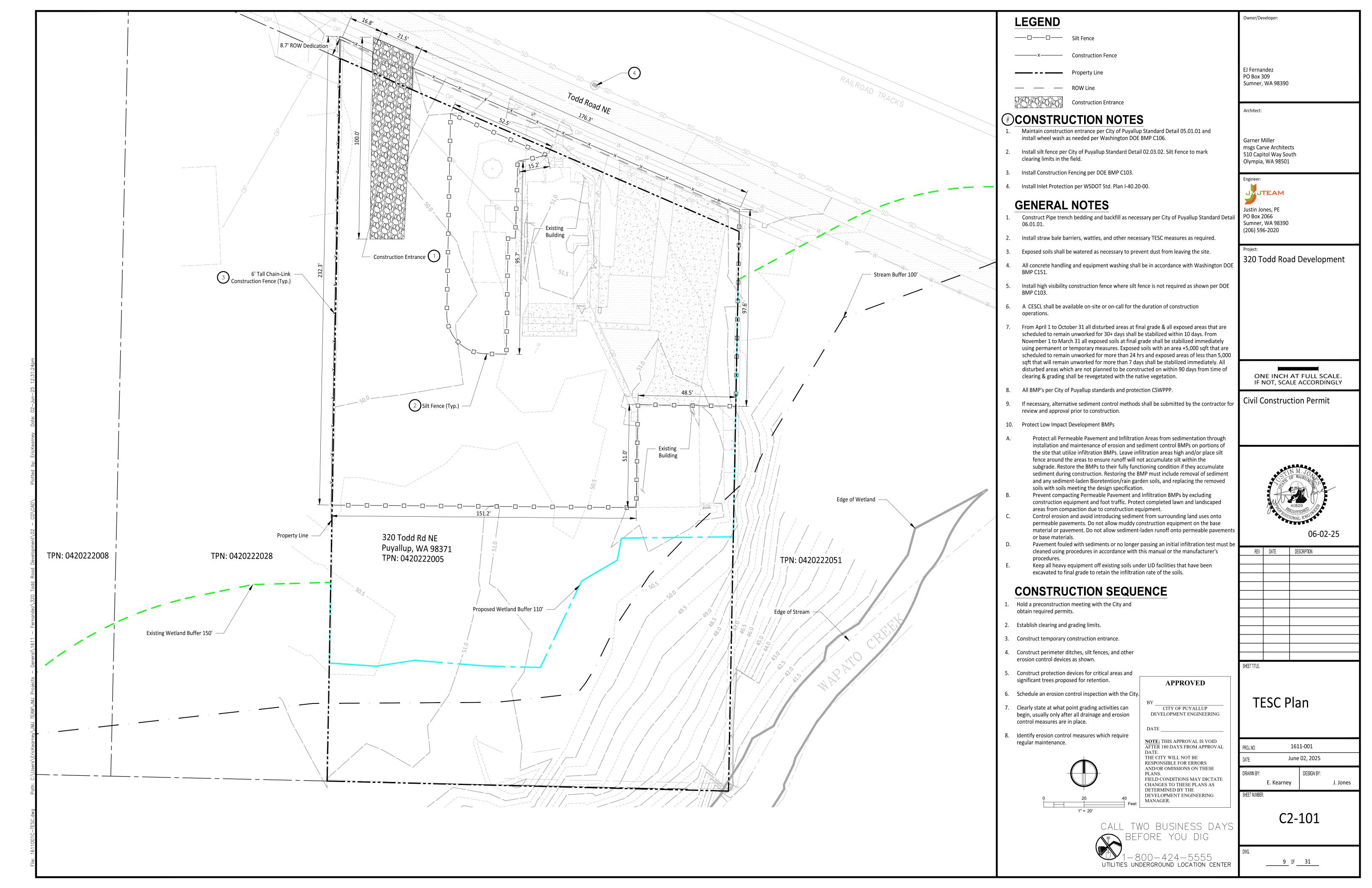
NOTE: THIS APPROVAL IS VOID AFTER 180 DAYS FROM APPROVAL DATE.	PROJ. NO:	161	1-001
THE CITY WILL NOT BE RESPONSIBLE FOR ERRORS	DATE:	June	02, 2025
AND/OR OMISSIONS ON THESE PLANS. FIELD CONDITIONS MAY DICTATE	DRAWN BY:	E. Kearney	DESIGN BY:
CHANGES TO THESE PLANS AS DETERMINED BY THE DEVELOPMENT ENGINEERING	SHEET NUMBE		

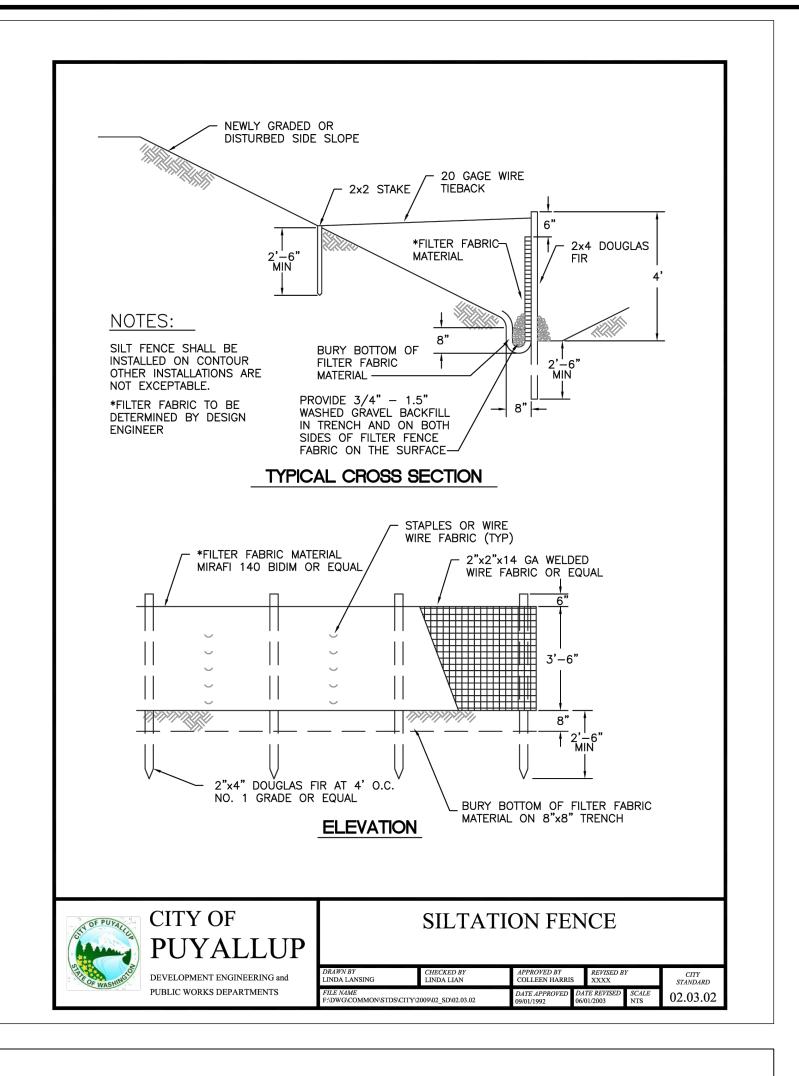
E. Kearney SHEET NUMBER.

C1-401

\_\_\_\_\_8 OF \_\_\_31







CONDITIONS WHERE PRACTICE APPLIES

AND FLAT AREA (LESS THAN 5% SLOPE).

BUT NO GREATER THAN 24-INCHES HIGH.

1/2-INCHES LONG.

CITY OF

1. BLOCK AND GRAVEL FILTER - APPLICABLE FOR AREAS GREATER THAN 5% SLOPE.

1. BLOCK AND GRAVEL FILTER - INSTALLATION PROCEDURE

OF MESH IS NECESSARY, OVERLAP THE STRIPS. PLACE FILTER FABRIC\* OVER WIRE MESH.

HIEGHT OF THE BARRIER CAN BE VARIED, DEPENDING ON DESIGN NEEDS, BY STACKING COMBINATIONS OF

D: PILE STONES AGAINST THE WIRE MESH TO THE TOP OF THE BLOCKS. USE 3/4" MINUS WASHED GRAVEL.

APART AND DRIVE THEM AT LEAST 8-INCHES INTO THE GROUND. THE STAKES MUST BE AT LEAST 3 FEET

B: EXCAVATE A TRENCH APPROXIMATELY 8-INCHES WIDE AND 12-INCHES DEEP AROUND THE OUTSIDE

C: STAPLE THE FILTER FABRIC\* TO THE WOODEN STAKES SO THAT 32-INCHES OF THE FABRIC EXTENDS AND CAN BE FORMED INTO THE TRENCH, AND USE HEAVY-DUTY WIRE STAPLES AT LEAST

A: EXCAVATE A 4-INCH DEEP TRENCH AROUND THE INLET. MAKE THE TRENCH AS WIDE AS A STRAW BALE.

B: ORIENT STRAW BALES WITH THE BINDINGS AROUND THE SIDES OF THE BALES RATHER THAN OVER AND

C: PLACE BALES LENGTHWISE AROUND THE INLET AND PRESS THE ENDS OF ADJACENT BALES SECURELY

F: WEDGE LOOSE STRAW BETWEEN BALES TO PREVENT WATER FROM FLOWING BETWEEN BALES.

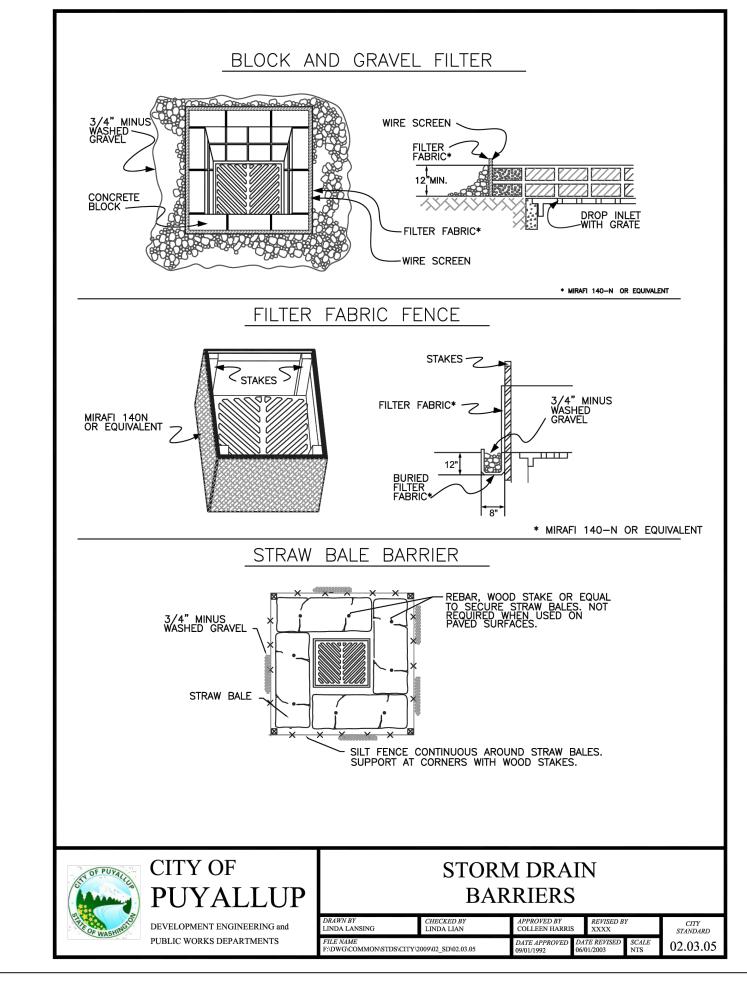
D: DRIVE TWO 2-INCH BY 2-INCH STAKES THROUGH EACH BALE TO ANCHOR THE BALE SECURELY IN PLACE.

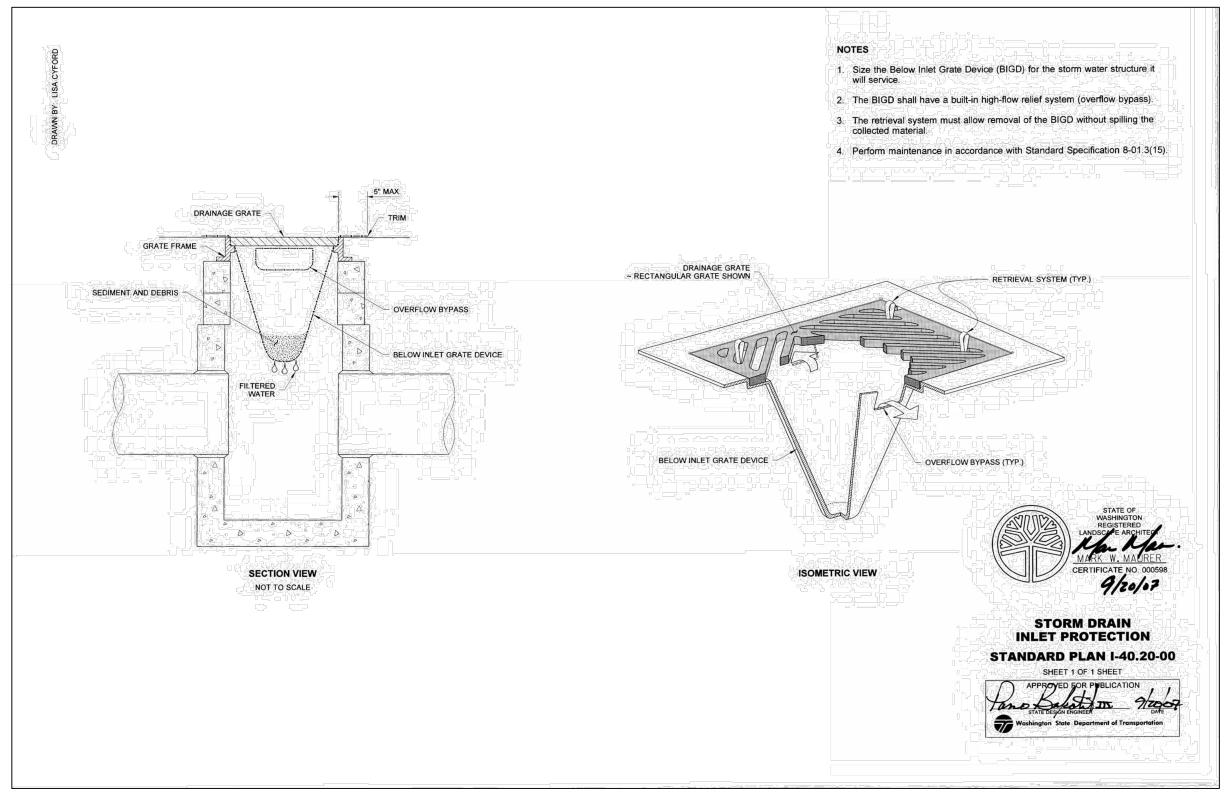
2. FILTER FABRIC FENCE - INSTALLATION PROCEDURE

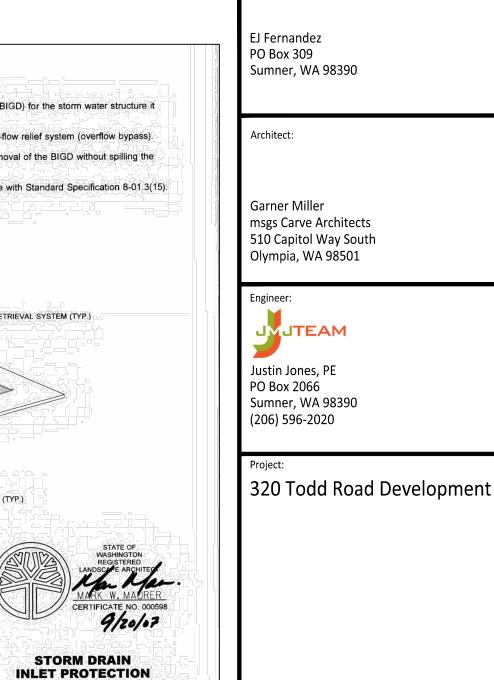
D: BACKFILL THE TRENCH WITH 3/4-INCH MINUS WASHED GRAVEL ALL THE WAY AROUND.

3. STRAW BALE BARRIER — INSTALLATION PROCEDURE

E: BACKFILL THE EXCAVATED SOIL AND COMPACT IT AGAINST THE BALE.







Owner/Developer:

ONE INCH AT FULL SCALE. IF NOT, SCALE ACCORDINGLY

**Civil Construction Permit** 



06-02-25

REV	DATE	DESCRIPTION
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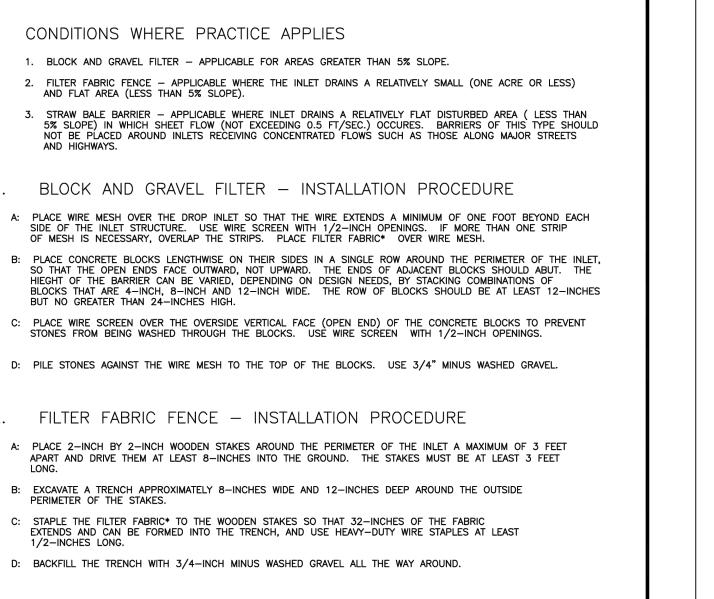
SHEET NUMBER.

**TESC Details** 

1611-001 June 02, 2025

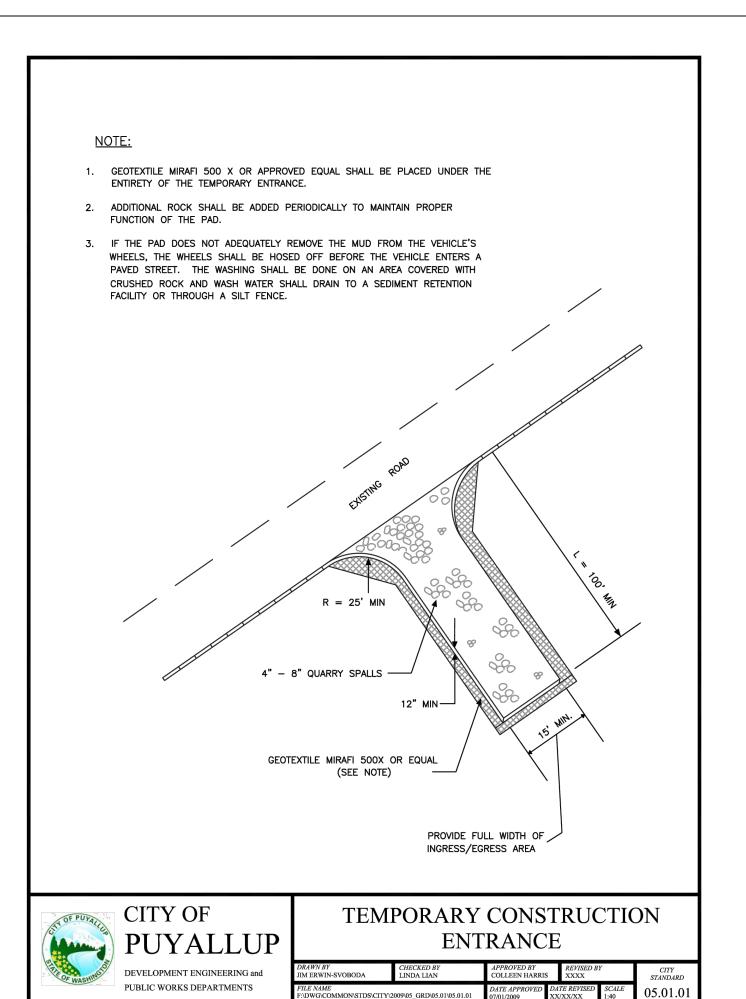
DESIGN BY: E. Kearney

C2-201



\* MIRAFI 140-N OR EQUIVALENT

STORM DRAIN



1. ALL LIMITS OF CLEARING AND AREAS OF VEGETATION PRESERVATION AS PRESCRIBED ON THE PLANS SHALL BE CLEARLY FLAGGET
IN THE FIELD AND OBSERVED DURING CONSTRUCTION.
2. ALL REQUIRED SEDIMENTATION AND EROSION CONTROL FACILITIES MUST BE CONSTRUCTED AND IN OPERATION PRIOR TO ANY LAM
CLEARING AND/OR OTHER CONSTRUCTION TO ENSURE THAT SEDIMENT LADEN WATER DOES NOT ENTER THE NATURAL DRAINAGE
SYSTEM. THE CONTRACTOR SHALL SCHEDULE AN INSPECTION OF THE EROSION CONTROL FACILITIES PRIOR TO ANY LAND CLEARING

AND/OR CONSTRUCTION. ALL EROSION AND SEDIMENT FACILITIES SHALL BE MAINTAINED IN A SATISFACTORY CONDITION AS DETERMINED BY THE CITY, UNTIL SUCH TIME THAT CLEARING AND/OR CONSTRUCTION IS COMPLETED AND THE POTENTIAL FOR ON-SITE EROSION HAS PASSED. THE IMPLEMENTATION, MAINTENANCE, REPLACEMENT, AND ADDITIONS TO THE EROSION AND SEDIMENTATION CONTROL SYSTEMS SHALL BE THE RESPONSIBILITY OF THE PERMITEE.

3. THE EROSION AND SEDIMENTATION CONTROL SYSTEM FACILITIES DEPICTED ON THESE PLANS ARE INTENDED TO BE MINIMUM REQUIREMENTS TO MEET ANTICIPATED SITE CONDITIONS. AS CONSTRUCTION PROGRESSES AND UNEXPECTED OR SEASONAL CONDITIONS DICTATE, FACILITIES WILL BE NECESSARY TO ENSURE COMPLETE SILTATION CONTROL ON THE SITE. DURING THE COURSE OF CONSTRUCTION, IT SHALL BE THE OBLIGATION AND RESPONSIBILITY OF THE PERMITEE TO ADDRESS ANY NEW CONDITIONS THAT MAY BE CREATED BY HIS ACTIVITIES AND TO PROVIDE ADDITIONAL FACILITIES, OVER AND ABOVE THE MINIMUM REQUIREMENTS, AS MAY BE NEEDED TO PROTECT ADJACENT PROPERTIES, SENSITIVE AREAS, NATURAL WATER COURSES, AND/OR STORM DRAINAGE SYSTEMS.

4. APPROVAL OF THESE PLANS IS FOR GRADING, TEMPORARY DRAINAGE, EROSION AND SEDIMENTATION CONTROL ONLY. IT DOES NOT CONSTITUTE AN APPROVAL OF PERMANENT STORM DRAINAGE DESIGN, SIZE OR LOCATION OF PIPES, RESTRICTORS, CHANNELS, OR RETENTION FACILITIES.

5. ANY DISTURBED AREA WHICH HAS BEEN STRIPPED OF VEGETATION AND WHERE NO FURTHER WORK IS ANTICIPATED FOR A PERIOD OF 30 DAYS OR MORE, MUST BE IMMEDIATELY STABILIZED WITH MULCHING, GRASS PLANTING, OR OTHER APPROVED EROSION CONTROL TREATMENT APPLICABLE TO THE TIME OF YEAR IN QUESTION. GRASS SEEDING ALONE WILL BE ACCEPTABLE ONLY DURING THE MONTHS OF APRIL THROUGH SEPTEMBER INCLUSVE. SEEDING MAY PROCEED OUTSIDE THE SPECIFIED TIME PERIOD WHENEVER IT IS IN THE INTEREST OF THE PERMITEE BUT MUST BE AUGMENTED WITH MULCHING, NETTING, OR OTHER TREATMENT APPROVED BY THE

6. IN CASE EROSION OR SEDIMENTATION OCCURS TO ADJACENT PROPERTIES, ALL CONSTRUCTION WORK WITHIN THE DEVELOPMENT THAT WILL FURTHER AGGRAVATE THE SITUATION MUST CEASE, AND THE OWNER/CONTRACTOR WILL IMMEDIATELY COMMENCE RESTORATION METHODS. RESTORATION ACTIVITY WILL CONTINUE UNTIL SUCH TIME AS THE AFFECTED PROPERTY OWNER IS SATISFIED.

7. NO TEMPORARY OR PERMANENT STOCKPILING OF MATERIALS OR EQUIPMENT SHALL OCCUR WITHIN CRITICAL AREAS OR ASSOCIATED BUFFERS, OR THE CRITICAL ROOT ZONE FOR VEGETATION PROPOSED FOR RETENTION.

TY OF PUYALL	CITY OF
	PUYALLUP
SET OF WASHINGTON	DEVELOPMENT ENGINEERING and PUBLIC WORKS DEPARTMENTS

GRADING, EROSION, AND SEDIMENTATION CONTROL NOTES

CALL TWO BUSINESS DAYS BEFORE YOU DIG

-800-424-5555 UTILITIES UNDERGROUND LOCATION CENTER

MANAGER.

APPROVED

CITY OF PUYALLUP

**NOTE:** THIS APPROVAL IS VOID

THE CITY WILL NOT BE

DETERMINED BY THE

RESPONSIBLE FOR ERRORS

AND/OR OMISSIONS ON THESE

FIELD CONDITIONS MAY DICTATE

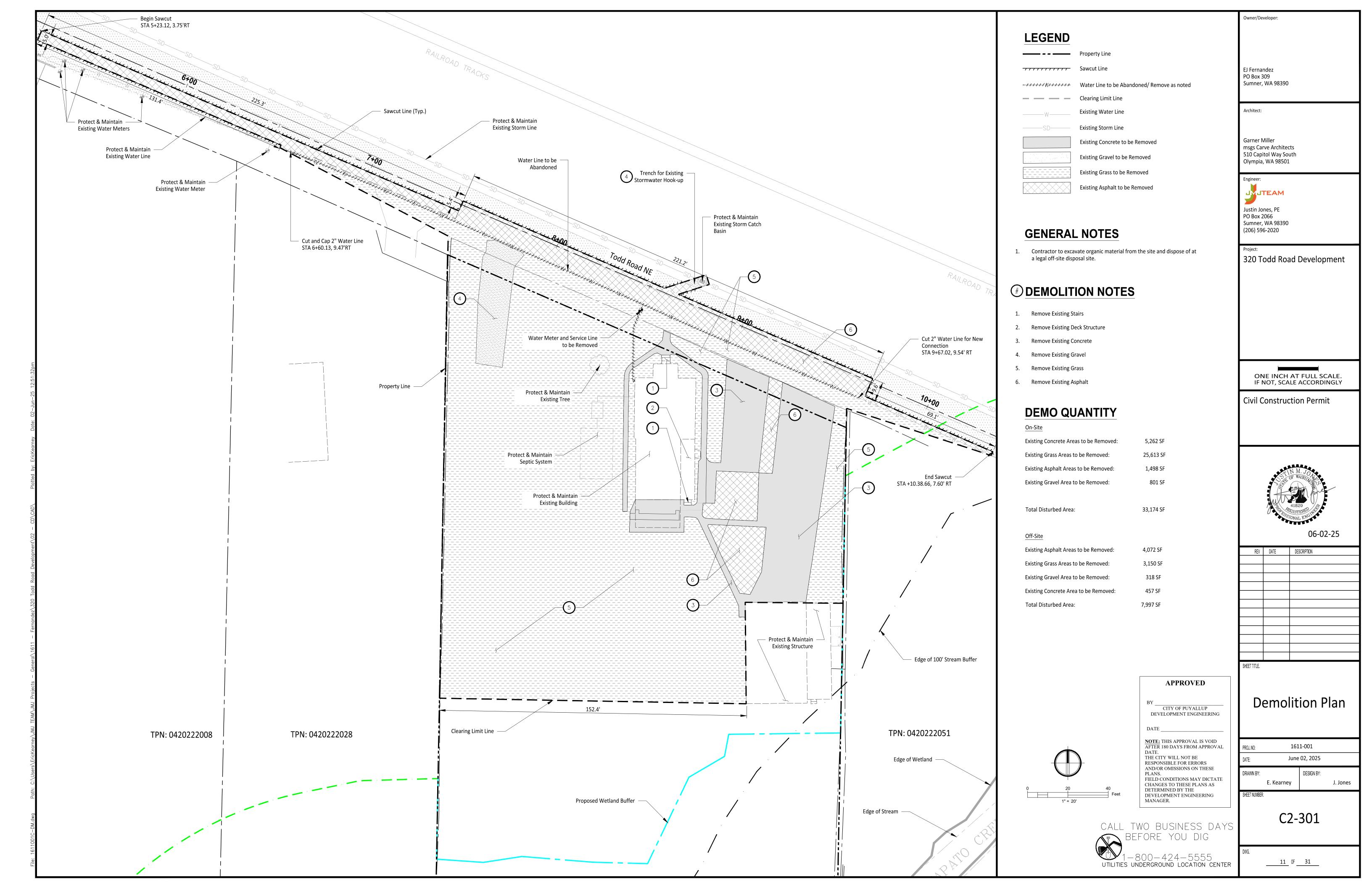
CHANGES TO THESE PLANS AS

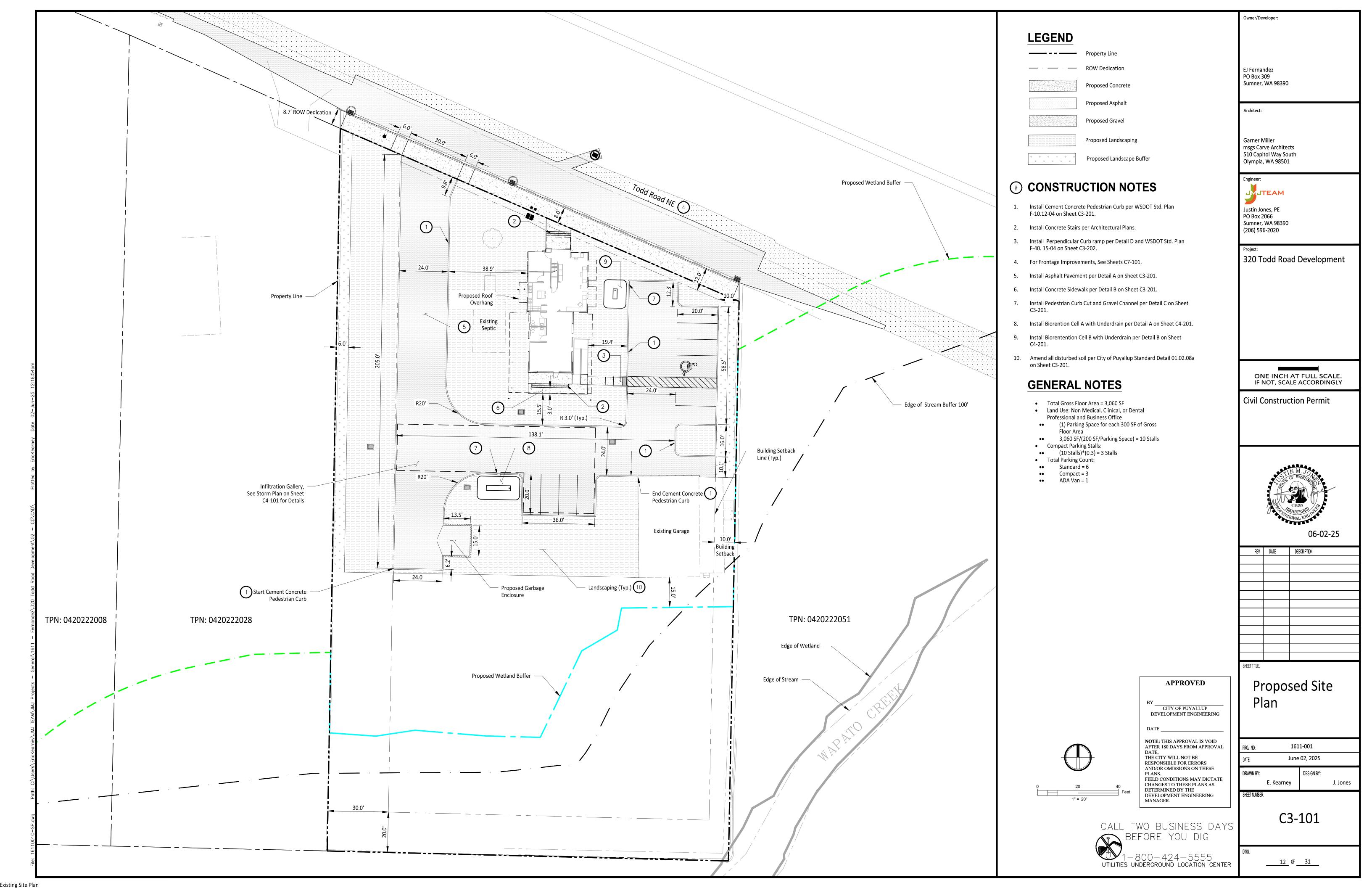
DEVELOPMENT ENGINEERING

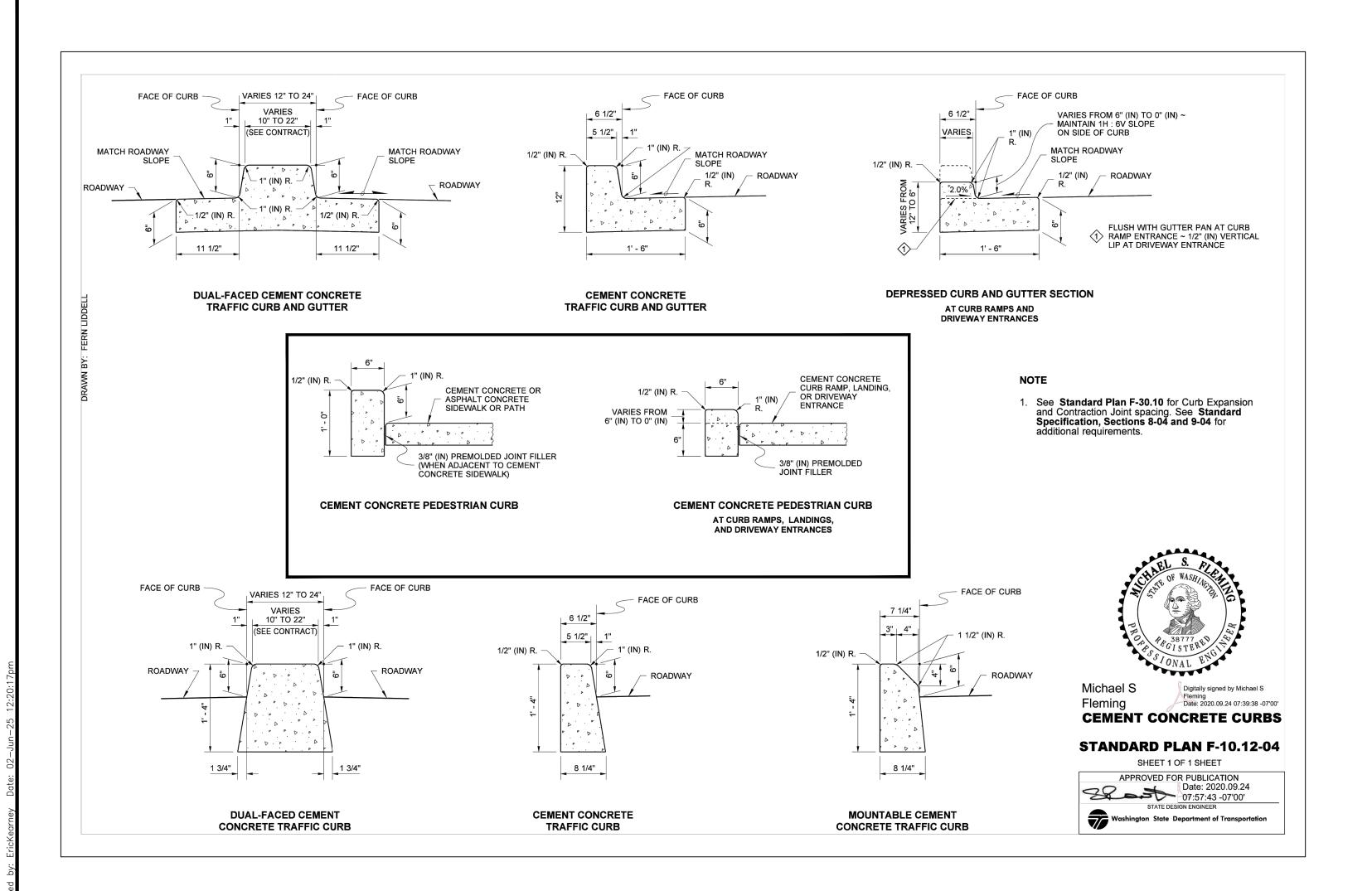
AFTER 180 DAYS FROM APPROVAL

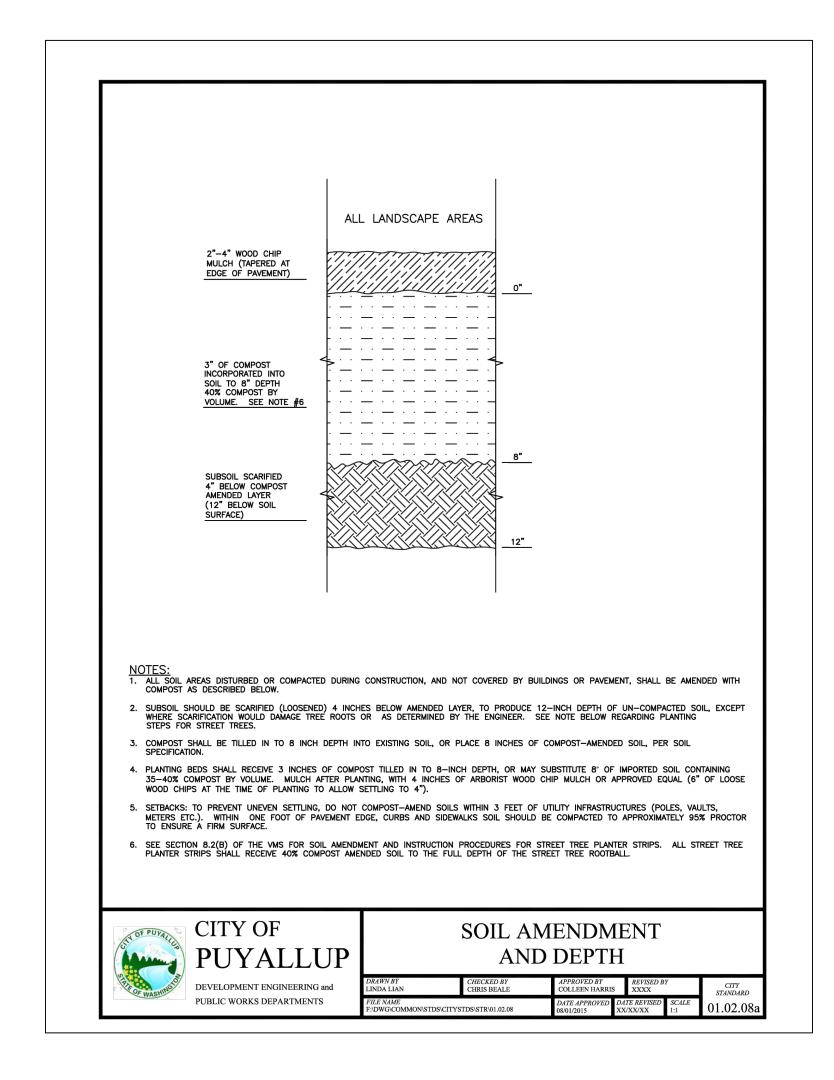
DEVELOPMENT ENGINEERING

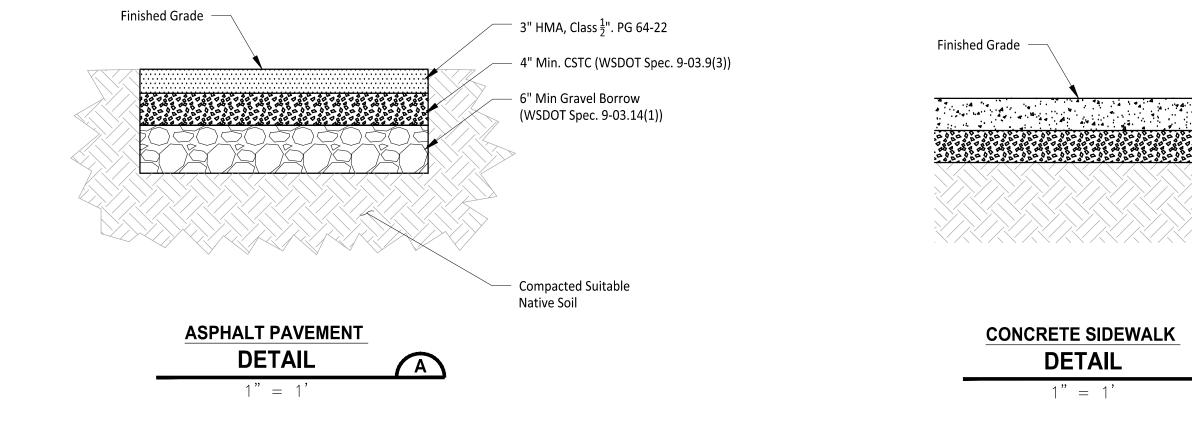
PUYALLUP **BARRIERS NOTES** PUBLIC WORKS DEPARTMENTS 02.03.06

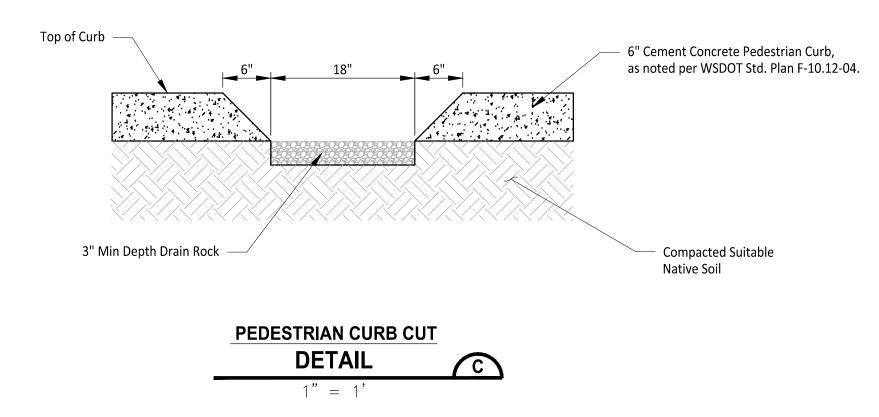












4" Min Class 3000 Concrete

(WSDOT Spec. 6-02.3(2)b)

4" Crushed Surfacing Base Course

Compacted Suitable

Native Soil

APPROVED

BY \_\_\_\_\_\_ CITY OF PUYALLUP DEVELOPMENT ENGINEERING

NOTE: THIS APPROVAL IS VOID
AFTER 180 DAYS FROM APPROVAL
DATE.
THE CUTY WILL NOT BE

AFTER 180 DAYS FROM APPROVAL DATE.
THE CITY WILL NOT BE
RESPONSIBLE FOR ERRORS
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PLANS.
FIELD CONDITIONS MAY DICTATE
CHANGES TO THESE PLANS AS
DETERMINED BY THE
DEVELOPMENT ENGINEERING
MANAGER.

CALL TWO BUSINESS DAYS
BEFORE YOU DIG

Garner Miller

msgs Carve Architects 510 Capitol Way South Olympia, WA 98501

Owner/Developer:

EJ Fernandez

PO Box 309

Architect:

Sumner, WA 98390



Justin Jones, PE PO Box 2066 Sumner, WA 98390 (206) 596-2020

Project:

320 Todd Road Development

ONE INCH AT FULL SCALE. IF NOT, SCALE ACCORDINGLY

Civil Construction Permit



DESCRIPTION

06-02-25

·	

SHEET TITLE.

REV DATE

Hardscape Details

 PROJ.NO:
 1611-001

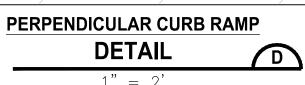
 DATE:
 June 02, 2025

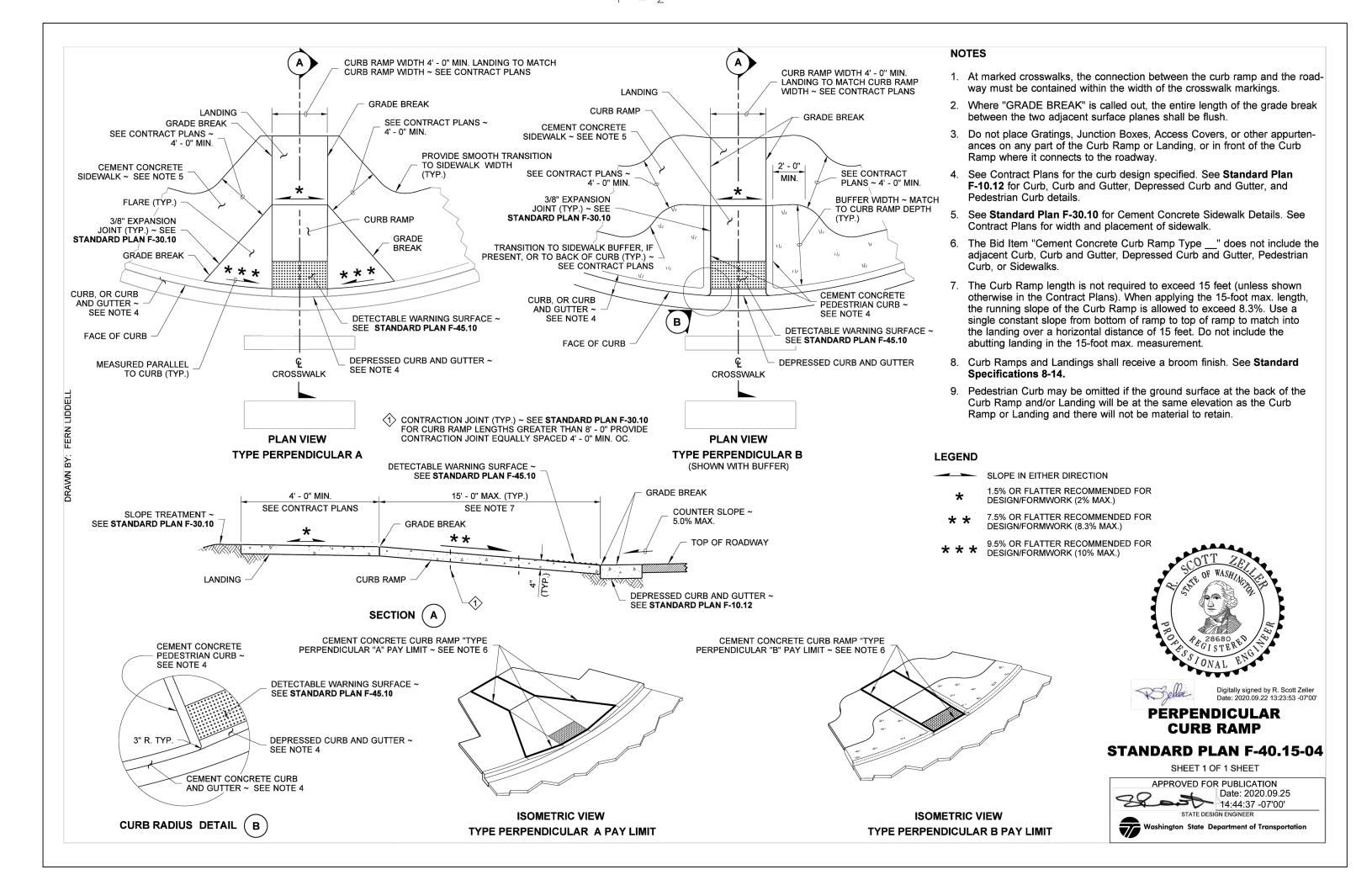
 DRAWN BY:
 DESIGN BY:

 E. Kearney
 J. Jones

SHEET NUMBER.

C3-201





Owner/Developer:

EJ Fernandez PO Box 309 Sumner, WA 98390

Architect:

Garner Miller msgs Carve Architects 510 Capitol Way South Olympia, WA 98501



Justin Jones, PE PO Box 2066 Sumner, WA 98390 (206) 596-2020

320 Todd Road Development

ONE INCH AT FULL SCALE. IF NOT, SCALE ACCORDINGLY

**Civil Construction Permit** 



DESCRIPTION

06-02-25

·	

DESIGN BY:

J. Jones

SHEET TITLE.

# Hardscape Details

**NOTE:** THIS APPROVAL IS VOID 1611-001 AFTER 180 DAYS FROM APPROVAL June 02, 2025

SHEET NUMBER.

THE CITY WILL NOT BE RESPONSIBLE FOR ERRORS AND/OR OMISSIONS ON THESE

**APPROVED** 

CITY OF PUYALLUP DEVELOPMENT ENGINEERING

FIELD CONDITIONS MAY DICTATE CHANGES TO THESE PLANS AS DETERMINED BY THE DEVELOPMENT ENGINEERING MANAGER.

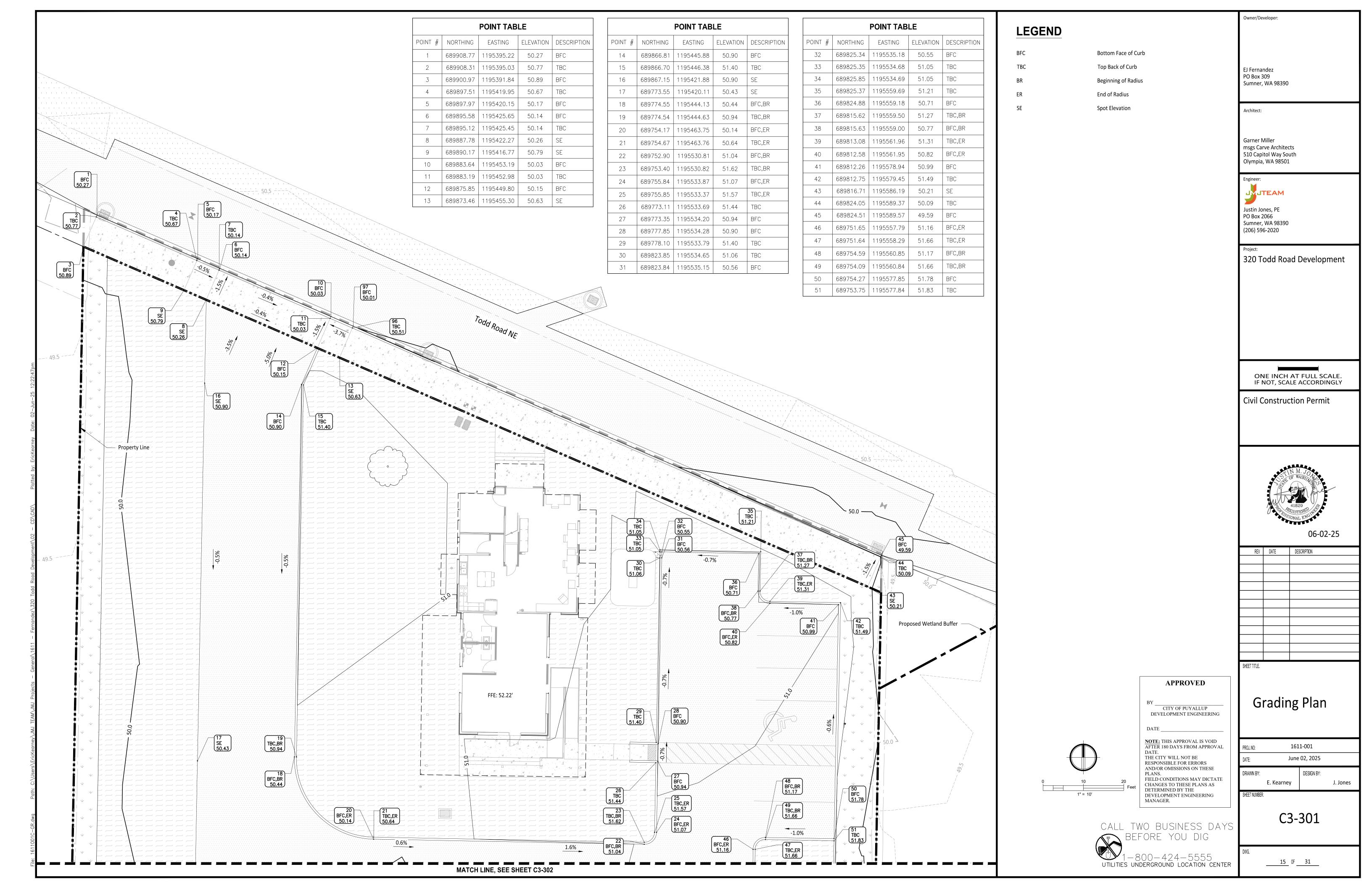
C3-202

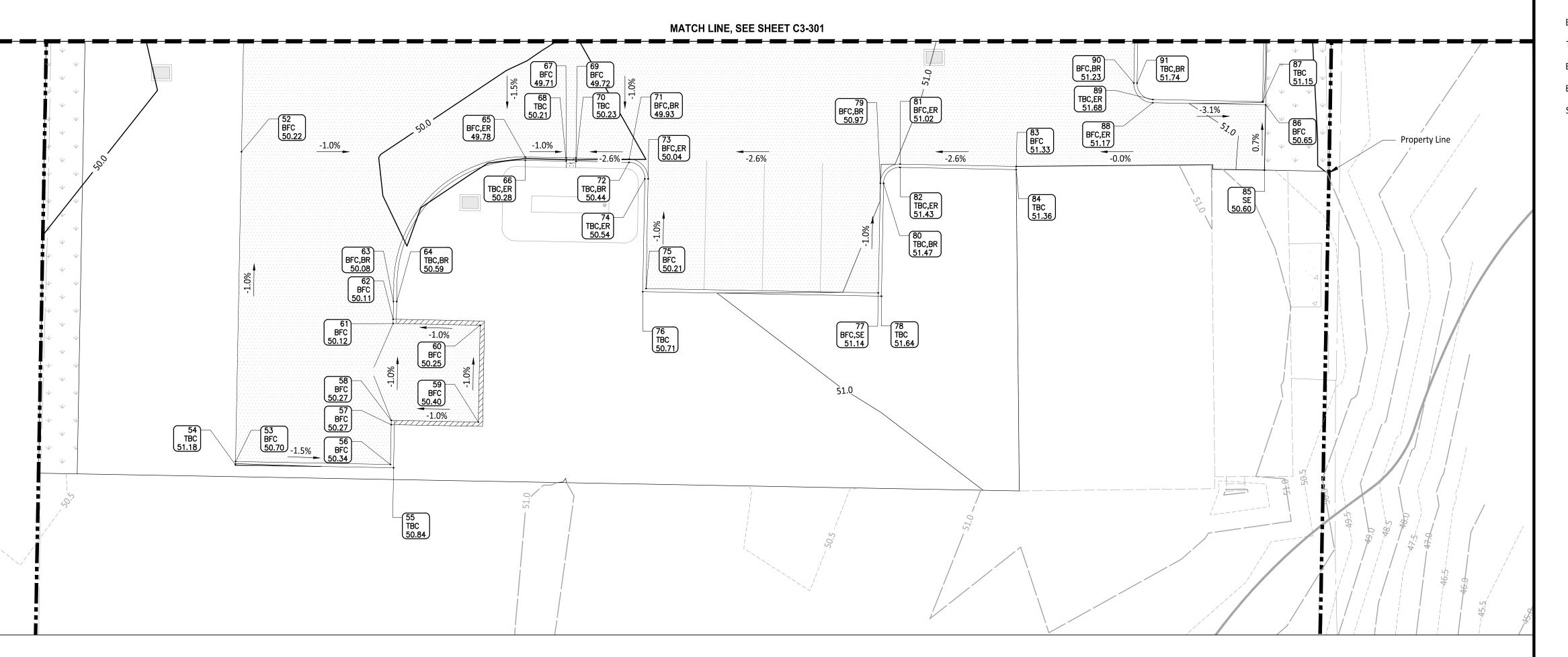
E. Kearney

\_\_\_\_14 OF \_\_\_31 UTILITIES UNDERGROUND LOCATION CENTER

CALL TWO BUSINESS DAYS BEFORE YOU DIG -800-424-5555

DATE





		POINT TAB	LE	
POINT #	NORTHING	EASTING	ELEVATION	DESCRIPTION
52	689731.00	1195419.30	50.22	BFC
53	689683.02	1195418.40	50.70	BFC
54	689682.52	1195418.39	51.18	TBC
55	689682.05	1195442.88	50.84	TBC
56	689682.56	1195442.39	50.34	BFC
57	689688.73	1195442.51	50.27	BFC
58	689689.39	1195442.52	50.27	BFC
59	689689.14	1195456.02	50.40	BFC
60	689704.14	1195456.30	50.25	BFC
61	689704.39	1195442.80	50.12	BFC
62	689705.06	1195442.82	50.11	BFC
63	689707.81	1195442.87	50.08	BFC,BR
64	689707.80	1195443.37	50.59	TBC,BR
65	689730.18	1195463.30	49.78	BFC,ER
66	689729.68	1195463.29	50.28	TBC,ER
67	689730.06	1195469.64	49.71	BFC
68	689729.56	1195469.63	50.21	TBC
69	689730.03	1195471.14	49.72	BFC
70	689729.50	1195471.16	50.23	TBC
71	689729.87	1195479.39	49.93	BFC,BR
72	689729.37	1195479.38	50.44	TBC,BR
73	689726.81	1195482.33	50.04	BFC,ER
74	689726.82	1195481.83	50.54	TBC,ER
75	689709.82	1195482.01	50.21	BFC

		POINT TAB	LE	
POINT #	NORTHING	EASTING	ELEVATION	DESCRIPTION
76	689709.33	1195481.50	50.71	TBC
77	689709.14	1195518.00	51.14	BFC,SE
78	689708.63	1195518.49	51.64	TBC
79	689726.13	1195518.32	50.97	BFC,BR
80	689726.12	1195518.82	51.47	TBC,BR
81	689729.08	1195521.38	51.02	BFC,ER
82	689728.58	1195521.37	51.43	TBC,ER
83	689728.74	1195539.38	51.33	BFC
84	689728.24	1195539.37	51.36	TBC
85	689728.16	1195577.85	50.60	SE
86	689738.26	1195578.04	50.65	BFC
87	689738.77	1195577.55	51.15	TBC
88	689738.59	1195560.55	51.17	BFC,ER
89	689739.09	1195560.55	51.68	TBC,ER
90	689741.65	1195557.60	51.23	BFC,BR
91	689741.64	1195558.10	51.74	TBC,BR
96	689880.80	1195458.48	50.51	TBC
97	689881.26	1195458.68	50.01	BFC

## **LEGEND**

Bottom Face of Curb Top Back of Curb Beginning of Radius **End of Radius** 

**Spot Elevation** 

Owner/Developer:

EJ Fernandez PO Box 309 Sumner, WA 98390

Architect:

Garner Miller msgs Carve Architects 510 Capitol Way South Olympia, WA 98501

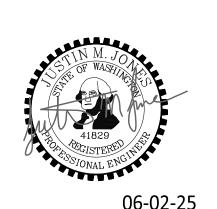


Justin Jones, PE PO Box 2066 Sumner, WA 98390 (206) 596-2020

320 Todd Road Development

ONE INCH AT FULL SCALE. IF NOT, SCALE ACCORDINGLY

Civil Construction Permit



**Grading Plan** 

1611-001

June 02, 2025

DESIGN BY:

NOTE: THIS APPROVAL IS VOID AFTER 180 DAYS FROM APPROVAL THE CITY WILL NOT BE
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CHANGES TO THESE PLANS AS
DETERMINED BY THE
DEVELOPMENT ENGINEERING MANAGER.

**APPROVED** 

BY \_\_\_\_\_\_\_CITY OF PUYALLUP
DEVELOPMENT ENGINEERING

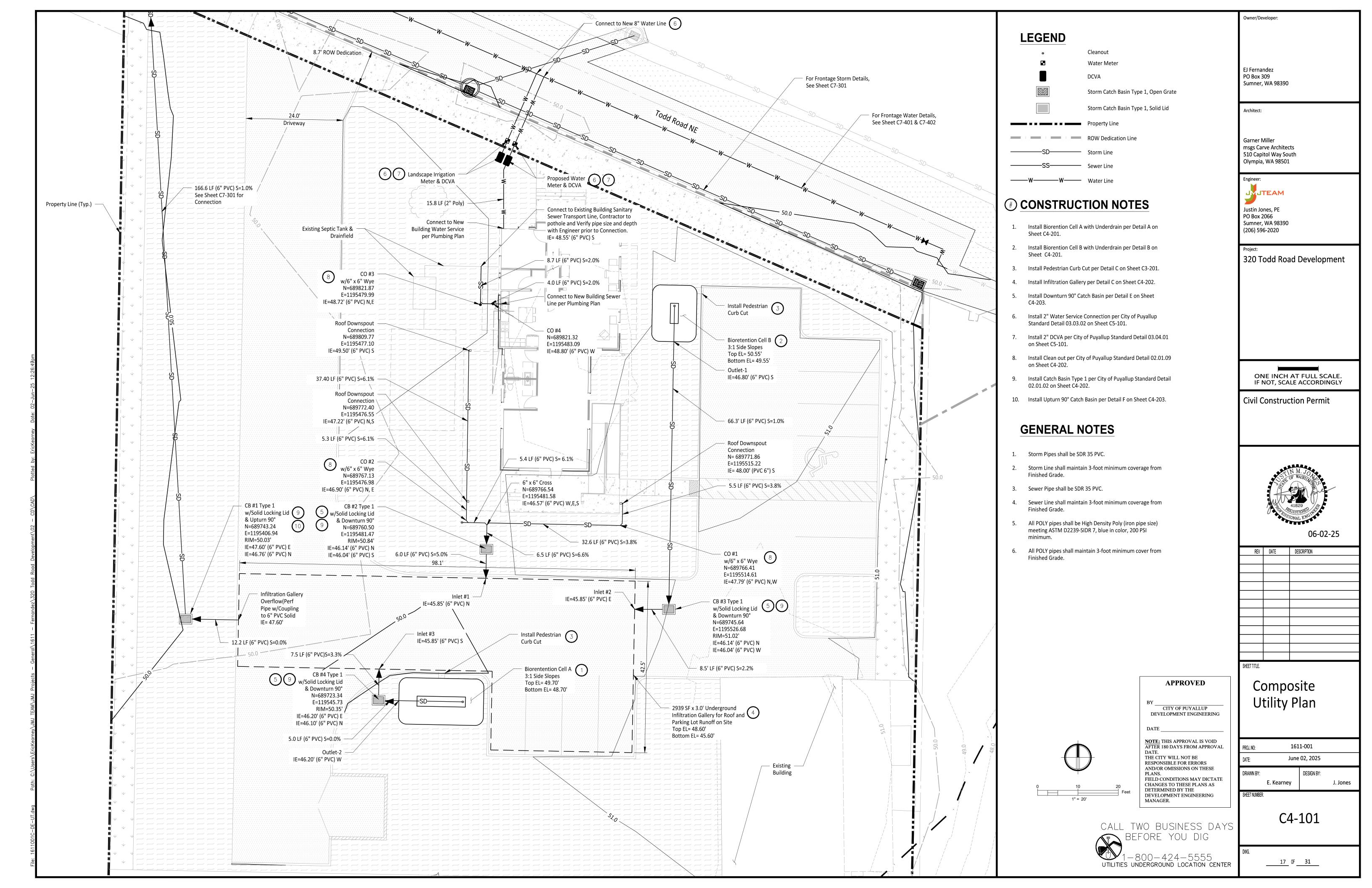
C3-302

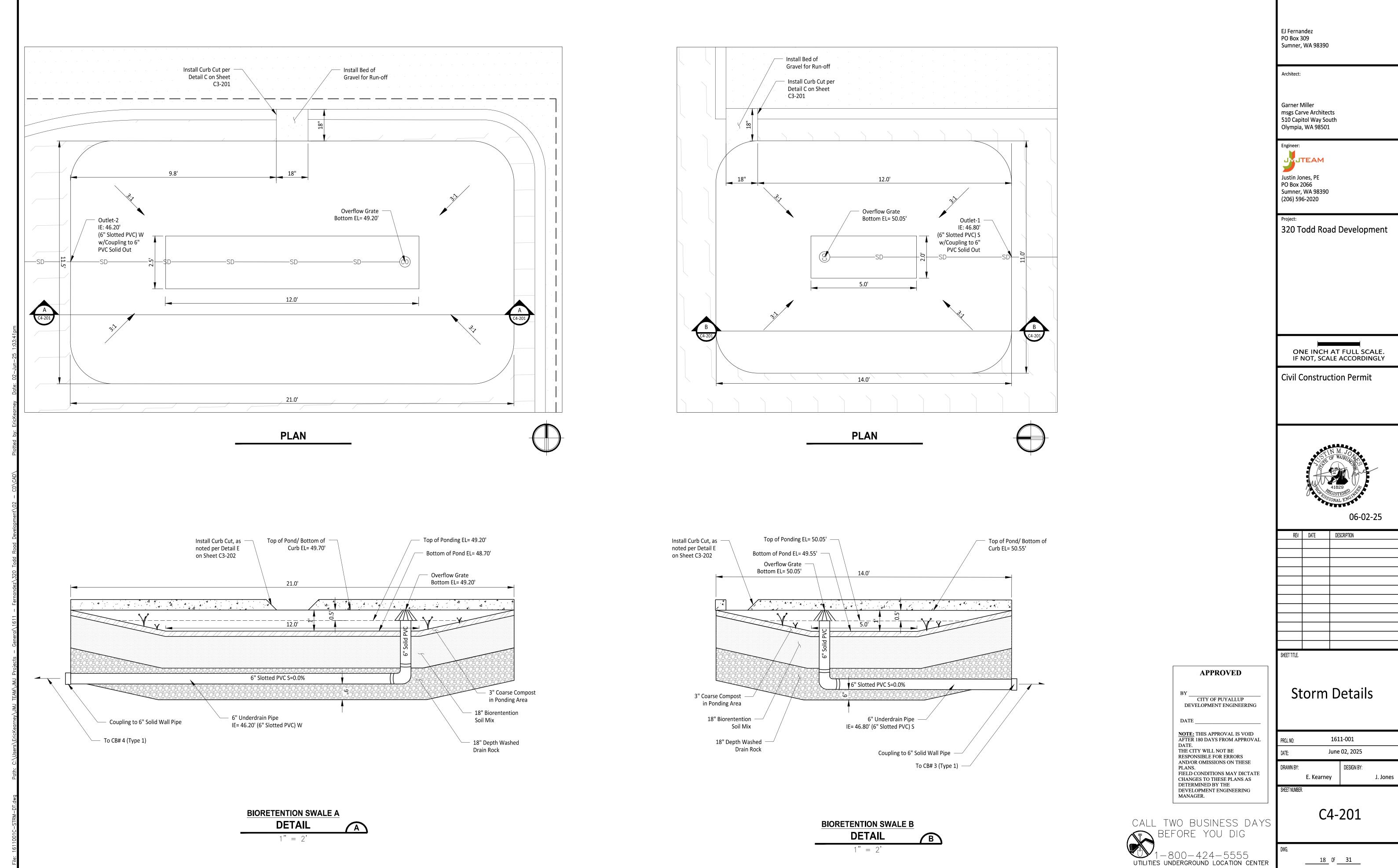
\_\_\_\_16 OF \_\_\_31

E. Kearney

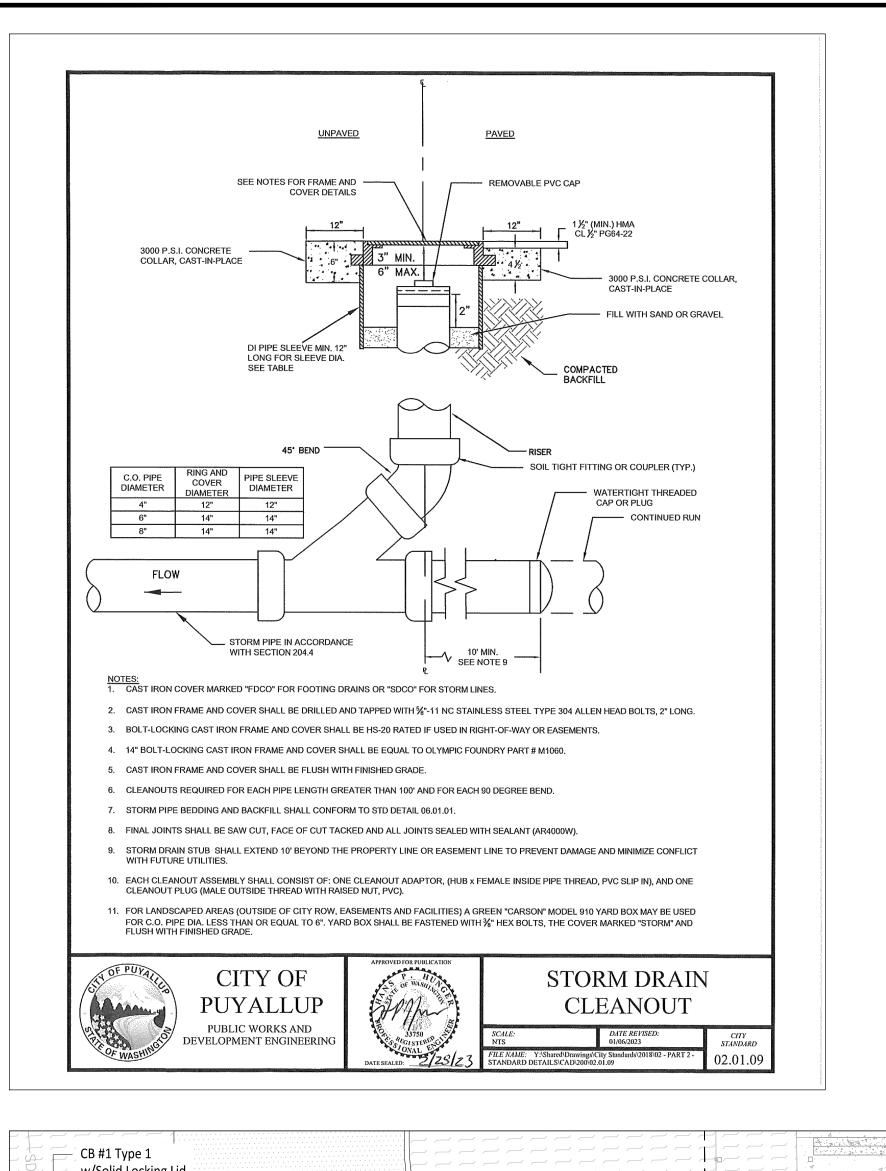
CALL TWO BUSINESS DAYS

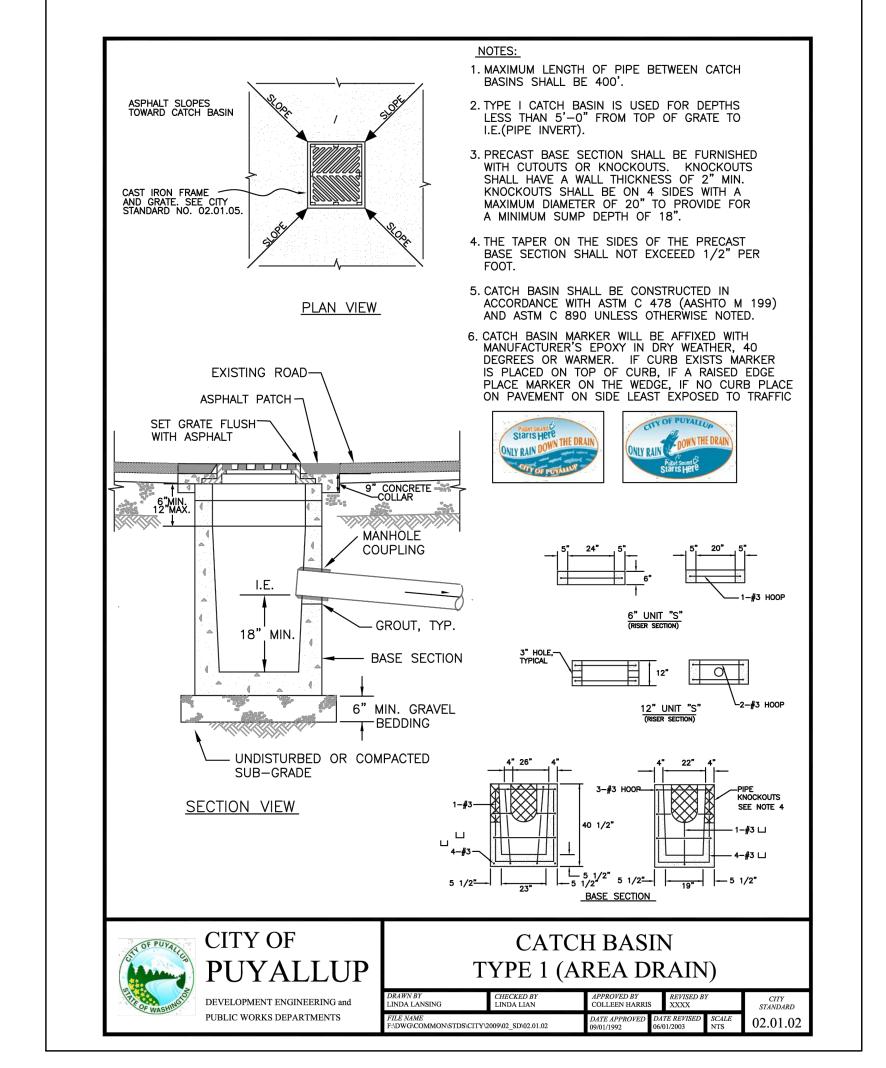
1-800-424-5555 UTILITIES UNDERGROUND LOCATION CENTER

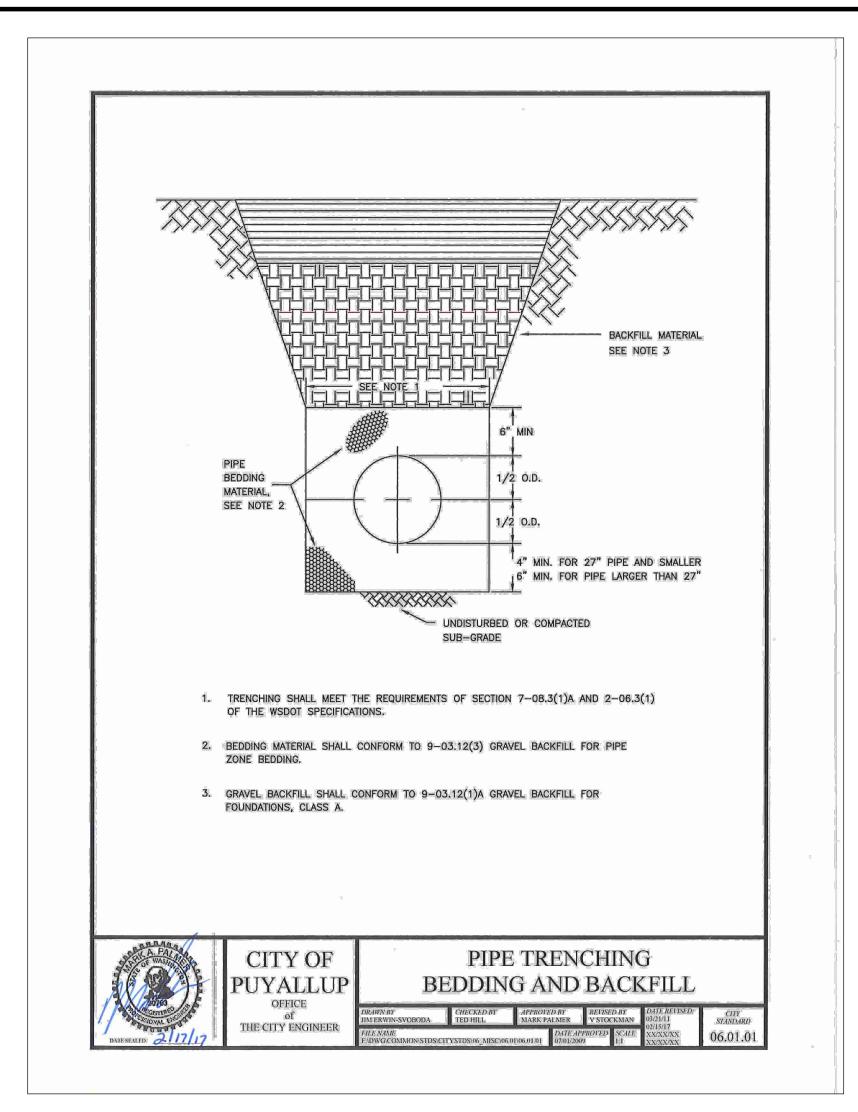




Owner/Developer:







- 2,939 SF x 3.0' Underground

Infiltration Gallery for Roof and

Asphalt Pavement Type 1,

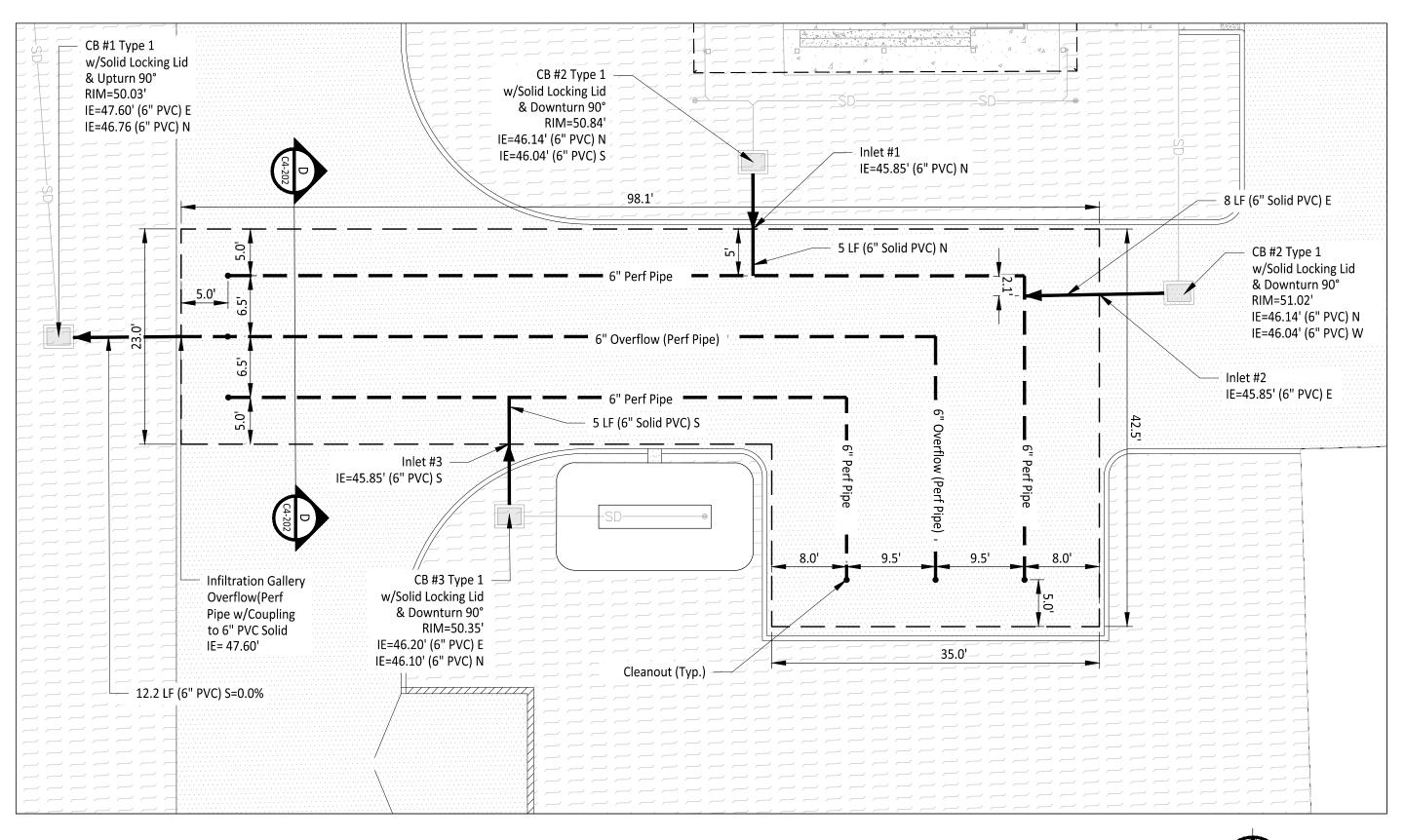
CALL TWO BUSINESS DAYS

BEFORE YOU DIG

-800-424-5555

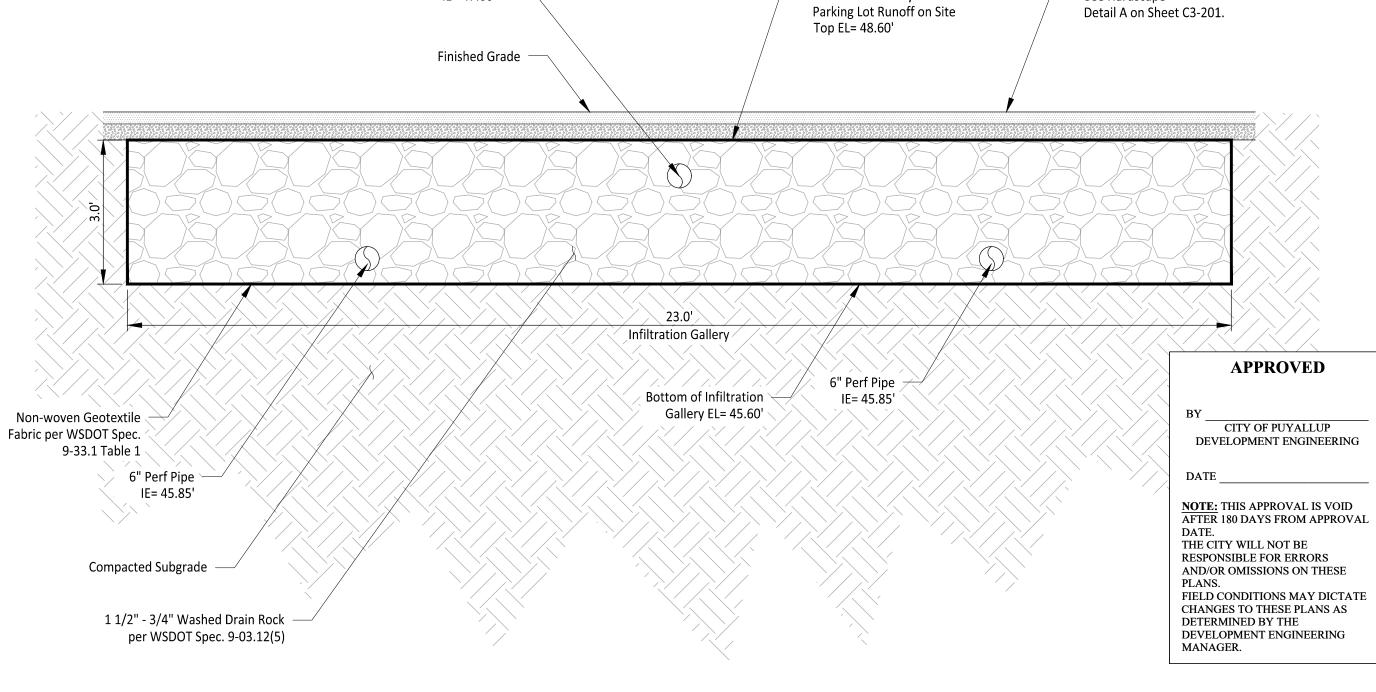
UTILITIES UNDERGROUND LOCATION CENTER

See Hardscape



**INFILTRATION GALLERY** 

1" = 10'



**INFILTRATION GALLERY** 

**DETAIL** 

1" = 2'

6" Overflow (Perf Pipe)

IE= 47.60'

Owner/Developer: EJ Fernandez PO Box 309 Sumner, WA 98390 Architect: Garner Miller msgs Carve Architects 510 Capitol Way South Olympia, WA 98501 Engineer: Justin Jones, PE PO Box 2066 Sumner, WA 98390 (206) 596-2020 320 Todd Road Development ONE INCH AT FULL SCALE. IF NOT, SCALE ACCORDINGLY **Civil Construction Permit** 

41829

GISTERED

OG-02-25

REV DATE DESCRIPTION

ET TITLE

Storm Details

PROJ. NO: 1611-001

DATE: June 02, 2025

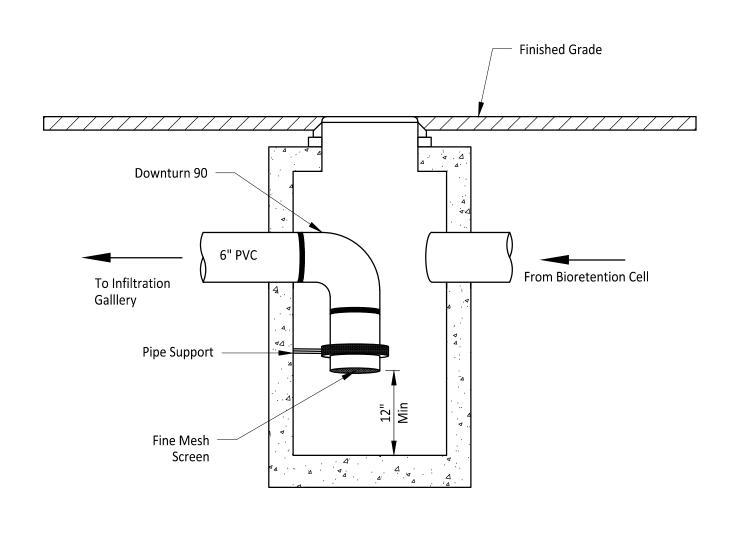
DRAWN BY: DESIGN BY:

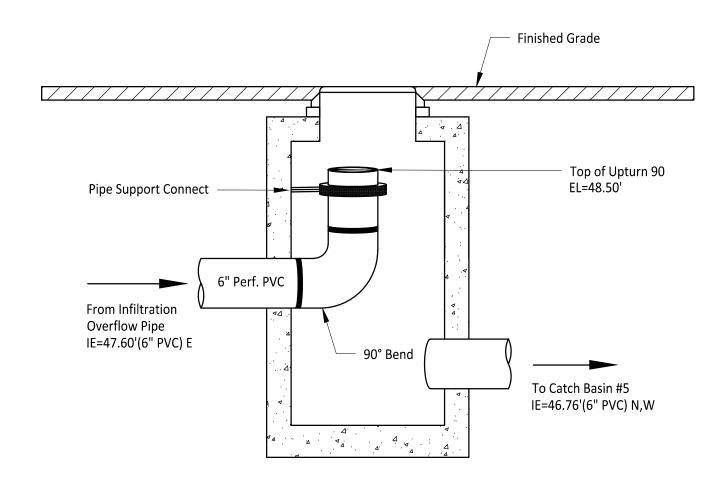
E. Kearney
SHEET NUMBER.

C4-202

J. Jones

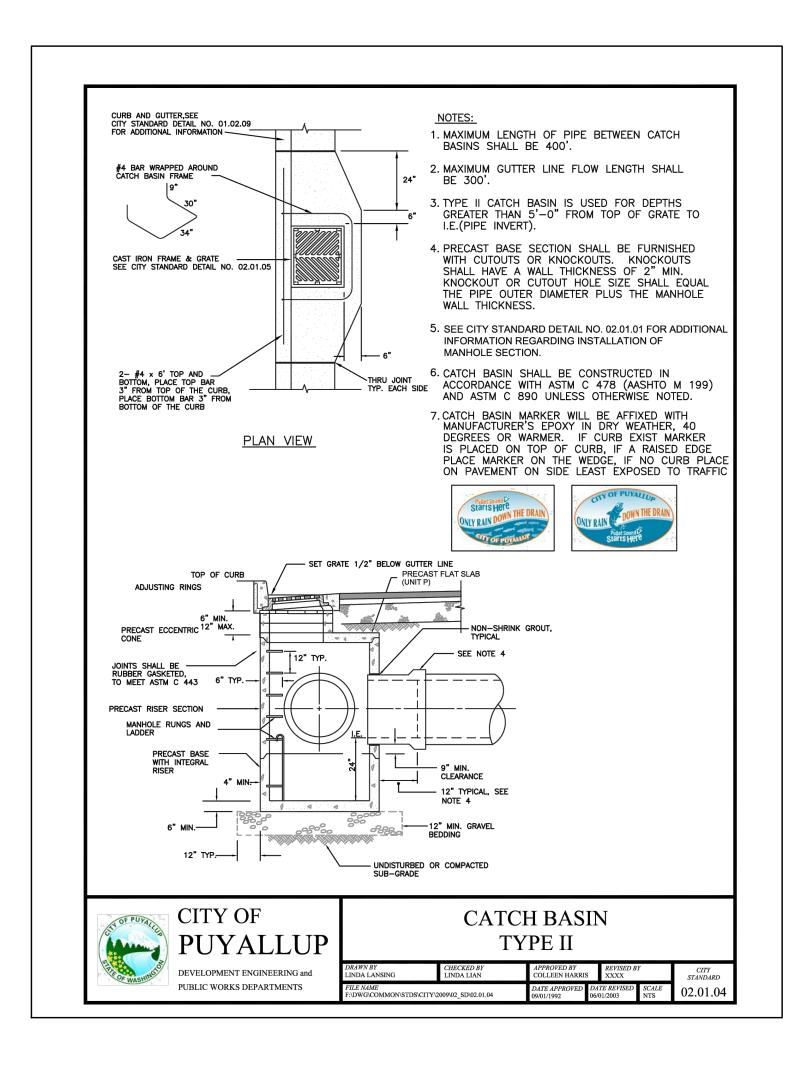
\_\_\_\_<u>19</u>\_0F\_\_\_<u>31\_\_</u>











Owner/Developer:

EJ Fernandez PO Box 309 Sumner, WA 98390

Architect:

Garner Miller msgs Carve Architects 510 Capitol Way South Olympia, WA 98501



Justin Jones, PE PO Box 2066 Sumner, WA 98390 (206) 596-2020

320 Todd Road Development

ONE INCH AT FULL SCALE. IF NOT, SCALE ACCORDINGLY

Civil Construction Permit



REV	DATE	DESCRIPTION

Storm Details

PROJ. NO:	161	1-001	
DATE:	June	02, 2025	
DRAWN BY:		DESIGN BY:	
	E. Kearney		J. Jones

C4-203

\_\_\_\_\_20\_ 0F \_\_\_31

CALL TWO BUSINESS DAYS

**APPROVED** 

NOTE: THIS APPROVAL IS VOID AFTER 180 DAYS FROM APPROVAL

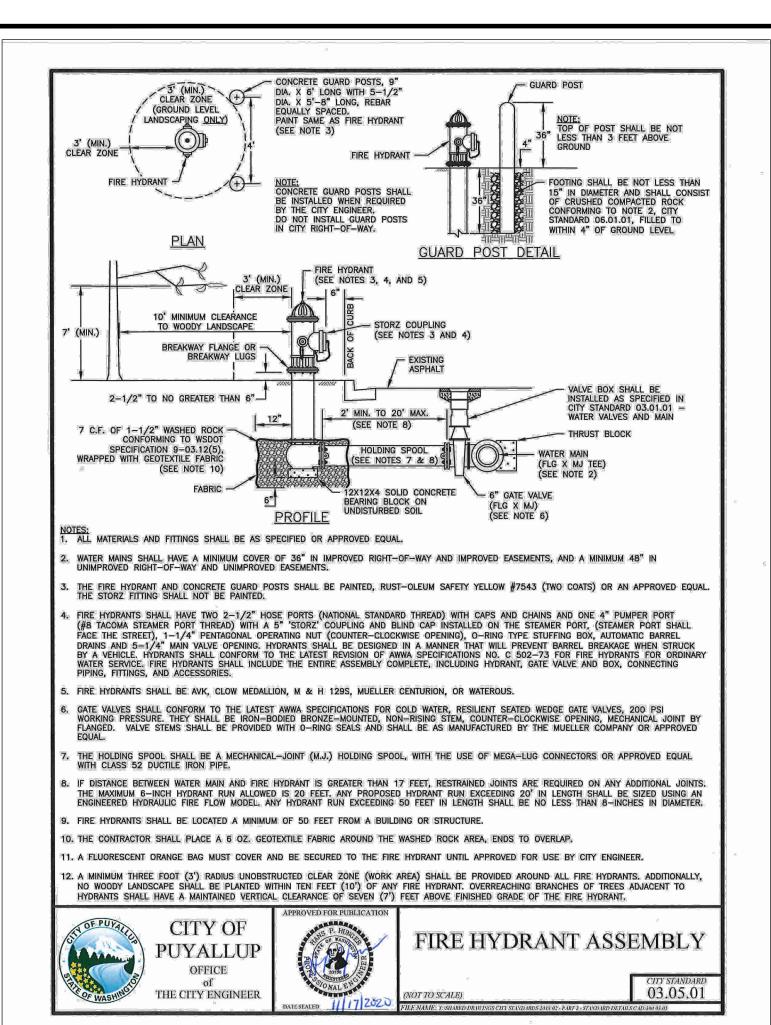
DATE.
THE CITY WILL NOT BE
RESPONSIBLE FOR ERRORS
AND/OR OMISSIONS ON THESE

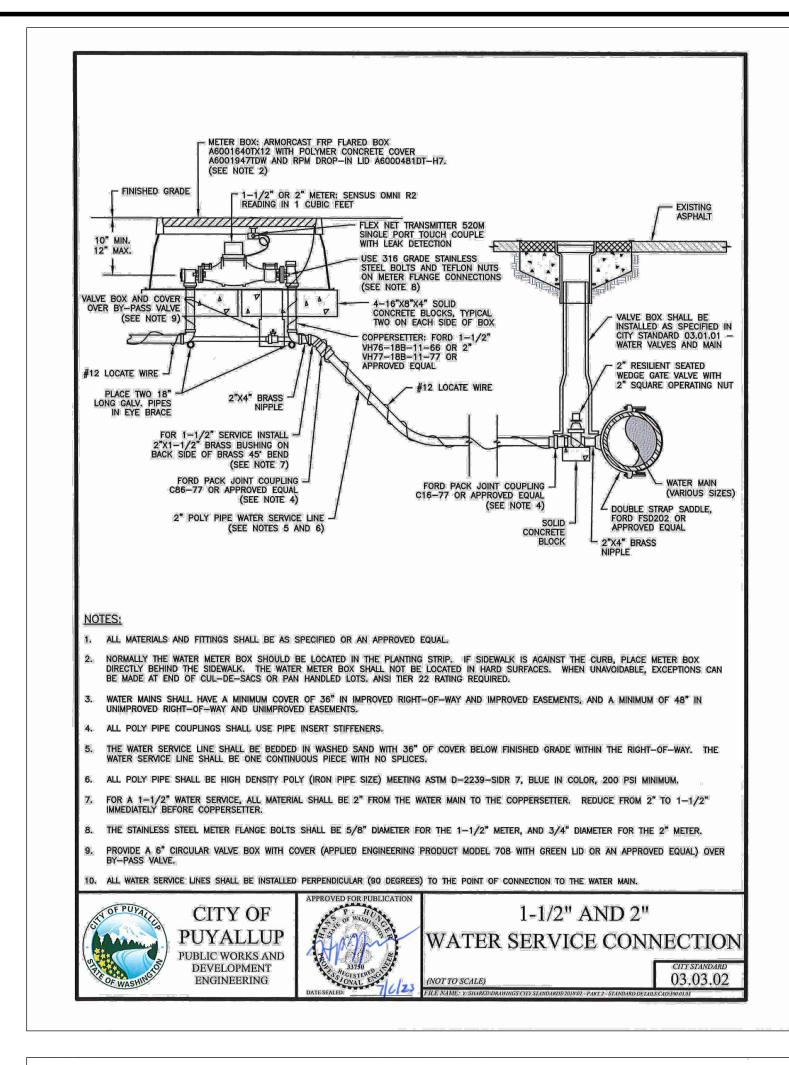
PLANS.
FIELD CONDITIONS MAY DICTATE

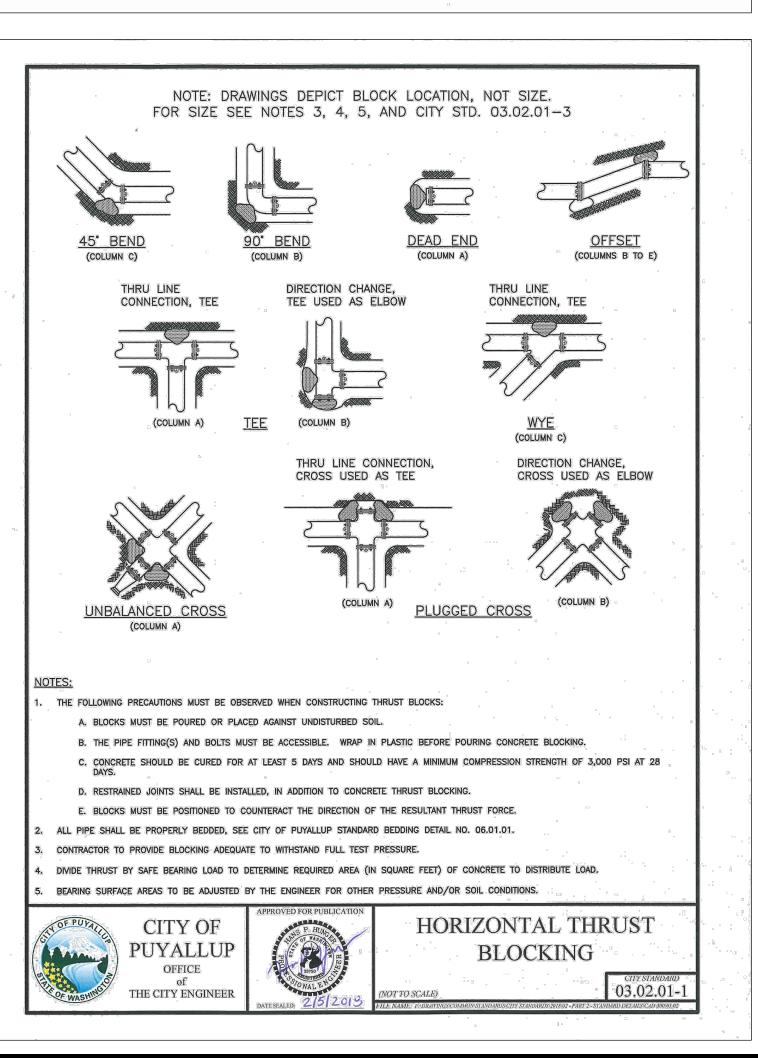
CHANGES TO THESE PLANS AS
DETERMINED BY THE
DEVELOPMENT ENGINEERING

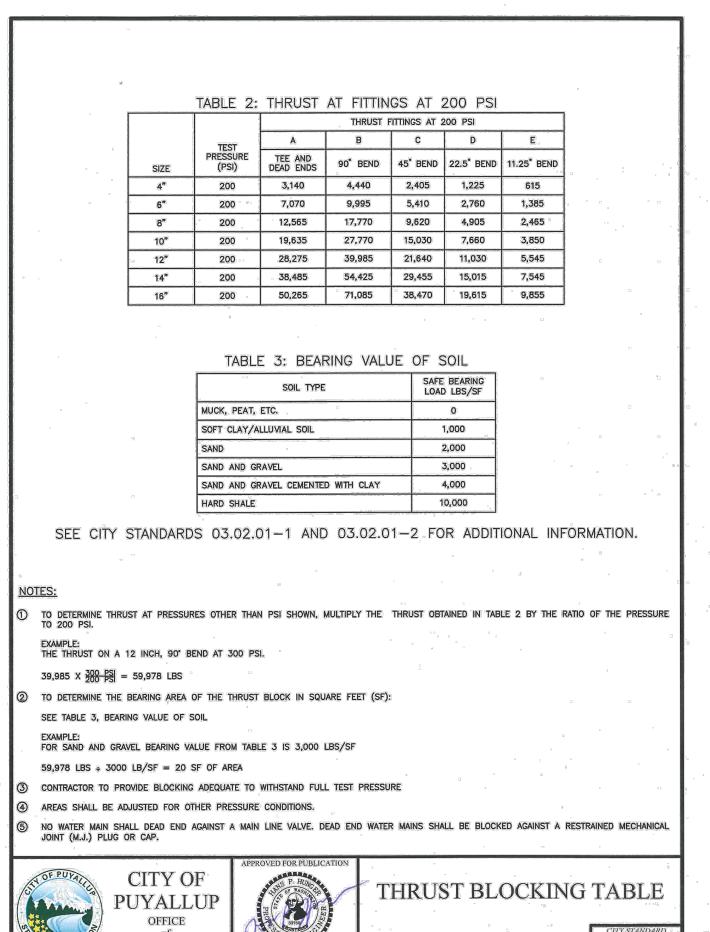
1-800-424-5555 UTILITIES UNDERGROUND LOCATION CENTER

MANAGER.

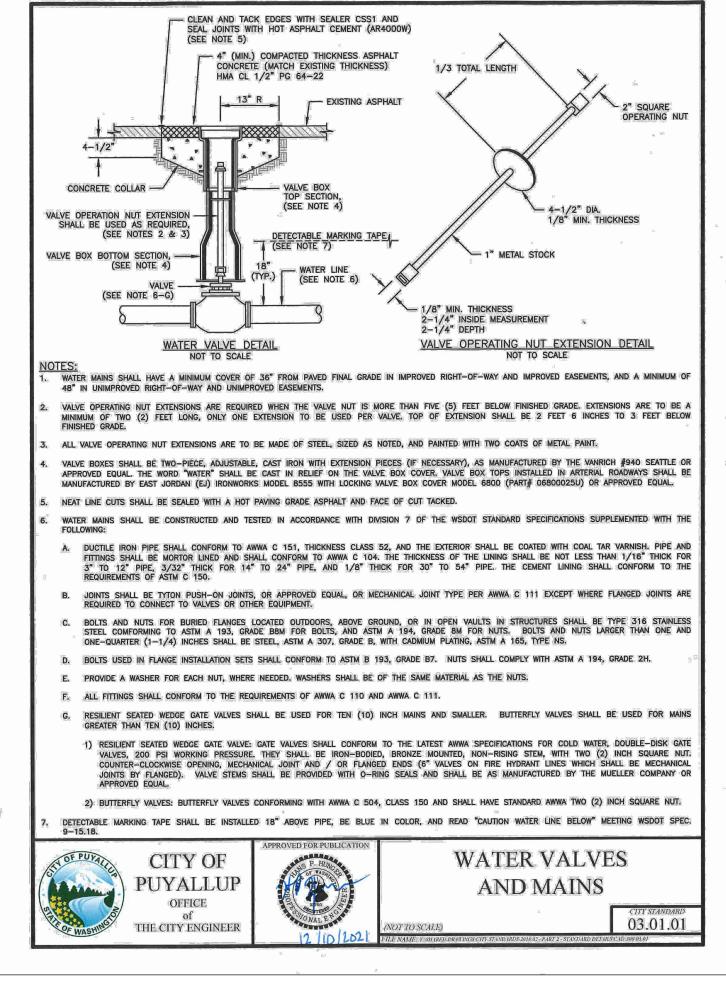


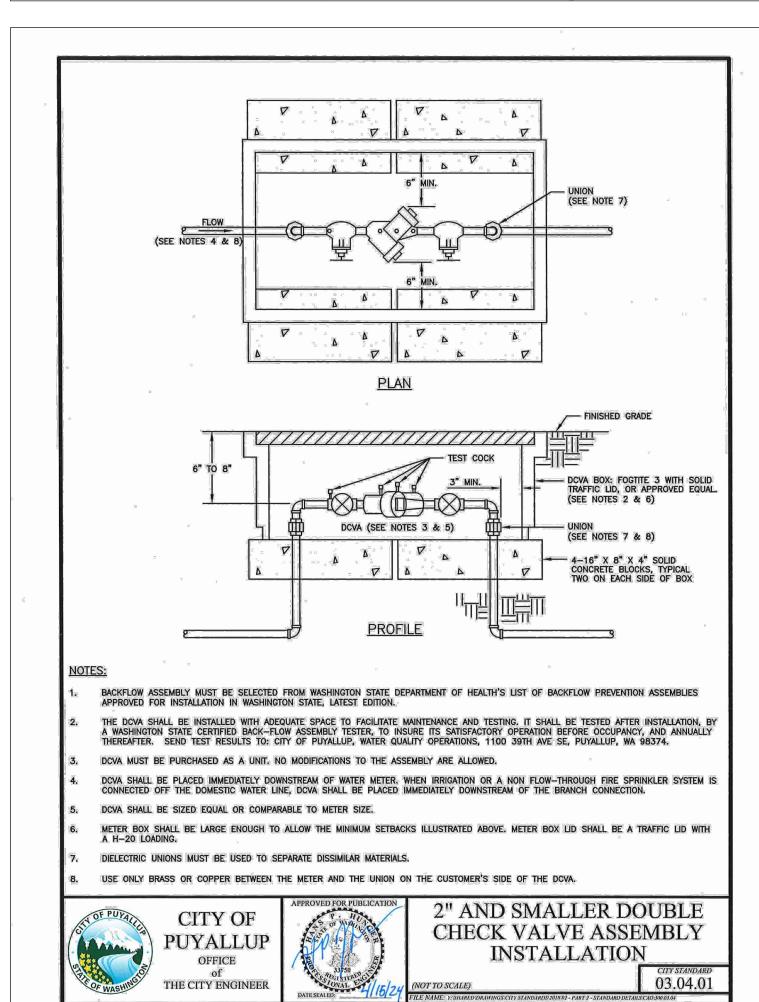






THE CITY ENGINEER









REV DATE DESCRIPTION

06-02-25

ALIEFT TITLE			

SHEET TITLE.

# Water Details

**NOTE:** THIS APPROVAL IS VOID 1611-001 AFTER 180 DAYS FROM APPROVAL June 02, 2025

THE CITY WILL NOT BE RESPONSIBLE FOR ERRORS AND/OR OMISSIONS ON THESE FIELD CONDITIONS MAY DICTATE E. Kearney CHANGES TO THESE PLANS AS

SHEET NUMBER.

C5-101

DESIGN BY:

\_\_\_\_21 OF \_\_\_31

CALL TWO BUSINESS DAYS BEFORE YOU DIG -800-424-5555

UTILITIES UNDERGROUND LOCATION CENTER

MANAGER.

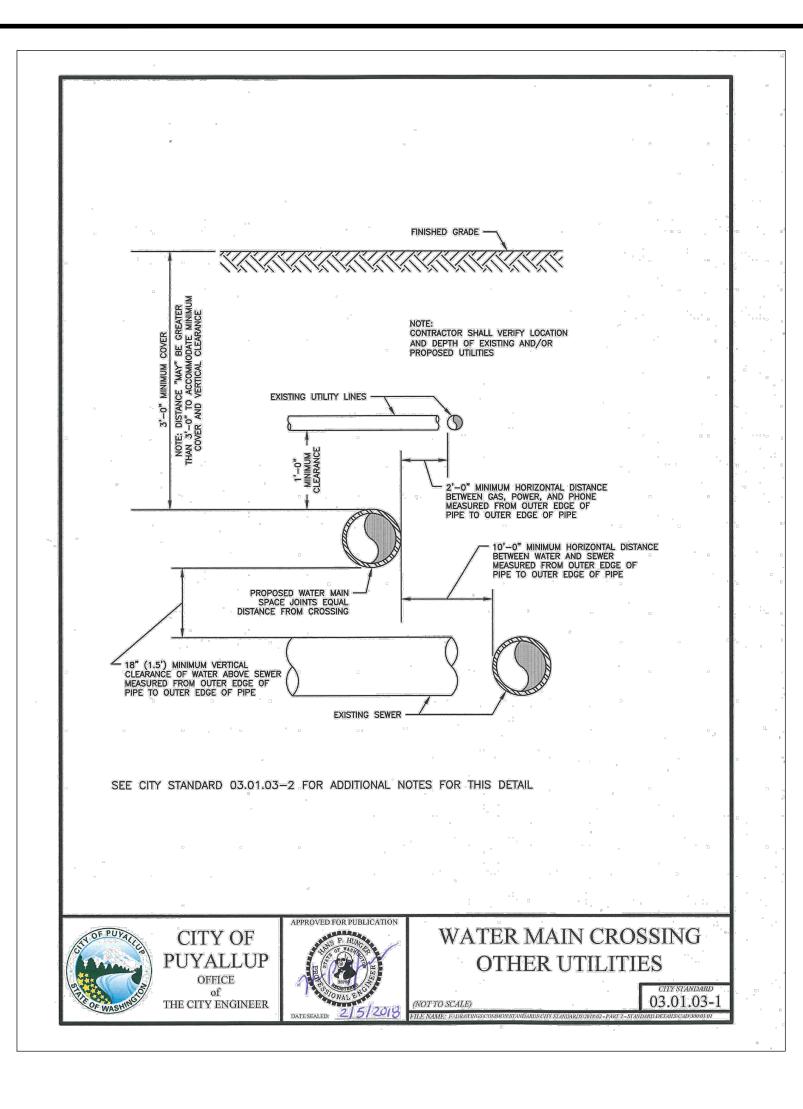
DETERMINED BY THE

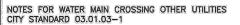
DEVELOPMENT ENGINEERING

APPROVED

CITY OF PUYALLUP

DEVELOPMENT ENGINEERING





WHEN LOCAL CONDITIONS PREVENT THE SEPARATIONS DESCRIBED ON CITY STANDARD 03.01.03—1, A SEWER MAY BE LAID CLOSER THAN 10—FEET HORIZONTALLY OR 18—INCHES VERTICALLY TO A WATER LINE, PROVIDED THE GUIDELINES BELOW ARE FOLLOWED:

#### UNUSUAL CONDITIONS (PARALLEL SYSTEMS)

- SEWER LINE IS LAID IN A SEPARATE TRENCH FROM THE WATER LINE.
   WHEN 18—INCHES VERTICAL SEPARATION CANNOT BE OBTAINED, THE SEWER SHALL BE CONSTRUCTED OF MATERIALS AND JOINTS THAT ARE EQUIVALENT TO WATER MAIN STANDARDS OF CONSTRUCTION AND SHALL BE PRESSURE TESTED TO ENSURE WATER TIGHTNESS PRIOR TO BACKFILLING.
- 3. THE WATER LINE SHALL BE PLACED ON A BENCH OF UNDISTURBED EARTH WITH THE BOTTOM OF THE WATER PIPE AT LEAST 18—INCHES ABOVE THE CROWN OF THE SEWER, AND SHALL HAVE AT LEAST 5—FEET OF HORIZONTAL SEPARATION AT ALL TIMES. THE CITY RESERVES THE RIGHT TO REQUIRE SUPPLEMENTAL MITIGATION EFFORTS, SUCH AS IMPERMEABLE BARRIERS OR OTHER MEANS, FOR ADDITIONAL PROTECTION.
- 4. THE SEWER SHALL NOT BE INSTALLED IN THE SAME DITCH AS A POTABLE WATER LINE WITHOUT PRIOR WRITTEN APPROVAL BY THE CITY OF PUYALLUP.

### UNUSUAL CONDITIONS (PERPENDICULAR SYSTEMS)

CONDITION A - GRAVITY SEWERS PASSING UNDER WATER LINES (ALL OF THE FOLLOWING APPLY)

- 1. ONE FULL SEGMENT (NOT LESS THAN 18-FEET LONG) OF DUCTILE IRON CLASS 52 WATER PIPE, AND THE LONGEST STANDARD SEWER PIPE LENGTH AVAILABLE FROM THE MANUFACTURER SHALL BE USED WITH THE PIPES CENTERED TO MAXIMIZE JOINT SEPARATION.
- STANDARD GRAVITY—SEWER MATERIAL ENCASED IN CONCRETE OR IN A ONE—QUARTER—INCH THICK CONTINUOUS STEEL, DUCTILE IRON, OR PRESSURE RATED PVC PIPE WITH A DIMENSION RATIO (THE RATIO OF THE OUTSIDE DIAMETER TO THE PIPE WALL THICKNESS) OF 18 OR LESS, WITH ALL VOIDS PRESSURE—GROUTED WITH SAND—CEMENT GROUT OR BENTONITE.

EXAMPLE OF DIMENSION RATIO (DR): OUTSIDE PIPE DIAMETER DIVIDED BY THE WALL THICKNESS OR OD/T. FOR 8-INCH SCH. 80 PVC PIPE (T=0.5 INCHES), THE DR IS 8.625/0.5=17.25

### CONDITION B - GRAVITY SEWER PASSING OVER WATER LINES

- WATER LINES SHALL BE PROTECTED BY PROVIDING:
- 1. A VERTICAL SEPARATION OF AT LEAST 18-INCHES BETWEEN THE INVERT OF THE SEWER AND THE CROWN OF THE WATER LINE.
- ADEQUATE STRUCTURAL SUPPORT FOR THE SEWER LINE TO PREVENT EXCESSIVE DEFLECTION OF JOINTS AND SETTLING ON AND BREAKING OF THE WATER LINE.
- 3. THE SEWER PIPE SHALL BE THE LONGEST STANDARD SEWER PIPE LENGTH AVAILABLE FROM THE MANUFACTURER WITH THE WATER AND SEWER PIPES CENTERED TO MAXIMIZE JOINT SEPARATION.
- 4. THE SEWER LINE CASING EQUIVALENT TO THAT SPECIFIED IN A(2) ABOVE.





WATER MAIN CROSSING OTHER UTILITIES (NOTES)

aranga sa inti

03.01.03-2

Owner/Developer:

EJ Fernandez PO Box 309 Sumner, WA 98390

Architect:

Garner Miller msgs Carve Architects 510 Capitol Way South Olympia, WA 98501



Justin Jones, PE PO Box 2066 Sumner, WA 98390 (206) 596-2020

Project:

320 Todd Road Development

ONE INCH AT FULL SCALE. IF NOT, SCALE ACCORDINGLY

Civil Construction Permit



06-02-25

REV	DATE	DESCRIPTION
•		

1611-001

June 02, 2025

DESIGN BY:

\_\_\_\_

Water Details

BY \_\_\_\_\_\_CITY OF PUYALLUP
DEVELOPMENT ENGINEERING

**APPROVED** 

DATE \_\_\_

NOTE: THIS APPROVAL IS VOID
AFTER 180 DAYS FROM APPROVAL
DATE.
THE CITY WILL NOT BE
RESPONSIBLE FOR ERRORS
AND/OR OMISSIONS ON THESE
PLANS.
FIELD CONDITIONS MAY DICTATE
CHANGES TO THESE PLANS AS
DETERMINED BY THE
DEVELOPMENT ENGINEERING

C5-1

E. Kearney

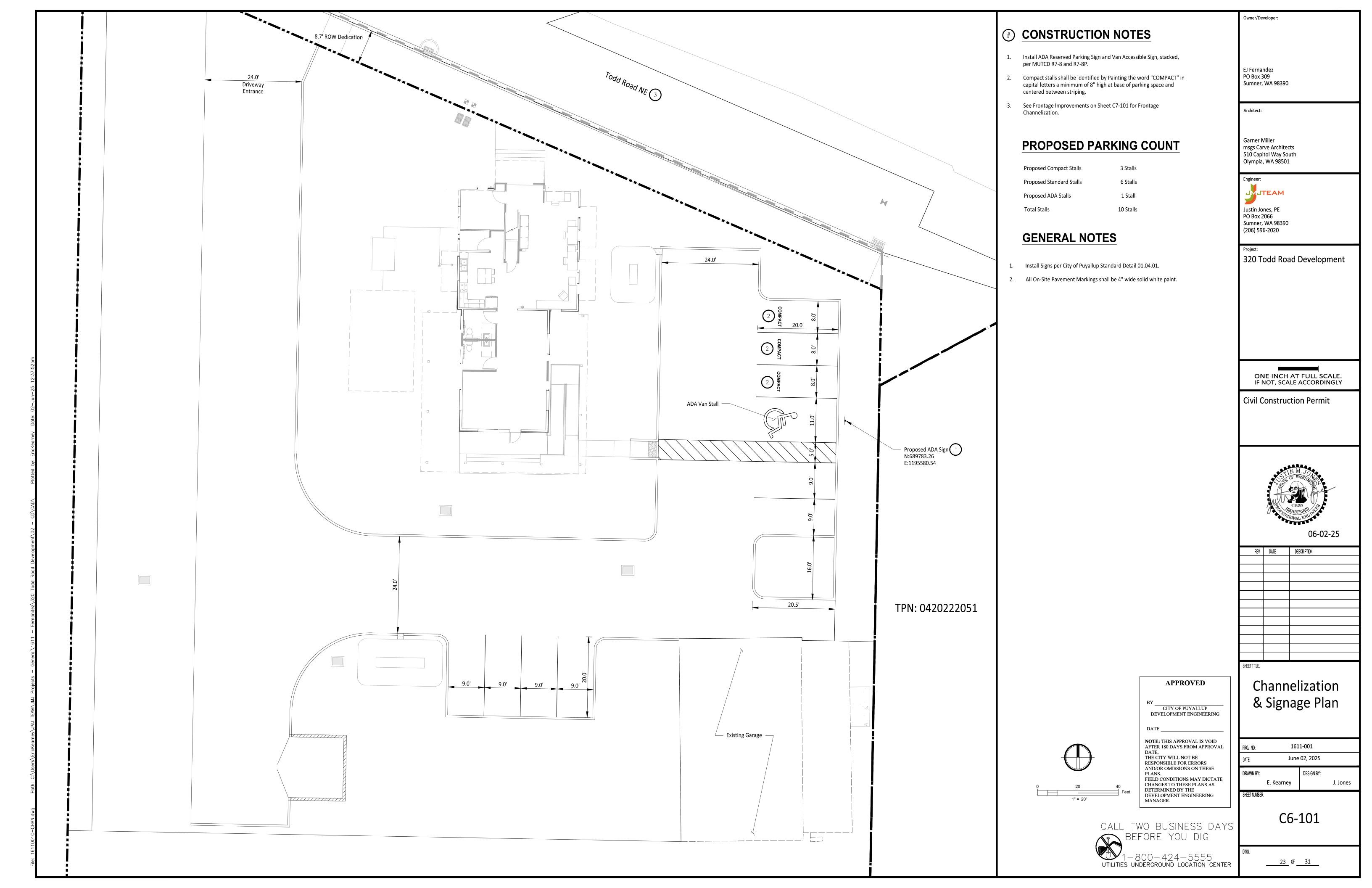
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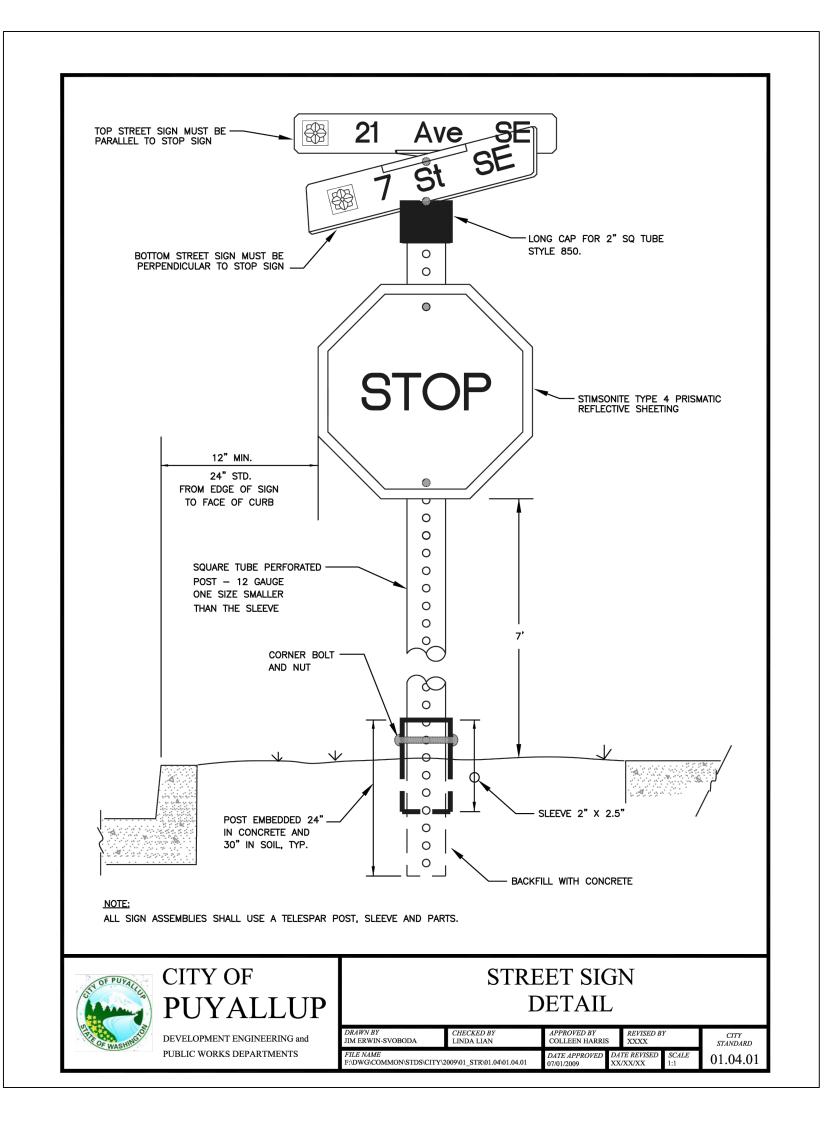
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CALL TWO BUSINESS DAYS
BEFORE YOU DIG

1-800-424-5555
UTILITIES UNDERGROUND LOCATION CENTER

MANAGER.





Owner/Developer:

EJ Fernandez PO Box 309 Sumner, WA 98390

Architect:

Garner Miller msgs Carve Architects 510 Capitol Way South Olympia, WA 98501



Justin Jones, PE PO Box 2066 Sumner, WA 98390 (206) 596-2020

Project:

320 Todd Road Development

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06-02-25

REV	DATE	DESCRIPTION

Channelization

SHFF

# APPROVED

BY \_\_\_\_\_\_\_CITY OF PUYALLUP
DEVELOPMENT ENGINEERING

DATE \_\_\_

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MANAGER.

CALL TWO BUSINESS DAYS

BEFORE YOU DIG

1-800-424-5555

UTILITIES UNDERGROUND LOCATION CENTER

PROJ. NO: 1611-001

DATE: June 02, 2025

DRAWN BY: DESIGN BY:

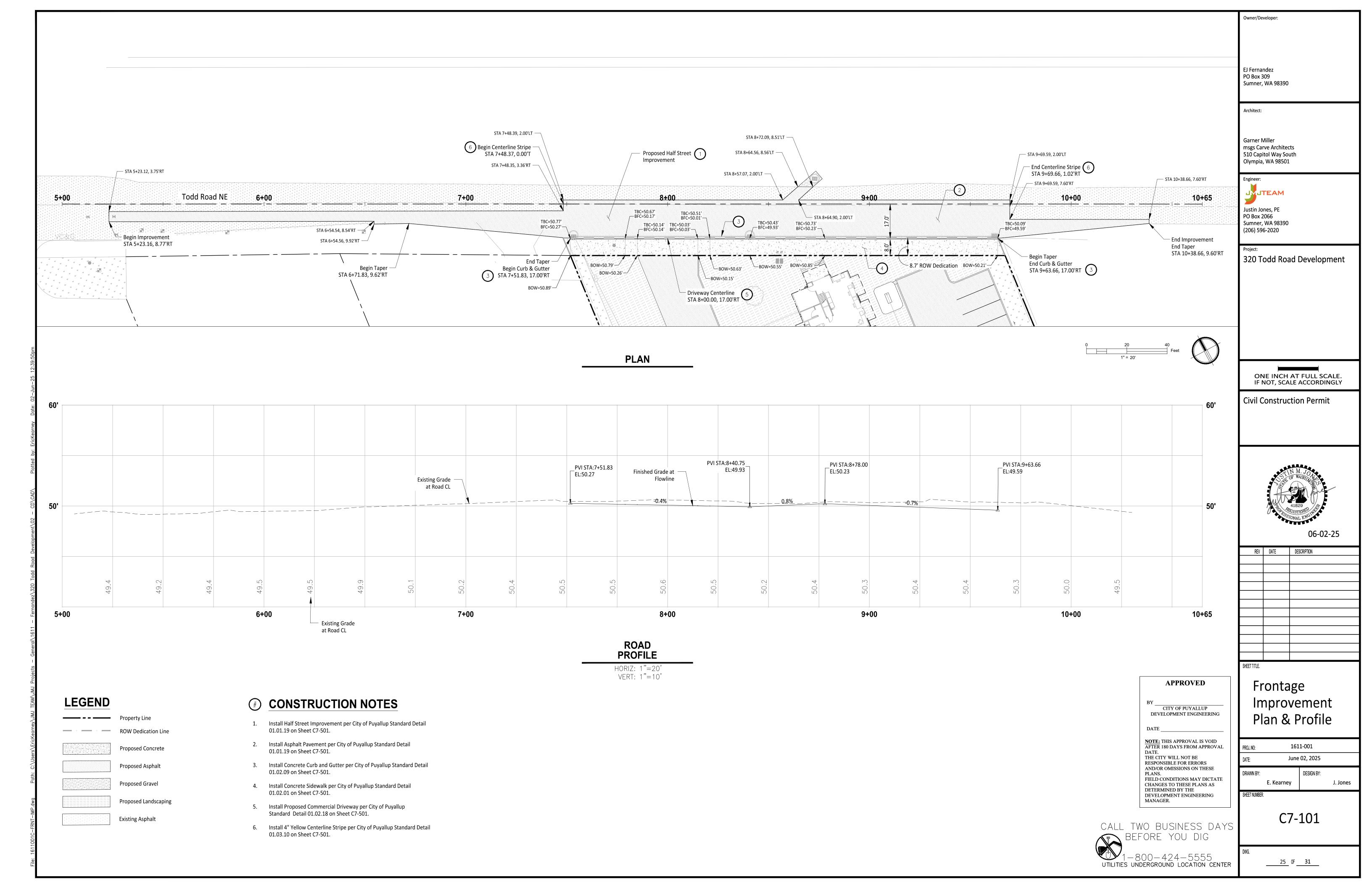
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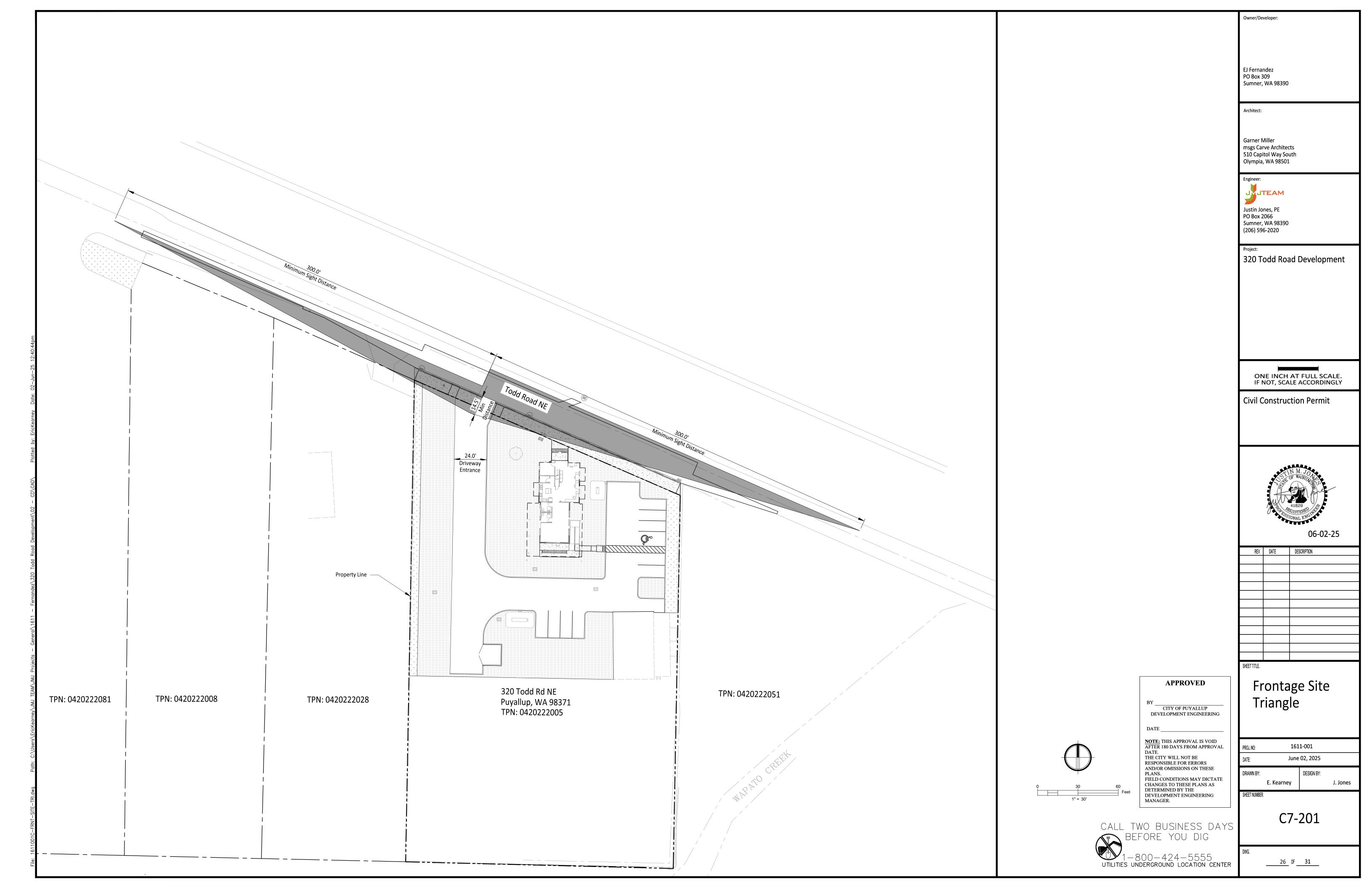
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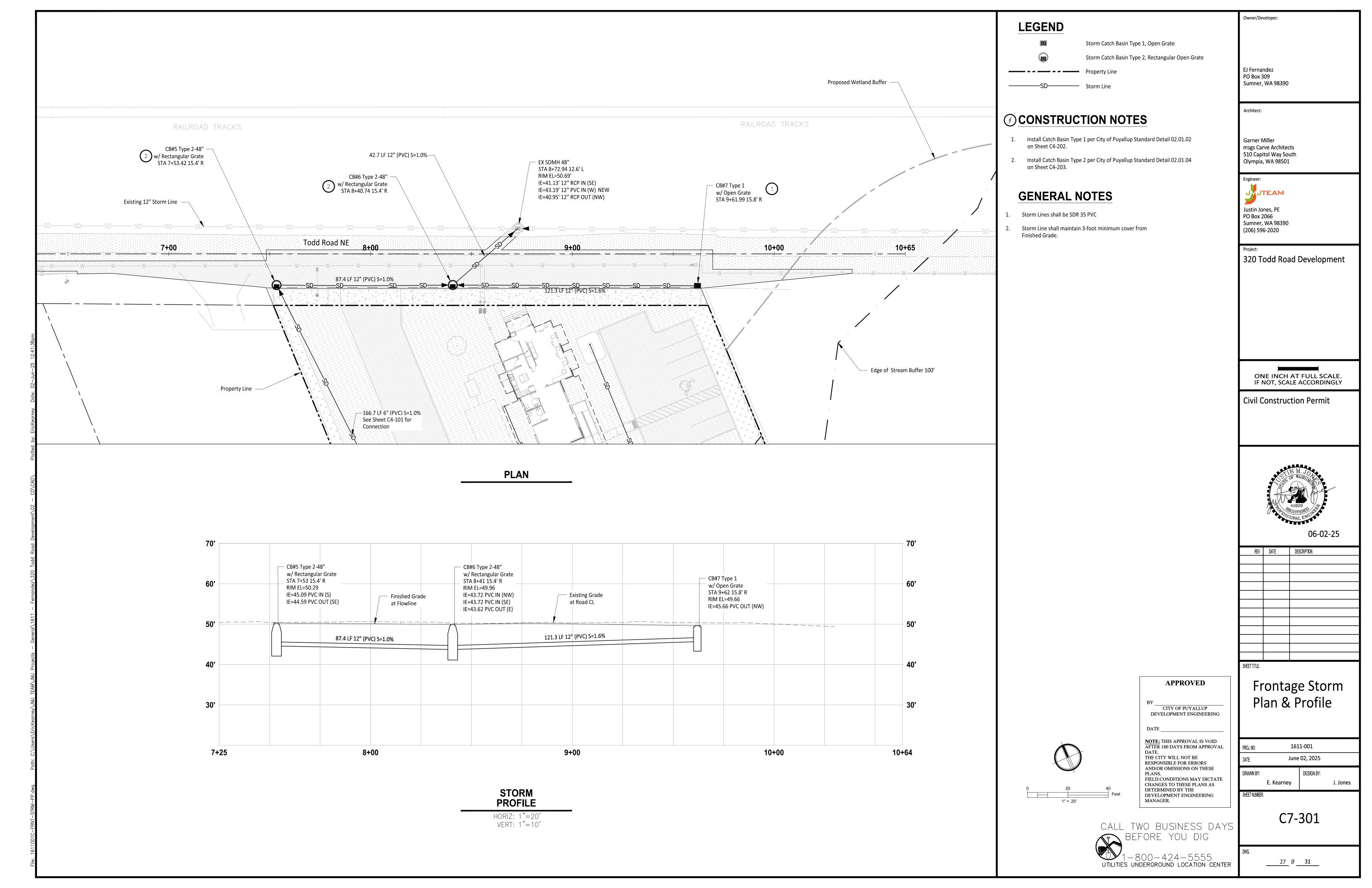
E. Kearney

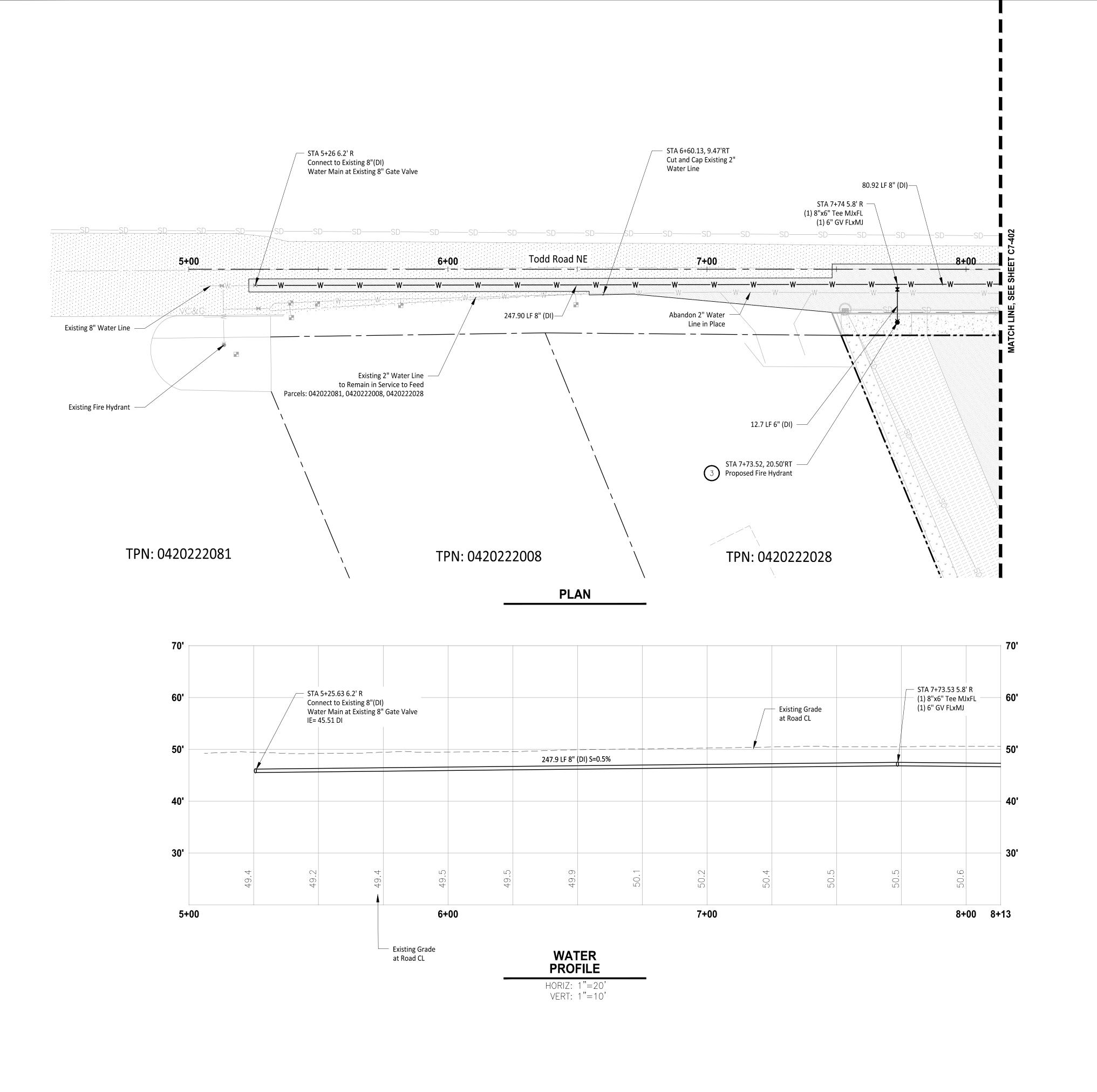
C6-102

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## **LEGEND**

Property Line

ROW Dedication

Water Line

Water Meter

Gate Valve

Fire Hydrant

## **CONSTRUCTION NOTES**

- 1. Install 2" Water Service Connection per City of Puyallup Standard Detail 03.03.02 on Sheet C5-101.
- 2. Install 2" DCVA per City of Puyallup Standard Detail 03.04.01 on Sheet C5-101.
- 3. Install Fire Hydrant per City of Puyallup Standard Detail 03.05.01 on Sheet C5.101.

## **GENERAL NOTES**

- 1. All Ductile Iron pipes shall be Class 52.
- 2. All Ductile Iron Pipes shall maintain 3-foot minimum cover from Finished Grade.
- 3. All POLY pipes shall be High Density Poly (Iron Pipe Size) meeting ASTM D-2239-SIDR 7, blue in color, 200 PSI minimum.
- 4. All POLY pipes shall maintain 3-foot minimum cover from Finished Grade.

Owner/Developer:

EJ Fernandez PO Box 309 Sumner, WA 98390

Architect:

Garner Miller msgs Carve Architects 510 Capitol Way South Olympia, WA 98501



Justin Jones, PE PO Box 2066 Sumner, WA 98390 (206) 596-2020

Project:

320 Todd Road Development

ONE INCH AT FULL SCALE. IF NOT, SCALE ACCORDINGLY

Civil Construction Permit



06-02-25

KEV	DAIE	DESCRIPTION

SHEET

Frontage Water Plan & Profile

 PROJ. NO:
 1611-001

 DATE:
 June 02, 2025

 DRAWN BY:
 DESIGN BY:

E. Kearney

C7-401

DWG. \_\_\_\_\_28\_ 0F \_\_\_31\_\_\_

CALL TWO BUSINESS DAYS
BEFORE YOU DIG

1-800-424-5555
UTILITIES UNDERGROUND LOCATION CENTER

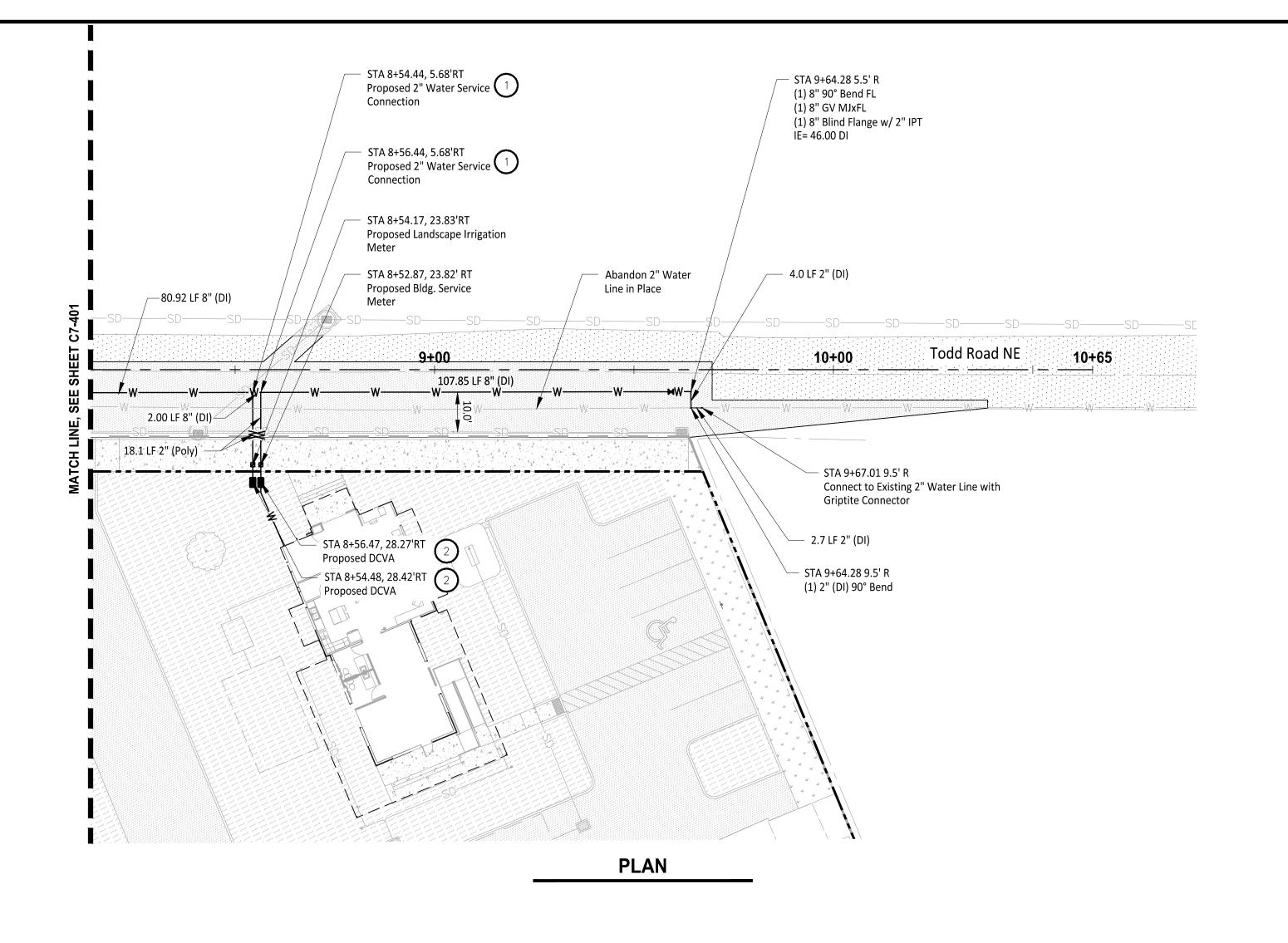
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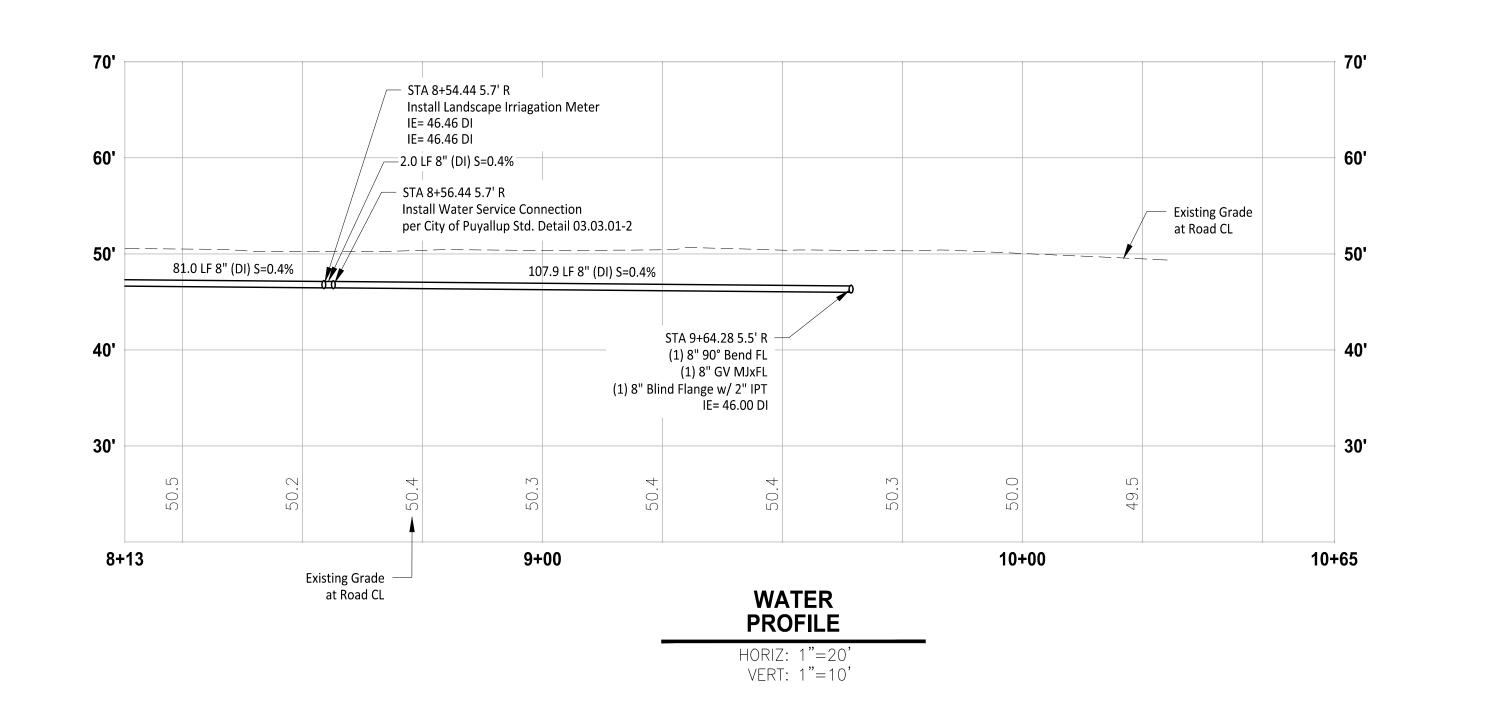
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THE CITY WILL NOT BE RESPONSIBLE FOR ERRORS

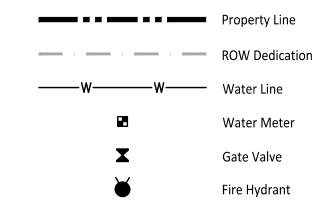
AND/OR OMISSIONS ON THESE

FIELD CONDITIONS MAY DICTATE
CHANGES TO THESE PLANS AS
DETERMINED BY THE
DEVELOPMENT ENGINEERING





## **LEGEND**



## **© CONSTRUCTION NOTES**

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Owner/Developer:

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Garner Miller msgs Carve Architects 510 Capitol Way South Olympia, WA 98501



Justin Jones, PE PO Box 2066 Sumner, WA 98390 (206) 596-2020

Project:

320 Todd Road Development

ONE INCH AT FULL SCALE. IF NOT, SCALE ACCORDINGLY

Civil Construction Permit



06-02-25

REV	DATE	DESCRIPTION
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SHEET TITL

Frontage Water Plan & Profile

 PROJ. NO:
 1611-001

 DATE:
 June 02, 2025

 DRAWN BY:
 DESIGN BY:

E. Kearney
SHEET NUMBER

C7-402

J. Jones

DWG. \_\_\_\_\_29\_ OF \_\_\_31\_\_\_

DATE

NOTE: THIS APPROVAL IS VOID
AFTER 180 DAYS FROM APPROVAL
DATE.
THE CITY WILL NOT BE
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AND/OR OMISSIONS ON THESE
PLANS

0 20 40 1" = 20'

CALL TWO BUSINESS DAYS
BEFORE YOU DIG

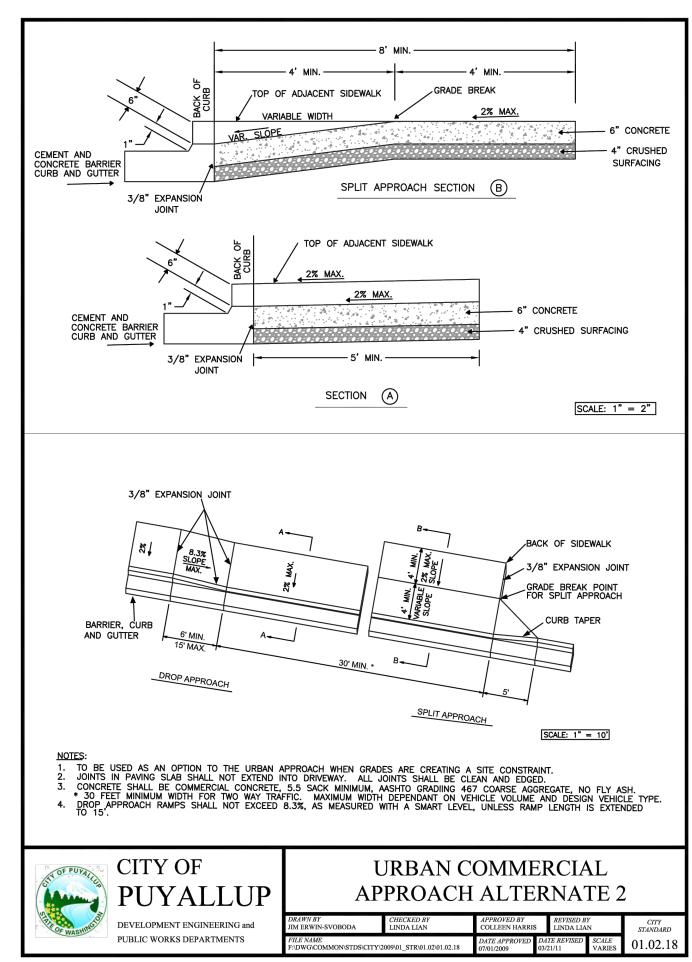
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UTILITIES UNDERGROUND LOCATION CENTER

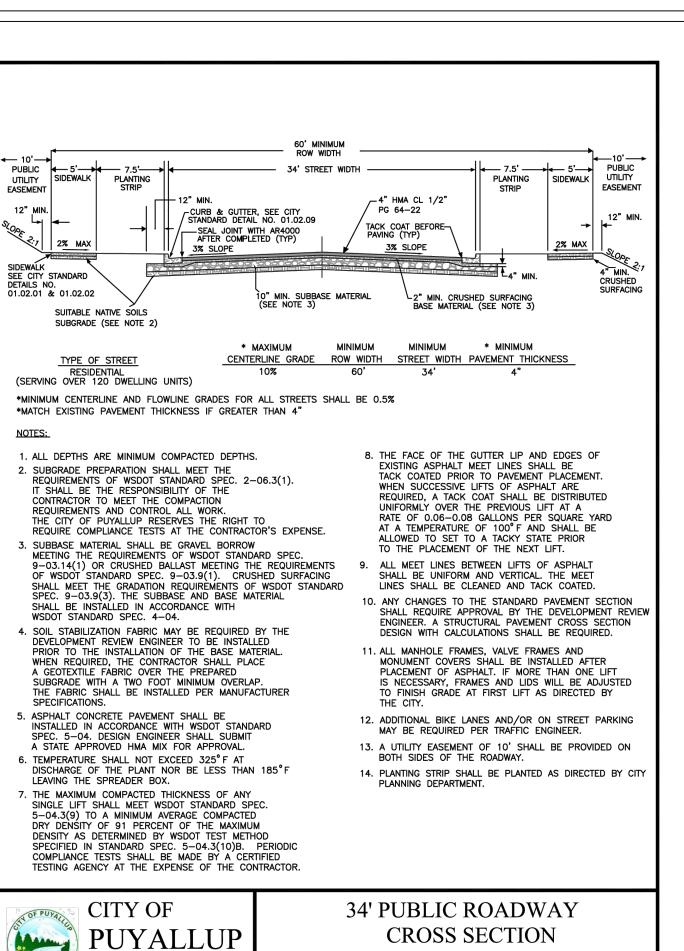
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CHANGES TO THESE PLANS AS DETERMINED BY THE

DEVELOPMENT ENGINEERING

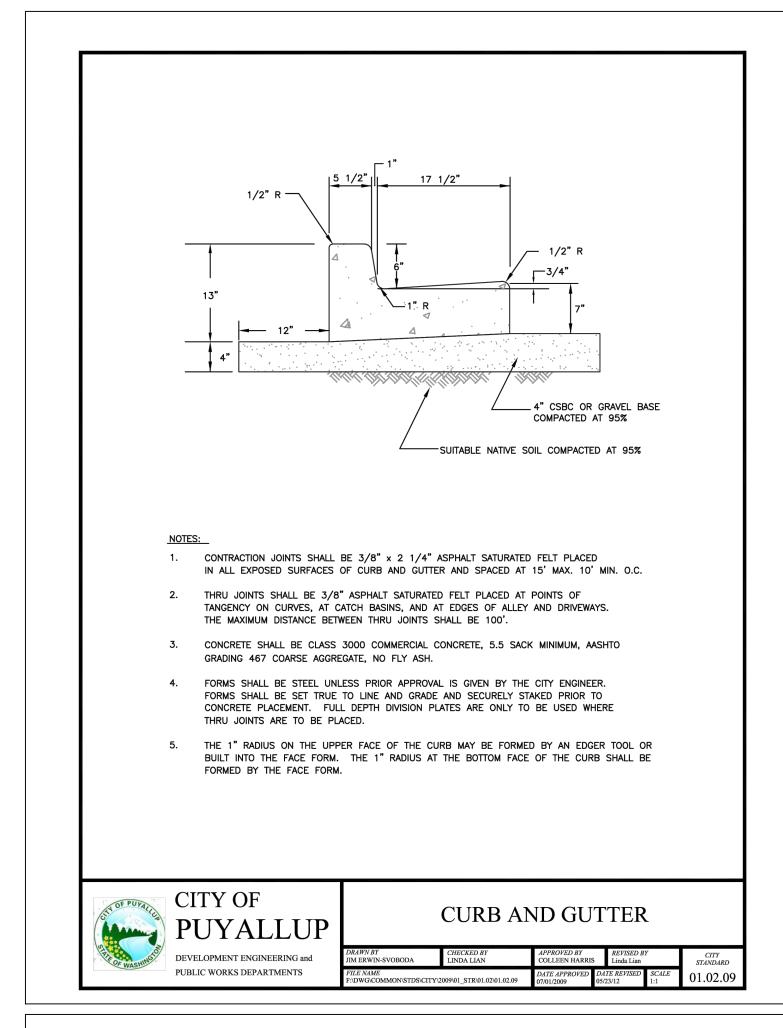
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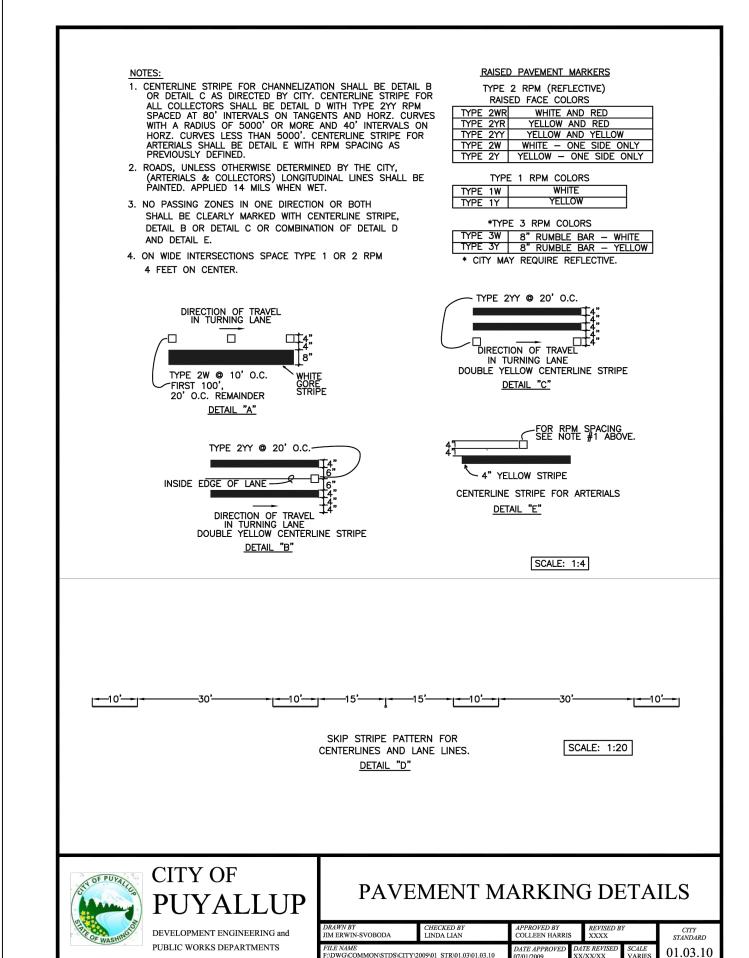


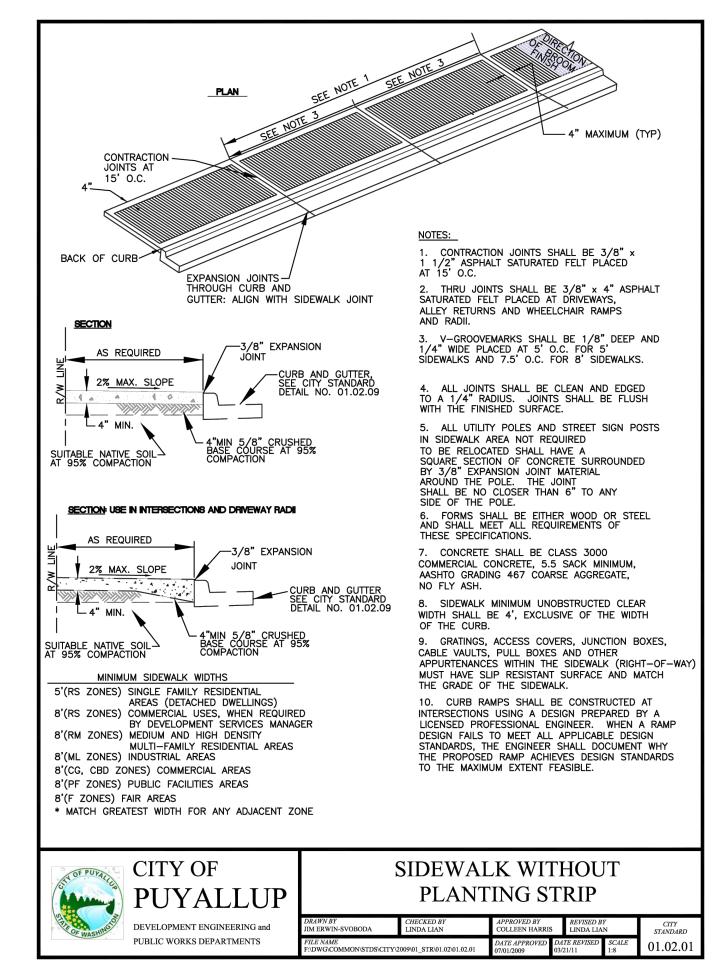


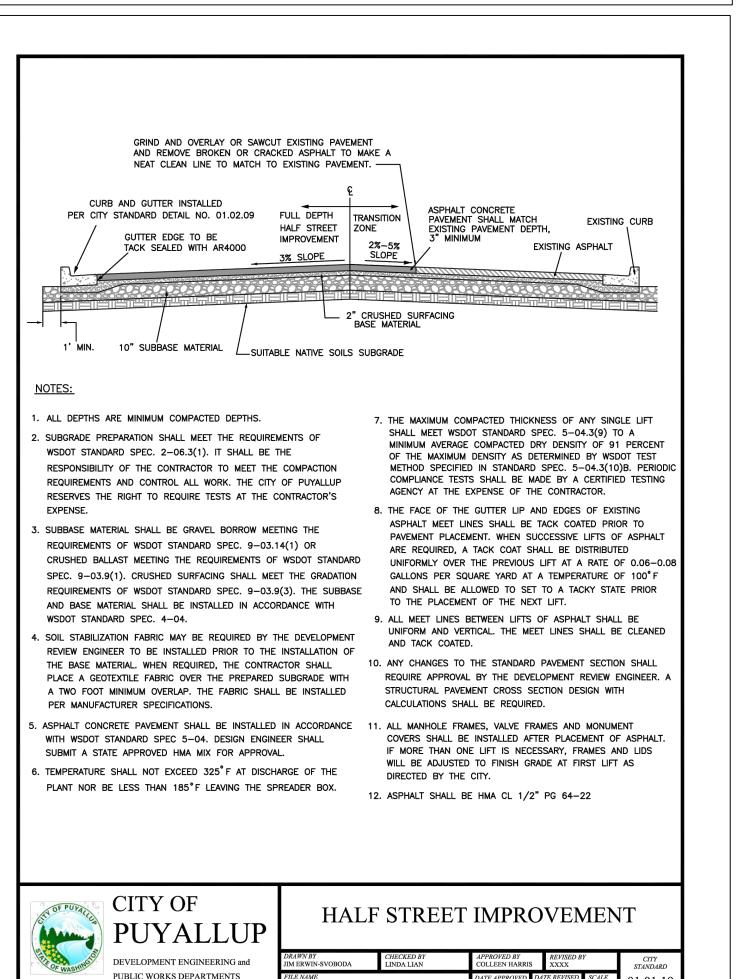
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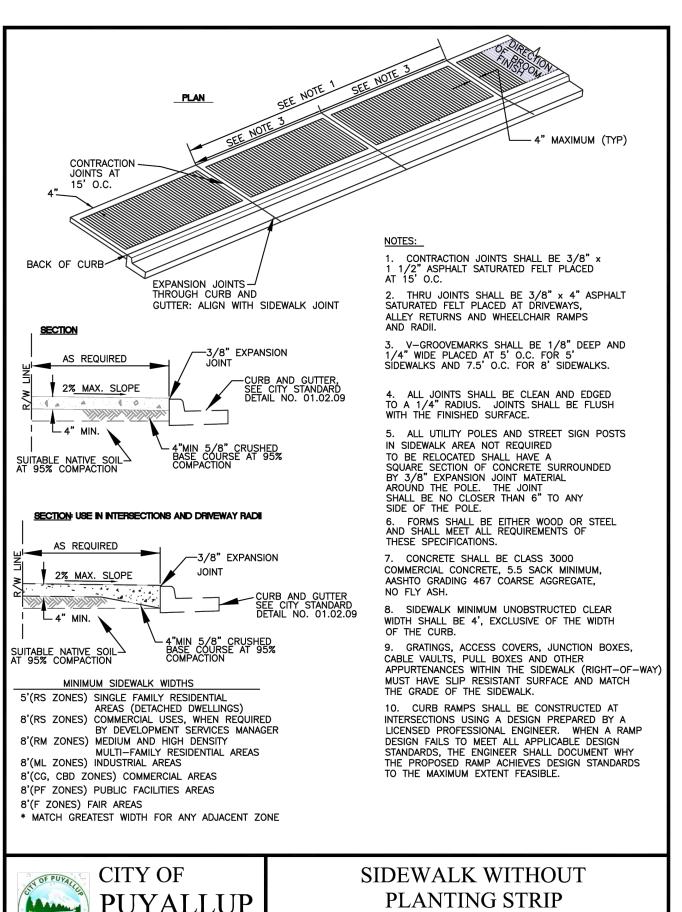
PUBLIC WORKS DEPARTMENTS











Architect: Garner Miller msgs Carve Architects 510 Capitol Way South Olympia, WA 98501 Engineer: Justin Jones, PE PO Box 2066 Sumner, WA 98390 (206) 596-2020 320 Todd Road Development

Owner/Developer:

EJ Fernandez

PO Box 309

Sumner, WA 98390

ONE INCH AT FULL SCALE. IF NOT, SCALE ACCORDINGLY

**Civil Construction Permit** 



06-02-25

REV DATE DESCRIPTION

# Frontage Details

**NOTE:** THIS APPROVAL IS VOID 1611-001 AFTER 180 DAYS FROM APPROVAL June 02, 2025

SHEET NUMBER.

THE CITY WILL NOT BE RESPONSIBLE FOR ERRORS AND/OR OMISSIONS ON THESE DRAWN BY: FIELD CONDITIONS MAY DICTATE E. Kearney CHANGES TO THESE PLANS AS

DESIGN BY:

J. Jones

C7-501

\_\_\_\_30 OF \_\_\_31

CALL TWO BUSINESS DAYS BEFORE YOU DIG -800-424-5555

MANAGER.

DATE

UTILITIES UNDERGROUND LOCATION CENTER

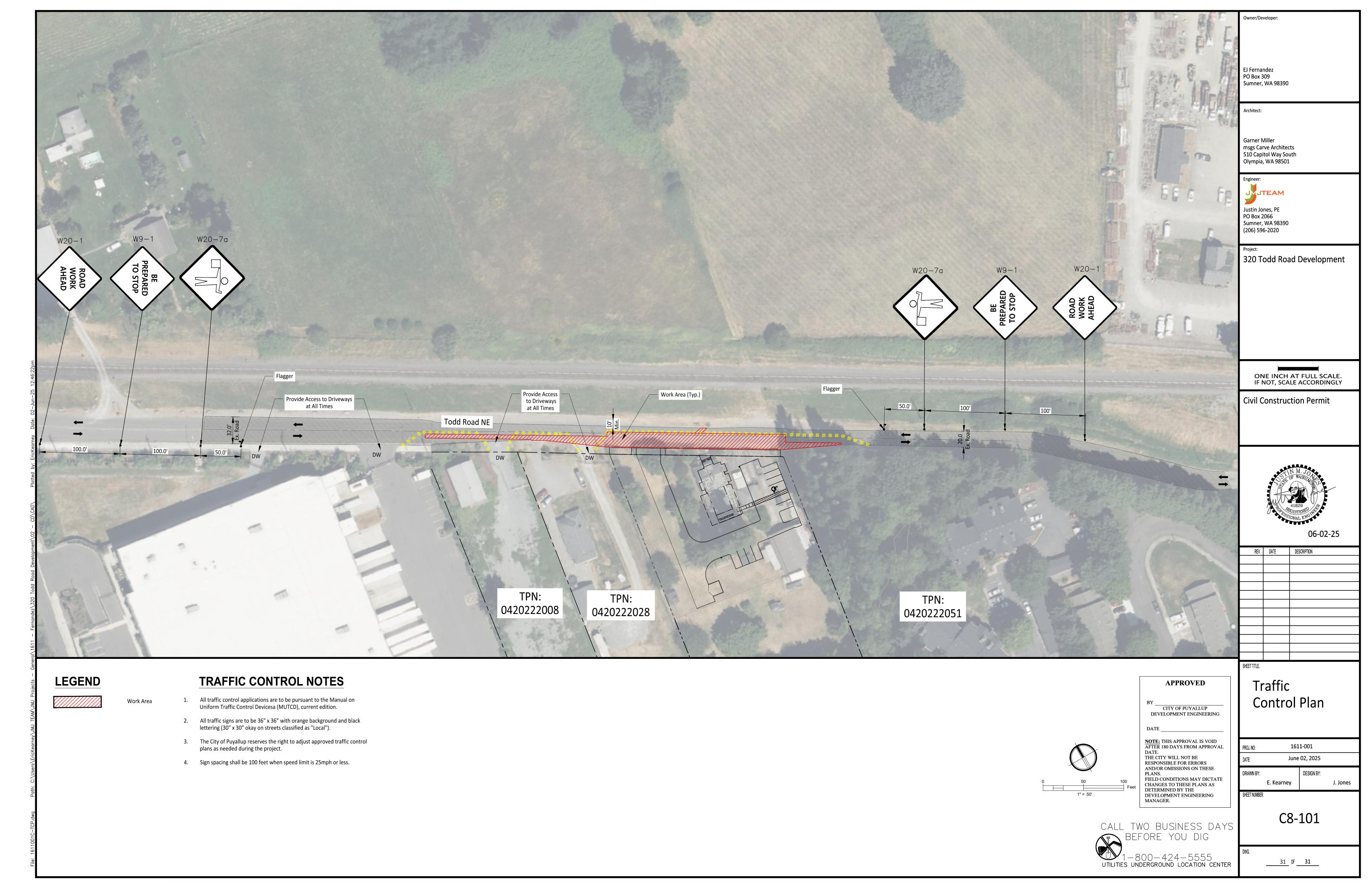
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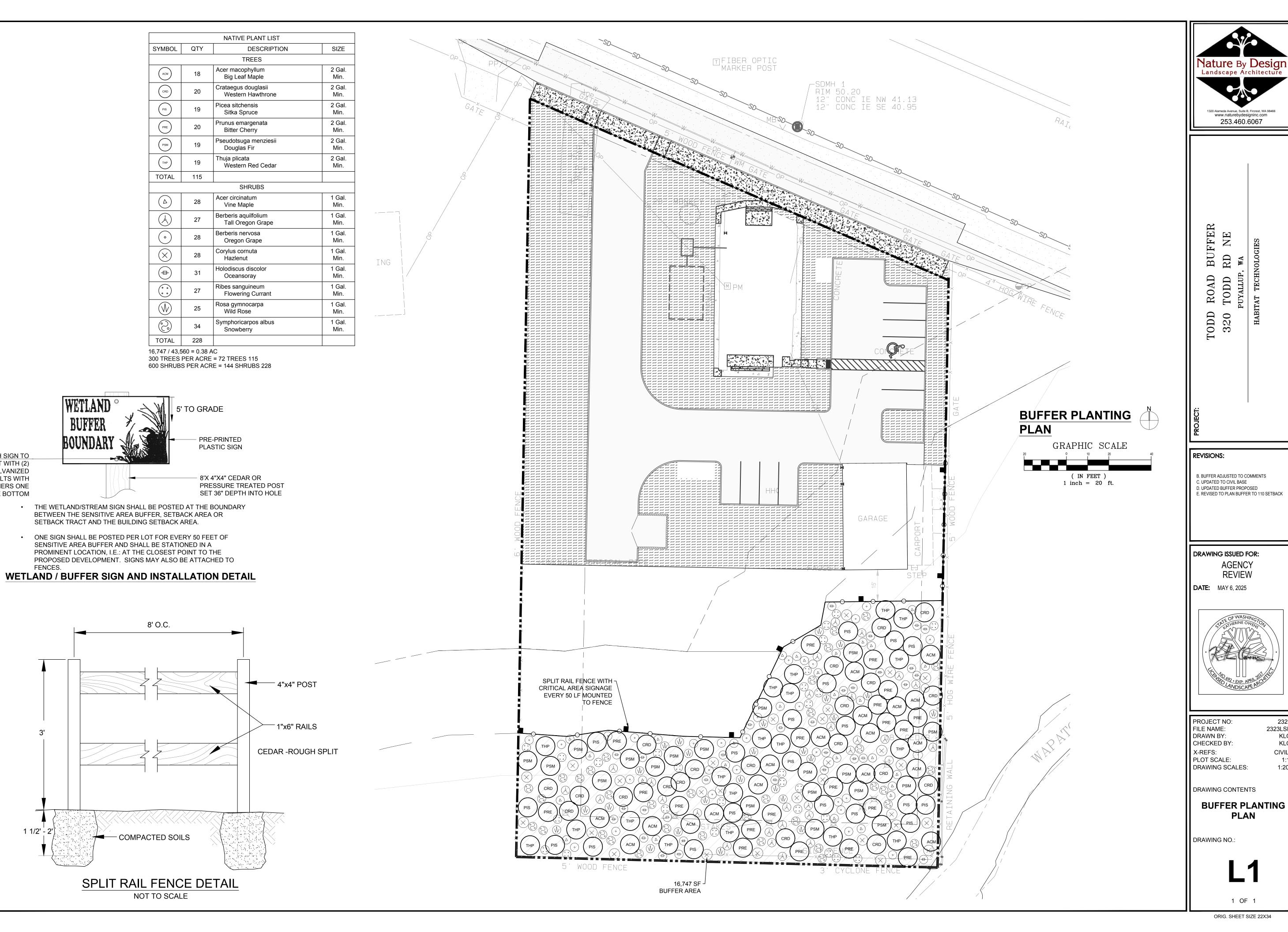
DETERMINED BY THE

**APPROVED** 

CITY OF PUYALLUP

DEVELOPMENT ENGINEERING





ATTACH SIGN TO

LAG BOLTS WITH

TOP, ONE BOTTOM

POST WITH (2) 5/16" GALVANIZED

WASHERS ONE

1 1/2' - 2'

Know what's below.

Call before you dig.

1 OF 1 ORIG. SHEET SIZE 22X34

**PLAN** 

2323 2323LSE KLO KLO

CIVIL

1:20

# GENERAL LANDSCAPE NOTES

- 1. Contractor is responsible for obtaining all necessary permits from the appropriate agency prior to commencing work. Contractor shall contact Line Locators (811) a min. of 48 hours prior to any digging or trenching. If there are any discrepancies with existing lines and landscaping, it is the contractor's responsibility to contact the landscape architect and request a site visit to address the conflicts. Contractor shall comply and conform to any and all local and state codes for work, schedules and any other project related requirements.
- 2. Contractor shall coordinate directly with the landscape architect for all landscape related issues, concerns, inspections and approvals. Contractor shall provide the landscape architect with a written request for a site visit to address any related items.
- 3. Scope of work shall include any and all specified and unspecified but related incidental work to achieve the design indicated on the landscape plans. All labor, materials, subcontractors, equipment, and related incidental items shall be supplied and installed to achieve a complete project, unless directed otherwise by the general contractor or landscape architect.
- 4. Contractor to verify all sub grades are set below required amendments to insure the finished grade will match what is intended by civil or drainage design. All sub grades and finished or final grades shall be graded to drain to the designed drainage system with positive drainage away from all structures.
- a. Slopes used for grass plantings or turf shall be less than 3:1 or 33 percent. Otherwise plantings should not require mechanized mowing equipment.

#### Soil Preparation.

- a. Where soils are compacted, planting beds should be deep tilled to a depth of at least 12 inches. Soils shall be enhanced through the addition of the following materials: bark and forestry by-products, organic matter such as composted yard waste, organics and other amendments as needed through a soils test. Where Pit Planting, see planting detail for planting ring sizes and depths. Scarify the edges of planting pits to encourage root expansion.
- b. On project sites where topsoil is limited or nonexistent, a minimum depth of 6 (six) inches of sandy loam topsoil should be tilled into the soil to a depth of 12 inches through all planting areas with compacted soils.
- c. For all newly planted areas, three cubic yards of composted organic matter per 1,000 square feet of landscape area
- should be added to a depth of four inches to the top of the soil and Tilled in.
- d. Seeded areas shall be fine graded and rolled. New Soil depths in lawn areas shall be 4 Inches.

## 6. Mulching of Newly Planted or Replanted Areas.

- a. Mulches must be applied to the following depths: a minimum 3 (three) inches over bare soil, and two inches where plant materials will cover.
- b. Mulches must include organic materials, such as wood chips and shredded bark.
- c. Nonporous materials, such as plastic sheeting, shall not be used in any area of the landscape because of down-slope erosion and potential soil contamination from herbicide washing.
- d. Mulch should be applied regularly to and maintained in all planting areas to assist soils in retaining moisture, reducing weed growth, and minimizing erosion.
- 7. Contractor shall field layout all plant material and contact the landscape architect for a site visit to approve the layout. Any field modifications shall be done by the landscape architect prior to planting.
- 8. Contractor shall immediately notify the landscape architect of any poor drainage condition in landscape areas. No standing water shall be permitted in any landscape areas - either on the surface or below the topsoil. The landscape architect shall coordinate the drainage solution with the general contractor and civil engineer. Once the concerns have been remedied planting shall commence.
- 9. All groundcover to be planted in a triangular spacing formation, equal in all directions to the centers of the groundcovers in distances indicated in the legend. Contractor shall verify all quantities of groundcovers by area calculations and spacing requirements.
- 10. Landscaping is to be per plan. Plant substitutions due to availability or otherwise will be allowed only with landscape architect, owner and agency approval. Any substitutions will be with material of similar size, growth characteristics, and quality.

# 11. All trees must be staked as necessary so as to maintain material in a healthy, vigorous growing condition.

- 12. Landscaping shall be installed in a professional workmanlike manner that is consistent and accepted throughout the industry. All landscape and irrigation work shall be performed by experienced persons familiar with scope of project.
- 13. All landscape material and labor is to be guaranteed for a period of one full year from the time of completion.
- 14. When planting 'Balled and Burlapped' product, remove all burlap, string & wire from any B&B plant material, cut and remove jute strings. Gently place in tact Rootbal into planting pit. If rootball breaks or is not solid - the plant is unacceptable and shall be replaced.

# 15. Street trees shall be high branching with canopy that starts at least 6' above finish grade.

- 16. All plant I.D. tags are to remain on the plant material until final inspection has been completed. Once approved all plant I.D. tags shall be removed and discarded appropriately.
- 17. Trees shall be cared for in accordance with the American National Standards Institute (ANSI) standard practices for trees, shrubs and other woody plant maintenance (ANSI 300) in order to allow them to reach there mature height and
- 18. Pruning of street trees shall be performed per the ANSI 300 standards so as to maintain the natural form of the tree, encourage vigorous growth to a mature spread and height, and avoid weakening the tree to create a hazard. Street trees shall not be topped pollarded, or otherwise pruned in a manner contrary to these goals, unless there is no practicable alternative that would preserve essential utility services.
- 19. Plant material selected is drought tolerant or native species. The project proponent (property Owner) shall be responsible for maintaining and watering all plant material throughout the first growing season and in times of drought.

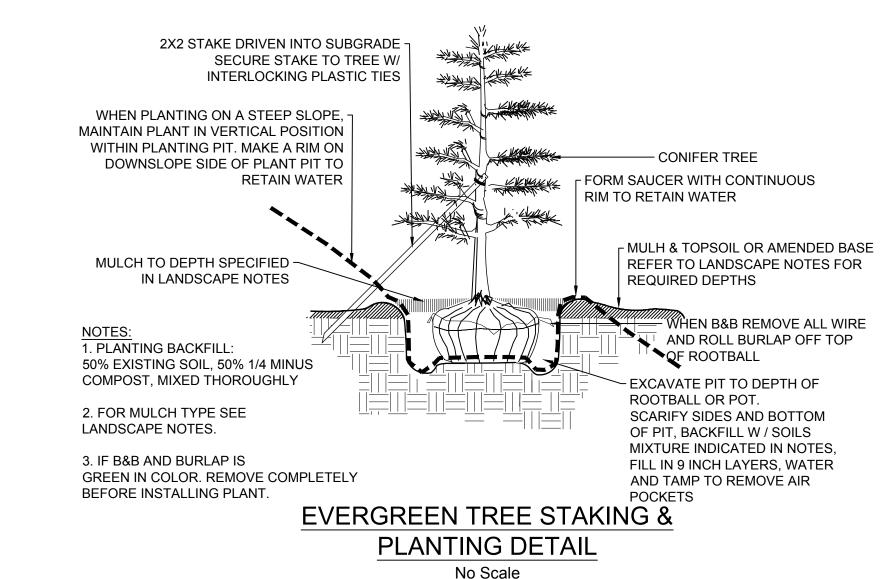
Temporary irrigation shall be provided via TREE GATOR BAGS attached to each tree. The bags shall be filled when  $\frac{1}{4}$  empty - approximately 1 time per week and as needed during drought months. The bags will remain on the trees for the establishment period of two summer seasons afterwhich they shall be removed by the owner.

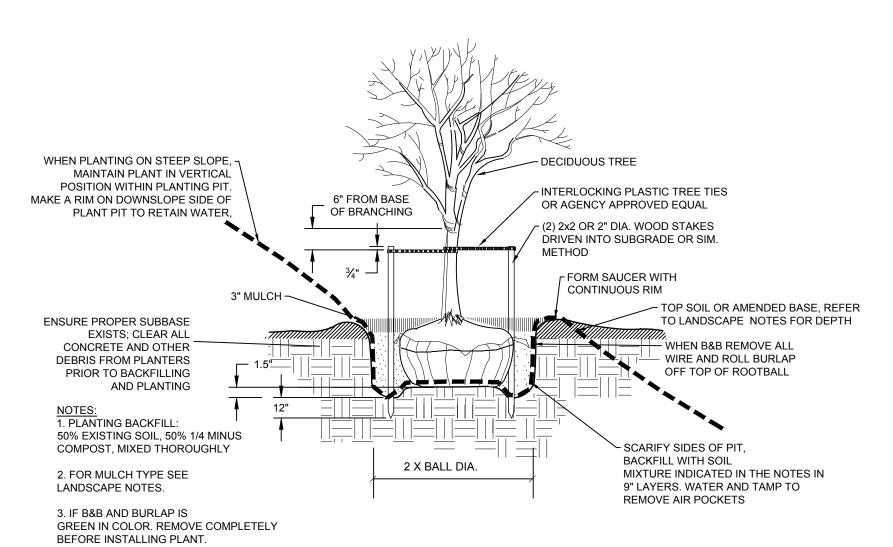
Owner may elect to have the contractor hired to water and warranty the plants for the establishment period. For planting warranties from contractor to be ensured, contractor shall be responsible for watering the plant material and keeping the mulch ring weed free for the first growing season as part of the contract.

It is recommended to install the landscaping in the Spring (February - April) or Fall (October - December)when dormant but before hard freeze.

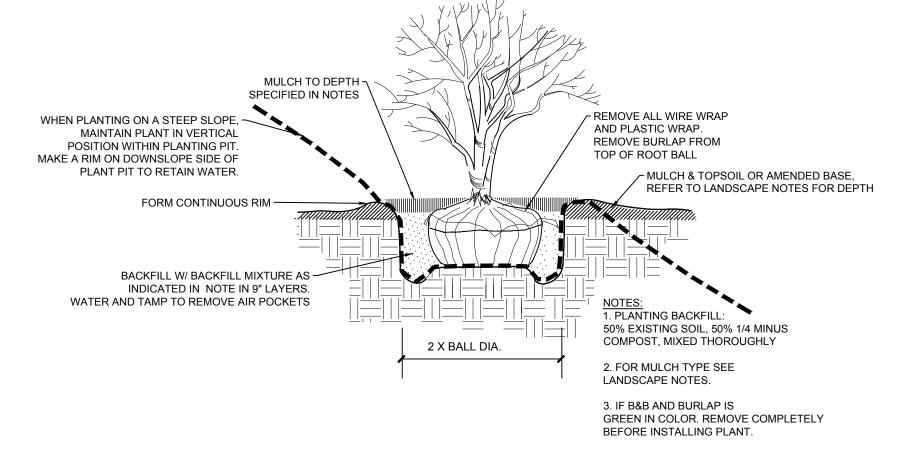
# **TEMPORARY IRRIGATION**

The project proponent shall ensure that a minimum of **one (1) inch of water is supplied each week** to the restoration area between May 1 and October 15 for a least the first two years following initial planting. The calculated amount of required water shall include both natural rainfall and temporary irrigation.

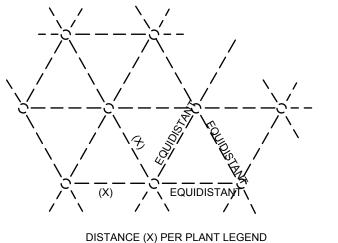




# **DECIDUOUS TREE PLANTING &** STAKING DETAIL No Scale



SHRUB PLANTING DETAIL No Scale



NOTES: ALL GROUNDCOVER SHALL BE PLANTED AT EQUAL TRIANGULAR SPACING AS SPECIFIED IN THE PLANT LEGEND.

No Scale

LOCATE GROUNDCOVER ONE-HALF OF SPECIFIED ON-CENTER SPACING FROM ANY CURB, SIDEWALK OR OTHER HARD SURFACE. Know what's below.

Call before you dig.

GROUNDCOVER PLANTING DETAIL

Landscape Architecture 253.460.6067

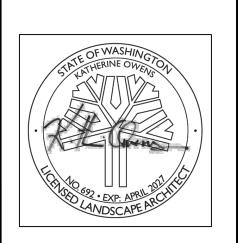
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**REVISIONS:** 

B. BUFFER ADJUSTED TO COMMENTS C. UPDATED TO CIVIL BASE D. UPDATED BUFFER PROPOSED E. REVISED TO PLAN BUFFER TO 110 SETBACK

DRAWING ISSUED FOR:

REVIEW **DATE:** MAY 6, 2025



2323

KLO

KLO

2323LSE

NONE

N.T.S.

PROJECT NO: FILE NAME: DRAWN BY: CHECKED BY: X-REFS: PLOT SCALE: DRAWING SCALES:

DRAWING CONTENTS

**LANDSCAPE DETAILS & NOTES** 

DRAWING NO.:

ORIG. SHEET SIZE 22X34

2 OF 2

# **APPENDIX C**

# **Construction Stormwater General Permit (CSWGP)**

# Stormwater Pollution Prevention Plan (SWPPP)

for 320 Todd Rd Devlopment

Prepared for:

Department of Ecology

City of Puyallup

Permittee / Owner	ner Developer Operator / Contrac	
EJ Fernandez		TBD

# 320 Todd Rd NE, Puyallup, WA 98371

## **Certified Erosion and Sediment Control Lead (CESCL)**

Name	Organization	Contact Phone Number

# **SWPPP Prepared By**

Name	Organization	Contact Phone Number
Justin Jones, PE	JMJ Team	(206) 596-2020

### **SWPPP Preparation Date**

06 / 02 / 2025

#### **Project Construction Dates**

Activity / Phase	Start Date	End Date
Begin Construction		

#### **GENERAL INSTRUCTIONS AND CAVEATS**

This template presents the recommended structure and content for preparation of a Construction Stormwater General Permit (CSWGP) Stormwater Pollution Prevention Plan (SWPPP).

The Department of Ecology's (Ecology) CSWGP requirements inform the structure and content of this SWPPP template; however, **you must customize this template to reflect the conditions of your site.** 

A Construction Stormwater Site Inspection Form can be found on Ecology's website.

#### **Using the SWPPP Template**

Each section will include instructions and space for information specific to your project. Please read the instructions for each section and provide the necessary information when prompted. This Word template can be modified electronically. You may add/delete text, copy and paste, edit tables, etc. Some sections may be completed with brief answers while others may require several pages of explanation.

Follow this link to a copy of the Construction Stormwater General Permit: <a href="https://www.ecology.wa.gov/Regulations-Permits/Permits-certifications/Stormwater-general-permits/Construction-stormwater-permit">https://www.ecology.wa.gov/Regulations-Permits/Permits-certifications/Stormwater-general-permits/Construction-stormwater-permit</a>

germits/ construction stormwater permit
Table of Contents
List of Tables
List of Appendices

### List of Acronyms and Abbreviations

Acronym / Abbreviation Explanation

**303(d)** Section of the Clean Water Act pertaining to Impaired Waterbodies

BFO Bellingham Field Office of the Department of Ecology

**BMP(s)** Best Management Practice(s)

CESCL Certified Erosion and Sediment Control Lead

CO<sub>2</sub> Carbon Dioxide

CRO Central Regional Office of the Department of Ecology

**CSWGP** Construction Stormwater General Permit

**CWA** Clean Water Act

**DMR** Discharge Monitoring Report

**DO** Dissolved Oxygen

**Ecology** Washington State Department of Ecology

EPA United States Environmental Protection Agency

ERO Eastern Regional Office of the Department of Ecology

ERTS Environmental Report Tracking System

ESC Erosion and Sediment Control

GULD General Use Level Designation

NPDES National Pollutant Discharge Elimination System

NTU Nephelometric Turbidity Units

NWRO Northwest Regional Office of the Department of Ecology

**pH** Power of Hydrogen

RCW Revised Code of Washington

SPCC Spill Prevention, Control, and Countermeasure

su Standard Units

**SWMMEW** Stormwater Management Manual for Eastern Washington **SWMMWW** Stormwater Management Manual for Western Washington

SWPPP Stormwater Pollution Prevention Plan

TESC Temporary Erosion and Sediment Control

SWRO Southwest Regional Office of the Department of Ecology

TMDL Total Maximum Daily Load

VFO Vancouver Field Office of the Department of Ecology

WAC Washington Administrative Code

WSDOT Washington Department of Transportation

WWHM Western Washington Hydrology Model

# **Project Information (1.0)**

Project/Site Name: 320 Todd Rd Devlopment

Street/Location: 320 Todd Rd NE

City: Puyallup State: WA Zip code: 98371

Subdivision:

Receiving waterbody: N/A

# **Existing Conditions (1.1)**

Total acreage (including support activities such as off-site equipment staging yards, material storage areas, borrow areas).

Total acreage: 0.762 Acres

Disturbed acreage: 0.762 Acres

Existing structures: None

Landscape topography: Flat

Drainage patterns: Overland Flow to existing landscaping

Existing Vegetation: Trees

Critical Areas (wetlands, streams, high erosion risk, steep or difficult to stabilize slopes):

None

List of known impairments for 303(d) listed or Total Maximum Daily Load (TMDL) for the receiving waterbody: None

Table 1 includes a list of suspected and/or known contaminants associated with the construction activity.

**Table 1 – Summary of Site Pollutant Constituents** 

Constituent (Pollutant)	Location	Depth	Concentration
None	N/A	N/A	N/A

### **Proposed Construction Activities (1.2)**

Description of site development (example: subdivision):

The project proposes the renovation of an existing two-story residential building and removal of an existing concrete driveway. The existing concrete will be replaced with an asphalt parking lot and driveway. Additionally, cement concrete walkways will be added to the site.

Description of construction activities (example: site preparation, demolition, excavation): Construction activities include: Clearing and Grubbing, Sawcutting, Fence Installation, Utility Installation, Asphalt Paving, and Installation of New Gravel.

Description of site drainage including flow from and onto adjacent properties. Must be consistent with Site Map in Appendix A:

The project proposes the construction of a new infiltration gallery, cement concrete pavement, and bioretention cells to allow for infiltration of stormwater into native soils below. An infiltration gallery will infiltrate 100% of the runoff from the proposed roof and asphalt parking lot and driveway. Runoff form the asphalt parking lot and driveway will first sheetflow to one of two bioretention cells to treat the PGIS before entering the underground infiltration gallery. The cement concrete pavement wills sheetflow into the existing landscaping onsite.

Description of final stabilization (example: extent of revegetation, paving, landscaping): Final stabilization of the site includes the following: On-site paving.

#### Contaminated Site Information:

Proposed activities regarding contaminated soils or groundwater (example: on-site treatment system, authorized sanitary sewer discharge):

Construction activities are not anticipated to disturb contaminated soils or groundwater on-site, as none are known to exist in the vicinity of the project.

# **Construction Stormwater Best Management Practices (BMPs) (2.0)**

The SWPPP is a living document reflecting current conditions and changes throughout the life of the project. These changes may be informal (i.e. hand-written notes and deletions). Update the SWPPP when the CESCL has noted a deficiency in BMPs or deviation from original design.

# The 12 Elements (2.1)

# **Element 1: Preserve Vegetation / Mark Clearing Limits (2.1.1)**

List and describe BMPs: BMP C102 – Buffer Zones

BMP C103 – High Visibility Plastic or Metal Fence

Lath & Flagging:

Prior to beginning land disturbing activities, including clearing and grading, all clearing limits and trees that are to be preserved within the construction area shall be clearly marked, both in the field and on the plans, to prevent damage and off-site impacts. Barrier fences shall be constructed as shown on the Temporary Erosion &

Sediment Control Plans and in accordance with BMP C103.

Installation Schedules:

Inspection and Maintenance plan:

# **Element 2: Establish Construction Access (2.1.2)**

List and describe BMPs: BMP C105 – Stabilized Construction Entrance: The Proposed

driveway entrance will be used as a construction entrance.

Contractor will maintain the existing driveway approach and road

to be free of sediment and debris.

BMP C107 – Construction Road/Parking Area Stabilization:

Adjacent roads and paved areas shall be cleaned thoroughly as needed. Sediment shall be removed from roads by shoveling or pickup sweeping and shall be transported to a controlled sediment disposal area.

Installation Schedules:

Inspection and Maintenance plan:

# **Element 3: Control Flow Rates (2.1.3)**

Will you construct stormwater retention and/or detention facilities? Yes No

Will you use permanent infiltration ponds or other low impact development (example: rain gardens, bio-retention, porous pavement) to control flow during construction?

Yes

No

List and describe BMPs: Properties downstream from the development site shall be

protected from erosion due to any increases in the volume, velocity, and peak flow rate stormwater runoff from the project site. If off-site discharges do occur, temporary basins shall be

installed prior to the points of discharge.

Installation Schedules:

Inspection and Maintenance plan:

# **Element 4: Install Sediment Controls (2.1.4)**

List and describe BMPs: BMP C230 – Straw Bale Barrier: Straw bale barriers shall be

installed as necessary to prevent sediment in construction

stormwater from entering existing storm systems.

BMP C233 – Silt Fence: A silt fence will be installed as noted on the TESC plan along existing vegetation to prevent stormwater

runoff from leaving the site.

BMP C235 – Straw Wattles: Straw wattle barriers shall be installed as necessary to prevent sediment in construction

stormwater from entering existing storm systems.

Installation Schedules:

Inspection and Maintenance plan:

# Element 5: Stabilize Soils (2.1.5)

#### **West of the Cascade Mountains Crest**

Season	Dates	Number of Days Soils Can be Left Exposed
During the Dry Season	May 1 – September 30	7 days
During the Wet Season	October 1 – April 30	2 days

Anticipated project dates: Start date: End date:

Will you construct during the wet season?



No

List and describe BMPs: BMP C122 – Nets & Blankets: Nets and Blankets shall be installed

to stabilize exposed soils/piles/slopes on site.

BMP C123 - Plastic Covering: Plastic Covering shall be installed

to stabilize exposed soils/piles/slopes on site.

All exposed and unworked soils shall be stabilized by application of effective BMPs, which protect the soil from the erosive forces of raindrop impact, flowing water, and wind erosion. From October 1 through April 30, no soils shall remain exposed and unworked for more than 2 days. From May 1 to September 30, no soils shall remain exposed and unworked for more than 7 days. This condition applies to all soils on site, whether at final grade or not. Additionally, except where approved chemical treatment, full dispersion, or infiltration is practiced, clearing, grading, and other soil disturbing activities are prohibited between November 1 and February 28.

In areas where the soils will remain unworked for more than 30 days or have reached final grade, the areas shall be graveled to stabilize exposed soils. If the slope is 2H:1V or greater with at least 10 feet of vertical relief, nets or blankets shall be used according to BMP C122. Sod shall be used in accordance with BMP C124 for disturbed areas that require immediate vegetative cover. Dust control shall be used as needed to prevent wind transport of dust from disturbed soil surfaces and in accordance with BMP C140.

Installation Schedules:

Inspection and Maintenance plan:

# **Element 6: Protect Slopes (2.1.6)**

Will steep slopes be present at the site during construction? Yes

List and describe BMPs:

Slopes will be stabilized as indicated in Element No. 5 above. In addition, the following BMPs may be implemented where appropriate:

BMP C130 – Surface Roughening BMP C200 – Interceptor Dike and Swale BMP C205 – Subsurface Drains BMP C207 – Check Dams

Installation Schedules:

Inspection and Maintenance plan:

# **Element 7: Protect Drain Inlets (2.1.7)**

List and describe BMPs:	N/A, no existing drainage structures onsite or downstream		
Installation Schedules:			
Inspection and Maintenance	e plan:		
Responsible Staff:			

# Element 8: Stabilize Channels and Outlets (2.1.8)

Provide stabilization, including armoring material, adequate to prevent erosion of outlets, adjacent stream banks, slopes, and downstream reaches, will be installed at the outlets of all conveyance systems.

List and describe BMPs: BMP C209 – Outlet Proection:

Stabilizing channel and outlets is not applicable as the project will continue to discharge stormwater to the existing stormwater

conveyance system on-site.

Installation Schedules:

Inspection and Maintenance plan:

# **Element 9: Control Pollutants (2.1.9)**

The following pollutants are anticipated to be present on-site:

#### Table 2 - Pollutants

Pollutant (and source, if applicable)	
N/A	

List and describe BMPs: BMP C152 - Sawcutting and Surface Pollution Prevention BMP C153 – Material Delivery, Storage Containment

All pollutants, including waste materials and demolition debris, that occur on site during construction shall be handled and disposed of in a manner that does not cause contamination of stormwater.

Cover, containment, and protection from vandalism shall be provided for all chemicals, liquid products, petroleum products, and non-inert wastes present on the site (see Chapter 173 304 WAC for the definition of inert waste). On-site fueling tanks shall include secondary containment.

Maintenance and repair of heavy equipment and vehicles involving oil changes, hydraulic system drain down, solvent and de-greasing cleaning operations, fuel tank drain down and removal, and other activities that may result in discharge or spillage of pollutants to the ground or into stormwater runoff must be conducted using spill prevention measures, such as drip pans. Contaminated surfaces shall be cleaned immediately following any discharge or spill incident. Spills should be reported to 911. Emergency repairs may be performed on-site using temporary plastic placed beneath and, if raining, over the vehicle. Application of agricultural chemicals, including fertilizers and pesticides, shall be conducted in a manner and at application rates that will not result in loss of chemical to stormwater runoff. Manufacturers' recommendations shall be followed for application rates and procedures.

Installation Schedules:

Inspection and Maintenance plan:

Responsible Staff:

Will maintenance, fueling, and/or repair of heavy equipment and vehicles occur on-site?

Installation Schedules:

Responsible Staff:

No

List and describe BMPs: BMP C152 - Sawcutting and Surface Pollution Prevention

BMP C153 – Material Delivery, Storage Containment

All pollutants, including waste materials and demolition debris, that occur on site during construction shall be handled and disposed of in a manner that does not cause contamination of stormwater.

Cover, containment, and protection from vandalism shall be provided for all chemicals, liquid products, petroleum products, and non-inert wastes present on the site (see Chapter 173 304 WAC for the definition of inert waste). On-site fueling tanks shall include secondary containment.

Maintenance and repair of heavy equipment and vehicles involving oil changes, hydraulic system drain down, solvent and de-greasing cleaning operations, fuel tank drain down and removal, and other activities that may result in discharge or spillage of pollutants to the ground or into stormwater runoff must be conducted using spill prevention measures, such as drip pans. Contaminated surfaces shall be cleaned immediately following any discharge or spill incident. Spills should be reported to 911. Emergency repairs may be performed on-site using temporary plastic placed beneath and, if raining, over the vehicle. Application of agricultural chemicals, including fertilizers and pesticides, shall be conducted in a manner and at application rates that will not result in loss of chemical to stormwater runoff. Manufacturers' recommendations shall be followed for application rates and procedures.

Inspection and Maintenance plan:
Responsible Staff:
Will wheel wash or tire bath system BMPs be used during construction? Yes  No
List and describe BMPs:
Installation Schedules:
Inspection and Maintenance plan:



No

If yes, check the source(s).

#### Table 3 – pH-Modifying Sources

None
Bulk cement
Cement kiln dust
Fly ash
Other cementitious materials
New concrete washing or curing waters
Waste streams generated from concrete grinding and sawing
Exposed aggregate processes
Dewatering concrete vaults
Concrete pumping and mixer washout waters
Recycled concrete
Other (i.e. calcium lignosulfate) [please describe]

List and describe BMPs: BMP C152 - Sawcutting and Surface Pollution Prevention

BMP C153 – Material Delivery, Storage Containment

All pollutants, including waste materials and demolition debris, that occur on site during construction shall be handled and disposed of in a manner that does not cause contamination of stormwater.

Cover, containment, and protection from vandalism shall be provided for all chemicals, liquid products, petroleum products, and non-inert wastes present on the site (see Chapter 173 304 WAC for the definition of inert waste). On-site fueling tanks shall include secondary containment.

Maintenance and repair of heavy equipment and vehicles involving oil changes, hydraulic system drain down, solvent and de-greasing cleaning operations, fuel tank drain down and removal, and other activities that may result in discharge or spillage of pollutants to the ground or into stormwater runoff must be conducted using spill prevention measures, such as drip pans. Contaminated surfaces shall be cleaned immediately following any discharge or spill incident. Spills should be reported to 911. Emergency repairs may be performed on-site using temporary plastic placed beneath and, if raining, over the vehicle. Application of agricultural chemicals, including fertilizers and pesticides, shall be conducted in a manner and at application rates that will not result in loss of chemical to stormwater runoff. Manufacturers' recommendations shall be followed for application rates and procedures.

Installation Schedules:

Inspection and Maintenance plan:

Responsible Staff:

Concrete trucks must not be washed out onto the ground, or into storm drains, open ditches, streets, or streams. Excess concrete must not be dumped on-site, except in designated concrete washout areas with appropriate BMPs installed.

# Element 10: Control Dewatering (2.1.10)

# Table 4 – Dewatering BMPs

	Infiltration
	Transport off-site in a vehicle (vacuum truck for legal disposal)
Χ	Ecology-approved on-site chemical treatment or other suitable treatment technologies
	Sanitary or combined sewer discharge with local sewer district approval (last resort)
	Use of sedimentation bag with discharge to ditch or swale (small volumes of localized dewatering)

ı	iet	and	describe	RMPs.
ı	∟iSt	anu	describe	DIVIES.

Installation Schedules:

Inspection and Maintenance plan:

# Element 11: Maintain BMPs (2.1.11)

All temporary and permanent Erosion and Sediment Control (ESC) BMPs shall be maintained and repaired as needed to ensure continued performance of their intended function.

Maintenance and repair shall be conducted in accordance with each particular BMP specification (see *Volume II of the SWMMWW or Chapter 7 of the SWMMEW*).

Visual monitoring of all BMPs installed at the site will be conducted at least once every calendar week and within 24 hours of any stormwater or non-stormwater discharge from the site. If the site becomes inactive and is temporarily stabilized, the inspection frequency may be reduced to once every calendar month.

All temporary ESC BMPs shall be removed within 30 days after final site stabilization is achieved or after the temporary BMPs are no longer needed.

Trapped sediment shall be stabilized on-site or removed. Disturbed soil resulting from removal of either BMPs or vegetation shall be permanently stabilized.

Additionally, protection must be provided for all BMPs installed for the permanent control of stormwater from sediment and compaction. BMPs that are to remain in place following completion of construction shall be examined and restored to full operating condition. If sediment enters these BMPs during construction, the sediment shall be removed and the facility shall be returned to conditions specified in the construction documents.

# **Element 12: Manage the Project (2.1.12)**

Clearing and grading activities for developments shall be permitted only if conducted pursuant to an approved site development plan (e.g., subdivision approval) that establishes permitted areas of clearing, grading, cutting, and filling. These permitted clearing and grading areas and any other areas required to preserve critical or sensitive areas, buffers, native growth protection easements, or tree retention areas as may be required by local jurisdictions, shall be delineated on the site plans and the development site.

Turbidity: For storms up to the water quality design event, turbidity downstream of a construction site may not increase more than 5 NTU, if upstream turbidity is 50 NTU or less, and may not increase more than 10 percent, if upstream turbidity is over 50 NTU. To the extent practicable, samples should be taken far enough downstream so that the construction site discharge has been well-mixed with the surface water. Whenever inspection and/or monitoring reveals that the BMPs identified in the Construction SWPPP are inadequate, due to the actual discharge of or potential to discharge a significant amount of any pollutant, appropriate BMPs or design changes shall be implemented as soon as possible.

pH: shall be within the range of 6.5 to 8.5 (freshwater) or 7.0 to 8.5 (marine water) with a human-caused variation within a range of less than 0.2 units. For Class A and lower water classifications, the permissible induced increase is 0.5 units (Stormwater Management Manual for Western Washington, Department of Ecology, February 2005 Edition).

A Certified Erosion and Sediment Control Specialist be identified by the contractor at a later date. This information will be added to this CSWPPP.

#### Table 5 – Management

Χ	Design the project to fit the existing topography, soils, and drainage patterns
Х	Emphasize erosion control rather than sediment control
Χ	Minimize the extent and duration of the area exposed
Х	Keep runoff velocities low
Х	Retain sediment on-site
Х	Thoroughly monitor site and maintain all ESC measures
Х	Schedule major earthwork during the dry season
	Other (please describe)

Table 6 – BMP Implementation Schedule

Phase of Construction Project	Stormwater BMPs	Date	Wet/Dry Season
[Insert construction activity]	[Insert BMP]	[MM/DD/YYYY]	[Insert Season]
Phase of Construction Project	Stormwater BMPs	Date	Wet/Dry Season

[Insert construction activity]	[Insert BMP]	[MM/DD/YYYY]	[Insert Season]

### Element 13: Protect Low Impact Development (LID) BMPs (2.1.13)

Protect all permeable pavement BMPs from sedimentation through installation and maintenance of erosion

and sediment control BMPs on portions of the site that drain into the permeable pavement BMPs. Restore the BMPs to their fully functioning condition if they accumulate sediment during construction. Restoring the BMP must include removal of sediment and any sediment-laden permeable pavement soils, and replacing the removed soils with soils meeting the design specification.

Prevent compacting of soils in areas of new permeable pavement BMPs by excluding construction equipment and foot traffic. Protect completed lawn and landscaped areas from compaction due to construction equipment.

Control erosion and avoid introducing sediment from surrounding land uses onto permeable pavements. Do not allow muddy construction equipment on the base material or pavement. Do not allow sediment-laden runoff onto permeable pavements or base materials.

Pavement fouled with sediments or no longer passing an initial infiltration test must be cleaned using procedures in accordance with this manual or the manufacturer's procedures.

Keep all heavy equipment off existing soils under LID facilities that have been excavated to final grade to retain the infiltration rate of the soils.

# Pollution Prevention Team (3.0)

**Table 7 – Team Information** 

Title	Name(s)	Phone Number
Certified Erosion and		
Sediment Control Lead		
(CESCL)		
Resident Engineer		
Emergency Ecology		
Contact		
Emergency Permittee/		
Owner Contact		
Non-Emergency Owner		
Contact		
Monitoring Personnel		
Ecology Regional Office	[Insert Regional Office]	[Insert General Number]

# **Monitoring and Sampling Requirements (4.0)**

Monitoring includes visual inspection, sampling for water quality parameters of concern, and documentation of the inspection and sampling findings in a site log book. A site log book will be maintained for all on-site construction activities and will include:

- A record of the implementation of the SWPPP and other permit requirements
- Site inspections
- Stormwater sampling data

File a blank form under Appendix D.

The site log book must be maintained on-site within reasonable access to the site and be made available upon request to Ecology or the local jurisdiction.

Numeric effluent limits may be required for certain discharges to 303(d) listed waterbodies. See CSWGP Special Condition S8 and Section 5 of this template.

Complete the following paragraph for sites that discharge to impaired waterbodies for fine sediment, turbidity, phosphorus, or pH:

The receiving waterbody, insert waterbody name, is impaired for: insert impairment. All stormwater and dewatering discharges from the site are subject to an **effluent limit** of 8.5 su for pH and/or 25 NTU for turbidity.

# Site Inspection (4.1)

Site inspections will be conducted at least once every calendar week and within 24 hours following any discharge from the site. For sites that are temporarily stabilized and inactive, the required frequency is reduced to once per calendar month.

The discharge point(s) are indicated on the <u>Site Map</u> (see Appendix A) and in accordance with the applicable requirements of the CSWGP.

# **Stormwater Quality Sampling (4.2)**

# **Turbidity Sampling (4.2.1)**

Requirements include calibrated turbidity meter or transparency tube to sample site discharges for compliance with the CSWGP. Sampling will be conducted at all discharge points at least once per calendar week.

Method for sampling turbidity:

#### Table 8 - Turbidity Sampling Method

	Turbidity Meter/Turbidimeter (required for disturbances 5 acres or greater in size)
Χ	Transparency Tube (option for disturbances less than 1 acre and up to 5 acres in size)

The benchmark for turbidity value is 25 nephelometric turbidity units (NTU) and a transparency less than 33 centimeters.

If the discharge's turbidity is 26 to 249 NTU <u>or</u> the transparency is less than 33 cm but equal to or greater than 6 cm, the following steps will be conducted:

- 1. Review the SWPPP for compliance with Special Condition S9. Make appropriate revisions within 7 days of the date the discharge exceeded the benchmark.
- 2. Immediately begin the process to fully implement and maintain appropriate source control and/or treatment BMPs as soon as possible. Address the problems within 10 days of the date the discharge exceeded the benchmark. If installation of necessary treatment BMPs is not feasible within 10 days, Ecology may approve additional time when the Permittee requests an extension within the initial 10-day response period.
- 3. Document BMP implementation and maintenance in the site log book.

If the turbidity exceeds 250 NTU <u>or</u> the transparency is 6 cm or less at any time, the following steps will be conducted:

- Telephone or submit an electronic report to the applicable Ecology Region's Environmental Report Tracking System (ERTS) within 24 hours. https://www.ecology.wa.gov/About-us/Get-involved/Report-an-environmental-issue
  - <u>Central Region</u> (Benton, Chelan, Douglas, Kittitas, Klickitat, Okanogan, Yakima): (509) 575-2490
  - Eastern Region (Adams, Asotin, Columbia, Ferry, Franklin, Garfield, Grant, Lincoln, Pend Oreille, Spokane, Stevens, Walla Walla, Whitman): (509) 329-3400
  - Northwest Region (King, Kitsap, Island, San Juan, Skagit, Snohomish, Whatcom): (425) 649-7000
  - Southwest Region (Clallam, Clark, Cowlitz, Grays Harbor, Jefferson, Lewis, Mason, Pacific, Pierce, Skamania, Thurston, Wahkiakum,): (360) 407-6300
- 2. Immediately begin the process to fully implement and maintain appropriate source control and/or treatment BMPs as soon as possible. Address the problems within 10 days of the date the discharge exceeded the benchmark. If installation of necessary treatment BMPs is not feasible within 10 days, Ecology may approve additional time when the Permittee requests an extension within the initial 10-day response period
- 3. Document BMP implementation and maintenance in the site log book.
- 4. Continue to sample discharges daily until one of the following is true:
  - Turbidity is 25 NTU (or lower).
  - Transparency is 33 cm (or greater).
  - Compliance with the water quality limit for turbidity is achieved.
    - 1 5 NTU over background turbidity, if background is less than 50 NTU
    - 1% 10% over background turbidity, if background is 50 NTU or greater
  - The discharge stops or is eliminated.

# pH Sampling (4.2.2)

pH monitoring is required for "Significant concrete work" (i.e. greater than 1000 cubic yards poured concrete or recycled concrete over the life of the project). The use of engineered soils (soil amendments including but not limited to Portland cement-treated base [CTB], cement kiln dust [CKD] or fly ash) also requires pH monitoring.

For significant concrete work, pH sampling will start the first day concrete is poured and continue until it is cured, typically three (3) weeks after the last pour.

For engineered soils and recycled concrete, pH sampling begins when engineered soils or recycled concrete are first exposed to precipitation and continues until the area is fully stabilized.

If the measured pH is 8.5 or greater, the following measures will be taken:

- 1. Prevent high pH water from entering storm sewer systems or surface water.
- 2. Adjust or neutralize the high pH water to the range of 6.5 to 8.5 su using appropriate technology such as carbon dioxide (CO<sub>2</sub>) sparging (liquid or dry ice).
- 3. Written approval will be obtained from Ecology prior to the use of chemical treatment other than CO<sub>2</sub> sparging or dry ice.

Method for sampling pH:

#### Table 8 – pH Sampling Method

pH meter
pH test kit
Wide range pH indicator paper

# Discharges to 303(d) or Total Maximum Daily Load (TMDL) Waterbodies (5.0)

# 303(d) Listed Waterbodies (5.1)

of discharge.

303(a) Listed waterbodies (5.1)
Is the receiving water 303(d) (Category 5) listed for turbidity, fine sediment, phosphorus, or pH?
Yes No
List the impairment(s):
[Insert text here]
The receiving waterbody, insert waterbody name, is impaired for: insert impairment. All stormwater and dewatering discharges from the site are subject to an <b>effluent limit</b> of 8.5 su for pH and/or 25 NTU for turbidity.
List and describe BMPs:
[Insert text here]
TMDL Waterbodies (5.2)
Waste Load Allocation for CWSGP discharges:
[Insert text here]
List and describe BMPs:
[Insert text here]
Discharges to TMDL receiving waterbodies will meet in-stream water quality criteria at the point

The Construction Stormwater General Permit Proposed New Discharge to an Impaired Water Body form is included in Appendix F.

# Reporting and Record Keeping (6.0)

## **Record Keeping (6.1)**

## Site Log Book (6.1.1)

A site log book will be maintained for all on-site construction activities and will include:

- A record of the implementation of the SWPPP and other permit requirements
- Site inspections
- Sample logs

### **Records Retention (6.1.2)**

Records will be retained during the life of the project and for a minimum of three (3) years following the termination of permit coverage in accordance with Special Condition S5.C of the CSWGP.

Permit documentation to be retained on-site:

- CSWGP
- Permit Coverage Letter
- SWPPP
- Site Log Book

Permit documentation will be provided within 14 days of receipt of a written request from Ecology. A copy of the SWPPP or access to the SWPPP will be provided to the public when requested in writing in accordance with Special Condition S5.G.2.b of the CSWGP.

# **Updating the SWPPP (6.1.3)**

The SWPPP will be modified if:

- Found ineffective in eliminating or significantly minimizing pollutants in stormwater discharges from the site.
- There is a change in design, construction, operation, or maintenance at the construction site that has, or could have, a significant effect on the discharge of pollutants to waters of the State.

The SWPPP will be modified within seven (7) days if inspection(s) or investigation(s) determine additional or modified BMPs are necessary for compliance. An updated timeline for BMP implementation will be prepared.

# Reporting (6.2)

# **Discharge Monitoring Reports (6.2.1)**

Cumulative soil disturbance is less than one (1) acre; therefore, Discharge Monitoring Reports (DMRs) will not be submitted to Ecology because water quality sampling is not being conducted at the site.

Cumulative soil disturbance is one (1) acre or larger; therefore, Discharge Monitoring Reports (DMRs) will be submitted to Ecology monthly. If there was no discharge during a given monitoring period the DMR will be submitted as required, reporting "No Discharge". The DMR due date is fifteen (15) days following the end of each calendar month.

DMRs will be reported online through Ecology's WQWebDMR System.

https://www.ecology.wa.gov/Regulations-Permits/Guidance-technical-assistance/Water-quality-permits-guidance/WQWebPortal-guidance

# **Notification of Noncompliance (6.2.2)**

If any of the terms and conditions of the permit is not met, and the resulting noncompliance may cause a threat to human health or the environment, the following actions will be taken:

- 1. Ecology will be notified within 24-hours of the failure to comply by calling the applicable Regional office ERTS phone number (Regional office numbers listed below).
- 2. Immediate action will be taken to prevent the discharge/pollution or otherwise stop or correct the noncompliance. If applicable, sampling and analysis of any noncompliance will be repeated immediately and the results submitted to Ecology within five (5) days of becoming aware of the violation.
- 3. A detailed written report describing the noncompliance will be submitted to Ecology within five (5) days, unless requested earlier by Ecology.

Anytime turbidity sampling indicates turbidity is 250 NTUs or greater, or water transparency is 6 cm or less, the Ecology Regional office will be notified by phone within 24 hours of analysis as required by Special Condition S5.A of the CSWGP.

 <u>Central Region</u> at (509) 575-2490 for Benton, Chelan, Douglas, Kittitas, Klickitat, Okanogan, or Yakima County

- <u>Eastern Region</u> at (509) 329-3400 for Adams, Asotin, Columbia, Ferry, Franklin, Garfield, Grant, Lincoln, Pend Oreille, Spokane, Stevens, Walla Walla, or Whitman County
- Northwest Region at (425) 649-7000 for Island, King, Kitsap, San Juan, Skagit, Snohomish, or Whatcom County
- <u>Southwest Region</u> at (360) 407-6300 for Clallam, Clark, Cowlitz, Grays Harbor, Jefferson, Lewis, Mason, Pacific, Pierce, Skamania, Thurston, or Wahkiakum

#### Include the following information:

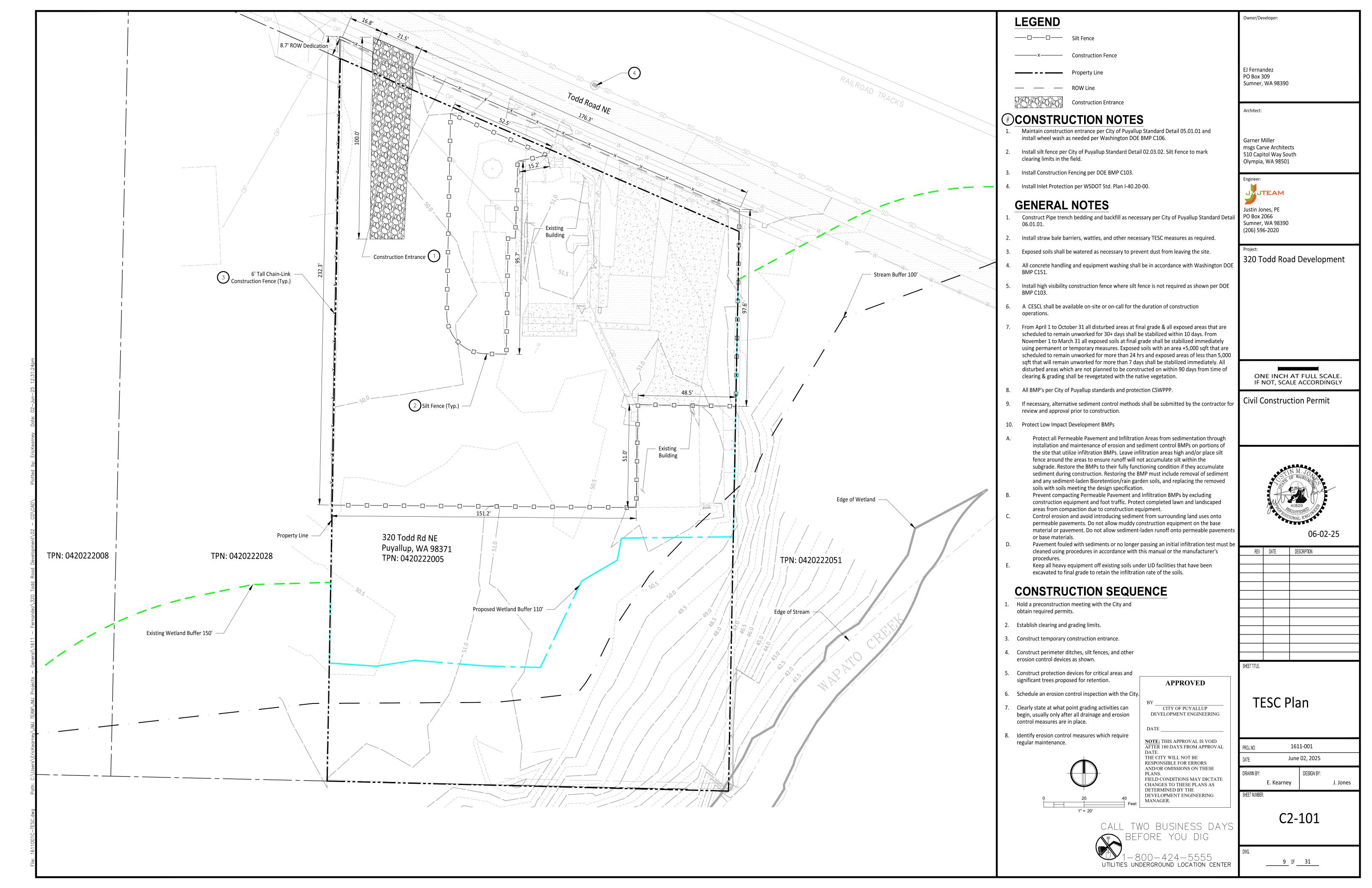
- 1. Your name and / Phone number
- 2. Permit number
- 3. City / County of project
- 4. Sample results
- 5. Date / Time of call
- 6. Date / Time of sample
- 7. Project name

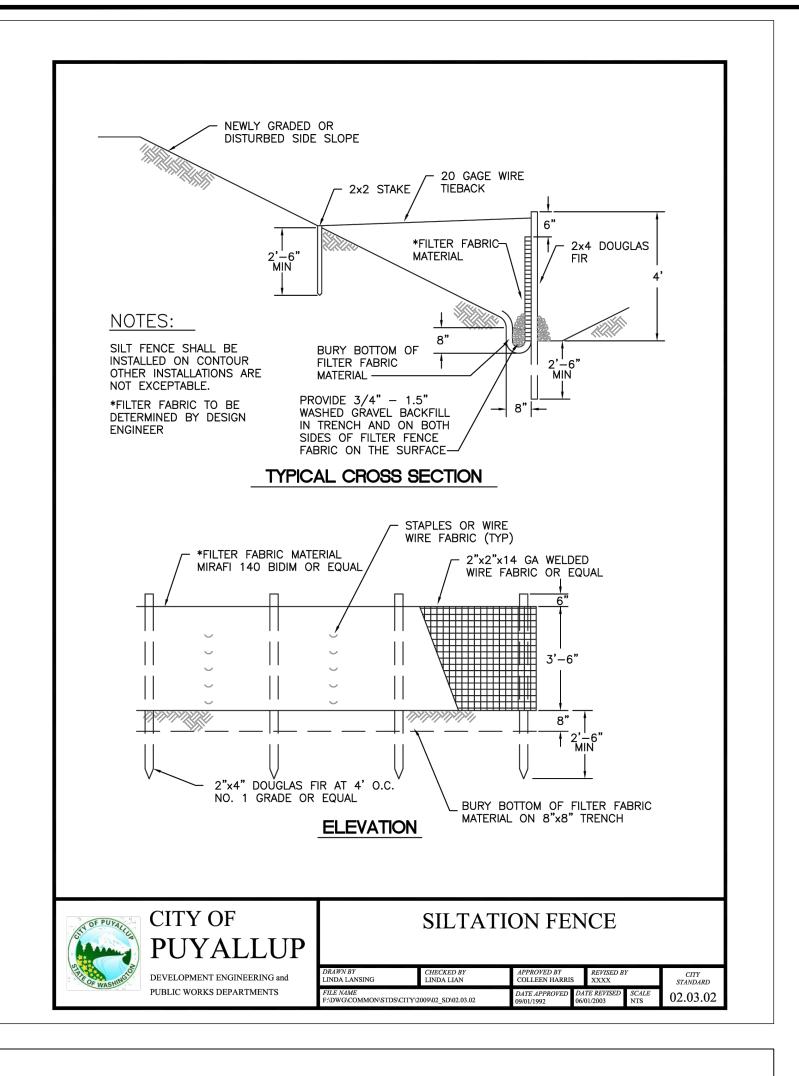
In accordance with Special Condition S4.D.5.b of the CSWGP, the Ecology Regional office will be notified if chemical treatment other than CO<sub>2</sub> sparging is planned for adjustment of high pH water.

# Appendix/Glossary

- A. Site Map
- B. BMP Detail
- C. Correspondence
- **D. Site Inspection Form**
- E. Construction Stormwater General Permit (CSWGP)
- F. 303(d) List Waterbodies / TMDL Waterbodies Information
- **G. Contaminated Site Information**
- **H. Engineering Calculations**

# Appendix A: Site Map





CONDITIONS WHERE PRACTICE APPLIES

AND FLAT AREA (LESS THAN 5% SLOPE).

BUT NO GREATER THAN 24-INCHES HIGH.

1/2-INCHES LONG.

CITY OF

1. BLOCK AND GRAVEL FILTER - APPLICABLE FOR AREAS GREATER THAN 5% SLOPE.

1. BLOCK AND GRAVEL FILTER - INSTALLATION PROCEDURE

OF MESH IS NECESSARY, OVERLAP THE STRIPS. PLACE FILTER FABRIC\* OVER WIRE MESH.

HIEGHT OF THE BARRIER CAN BE VARIED, DEPENDING ON DESIGN NEEDS, BY STACKING COMBINATIONS OF

D: PILE STONES AGAINST THE WIRE MESH TO THE TOP OF THE BLOCKS. USE 3/4" MINUS WASHED GRAVEL.

APART AND DRIVE THEM AT LEAST 8-INCHES INTO THE GROUND. THE STAKES MUST BE AT LEAST 3 FEET

B: EXCAVATE A TRENCH APPROXIMATELY 8-INCHES WIDE AND 12-INCHES DEEP AROUND THE OUTSIDE

C: STAPLE THE FILTER FABRIC\* TO THE WOODEN STAKES SO THAT 32-INCHES OF THE FABRIC EXTENDS AND CAN BE FORMED INTO THE TRENCH, AND USE HEAVY-DUTY WIRE STAPLES AT LEAST

A: EXCAVATE A 4-INCH DEEP TRENCH AROUND THE INLET. MAKE THE TRENCH AS WIDE AS A STRAW BALE.

B: ORIENT STRAW BALES WITH THE BINDINGS AROUND THE SIDES OF THE BALES RATHER THAN OVER AND

C: PLACE BALES LENGTHWISE AROUND THE INLET AND PRESS THE ENDS OF ADJACENT BALES SECURELY

F: WEDGE LOOSE STRAW BETWEEN BALES TO PREVENT WATER FROM FLOWING BETWEEN BALES.

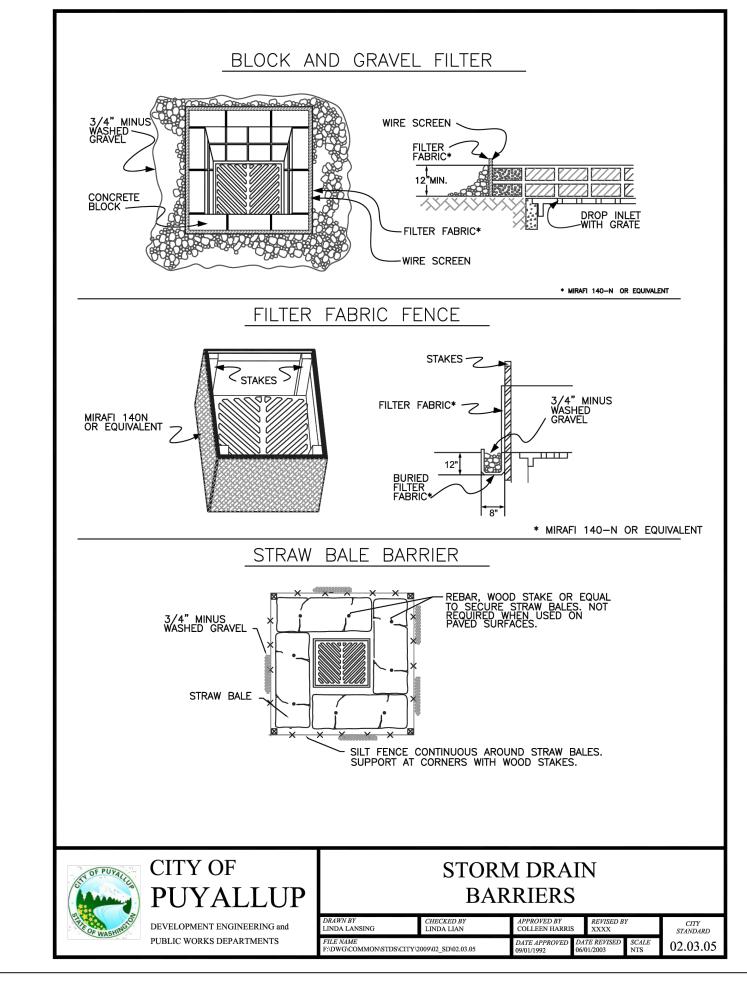
D: DRIVE TWO 2-INCH BY 2-INCH STAKES THROUGH EACH BALE TO ANCHOR THE BALE SECURELY IN PLACE.

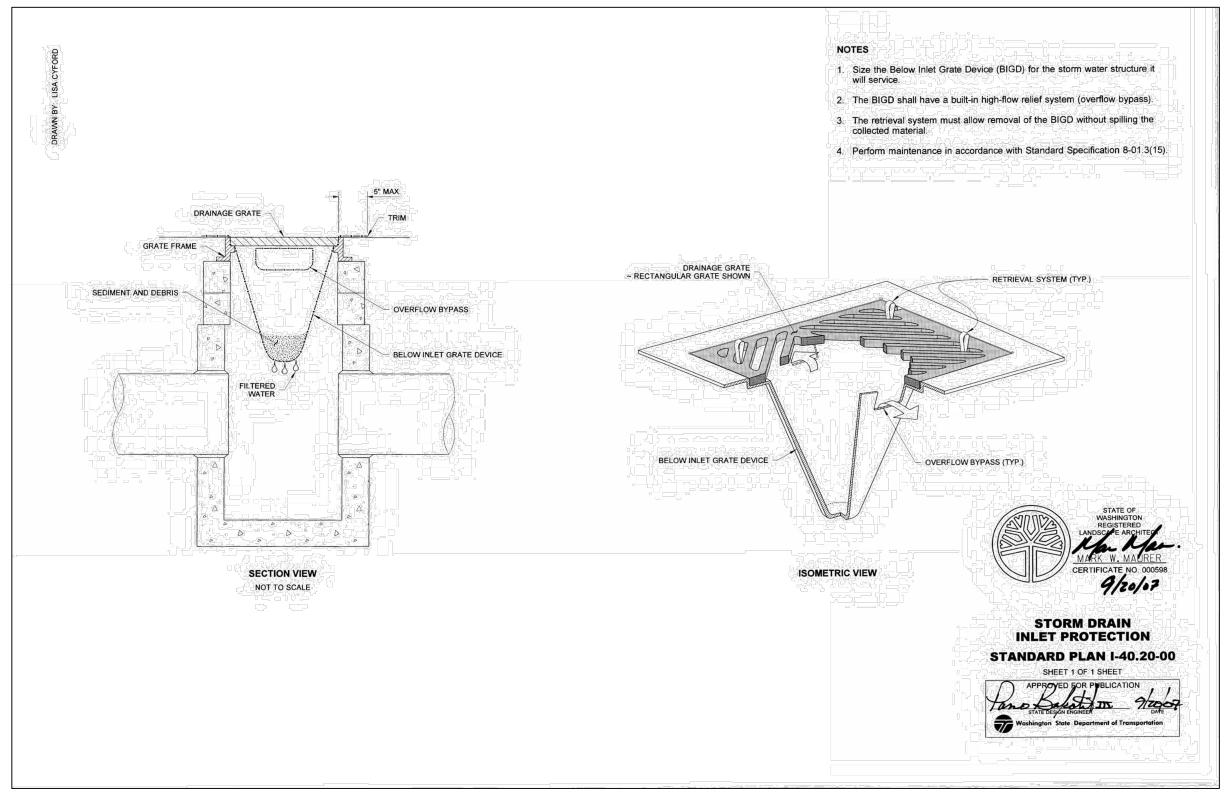
2. FILTER FABRIC FENCE - INSTALLATION PROCEDURE

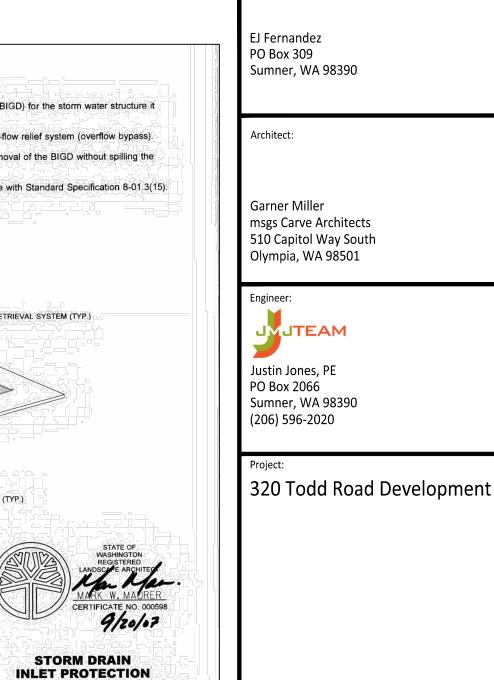
D: BACKFILL THE TRENCH WITH 3/4-INCH MINUS WASHED GRAVEL ALL THE WAY AROUND.

3. STRAW BALE BARRIER — INSTALLATION PROCEDURE

E: BACKFILL THE EXCAVATED SOIL AND COMPACT IT AGAINST THE BALE.







Owner/Developer:

ONE INCH AT FULL SCALE. IF NOT, SCALE ACCORDINGLY

**Civil Construction Permit** 



06-02-25

REV	DATE	DESCRIPTION
	1	

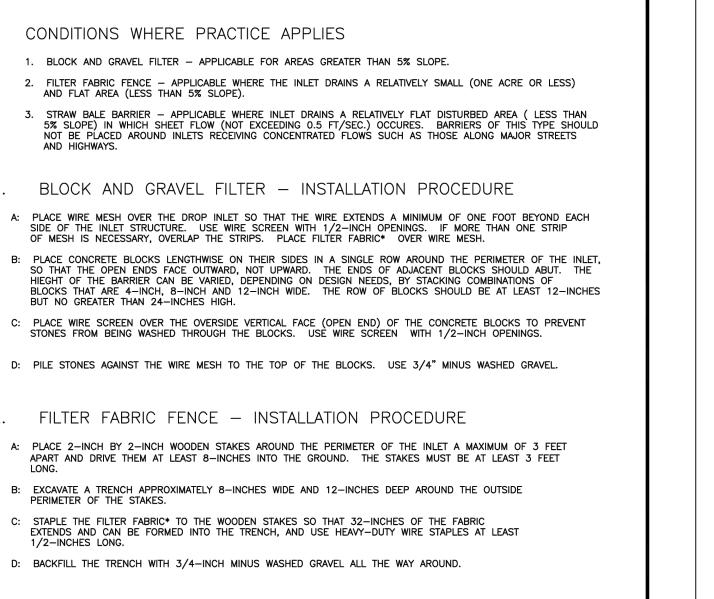
SHEET NUMBER.

**TESC Details** 

1611-001 June 02, 2025

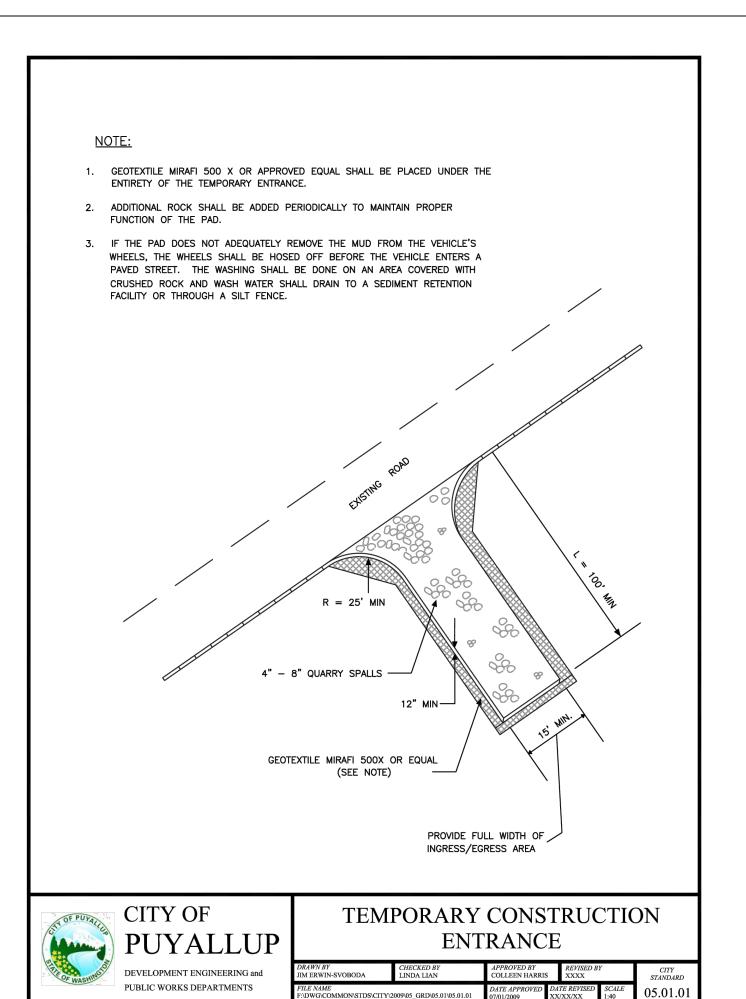
DESIGN BY: E. Kearney

C2-201



\* MIRAFI 140-N OR EQUIVALENT

STORM DRAIN



1. ALL LIMITS OF CLEARING AND AREAS OF VEGETATION PRESERVATION AS PRESCRIBED ON THE PLANS SHALL BE CLEARLY FLAGGET
IN THE FIELD AND OBSERVED DURING CONSTRUCTION.
2. ALL REQUIRED SEDIMENTATION AND EROSION CONTROL FACILITIES MUST BE CONSTRUCTED AND IN OPERATION PRIOR TO ANY LAM
CLEARING AND/OR OTHER CONSTRUCTION TO ENSURE THAT SEDIMENT LADEN WATER DOES NOT ENTER THE NATURAL DRAINAGE
SYSTEM. THE CONTRACTOR SHALL SCHEDULE AN INSPECTION OF THE EROSION CONTROL FACILITIES PRIOR TO ANY LAND CLEARING

AND/OR CONSTRUCTION. ALL EROSION AND SEDIMENT FACILITIES SHALL BE MAINTAINED IN A SATISFACTORY CONDITION AS DETERMINED BY THE CITY, UNTIL SUCH TIME THAT CLEARING AND/OR CONSTRUCTION IS COMPLETED AND THE POTENTIAL FOR ON-SITE EROSION HAS PASSED. THE IMPLEMENTATION, MAINTENANCE, REPLACEMENT, AND ADDITIONS TO THE EROSION AND SEDIMENTATION CONTROL SYSTEMS SHALL BE THE RESPONSIBILITY OF THE PERMITEE.

3. THE EROSION AND SEDIMENTATION CONTROL SYSTEM FACILITIES DEPICTED ON THESE PLANS ARE INTENDED TO BE MINIMUM REQUIREMENTS TO MEET ANTICIPATED SITE CONDITIONS. AS CONSTRUCTION PROGRESSES AND UNEXPECTED OR SEASONAL CONDITIONS DICTATE, FACILITIES WILL BE NECESSARY TO ENSURE COMPLETE SILTATION CONTROL ON THE SITE. DURING THE COURSE OF CONSTRUCTION, IT SHALL BE THE OBLIGATION AND RESPONSIBILITY OF THE PERMITEE TO ADDRESS ANY NEW CONDITIONS THAT MAY BE CREATED BY HIS ACTIVITIES AND TO PROVIDE ADDITIONAL FACILITIES, OVER AND ABOVE THE MINIMUM REQUIREMENTS, AS MAY BE NEEDED TO PROTECT ADJACENT PROPERTIES, SENSITIVE AREAS, NATURAL WATER COURSES, AND/OR STORM DRAINAGE SYSTEMS.

4. APPROVAL OF THESE PLANS IS FOR GRADING, TEMPORARY DRAINAGE, EROSION AND SEDIMENTATION CONTROL ONLY. IT DOES NOT CONSTITUTE AN APPROVAL OF PERMANENT STORM DRAINAGE DESIGN, SIZE OR LOCATION OF PIPES, RESTRICTORS, CHANNELS, OR RETENTION FACILITIES.

5. ANY DISTURBED AREA WHICH HAS BEEN STRIPPED OF VEGETATION AND WHERE NO FURTHER WORK IS ANTICIPATED FOR A PERIOD OF 30 DAYS OR MORE, MUST BE IMMEDIATELY STABILIZED WITH MULCHING, GRASS PLANTING, OR OTHER APPROVED EROSION CONTROL TREATMENT APPLICABLE TO THE TIME OF YEAR IN QUESTION. GRASS SEEDING ALONE WILL BE ACCEPTABLE ONLY DURING THE MONTHS OF APRIL THROUGH SEPTEMBER INCLUSVE. SEEDING MAY PROCEED OUTSIDE THE SPECIFIED TIME PERIOD WHENEVER IT IS IN THE INTEREST OF THE PERMITEE BUT MUST BE AUGMENTED WITH MULCHING, NETTING, OR OTHER TREATMENT APPROVED BY THE

6. IN CASE EROSION OR SEDIMENTATION OCCURS TO ADJACENT PROPERTIES, ALL CONSTRUCTION WORK WITHIN THE DEVELOPMENT THAT WILL FURTHER AGGRAVATE THE SITUATION MUST CEASE, AND THE OWNER/CONTRACTOR WILL IMMEDIATELY COMMENCE RESTORATION METHODS. RESTORATION ACTIVITY WILL CONTINUE UNTIL SUCH TIME AS THE AFFECTED PROPERTY OWNER IS SATISFIED.

7. NO TEMPORARY OR PERMANENT STOCKPILING OF MATERIALS OR EQUIPMENT SHALL OCCUR WITHIN CRITICAL AREAS OR ASSOCIATED BUFFERS, OR THE CRITICAL ROOT ZONE FOR VEGETATION PROPOSED FOR RETENTION.

TY OF PUYALL	CITY OF
	PUYALLUP
SET OF WASHINGTON	DEVELOPMENT ENGINEERING and PUBLIC WORKS DEPARTMENTS

GRADING, EROSION, AND SEDIMENTATION CONTROL NOTES

CALL TWO BUSINESS DAYS BEFORE YOU DIG

-800-424-5555 UTILITIES UNDERGROUND LOCATION CENTER

MANAGER.

APPROVED

CITY OF PUYALLUP

**NOTE:** THIS APPROVAL IS VOID

THE CITY WILL NOT BE

DETERMINED BY THE

RESPONSIBLE FOR ERRORS

AND/OR OMISSIONS ON THESE

FIELD CONDITIONS MAY DICTATE

CHANGES TO THESE PLANS AS

DEVELOPMENT ENGINEERING

AFTER 180 DAYS FROM APPROVAL

DEVELOPMENT ENGINEERING

PUYALLUP **BARRIERS NOTES** PUBLIC WORKS DEPARTMENTS 02.03.06

# Appendix B: BMP Detail

# Appendix C: correspondence

# Appendix D: Site Inspection Form

**Appendix E: Construction Stormwater General Permit (CSWGP)** 

Appendix F: 303(d) List Waterbodies / TMDL Waterbodies Information

# Appendix G: Contaminated Site Information

# **Appendix H: Engineering Calculations**

# **APPENDIX D**

# WWHM2012 PROJECT REPORT

## General Model Information

WWHM2012 Project Name: Flow Control and Treatment

Site Name: Site Address:

City:

Report Date: 6/2/2025

Gage: 38 IN CENTRAL

Data Start: 10/01/1901
Data End: 09/30/2059
Timestep: 15 Minute
Precip Scale: 1.000

Version Date: 2024/06/28

Version: 4.3.1

#### **POC Thresholds**

Low Flow Threshold for POC1: 50 Percent of the 2 Year

High Flow Threshold for POC1: 50 Year

# Landuse Basin Data Predeveloped Land Use

#### Basin 1

Bypass: No

GroundWater: No

Pervious Land Use acre C, Forest, Flat 0.762

Pervious Total 0.762

Impervious Land Use acre

Impervious Total 0

Basin Total 0.762

Element Flow Componants: Surface Interflow

Componant Flows To:

POC 1 POC 1

Groundwater

#### Mitigated Land Use

#### West Drive Aisle and Curbing

Bypass: No

GroundWater: No

Pervious Land Use acre

Pervious Total 0

Impervious Land Use acre ROADS FLAT 0.19

Impervious Total 0.19

Basin Total 0.19

Element Flow Componants:

Surface Interflow Groundwater

Componant Flows To:

Surface retention 1 Surface retention 1

East Drive Aisle, Curbing, and Ramp

Bypass: No

GroundWater: No

Pervious Land Use acre

Pervious Total 0

Impervious Land Use acre ROADS FLAT 0.088 SIDEWALKS FLAT 0.002

Impervious Total 0.09

Basin Total 0.09

Element Flow Componants:

Surface Interflow Groundwater

Componant Flows To:

Surface retention 2 Surface retention 2

## Landscaping and Concrete Bypass

Bypass: Yes

GroundWater: No

Pervious Land Use acre A B, Pasture, Flat 0.417

Pervious Total 0.417

Impervious Land Use acre SIDEWALKS FLAT 0.002

Impervious Total 0.002

Basin Total 0.419

Element Flow Componants: Surface Interflow

Componant Flows To:

POC 1

Flow Control and Treatment 6/2/2025 9:58:56 AM Page 6

Groundwater

Roof

Bypass: No

GroundWater: No

Pervious Land Use acre

Pervious Total 0

Impervious Land Use acre ROOF TOPS FLAT 0.063

Impervious Total 0.063

Basin Total 0.063

Element Flow Componants: Surface Interflow

Componant Flows To: Gravel Trench Bed 1 Groundwater

# Routing Elements Predeveloped Routing

#### Mitigated Routing

#### **Gravel Trench Bed 1**

Bottom Length: 84.00 ft. Bottom Width: 23.00 ft. Trench bottom slope 1: 0 To 1 Trench Left side slope 0: 0 To 1 Trench right side slope 2: 0 To 1 Material thickness of first layer: 3 Pour Space of material for first layer: 0.33 Material thickness of second layer: 0 Pour Space of material for second layer: 0 Material thickness of third layer: 0 Pour Space of material for third layer: 0 Infiltration On

Infiltration rate: 0.85
Infiltration safety factor: 1

Total Volume Infiltrated (ac-ft.):

Total Volume Through Riser (ac-ft.):

Total Volume Through Facility (ac-ft.):

Total Volume Through Facility (ac-ft.):

145.951

0.025

145.976

Percent Infiltrated:

99.98

Total Precip Applied to Facility:

0

Total Precip Applied to Facility: 0
Total Evap From Facility: 0

Discharge Structure

Riser Height: 2.9 ft. Riser Diameter: 4 in.

Element Outlets:

Outlet 1 Outlet 2

Outlet Flows To:

#### Gravel Trench Bed Hydraulic Table

Stage(feet) 0.0000	<b>Area(ac.)</b> 0.044	Volume(ac-ft.)	Discharge(cfs)	Infilt(cfs) 0.000
0.0333	0.044	0.000	0.000	0.000
0.0667	0.044	0.001	0.000	0.038
0.1000	0.044	0.001	0.000	0.038
0.1333	0.044	0.002	0.000	0.038
0.1667	0.044	0.002	0.000	0.038
0.2000	0.044	0.002	0.000	0.038
0.2333	0.044	0.003	0.000	0.038
0.2667	0.044	0.003	0.000	0.038
0.3000	0.044	0.004	0.000	0.038
0.3333	0.044	0.004	0.000	0.038
0.3667	0.044	0.005	0.000	0.038
0.4000	0.044	0.005	0.000	0.038
0.4333	0.044	0.006	0.000	0.038
0.4667	0.044	0.006	0.000	0.038
0.5000	0.044	0.007	0.000	0.038
0.5333	0.044	0.007	0.000	0.038
0.5667	0.044	0.008	0.000	0.038
0.6000	0.044	0.008	0.000	0.038
0.6333	0.044	0.009	0.000	0.038
0.6667	0.044	0.009	0.000	0.038
0.7000	0.044	0.010	0.000	0.038
0.7333	0.044	0.010	0.000	0.038

0.7667	0.044	0.011	0.000	0.038
0.8000	0.044	0.011	0.000	0.038
0.8333	0.044	0.012	0.000	0.038
0.8667	0.044	0.012	0.000	0.038
0.9000	0.044	0.013	0.000	0.038
0.9333	0.044	0.013	0.000	0.038
0.9667	0.044	0.014	0.000	0.038
1.0000	0.044	0.014	0.000	0.038
1.0333	0.044	0.015	0.000	0.038
1.0667	0.044	0.015	0.000	0.038
1.1000	0.044	0.016	0.000	0.038
1.1333	0.044	0.016	0.000	0.038
1.1667	0.044	0.017	0.000	0.038
1.2000	0.044	0.017	0.000	0.038
1.2333	0.044	0.018	0.000	0.038
1.2667	0.044	0.018	0.000	0.038
1.3000	0.044	0.019	0.000	0.038
1.3333	0.044	0.019	0.000	0.038
1.3667	0.044	0.020	0.000	0.038
1.4000	0.044	0.020	0.000	0.038
1.4333	0.044	0.021	0.000	0.038
1.4667	0.044	0.021	0.000	0.038
1.5000	0.044	0.022	0.000	0.038
1.5333	0.044	0.022	0.000	0.038
1.5667	0.044	0.022	0.000	0.038
1.6000	0.044	0.023	0.000	0.038
1.6333	0.044	0.023	0.000	0.038
1.6667	0.044	0.024	0.000	0.038
1.7000	0.044	0.024	0.000	0.038
1.7333	0.044	0.025	0.000	0.038
1.7667	0.044	0.025	0.000	0.038
1.8000	0.044	0.026	0.000	0.038
1.8333	0.044	0.026	0.000	0.038
1.8667	0.044	0.027	0.000	0.038
1.9000	0.044	0.027	0.000	0.038
1.9333	0.044	0.028	0.000	0.038
1.9667	0.044	0.028	0.000	0.038
2.0000	0.044	0.029	0.000	0.038
2.0333	0.044	0.029	0.000	0.038
2.0667	0.044	0.030	0.000	0.038
2.1000	0.044	0.030	0.000	0.038
2.1333	0.044	0.031	0.000	0.038
2.1667	0.044	0.031	0.000	0.038
2.2000	0.044	0.032	0.000	0.038
2.2333	0.044	0.032	0.000	0.038
2.2667	0.044	0.033	0.000	0.038
2.3000	0.044	0.033	0.000	0.038
2.3333	0.044	0.034	0.000	0.038
2.3667	0.044	0.034	0.000	0.038
2.4000	0.044	0.035	0.000	0.038
2.4333	0.044	0.035	0.000	0.038
2.4667	0.044	0.036	0.000	0.038
2.5000	0.044	0.036	0.000	0.038
2.5333	0.044	0.037	0.000	0.038
2.5667	0.044	0.037	0.000	0.038
2.6000	0.044	0.038	0.000	0.038
2.6333	0.044	0.038	0.000	0.038
2.6667	0.044	0.039	0.000	0.038

2.7000	0.044	0.039	0.000	0.038
2.7333	0.044	0.040	0.000	0.038
2.7667	0.044	0.040	0.000	0.038
2.8000	0.044	0.041	0.000	0.038
2.8333	0.044	0.041	0.000	0.038
2.8667	0.044	0.042	0.000	0.038
2.9000	0.044	0.042	0.000	0.038
2.9333	0.044	0.042	0.021	0.038
2.9667	0.044	0.043	0.058	0.038
3.0000	0.044	0.043	0.096	0.038

#### Bioretention 1

Bottom Length: 12.00 ft.
Bottom Width: 2.50 ft.
Material thickness of first layer: 0.25

Material type for first layer: SMMWW 12 in/hr

Material thickness of second layer: 1.5

Material type for second layer: SMMWW 12 in/hr

0.5

6

0

Material thickness of third layer: 1.5
Material type for third layer: GRAVEL

Underdrain used

Underdrain Diameter (feet):
Orifice Diameter (in.):
Offset (in.):
Flow Through Underdrain (ac-ft.):

Flow Through Underdrain (ac-ft.): 74.393 Total Outflow (ac-ft.): 80.785 Percent Through Underdrain: 92.09

Discharge Structure

Riser Height: 0.5 ft. Riser Diameter: 8 in.

**Element Outlets:** 

Outlet 1 Outlet 2

Outlet Flows To: Gravel Trench Bed 1

#### Bioretention Hydraulic Table

Stage(feet)	Area(ac.)	Volume(ac-ft.)	Discharge(cfs)	Infilt(cfs)
0.0000	0.0159	0.0000	0.0000	0.0000
0.0467	0.0157	0.0000	0.0000	0.0000
0.0934	0.0154	0.0000	0.0000	0.0000
0.1401	0.0150	0.0001	0.0000	0.0000
0.1868	0.0147	0.0001	0.0000	0.0000
0.2335	0.0144	0.0001	0.0000	0.0000
0.2802	0.0140	0.0001	0.0000	0.0000
0.3269	0.0137	0.0002	0.0000	0.0000
0.3736	0.0134	0.0002	0.0000	0.0000
0.4203	0.0131	0.0002	0.0001	0.0000
0.4670	0.0128	0.0003	0.0001	0.0000
0.5137	0.0125	0.0003	0.0001	0.0000
0.5604	0.0122	0.0003	0.0002	0.0000
0.6071	0.0119	0.0004	0.0002	0.0000
0.6538	0.0116	0.0004	0.0002	0.0000
0.7005	0.0113	0.0005	0.0003	0.0000
0.7473	0.0110	0.0005	0.0003	0.0000
0.7940	0.0107	0.0006	0.0004	0.0000
0.8407	0.0104	0.0007	0.0005	0.0000
0.8874	0.0101	0.0007	0.0006	0.0000
0.9341	0.0099	0.0008	0.0006	0.0000
0.9808	0.0096	0.0009	0.0006	0.0000
1.0275	0.0093	0.0009	0.0007	0.0000
1.0742	0.0091	0.0010	0.0008	0.0000
1.1209	0.0088	0.0011	0.0009	0.0000
1.1676	0.0085	0.0012	0.0010	0.0000
1.2143	0.0083	0.0013	0.0011	0.0000
1.2610	0.0080	0.0014	0.0012	0.0000
1.3077	0.0078	0.0015	0.0012	0.0000
1.3544	0.0075	0.0016	0.0013	0.0000

1.4011       0.0073       0.0017       0.0015       0.0000         1.4478       0.0071       0.0018       0.0017       0.0000         1.5412       0.0068       0.0019       0.0019       0.0001         1.5879       0.0064       0.0022       0.0021       0.0002         1.6813       0.0059       0.0024       0.0023       0.0002         1.7280       0.0057       0.0026       0.0025       0.0007         1.7747       0.0055       0.0027       0.0027       0.0027         1.8214       0.0053       0.0028       0.0030       0.0000         1.8681       0.0051       0.0030       0.0030       0.0000         1.9148       0.0049       0.0031       0.0030       0.0000         1.9615       0.0047       0.0033       0.0036       0.0000         2.0549       0.0043       0.0034       0.0037       0.0000         2.1484       0.0040       0.0034       0.0037       0.0000         2.1484       0.0041       0.0037       0.0053       0.0000         2.0549       0.0043       0.0036       0.0038       0.0000         2.1484       0.0040       0.0039       0.0057					
1.4478       0.0071       0.0018       0.0017       0.0000         1.4945       0.0068       0.0019       0.0019       0.0000         1.5412       0.0066       0.0020       0.0019       0.0000         1.5879       0.0064       0.0022       0.0021       0.0000         1.6346       0.0059       0.0024       0.0023       0.0000         1.7280       0.0057       0.0026       0.0027       0.0027         1.7747       0.0055       0.0027       0.0027       0.0000         1.8214       0.0053       0.0028       0.0030       0.0000         1.8188       0.0049       0.0031       0.0030       0.0000         1.9615       0.0047       0.0033       0.0036       0.0000         2.082       0.0045       0.0034       0.0037       0.0000         2.0549       0.0043       0.0036       0.0038       0.0000         2.1484       0.0040       0.0037       0.0053       0.0000         2.1484       0.0041       0.0036       0.0038       0.0000         2.0549       0.0043       0.0036       0.0038       0.0000         2.1951       0.0036       0.0041       0.0063	1.4011	0.0073	0.0017	0.0015	0.0000
1.4945       0.0068       0.0019       0.0019       0.0000         1.5412       0.0066       0.0020       0.0019       0.0000         1.5879       0.0064       0.0022       0.0023       0.0002         1.6346       0.0062       0.0023       0.0023       0.0000         1.6813       0.0059       0.0024       0.0025       0.0000         1.7747       0.0055       0.0027       0.0027       0.0027         1.8214       0.0053       0.0028       0.0030       0.0000         1.8681       0.0051       0.0030       0.0030       0.0000         1.8681       0.0047       0.0031       0.0033       0.0000         1.9148       0.0049       0.0031       0.0033       0.0000         1.9615       0.0047       0.0033       0.0036       0.0000         2.0549       0.0043       0.0036       0.0037       0.0002         2.1016       0.0041       0.0037       0.0053       0.0002         2.1484       0.0040       0.0039       0.0057       0.0002         2.1418       0.0036       0.0041       0.0063       0.0002         2.2418       0.0036       0.0044       0.0063					
1.5412       0.0066       0.0020       0.0019       0.0000         1.5879       0.0064       0.0022       0.0021       0.0000         1.6346       0.0062       0.0023       0.0023       0.0000         1.6813       0.0059       0.0024       0.0025       0.0000         1.77280       0.0057       0.0026       0.0025       0.0000         1.7747       0.0055       0.0027       0.0027       0.0000         1.8214       0.0053       0.0028       0.0030       0.0000         1.9148       0.0051       0.0030       0.0030       0.0000         1.9148       0.0047       0.0033       0.0036       0.0000         2.0082       0.0045       0.0034       0.0037       0.0000         2.0549       0.0043       0.0036       0.0037       0.0000         2.1016       0.0041       0.0037       0.0053       0.0000         2.1484       0.0040       0.0039       0.0057       0.0000         2.1484       0.0040       0.0039       0.0057       0.0000         2.2418       0.0038       0.0041       0.0063       0.0000         2.2885       0.0034       0.0044       0.0063					
1.5879       0.0064       0.0022       0.0021       0.0003         1.6346       0.0062       0.0023       0.0023       0.0000         1.7280       0.0057       0.0026       0.0025       0.0000         1.7747       0.0055       0.0027       0.0027       0.0000         1.8214       0.0053       0.0030       0.0030       0.0030         1.8681       0.0049       0.0031       0.0030       0.0030         1.9418       0.0047       0.0033       0.0036       0.0000         1.9615       0.0047       0.0033       0.0036       0.0000         2.0082       0.0045       0.0034       0.0037       0.0000         2.0549       0.0043       0.0036       0.0038       0.0000         2.1016       0.0041       0.0037       0.0053       0.0000         2.1484       0.0040       0.0039       0.0057       0.0000         2.1951       0.0038       0.0041       0.0063       0.0000         2.2418       0.0038       0.0041       0.0063       0.0000         2.2885       0.0034       0.0044       0.0063       0.0000         2.3352       0.0033       0.0063       0.0063					
1.6346       0.0062       0.0023       0.0023       0.0000         1.6813       0.0059       0.0024       0.0023       0.0000         1.7280       0.0057       0.0026       0.0025       0.0000         1.7747       0.0055       0.0027       0.0027       0.0000         1.8214       0.0053       0.0030       0.0030       0.0000         1.8681       0.0051       0.0030       0.0030       0.0000         1.9148       0.0049       0.0031       0.0033       0.0006         1.9615       0.0047       0.0033       0.0036       0.0002         2.0082       0.0045       0.0034       0.0037       0.0002         2.0549       0.0043       0.0036       0.0038       0.0002         2.1016       0.0041       0.0037       0.0053       0.0002         2.1484       0.0040       0.0039       0.0057       0.0002         2.1484       0.0040       0.0039       0.0057       0.0002         2.1951       0.0038       0.0041       0.0063       0.0002         2.2418       0.0036       0.0042       0.0063       0.0002         2.2885       0.0034       0.0044       0.0063					
1.6813       0.0059       0.0024       0.0023       0.0006         1.7280       0.0057       0.0026       0.0025       0.0000         1.7747       0.0055       0.0027       0.0027       0.0000         1.8214       0.0053       0.0028       0.0030       0.0000         1.948       0.0049       0.0031       0.0033       0.0006         1.9615       0.0047       0.0033       0.0036       0.0000         2.0082       0.0045       0.0034       0.0037       0.0000         2.0549       0.0043       0.0036       0.0038       0.0000         2.1016       0.0041       0.0037       0.0053       0.0000         2.1484       0.0040       0.0039       0.057       0.0000         2.1951       0.0038       0.0041       0.0063       0.0000         2.2418       0.0036       0.0042       0.0063       0.0000         2.2885       0.0034       0.0044       0.0063       0.0000         2.3819       0.0031       0.0048       0.0063       0.0000         2.4286       0.0030       0.0050       0.0063       0.0000         2.4286       0.0030       0.0050       0.0063					
1.7280         0.0057         0.0026         0.0025         0.0000           1.7747         0.0055         0.0027         0.0027         0.0000           1.8214         0.0053         0.0028         0.0030         0.0000           1.8681         0.0049         0.0031         0.0033         0.0000           1.9448         0.0049         0.0031         0.0033         0.0036         0.0000           2.0082         0.0045         0.0034         0.0037         0.0000           2.0549         0.0043         0.0036         0.0038         0.0000           2.1016         0.0041         0.0037         0.0053         0.0000           2.1484         0.0040         0.0039         0.057         0.0000           2.1951         0.0038         0.0041         0.0063         0.0000           2.2418         0.0036         0.0042         0.0063         0.0000           2.2885         0.0034         0.0044         0.0063         0.0000           2.3352         0.0033         0.0046         0.0063         0.0000           2.4286         0.0031         0.0048         0.0063         0.0000           2.4286         0.0030         0.0050					
1.7747         0.0055         0.0027         0.0027         0.0000           1.8214         0.0053         0.0028         0.0030         0.0000           1.8681         0.0051         0.0030         0.0030         0.0000           1.9148         0.0049         0.0031         0.0033         0.0006           2.0082         0.0045         0.0034         0.0037         0.0000           2.0549         0.0043         0.0036         0.0038         0.0000           2.1016         0.0041         0.0037         0.0053         0.0000           2.1484         0.0040         0.0039         0.057         0.0000           2.1418         0.0036         0.0042         0.0063         0.0000           2.2885         0.0034         0.0044         0.0063         0.0000           2.3819         0.0031         0.0044         0.0063         0.0000           2.4286         0.0030         0.0050         0.0063         0.0000           2.4286         0.0030         0.0050         0.0063         0.0000           2.5220         0.0026         0.0054         0.0063         0.0000           2.6621         0.0025         0.0056         0.0063					
1.8214         0.0053         0.0028         0.0030         0.0000           1.8681         0.0051         0.0030         0.0030         0.0000           1.9148         0.0049         0.0031         0.0033         0.0006           1.9615         0.0047         0.0033         0.0036         0.0000           2.0822         0.0045         0.0034         0.0037         0.0000           2.0549         0.0043         0.0036         0.0038         0.0000           2.1016         0.0041         0.0037         0.0053         0.0000           2.1484         0.0040         0.0039         0.057         0.0000           2.1951         0.0038         0.0041         0.0063         0.0000           2.2418         0.0036         0.0042         0.0063         0.0000           2.2885         0.0034         0.0044         0.0063         0.0000           2.3352         0.0033         0.0046         0.0063         0.0000           2.4286         0.0030         0.0050         0.0063         0.0000           2.4753         0.0028         0.0052         0.0063         0.0000           2.5687         0.0025         0.0056         0.0063					
1.8681         0.0051         0.0030         0.0030         0.0000           1.9148         0.0049         0.0031         0.0033         0.0000           2.0082         0.0045         0.0034         0.0037         0.0000           2.0549         0.0043         0.0036         0.0038         0.0000           2.1016         0.0041         0.0037         0.0053         0.0000           2.1484         0.0040         0.0039         0.0057         0.0000           2.1951         0.0038         0.0041         0.0063         0.0000           2.2418         0.0036         0.0042         0.0063         0.0000           2.2885         0.0034         0.0044         0.0063         0.0000           2.3819         0.0031         0.0048         0.0063         0.0000           2.4286         0.0030         0.0050         0.0063         0.0000           2.4753         0.0028         0.0052         0.0063         0.0000           2.5220         0.0026         0.0054         0.0063         0.0000           2.6154         0.0023         0.0059         0.0063         0.0000           2.7088         0.0021         0.0063         0.006					
1.9148       0.0049       0.0031       0.0033       0.0006         1.9615       0.0047       0.0033       0.0036       0.0000         2.0549       0.0043       0.0036       0.0038       0.0000         2.1016       0.0041       0.0037       0.0053       0.0000         2.1484       0.0040       0.0039       0.0057       0.0000         2.1951       0.0038       0.0041       0.0063       0.0000         2.2418       0.0036       0.0042       0.0063       0.0000         2.2885       0.0034       0.0044       0.0063       0.0000         2.3352       0.0033       0.0046       0.0063       0.0000         2.3819       0.0031       0.0048       0.0063       0.0000         2.4286       0.0030       0.0050       0.0063       0.0000         2.4753       0.0028       0.0052       0.0063       0.0000         2.5220       0.0026       0.0054       0.0063       0.0000         2.6621       0.0022       0.0061       0.0063       0.0000         2.7555       0.0019       0.0066       0.0063       0.0000         2.8489       0.0017       0.0066       0.0063					
1.9615         0.0047         0.0033         0.0036         0.0000           2.0082         0.0045         0.0034         0.0037         0.0000           2.0549         0.0043         0.0036         0.0038         0.0000           2.1016         0.0041         0.0037         0.0053         0.0000           2.1484         0.0040         0.0039         0.0057         0.0000           2.1951         0.0038         0.0041         0.0063         0.0000           2.2418         0.0036         0.0042         0.0063         0.0000           2.2885         0.0034         0.0044         0.0063         0.0000           2.3352         0.0033         0.0046         0.0063         0.0000           2.3819         0.0031         0.0048         0.0063         0.0000           2.4286         0.0030         0.0050         0.0063         0.0000           2.4753         0.0028         0.0052         0.0063         0.0000           2.5220         0.0026         0.0054         0.0063         0.0000           2.6687         0.0025         0.0056         0.0063         0.0000           2.6154         0.0023         0.0059         0.006					
2.0082         0.0045         0.0034         0.0037         0.0000           2.0549         0.0043         0.0036         0.0038         0.0000           2.1016         0.0041         0.0037         0.0053         0.0000           2.1484         0.0040         0.0039         0.0057         0.0000           2.1951         0.0038         0.0041         0.0063         0.0000           2.2418         0.0036         0.0042         0.0063         0.0000           2.2885         0.0034         0.0044         0.0063         0.0000           2.3819         0.0031         0.0048         0.0063         0.0000           2.4286         0.0030         0.0050         0.0063         0.0000           2.4753         0.0028         0.0052         0.0063         0.0000           2.5220         0.0026         0.0054         0.0063         0.0000           2.6154         0.0023         0.0059         0.0063         0.0000           2.6621         0.0022         0.0061         0.0063         0.0000           2.7088         0.0021         0.0063         0.0063         0.0000           2.8489         0.0017         0.0066         0.006					
2.0549         0.0043         0.0036         0.0038         0.0000           2.1016         0.0041         0.0037         0.0053         0.0000           2.1484         0.0040         0.0039         0.0057         0.0000           2.1951         0.0038         0.0041         0.0063         0.0000           2.2418         0.0036         0.0042         0.0063         0.0000           2.2885         0.0034         0.0044         0.0063         0.0000           2.3352         0.0033         0.0046         0.0063         0.0000           2.3819         0.0031         0.0048         0.0063         0.0000           2.4286         0.0030         0.0050         0.0063         0.0000           2.4753         0.0028         0.0052         0.0063         0.0000           2.5220         0.0026         0.0052         0.0063         0.0000           2.5687         0.0025         0.0056         0.0063         0.0000           2.6154         0.0023         0.0059         0.0063         0.0000           2.7088         0.0021         0.0063         0.0063         0.0000           2.8489         0.0017         0.0066         0.006					
2.1016       0.0041       0.0037       0.0053       0.0000         2.1484       0.0040       0.0039       0.0057       0.0000         2.1951       0.0038       0.0041       0.0063       0.0000         2.2418       0.0036       0.0042       0.0063       0.0000         2.2885       0.0034       0.0044       0.0063       0.0000         2.3819       0.0031       0.0048       0.0063       0.0000         2.4286       0.0030       0.0050       0.0063       0.0000         2.4753       0.0028       0.0052       0.0063       0.0000         2.5220       0.0026       0.0054       0.0063       0.0000         2.5687       0.0025       0.0054       0.0063       0.0000         2.6154       0.0023       0.0059       0.0063       0.0000         2.6621       0.0022       0.0061       0.0063       0.0000         2.7088       0.0021       0.0063       0.0063       0.0000         2.8022       0.0018       0.0068       0.0063       0.0000         2.8489       0.0017       0.0071       0.0063       0.0000         2.9980       0.0014       0.0076       0.0063					
2.1484       0.0040       0.0039       0.0057       0.0000         2.1951       0.0038       0.0041       0.0063       0.0000         2.2418       0.0036       0.0042       0.0063       0.0000         2.2885       0.0034       0.0044       0.0063       0.0000         2.3352       0.0033       0.0046       0.0063       0.0000         2.4286       0.0030       0.0050       0.0063       0.0000         2.4753       0.0028       0.0052       0.0063       0.0000         2.5220       0.0026       0.0054       0.0063       0.0000         2.5687       0.0025       0.0056       0.0063       0.0000         2.6154       0.0023       0.0059       0.0063       0.0000         2.7088       0.0021       0.0063       0.0063       0.0000         2.7555       0.0019       0.0063       0.0063       0.0000         2.8489       0.0017       0.0071       0.0063       0.0000         2.8956       0.0016       0.0073       0.0063       0.0000         2.9423       0.0014       0.0076       0.0063       0.0000         2.9890       0.0013       0.0078       0.0063					
2.1951       0.0038       0.0041       0.0063       0.0000         2.2418       0.0036       0.0042       0.0063       0.0000         2.2885       0.0034       0.0044       0.0063       0.0000         2.3352       0.0033       0.0046       0.0063       0.0000         2.4286       0.0030       0.0050       0.0063       0.0000         2.4753       0.0028       0.0052       0.0063       0.0000         2.5220       0.0026       0.0054       0.0063       0.0000         2.5687       0.0025       0.0056       0.0063       0.0000         2.6154       0.0023       0.0059       0.0063       0.0000         2.7088       0.0021       0.0063       0.0063       0.0000         2.7555       0.0019       0.0066       0.0063       0.0000         2.8489       0.0017       0.0071       0.0063       0.0000         2.8956       0.0016       0.0073       0.0063       0.0000         2.9423       0.0014       0.0076       0.0063       0.0000         2.9890       0.0012       0.0081       0.0063       0.0000         3.0824       0.0011       0.0084       0.0063					
2.2418       0.0036       0.0042       0.0063       0.0000         2.2885       0.0034       0.0044       0.0063       0.0000         2.3352       0.0033       0.0046       0.0063       0.0000         2.4286       0.0030       0.0050       0.0063       0.0000         2.4753       0.0028       0.0052       0.0063       0.0000         2.5220       0.0026       0.0054       0.0063       0.0000         2.5687       0.0025       0.0056       0.0063       0.0000         2.6154       0.0023       0.0059       0.0063       0.0000         2.7088       0.0021       0.0063       0.0063       0.0000         2.7555       0.0019       0.0066       0.0063       0.0000         2.8489       0.0017       0.0068       0.0063       0.0000         2.8489       0.0017       0.0071       0.0063       0.0000         2.9423       0.0014       0.0073       0.0063       0.0000         2.9890       0.0013       0.0078       0.0063       0.0000         3.0824       0.0011       0.0087       0.0063       0.0000         3.1758       0.0009       0.0093       0.0063					
2.2885       0.0034       0.0044       0.0063       0.0000         2.3352       0.0033       0.0046       0.0063       0.0000         2.3819       0.0031       0.0048       0.0063       0.0000         2.4286       0.0030       0.0050       0.0063       0.0000         2.4753       0.0028       0.0052       0.0063       0.0000         2.5220       0.0026       0.0054       0.0063       0.0000         2.5687       0.0025       0.0056       0.0063       0.0000         2.6154       0.0023       0.0059       0.0063       0.0000         2.6621       0.0022       0.0061       0.0063       0.0000         2.7088       0.0021       0.0063       0.0063       0.0000         2.8022       0.0018       0.0068       0.0063       0.0000         2.8489       0.0017       0.0071       0.0063       0.0000         2.9423       0.0014       0.0073       0.0063       0.0000         2.9890       0.0013       0.0078       0.0063       0.0000         3.0824       0.0011       0.0084       0.0063       0.0000         3.1758       0.0009       0.0093       0.0063					
2.3352       0.0033       0.0046       0.0063       0.0000         2.3819       0.0031       0.0048       0.0063       0.0000         2.4286       0.0030       0.0050       0.0063       0.0000         2.4753       0.0028       0.0052       0.0063       0.0000         2.5220       0.0026       0.0054       0.0063       0.0000         2.5687       0.0025       0.0056       0.0063       0.0000         2.6154       0.0023       0.0059       0.0063       0.0000         2.6621       0.0022       0.0061       0.0063       0.0000         2.7088       0.0021       0.0063       0.0063       0.0000         2.7555       0.0019       0.0066       0.0063       0.0000         2.8022       0.0018       0.0068       0.0063       0.0000         2.8489       0.0017       0.0071       0.0063       0.0000         2.9423       0.0014       0.0073       0.0063       0.0000         2.9890       0.0013       0.0078       0.0063       0.0000         3.0824       0.0011       0.0084       0.0063       0.0000         3.1758       0.0009       0.0090       0.0063					
2.3819       0.0031       0.0048       0.0063       0.0000         2.4286       0.0030       0.0050       0.0063       0.0000         2.4753       0.0028       0.0052       0.0063       0.0000         2.5220       0.0026       0.0054       0.0063       0.0000         2.5687       0.0025       0.0056       0.0063       0.0000         2.6154       0.0023       0.0059       0.0063       0.0000         2.6621       0.0022       0.0061       0.0063       0.0000         2.7088       0.0021       0.0063       0.0063       0.0000         2.7555       0.0019       0.0066       0.0063       0.0000         2.8022       0.0018       0.0068       0.0063       0.0000         2.8489       0.0017       0.0071       0.0063       0.0000         2.8956       0.0016       0.0073       0.0063       0.0000         2.9890       0.0013       0.0078       0.0063       0.0000         3.0357       0.0012       0.0081       0.0063       0.0000         3.1291       0.0010       0.0087       0.0063       0.0000         3.1758       0.0009       0.0093       0.0063					
2.4286       0.0030       0.0050       0.0063       0.0000         2.4753       0.0028       0.0052       0.0063       0.0000         2.5220       0.0026       0.0054       0.0063       0.0000         2.5687       0.0025       0.0056       0.0063       0.0000         2.6154       0.0023       0.0059       0.0063       0.0000         2.6621       0.0022       0.0061       0.0063       0.0000         2.7088       0.0021       0.0063       0.0063       0.0000         2.8022       0.0018       0.0068       0.0063       0.0000         2.8489       0.0017       0.0071       0.0063       0.0000         2.8956       0.0016       0.0073       0.0063       0.0000         2.9423       0.0014       0.0076       0.0063       0.0000         2.9890       0.0013       0.0078       0.0063       0.0000         3.0357       0.0012       0.0081       0.0063       0.0000         3.024       0.0011       0.0084       0.0063       0.0000         3.1758       0.0009       0.0090       0.0063       0.0000         3.2225       0.0008       0.0093       0.0063					
2.4753       0.0028       0.0052       0.0063       0.0000         2.5220       0.0026       0.0054       0.0063       0.0000         2.5687       0.0025       0.0056       0.0063       0.0000         2.6154       0.0023       0.0059       0.0063       0.0000         2.6621       0.0022       0.0061       0.0063       0.0000         2.7088       0.0021       0.0063       0.0063       0.0000         2.8022       0.0018       0.0068       0.0063       0.0000         2.8489       0.0017       0.0071       0.0063       0.0000         2.8956       0.0016       0.0073       0.0063       0.0000         2.9890       0.0013       0.0078       0.0063       0.0000         3.0357       0.0012       0.0081       0.0063       0.0000         3.0824       0.0011       0.0084       0.0063       0.0000         3.1291       0.0010       0.0087       0.0063       0.0000         3.1758       0.0009       0.0090       0.0063       0.0000         3.2225       0.0008       0.0093       0.0063       0.0000					
2.5220       0.0026       0.0054       0.0063       0.0000         2.5687       0.0025       0.0056       0.0063       0.0000         2.6154       0.0023       0.0059       0.0063       0.0000         2.6621       0.0022       0.0061       0.0063       0.0000         2.7088       0.0021       0.0063       0.0063       0.0000         2.7555       0.0019       0.0066       0.0063       0.0000         2.8022       0.0018       0.0068       0.0063       0.0000         2.8489       0.0017       0.0071       0.0063       0.0000         2.8956       0.0016       0.0073       0.0063       0.0000         2.9890       0.0013       0.0078       0.0063       0.0000         3.0357       0.0012       0.0081       0.0063       0.0000         3.0824       0.0011       0.0084       0.0063       0.0000         3.1291       0.0010       0.0087       0.0063       0.0000         3.1758       0.0009       0.0093       0.0063       0.0000         3.2225       0.0008       0.0093       0.0063       0.0000					
2.5687       0.0025       0.0056       0.0063       0.0000         2.6154       0.0023       0.0059       0.0063       0.0000         2.6621       0.0022       0.0061       0.0063       0.0000         2.7088       0.0021       0.0063       0.0063       0.0000         2.7555       0.0019       0.0066       0.0063       0.0000         2.8022       0.0018       0.0068       0.0063       0.0000         2.8489       0.0017       0.0071       0.0063       0.0000         2.8956       0.0016       0.0073       0.0063       0.0000         2.9423       0.0014       0.0076       0.0063       0.0000         2.9890       0.0013       0.0078       0.0063       0.0000         3.0357       0.0012       0.0081       0.0063       0.0000         3.1291       0.0010       0.0087       0.0063       0.0000         3.1758       0.0009       0.0093       0.0063       0.0000         3.2225       0.0008       0.0093       0.0063       0.0000					
2.6154       0.0023       0.0059       0.0063       0.0000         2.6621       0.0022       0.0061       0.0063       0.0000         2.7088       0.0021       0.0063       0.0063       0.0000         2.7555       0.0019       0.0066       0.0063       0.0000         2.8022       0.0018       0.0068       0.0063       0.0000         2.8489       0.0017       0.0071       0.0063       0.0000         2.8956       0.0016       0.0073       0.0063       0.0000         2.9423       0.0014       0.0076       0.0063       0.0000         2.9890       0.0013       0.0078       0.0063       0.0000         3.0357       0.0012       0.0081       0.0063       0.0000         3.0824       0.0011       0.0084       0.0063       0.0000         3.1291       0.0010       0.0087       0.0063       0.0000         3.1758       0.0009       0.0090       0.0063       0.0000         3.2225       0.0008       0.0093       0.0063       0.0000					
2.6621       0.0022       0.0061       0.0063       0.0000         2.7088       0.0021       0.0063       0.0063       0.0000         2.7555       0.0019       0.0066       0.0063       0.0000         2.8022       0.0018       0.0068       0.0063       0.0000         2.8489       0.0017       0.0071       0.0063       0.0000         2.8956       0.0016       0.0073       0.0063       0.0000         2.9423       0.0014       0.0076       0.0063       0.0000         2.9890       0.0013       0.0078       0.0063       0.0000         3.0357       0.0012       0.0081       0.0063       0.0000         3.0824       0.0011       0.0084       0.0063       0.0000         3.1291       0.0010       0.0087       0.0063       0.0000         3.1758       0.0009       0.0090       0.0063       0.0000         3.2225       0.0008       0.0093       0.0063       0.0000					
2.7088       0.0021       0.0063       0.0063       0.0000         2.7555       0.0019       0.0066       0.0063       0.0000         2.8022       0.0018       0.0068       0.0063       0.0000         2.8489       0.0017       0.0071       0.0063       0.0000         2.8956       0.0016       0.0073       0.0063       0.0000         2.9423       0.0014       0.0076       0.0063       0.0000         2.9890       0.0013       0.0078       0.0063       0.0000         3.0357       0.0012       0.0081       0.0063       0.0000         3.0824       0.0011       0.0084       0.0063       0.0000         3.1291       0.0010       0.0087       0.0063       0.0000         3.1758       0.0009       0.0090       0.0063       0.0000         3.2225       0.0008       0.0093       0.0063       0.0000					
2.7555       0.0019       0.0066       0.0063       0.0000         2.8022       0.0018       0.0068       0.0063       0.0000         2.8489       0.0017       0.0071       0.0063       0.0000         2.8956       0.0016       0.0073       0.0063       0.0000         2.9423       0.0014       0.0076       0.0063       0.0000         2.9890       0.0013       0.0078       0.0063       0.0000         3.0357       0.0012       0.0081       0.0063       0.0000         3.0824       0.0011       0.0084       0.0063       0.0000         3.1291       0.0010       0.0087       0.0063       0.0000         3.1758       0.0009       0.0090       0.0063       0.0000         3.2225       0.0008       0.0093       0.0063       0.0000					
2.8022       0.0018       0.0068       0.0063       0.0000         2.8489       0.0017       0.0071       0.0063       0.0000         2.8956       0.0016       0.0073       0.0063       0.0000         2.9423       0.0014       0.0076       0.0063       0.0000         2.9890       0.0013       0.0078       0.0063       0.0000         3.0357       0.0012       0.0081       0.0063       0.0000         3.0824       0.0011       0.0084       0.0063       0.0000         3.1291       0.0010       0.0087       0.0063       0.0000         3.1758       0.0009       0.0090       0.0063       0.0000         3.2225       0.0008       0.0093       0.0063       0.0000					
2.8489       0.0017       0.0071       0.0063       0.0000         2.8956       0.0016       0.0073       0.0063       0.0000         2.9423       0.0014       0.0076       0.0063       0.0000         2.9890       0.0013       0.0078       0.0063       0.0000         3.0357       0.0012       0.0081       0.0063       0.0000         3.0824       0.0011       0.0084       0.0063       0.0000         3.1291       0.0010       0.0087       0.0063       0.0000         3.1758       0.0009       0.0090       0.0063       0.0000         3.2225       0.0008       0.0093       0.0063       0.0000					
2.8956       0.0016       0.0073       0.0063       0.0000         2.9423       0.0014       0.0076       0.0063       0.0000         2.9890       0.0013       0.0078       0.0063       0.0000         3.0357       0.0012       0.0081       0.0063       0.0000         3.0824       0.0011       0.0084       0.0063       0.0000         3.1291       0.0010       0.0087       0.0063       0.0000         3.1758       0.0009       0.0090       0.0063       0.0000         3.2225       0.0008       0.0093       0.0063       0.0000					
2.9423       0.0014       0.0076       0.0063       0.0000         2.9890       0.0013       0.0078       0.0063       0.0000         3.0357       0.0012       0.0081       0.0063       0.0000         3.0824       0.0011       0.0084       0.0063       0.0000         3.1291       0.0010       0.0087       0.0063       0.0000         3.1758       0.0009       0.0090       0.0063       0.0000         3.2225       0.0008       0.0093       0.0063       0.0000	2.8489				
2.9890       0.0013       0.0078       0.0063       0.0000         3.0357       0.0012       0.0081       0.0063       0.0000         3.0824       0.0011       0.0084       0.0063       0.0000         3.1291       0.0010       0.0087       0.0063       0.0000         3.1758       0.0009       0.0090       0.0063       0.0000         3.2225       0.0008       0.0093       0.0063       0.0000					
3.0357       0.0012       0.0081       0.0063       0.0000         3.0824       0.0011       0.0084       0.0063       0.0000         3.1291       0.0010       0.0087       0.0063       0.0000         3.1758       0.0009       0.0090       0.0063       0.0000         3.2225       0.0008       0.0093       0.0063       0.0000					
3.0824       0.0011       0.0084       0.0063       0.0000         3.1291       0.0010       0.0087       0.0063       0.0000         3.1758       0.0009       0.0090       0.0063       0.0000         3.2225       0.0008       0.0093       0.0063       0.0000					
3.1291       0.0010       0.0087       0.0063       0.0000         3.1758       0.0009       0.0090       0.0063       0.0000         3.2225       0.0008       0.0093       0.0063       0.0000					
3.1758 0.0009 0.0090 0.0063 0.0000 3.2225 0.0008 0.0093 0.0063 0.0000					
3.2225 0.0008 0.0093 0.0063 0.0000					
3.2500 0.0007 0.0095 0.0063 0.0000					
	3.2500	0.0007	0.0095	0.0063	0.0000

Bioretention Surface Hydraulic Table

# Stage(feet)Area(ac.)Volume(ac-ft.)Discharge(cfs)To Amended(cfs)Infilt(cfs)

0.0159090.009468	0.0000	0.0042	0.0000
0.0162550.010219	0.0000	0.0042	0.0000
0.0166050.010986	0.0000	0.0051	0.0000
0.0169580.011770	0.0000	0.0053	0.0000
0.0173150.012570	0.0000	0.0054	0.0000
0.0176750.013387	0.0000	0.0055	0.0000
0.0180390.014221	0.0000	0.0056	0.0000
0.0184070.015072	0.0000	0.0058	0.0000
0.0187780.015941	0.0000	0.0059	0.0000
0.0191530.016827	0.0000	0.0060	0.0000
0.0195310.017730	0.0000	0.0062	0.0000
0.0199130.018651	0.0114	0.0063	0.0000
0.0202990.019590	0.1046	0.0064	0.0000
0.0206880.020547	0.2424	0.0065	0.0000
	0.0162550.010219 0.0166050.010986 0.0169580.011770 0.0173150.012570 0.0176750.013387 0.0180390.014221 0.0184070.015072 0.0187780.015941 0.0191530.016827 0.0195310.017730 0.0199130.018651 0.0202990.019590	0.0162550.010219       0.0000         0.0166050.010986       0.0000         0.0169580.011770       0.0000         0.0173150.012570       0.0000         0.0176750.013387       0.0000         0.0180390.014221       0.0000         0.0184070.015072       0.0000         0.0187780.015941       0.0000         0.0191530.016827       0.0000         0.0195310.017730       0.0000         0.0199130.018651       0.0114         0.0202990.019590       0.1046	0.016255 0.010219       0.0000       0.0042         0.016605 0.010986       0.0000       0.0051         0.016958 0.011770       0.0000       0.0053         0.017315 0.012570       0.0000       0.0054         0.017675 0.013387       0.0000       0.0055         0.018039 0.014221       0.0000       0.0056         0.018407 0.015072       0.0000       0.0058         0.018778 0.015941       0.0000       0.0059         0.019153 0.016827       0.0000       0.0060         0.019531 0.017730       0.0000       0.0062         0.019913 0.018651       0.0114       0.0063         0.020299 0.019590       0.1046       0.0064

3.9038	0.0210810.021522	0.3989	0.0067	0.0000
3.9505	0.0214770.022516	0.5495	0.0068	0.0000
3.9973	0.0218770.023529	0.6720	0.0069	0.0000
4.0440	0.022281 0.024560	0.7547	0.0071	0.0000
4.0907	0.0226880.025610	0.8170	0.0072	0.0000
4.1374	0.0230990.026679	0.8712	0.0073	0.0000
4.1841	0.0235130.027768	0.9223	0.0075	0.0000
4.2308	0.023931 0.028875	0.9706	0.0076	0.0000
4.2500	0.0241050.029337	1.0167	0.0076	0.0000

#### Bioretention 2

Bottom Length: 5.00 ft.
Bottom Width: 2.00 ft.
Material thickness of first layer: 0.25

Material type for first layer: SMMWW 12 in/hr

Material thickness of second layer: 1.5

Material type for second layer: SMMWW 12 in/hr

Material thickness of third layer: 1.5
Material type for third layer: GRAVEL

Underdrain used

Underdrain Diameter (feet):

Orifice Diameter (in.):

Offset (in.):

Flow Through Underdrain (ac-ft.):

36.4

Flow Through Underdrain (ac-ft.): 36.563 Total Outflow (ac-ft.): 39.875 Percent Through Underdrain: 91.69

Discharge Structure

Riser Height: 0.5 ft. Riser Diameter: 8 in.

**Element Outlets:** 

Outlet 1 Outlet 2

Outlet Flows To: Gravel Trench Bed 1

#### Bioretention Hydraulic Table

Stage(feet)	Area(ac.)	Volume(ac-ft.)	Discharge(cfs)	
0.0000	0.0121	0.0000	0.0000	0.0000
0.0467	0.0119	0.0000	0.0000	0.0000
0.0934	0.0116	0.0000	0.0000	0.0000
0.1401	0.0113	0.0000	0.0000	0.0000
0.1868	0.0111	0.0000	0.0000	0.0000
0.2335	0.0108	0.0000	0.0000	0.0000
0.2802	0.0105	0.0000	0.0000	0.0000
0.3269	0.0102	0.0001	0.0000	0.0000
0.3736	0.0100	0.0001	0.0000	0.0000
0.4203	0.0097	0.0001	0.0000	0.0000
0.4670	0.0094	0.0001	0.0000	0.0000
0.5137	0.0092	0.0001	0.0000	0.0000
0.5604	0.0089	0.0002	0.0001	0.0000
0.6071	0.0087	0.0002	0.0001	0.0000
0.6538	0.0084	0.0002	0.0001	0.0000
0.7005	0.0082	0.0002	0.0001	0.0000
0.7473	0.0079	0.0003	0.0001	0.0000
0.7940	0.0077	0.0003	0.0001	0.0000
0.8407	0.0074	0.0003	0.0002	0.0000
0.8874	0.0072	0.0004	0.0002	0.0000
0.9341	0.0070	0.0004	0.0002	0.0000
0.9808	0.0068	0.0004	0.0002	0.0000
1.0275	0.0065	0.0005	0.0002	0.0000
1.0742	0.0063	0.0005	0.0003	0.0000
1.1209	0.0061	0.0006	0.0003	0.0000
1.1676	0.0059	0.0006	0.0003	0.0000
1.2143	0.0057	0.0007	0.0004	0.0000
1.2610	0.0055	0.0007	0.0004	0.0000
1.3077	0.0053	0.0008	0.0004	0.0000
1.3544	0.0051	0.0009	0.0004	0.0000

1.4011	0.0049	0.0009	0.0005	0.0000
1.4478	0.0047	0.0010	0.0006	0.0000
1.4945	0.0045	0.0011	0.0006	0.0000
1.5412	0.0044	0.0011	0.0006	0.0000
1.5879 1.6346	0.0042 0.0040	0.0012 0.0013	0.0007 0.0008	0.0000 0.0000
1.6813	0.0040	0.0013	0.0008	0.0000
1.7280	0.0037	0.0014	0.0008	0.0000
1.7747	0.0035	0.0016	0.0009	0.0000
1.8214	0.0034	0.0017	0.0010	0.0000
1.8681	0.0032	0.0018	0.0010	0.0000
1.9148	0.0031	0.0019	0.0011	0.0000
1.9615	0.0029	0.0020	0.0012	0.0000
2.0082	0.0028	0.0021	0.0012	0.0000
2.0549	0.0026	0.0022	0.0013	0.0000
2.1016	0.0025	0.0023	0.0018	0.0000
2.1484	0.0023	0.0024	0.0019	0.0000
2.1951 2.2418	0.0022 0.0021	0.0025 0.0026	0.0021 0.0021	0.0000 0.0000
2.2885	0.0021	0.0028	0.0021	0.0000
2.3352	0.0020	0.0028	0.0021	0.0000
2.3819	0.0017	0.0030	0.0021	0.0000
2.4286	0.0016	0.0032	0.0021	0.0000
2.4753	0.0015	0.0033	0.0021	0.0000
2.5220	0.0014	0.0035	0.0021	0.0000
2.5687	0.0013	0.0036	0.0021	0.0000
2.6154	0.0012	0.0038	0.0021	0.0000
2.6621	0.0011	0.0040	0.0021	0.0000
2.7088	0.0010	0.0041	0.0021	0.0000
2.7555	0.0009	0.0043	0.0021	0.0000
2.8022 2.8489	0.0009 0.0008	0.0045 0.0047	0.0021 0.0021	0.0000
2.8956	0.0007	0.0047	0.0021	0.0000
2.9423	0.0007	0.0051	0.0021	0.0000
2.9890	0.0006	0.0053	0.0021	0.0000
3.0357	0.0005	0.0055	0.0021	0.0000
3.0824	0.0004	0.0057	0.0021	0.0000
3.1291	0.0004	0.0059	0.0021	0.0000
3.1758	0.0003	0.0061	0.0021	0.0000
3.2225	0.0003	0.0063	0.0021	0.0000
3.2500	0.0002	0.0065_	0.0021	0.0000

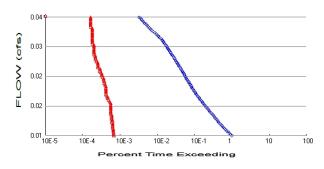
Bioretention Surface Hydraulic Table

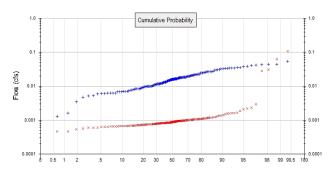
# Stage(feet)Area(ac.)Volume(ac-ft.)Discharge(cfs)To Amended(cfs)Infilt(cfs)

• •	, , ,	,	<b>'</b>	, , , ,
3.2500	0.0120930.006486	0.0000	0.0014	0.0000
3.2967	0.0123900.007057	0.0000	0.0014	0.0000
3.3434	0.0126920.007643	0.0000	0.0017	0.0000
3.3901	0.0129960.008243	0.0000	0.0018	0.0000
3.4368	0.0133050.008857	0.0000	0.0018	0.0000
3.4835	0.0136170.009486	0.0000	0.0018	0.0000
3.5302	0.0139330.010129	0.0000	0.0019	0.0000
3.5769	0.0142520.010787	0.0000	0.0019	0.0000
3.6236	0.0145750.011460	0.0000	0.0020	0.0000
3.6703	0.0149020.012149	0.0000	0.0020	0.0000
3.7170	0.0152320.012852	0.0000	0.0021	0.0000
3.7637	0.0155660.013572	0.0114	0.0021	0.0000
3.8104	0.0159030.014306	0.1046	0.0021	0.0000
3 8571	0.016244.0.015057	0 2424	0.0022	0.000

3.9038	0.0165890.015824	0.3989	0.0022	0.0000
3.9505	0.0169370.016607	0.5495	0.0023	0.0000
3.9973	0.0172890.017406	0.6720	0.0023	0.0000
4.0440	0.0176440.018222	0.7547	0.0024	0.0000
4.0907	0.0180030.019054	0.8170	0.0024	0.0000
4.1374	0.0183660.019903	0.8712	0.0024	0.0000
4.1841	0.0187320.020770	0.9223	0.0025	0.0000
4.2308	0.0191020.021653	0.9706	0.0025	0.0000
4.2500	0.0192550.022022	1.0167	0.0025	0.0000

# Analysis Results POC 1





+ Predeveloped x Mitigated

Predeveloped Landuse Totals for POC #1

Total Pervious Area: 0.762
Total Impervious Area: 0

Mitigated Landuse Totals for POC #1 Total Pervious Area: 0.417 Total Impervious Area: 0.345

Flow Frequency Method: Log Pearson Type III 17B

Flow Frequency Return Periods for Predeveloped. POC #1

 Return Period
 Flow(cfs)

 2 year
 0.016057

 5 year
 0.024981

 10 year
 0.029829

 25 year
 0.034764

 50 year
 0.037697

 100 year
 0.040109

Flow Frequency Return Periods for Mitigated. POC #1

 Return Period
 Flow(cfs)

 2 year
 0.000911

 5 year
 0.001721

 10 year
 0.002521

 25 year
 0.003934

 50 year
 0.00536

 100 year
 0.007184

#### **Annual Peaks**

Annual Peaks for Predeveloped and Mitigated. POC #1

Year	Predeveloped	Mitigated
1902	0.012	0.001
1903	0.010	0.001
1904	0.016	0.001
1905	0.008	0.001
1906	0.003	0.001
1907	0.025	0.001
1908	0.018	0.001
1909	0.018	0.001
1910	0.025	0.001
1911	0.016	0.001

#### Ranked Annual Peaks

Ranked Annual Peaks for Predeveloped and Mitigated. POC #1

Rank	Predeveloped	Mitigated
1	0.0535	0.1064
2	0.0450	0.0631
3	0.0450	0.0310
4 5	0.0435	0.0281
	0.0420	0.0029
6	0.0406	0.0023
7	0.0383	0.0022
8	0.0373	0.0021
9	0.0353	0.0019
10	0.0352	0.0017
11	0.0345	0.0016
12	0.0342	0.0016
13	0.0340	0.0015
14	0.0336	0.0015
15	0.0330	0.0015
16	0.0326	0.0014
17	0.0322	0.0014
18	0.0307	0.0013
19	0.0305	0.0013
20	0.0302	0.0012
21	0.0296	0.0012
22	0.0272	0.0012

81 82 83 84 85 86 87 88 90 91 92 93 94 95 96 97 98 99 101 102 103 104 105 107 108 109 110 111 113 114 115 116 117 118 119 119 119 119 119 119 119 119 119	0.0156 0.0155 0.0154 0.0152 0.0147 0.0146 0.0146 0.0145 0.0137 0.0136 0.0133 0.0132 0.0132 0.0132 0.0127 0.0124 0.0123 0.0121 0.0120 0.0119 0.0118 0.0117 0.0118 0.0117 0.0114 0.0113 0.0110 0.0103 0.0103 0.0101 0.0100 0.0100 0.0100 0.0100 0.0100 0.0100 0.0099 0.0099 0.0099 0.0099 0.0099 0.0097 0.0097 0.0097 0.0088 0.0084 0.0084 0.0084 0.0084 0.0084 0.0083 0.0087 0.0076	0.0009 0.0008 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007
137 138	0.0077 0.0076 0.0071	0.0007 0.0007 0.0007

139	0.0070	0.0007
140	0.0070	0.0007
141	0.0070	0.0007
142	0.0068	0.0007
143	0.0068	0.0007
144	0.0067	0.0007
145	0.0063	0.0007
146	0.0063	0.0007
147	0.0063	0.0006
148	0.0062	0.0006
140	0.0062	0.0006
149	0.0061	0.0006
150	0.0061	0.0006
151	0.0059	0.0006
152	0.0053	0.0006
153	0.0052	0.0006
154	0.0048	0.0006
155	0.0034	0.0005
156	0.0016	0.0005
157	0.0013	0.0005
158	0.0008	0.0004
100	0.000	0.0004

## **Duration Flows**

# The Facility PASSED

Flow(cfs) 0.0080 0.0083 0.0086 0.0089 0.0092	Predev 54293 50160 46575 43312 40260	Mit 38 37 37 37 36	Percentage 0 0 0 0 0 0	Pass/Fail Pass Pass Pass Pass Pass Pass
0.0095 0.0098 0.0101 0.0104 0.0107	37456 34913 32609 30360 28299	36 36 35 35 35	0 0 0 0	Pass Pass Pass Pass Pass
0.0110 0.0113 0.0116 0.0119 0.0122 0.0125	26448 24803 23313 21939 20648 19435	35 34 34 34 33 33	0 0 0 0 0	Pass Pass Pass Pass Pass Pass
0.0128 0.0131 0.0134 0.0137 0.0140 0.0143	18293 17224 16160 15147 14271 13451	33 33 31 31 31 31	0 0 0 0 0	Pass Pass Pass Pass Pass Pass
0.0146 0.0149 0.0152 0.0155 0.0158	12665 11939 11235 10559 9972	31 31 31 31 31	0 0 0 0	Pass Pass Pass Pass Pass
0.0161 0.0164 0.0167 0.0170 0.0173 0.0176	9390 8864 8343 7872 7468 7041	31 30 29 27 26 26	0 0 0 0 0	Pass Pass Pass Pass Pass Pass
0.0179 0.0182 0.0185 0.0188 0.0191	6620 6277 5983 5712 5444	25 24 23 23 23	0 0 0 0	Pass Pass Pass Pass Pass
0.0194 0.0197 0.0200 0.0203 0.0206 0.0209	5199 4946 4706 4515 4339 4159	23 23 23 23 22 22	0 0 0 0 0	Pass Pass Pass Pass Pass Pass
0.0212 0.0215 0.0218 0.0221 0.0224 0.0227 0.0230 0.0233	3958 3770 3581 3414 3265 3134 3027 2927	21 21 20 20 20 19 18	0 0 0 0 0 0	Pass Pass Pass Pass Pass Pass Pass Pass
0.0236	2814	18	0	Pass

0.0239	2682	17	0	Pass
0.0242	2555	16	Ö	Pass
0.0245	2451	16	0	Pass
0.0248	2359	16	0	Pass
0.0251	2256	14	0	Pass
0.0254	2139	14	0	Pass
0.0257	2041	14	0	Pass
0.0260 0.0263	1952 1862	14 14	0 0	Pass Pass
0.0266	1779	13	0	Pass
0.0269	1692	13	Ö	Pass
0.0272	1619	12	ŏ	Pass
0.0275	1561	12	Ö	Pass
0.0278	1483	12	0	Pass
0.0281	1408	12	0	Pass
0.0284	1340	11	0	Pass
0.0287	1271	11	0	Pass
0.0290	1218	11	0	Pass
0.0293	1163	11	0	Pass
0.0296 0.0299	1103 1055	11 11	0 1	Pass Pass
0.0299	1006	11	1	Pass
0.0305	964	11	1	Pass
0.0308	919	11	<u>i</u>	Pass
0.0311	872	10	1	Pass
0.0314	815	10	1	Pass
0.0317	774	10	1	Pass
0.0320	738	10	1	Pass
0.0323	694	10	1	Pass
0.0326	636	10	1	Pass
0.0329 0.0332	601 553	10 10	1 1	Pass Pass
0.0335	533 517	10	1	Pass
0.0338	478	10	-	Pass
0.0341	433	10	2 2 2 2	Pass
0.0344	394	10	2	Pass
0.0347	363	10	2	Pass
0.0350	340	10	2	Pass
0.0353	310	9	2	Pass
0.0356	297	9	3	Pass
0.0359	273	9 9	3	Pass
0.0362 0.0365	252 237	9	ა ვ	Pass Pass
0.0368	237	9	2 2 3 3 3 4	Pass
0.0371	206	9	4	Pass
0.0374	195	9	4	Pass
0.0377	180	9	5	Pass

# Water Quality

Water Quality
Water Quality BMP Flow and Volume for POC #1
On-line facility volume: 0 acre-feet
On-line facility target flow: 0 cfs.
Adjusted for 15 min: 0 cfs.
Off-line facility target flow: 0 cfs.
Adjusted for 15 min: 0 cfs.

Flow Control and Treatment 6/2/2025 9:59:56 AM Page 27

## Model Default Modifications

Total of 0 changes have been made.

## **PERLND Changes**

No PERLND changes have been made.

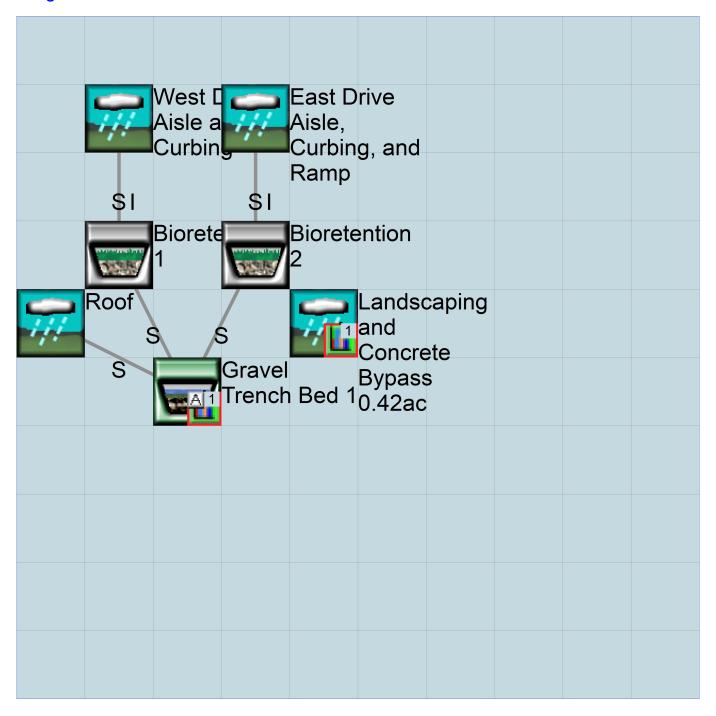
## **IMPLND Changes**

No IMPLND changes have been made.

# Appendix Predeveloped Schematic

Basin 1 0.76ac		

## Mitigated Schematic



Predeveloped UCI File RUN GLOBAL WWHM4 model simulation START 1901 10 01 END 2059 09 30 RUN INTERP OUTPUT LEVEL 3 0 RESUME 0 RUN 1 UNIT SYSTEM 1 END GLOBAL FILES <File> <Un#> <---->\*\*\* <-ID-> WDM 26 Flow Control and Treatment.wdm MESSII 25 PreFlow Control and Treatment.MES 27 PreFlow Control and Treatment.L61 PreFlow Control and Treatment.L62 POCFlow Control and Treatment1.dat 30 END FILES OPN SEQUENCE INGRP 10 INDELT 00:15 PERLND 501 COPY DISPLY END INGRP END OPN SEQUENCE DISPLY DISPLY-INFO1 # - #<-----Title---->\*\*\*TRAN PIVL DIG1 FIL1 PYR DIG2 FIL2 YRND Basin 1 1 2 30 9 END DISPLY-INFO1 END DISPLY COPY TIMESERIES # - # NPT NMN \*\*\* 1 1 )1 1 1 1 501 END TIMESERIES END COPY GENER OPCODE # # OPCD \*\*\* END OPCODE PARM K \*\*\* # END PARM END GENER PERLND GEN-INFO <PLS ><----Name---->NBLKS Unit-systems Printer \*\*\* User t-series Engl Metr \*\*\* in out 1 10 C, Forest, Flat END GEN-INFO \*\*\* Section PWATER\*\*\* ACTIVITY # - # ATMP SNOW PWAT SED PST PWG PQAL MSTL PEST NITR PHOS TRAC \*\*\*
10 0 0 1 0 0 0 0 0 0 0 0 END ACTIVITY

PRINT-INFO

END PRINT-INFO

```
PWAT-PARM1
   <PLS > PWATER variable monthly parameter value flags ***
  # - # CSNO RTOP UZFG VCS VUZ VNN VIFW VIRC VLE INFC HWT ***
10 0 0 0 0 0 0 0 0 0 0
 END PWAT-PARM1
 PWAT-PARM2
  END PWAT-PARM2
 PWAT-PARM3
  PWAT-PARM3

<PLS > PWATER input info: Part 3 ***

# - # ***PETMAX PETMIN INFEXP INFILD DEEPFR

10 0 0 2 2 0
                                                          BASETP
                                                0 0
 END PWAT-PARM3
 PWAT-PARM4
   <PLS > PWATER input info: Part 4
  # - # CEPSC UZSN NSUR INTFW IRC LZETP ***
10 0.2 0.5 0.35 6 0.5 0.7
 END PWAT-PARM4
 PWAT-STATE1
   <PLS > *** Initial conditions at start of simulation
    ran from 1990 to end of 1992 (pat 1-11-95) RUN 21 ***
   # - # *** CEPS SURS UZS IFWS LZS AGWS LO 0 0 0 2.5 1
                                                                    GWVS
  10
 END PWAT-STATE1
END PERLND
IMPLND
 GEN-INFO
   <PLS ><-----Name----> Unit-systems Printer ***
   # - #
                           User t-series Engl Metr ***
                                  in out
 END GEN-INFO
 *** Section IWATER***
 ACTIVITY
   <PLS > ******** Active Sections **********************
   # - # ATMP SNOW IWAT SLD IWG IQAL ***
 END ACTIVITY
 PRINT-INFO
   <ILS > ******* Print-flags ******* PIVL PYR
   # - # ATMP SNOW IWAT SLD IWG IQAL *******
 END PRINT-INFO
  <PLS > IWATER variable monthly parameter value flags ***
   # - # CSNO RTOP VRS VNN RTLI ***
 END IWAT-PARM1
 IWAT-PARM2
   <PLS > IWATER input info: Part 2 ***
# - # *** LSUR SLSUR NSUR RETSC
 END IWAT-PARM2
 IWAT-PARM3
   <PLS > IWATER input info: Part 3
   # - # ***PETMAX PETMIN
 END IWAT-PARM3
   <PLS > *** Initial conditions at start of simulation
   # - # *** RETS SURS
 END IWAT-STATE1
```

```
SCHEMATIC
                  <--Area--> <-Target-> MBLK ***
<-factor-> <Name> # Tbl# ***
<-Source->
<Name> #
Basin 1***
                        0.762 COPY 501 12
0.762 COPY 501 13
PERLND 10
PERLND 10
*****Routing****
END SCHEMATIC
NETWORK
<-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Target vols> <-Grp> <-Member-> ***
<-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Target vols> <-Grp> <-Member-> ***
END NETWORK
RCHRES
 GEN-INFO
  RCHRES Name Nexits Unit Systems Printer
  # - #<----- User T-series Engl Metr LKFG
                                                         * * *
                                                         * * *
                               in out
 END GEN-INFO
 *** Section RCHRES***
 ACTIVITY
  # - # HYFG ADFG CNFG HTFG SDFG GQFG OXFG NUFG PKFG PHFG ***
 END ACTIVITY
 PRINT-INFO
  <PLS > ******** Print-flags ******** PIVL PYR
   # - # HYDR ADCA CONS HEAT SED GQL OXRX NUTR PLNK PHCB PIVL PYR *******
 END PRINT-INFO
 HYDR-PARM1
  RCHRES Flags for each HYDR Section
  # - # VC A1 A2 A3 ODFVFG for each *** ODGTFG for each FUNCT for each FG FG FG possible exit *** possible exit possible exit ***
 END HYDR-PARM1
 HYDR-PARM2
 # - # FTABNO LEN DELTH STCOR
                                         KS
                                               DB50
 <----><----><---->
                                                        * * *
 END HYDR-PARM2
  RCHRES Initial conditions for each HYDR section
  <---->
                 <---><---><---> *** <---><---><--->
 END HYDR-INIT
END RCHRES
SPEC-ACTIONS
END SPEC-ACTIONS
FTABLES
END FTABLES
EXT SOURCES
<-Volume-> <Member> SsysSgap<--Mult-->Tran <-Target vols> <-Grp> <-Member-> ***
      <Name> # # ***
WDM
WDM
```

	EVAP EVAP	ENGL ENGL	1 1		1 999 1 999	EXTNL EXTNL	PETINP PETINP	
END EXT SO	URCES							
<name> #</name>	<-Grp>	<name> # #</name>	<pre>&gt;<mult>Tran t&lt;-factor-&gt;strg 48.4</mult></pre>	<name></name>		ne>	tem strg	
<name> MASS-LIN</name>	K	<name> # ‡ 12</name>	<pre><mult> &lt;-factor-&gt;</mult></pre>	<target></target>		-	<-Member	
PERLND END MASS	PWATER -LINK	12	0.083333	COPY		INPUT	MEAN	
MASS-LIN PERLND END MASS	PWATER	13 IFWO 13	0.083333	COPY		INPUT	MEAN	

END MASS-LINK

END RUN

## Mitigated UCI File

RUN

```
GLOBAL
 WWHM4 model simulation
 START 1901 10 01 END 2059 09 30 RUN INTERP OUTPUT LEVEL 3 0
 RESUME 0 RUN 1
                                   UNIT SYSTEM 1
END GLOBAL
FILES
<File> <Un#>
           <---->***
<-ID->
WDM
         26 Flow Control and Treatment.wdm
MESSU
         25
           MitFlow Control and Treatment.MES
             MitFlow Control and Treatment.L61
         27
         28
             MitFlow Control and Treatment.L62
             POCFlow Control and Treatment1.dat
         30
END FILES
OPN SEQUENCE
   INGRP
                  INDELT 00:15
              1 8
     IMPLND
     IMPLND
     PERLND
               4
     IMPLND
     GENER
    RCHRES
    RCHRES
     GENER
    RCHRES
    RCHRES
              5
    RCHRES
               1
    COPY
              501
     COPY
     COPY
              601
    DISPLY
              1
   END INGRP
END OPN SEQUENCE
DISPLY
 DISPLY-INFO1
   END DISPLY-INFO1
END DISPLY
COPY
 TIMESERIES
   # - # NPT NMN ***
      1 1
   1
 601
          1
               1
 END TIMESERIES
END COPY
GENER
 OPCODE
       # OPCD ***
  #
   2
         24
  4
          24
 END OPCODE
 PARM
              K ***
   #
   2
              0.
   4
              0.
 END PARM
END GENER
PERLND
 GEN-INFO
                              Unit-systems Printer ***
   <PLS ><---->NBLKS
                              User t-series Engl Metr ***
```

```
in out A/B, Pasture, Flat 1 1 1 27 0
 END GEN-INFO
 *** Section PWATER***
 ACTIVITY
   <PLS > ******* Active Sections **********************
   \# - \# ATMP SNOW PWAT SED PST PWG PQAL MSTL PEST NITR PHOS TRAC *** 4 0 0 1 0 0 0 0 0 0 0 0 0
 END ACTIVITY
 PRINT-INFO
   <PLS > *********** Print-flags ************************* PIVL PYR
   # - # ATMP SNOW PWAT SED PST PWG PQAL MSTL PEST NITR PHOS TRAC ********
   END PRINT-INFO
 PWAT-PARM1
   <PLS > PWATER variable monthly parameter value flags ***
   # - # CSNO RTOP UZFG VCS VUZ VNN VIFW VIRC VLE INFC HWT ***
4 0 0 0 0 0 0 0 0 0 0 0
 END PWAT-PARM1
   WAT-PARM2

<PLS > PWATER input info: Part 2 ***

# - # ***FOREST LZSN INFILT LSUR SLSUR KVARY AGWRC

O 5 1.5 400 0.05 0.3 0.996
 PWAT-PARM2
 END PWAT-PARM2
 PWAT-PARM3
             PWATER input info: Part 3
  <PLS >
   # - # ***PETMAX PETMIN INFEXP
4 0 0 2
                                        INFILD DEEPFR
                                                           BASETP
                                        2
                                                 0
                                                          0
 END PWAT-PARM3
 PWAT-PARM4
   <PLS > PWATER input info: Part 4
                                       INTFW IRC LZETP ***
0 0.7 0.4
   # - # CEPSC UZSN NSUR
4 0.15 0.5 0.3
 END PWAT-PARM4
 PWAT-STATE1
   <PLS > *** Initial conditions at start of simulation
          ran from 1990 to end of 1992 (pat 1-11-95) RUN 21 ***
       # *** CEPS SURS UZS IFWS LZS AGWS 0 0 0 0 3 1
                                                                     GWVS
   4
                       0
 END PWAT-STATE1
END PERLND
TMPT.ND
 GEN-INFO
   <PLS ><----- Name----> Unit-systems Printer ***
                           User t-series Engl Metr ***
                                  in out
                              1 1 1 27 0
1 1 1 27 0
1 1 1 27 0
   1
         ROADS/FLAT
         SIDEWALKS/FLAT
         ROOF TOPS/FLAT
 END GEN-INFO
 *** Section IWATER***
 ACTIVITY
   <PLS > ********* Active Sections *********************
   # - # ATMP SNOW IWAT SLD IWG IQAL
       0 0 1 0 0 0
0 0 1 0 0 0
0 0 1 0 0 0
   1
   8
 END ACTIVITY
 PRINT-INFO
   <ILS > ****** Print-flags ****** PIVL PYR
```

```
*****
   # - # ATMP SNOW IWAT SLD IWG IQAL
                         0
                                         1
               0 4
                              0 4
                                             9
   1
            Ω
   8
             0
                 Ω
                      4
                          0
                               0
                                    0
                                         1
                                             9
                                              9
             0
                          0
                               0
 END PRINT-INFO
 IWAT-PARM1
   <PLS > IWATER variable monthly parameter value flags ***
   # - # CSNO RTOP VRS VNN RTLI
                         0
           0
               0
                     0
                             0
             0
                 0
                     0
                          0
                               0
   8
             0
                     0
                          0
   4
                 0
                               0
 END IWAT-PARM1
  IWAT-PARM2
   <PLS >
               IWATER input info: Part 2
              LSUR SLSUR NSUR
                                          RETSC
                       0.01
                                         0.1
   1
               400
                                 0.1
                400
                       0.01
                                  0.1
                                           0.1
   4
                400
                        0.01
                                  0.1
                                           0.1
 END IWAT-PARM2
 IWAT-PARM3
                                             ***
              IWATER input info: Part 3
   <PLS >
   # - # ***PETMAX
                      PETMIN
               0
                       0
   1
   8
                 0
                           0
   4
                 0
                           0
 END IWAT-PARM3
 IWAT-STATE1
   <PLS > *** Initial conditions at start of simulation
   # - # *** RETS SURS
   1
                 0
                        0
                 0
                           0
   8
   4
                 0
                           0
 END IWAT-STATE1
END IMPLND
SCHEMATIC
<-Source->
                          <--Area-->
                                        <-Target-> MBLK
                                                           * * *
                                                           * * *
<Name> #
                          <-factor->
                                        <Name> # Tbl#
West Drive Aisle***
                                                       5
IMPLND 1
                               0.19
                                        RCHRES
                                                1
East Drive Aisle***
IMPLND
      1
                               0.088
                                        RCHRES
                                                3
                                                       5
IMPLND
                               0.002
                                        RCHRES
                                                3
                                                       5
Basin 4***
IMPLND 4
                               0.063
                                        RCHRES 5
                                                      5
Basin 3***
PERLND 4
                               0.417
                                        COPY
                                              501
                                                     12
PERLND 4
                               0.417
                                        COPY
                                              601
                                                     12
                               0.002
IMPLND 8
                                        COPY
                                              501
                                                     15
       8
                               0.002
                                        COPY
                                             601
                                                      15
IMPLND
*****Routing****
                                  1
                                        RCHRES
                                                5
                                                      6
RCHRES
       2
        2
RCHRES
                                        COPY
                                                1
                                                      16
RCHRES
        1
                                  1
                                        RCHRES
                                                      7
                                                     17
RCHRES
        1
                                        COPY
                                                1
RCHRES
                                  1
                                        RCHRES
                                                5
                                                      6
RCHRES
                                  1
                                        RCHRES
       4
                                                1
RCHRES
                                        COPY
                                                     16
RCHRES
        3
                                  1
                                        RCHRES
                                                5
                                                      7
RCHRES
        3
                                        COPY
                                                1
                                                      17
                                  1
RCHRES
                                        RCHRES
                                                4
                                                       8
                               0.063
                                                1
                                                      15
IMPLND
        4
                                        COPY
       5
                                  1
                                               501
                                                      17
RCHRES
                                        COPY
END SCHEMATIC
```

```
NETWORK
<-Volume-> <-Grp> <-Member-><-Tran <-Target vols> <-Grp> <-Member->
<Name> # # ***
<-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Target vols> <-Grp> <-Member-> ***
END NETWORK
RCHRES
  GEN-INFO
            Name Nexits Unit Systems Printer
                                                                         * * *
   RCHRES
   # - #<----><---> User T-series Engl Metr LKFG
                                                                         * * *
                                                                         * * *
                                        in out
       Surface retentio-009 2 1 1 28
Bioretention 1 1 1 1 28
Surface retentio-011 2 1 1 1 28
Bioretention 2 1 1 1 28
Gravel Trench Be-007 2 1 1 1 28
                                                            1
                                                            1
                                                            1
   5
  END GEN-INFO
  *** Section RCHRES***
  ACTIVITY
   <PLS > ******** Active Sections *********************
    # - # HYFG ADFG CNFG HTFG SDFG GOFG OXFG NUFG PKFG PHFG ***
   END ACTIVITY
  PRINT-INFO
    <PLS > ******** Print-flags ******** PIVL PYR
    # - # HYDR ADCA CONS HEAT SED GQL OXRX NUTR PLNK PHCB PIVL
                                                               PYR
        # HIDR ADCA CONS REAT SED GQL OARX NOTR PLINK PHCB PIVE

4 0 0 0 0 0 0 0 0 0 0 0 1

4 0 0 0 0 0 0 0 0 0 0 0 1

4 0 0 0 0 0 0 0 0 0 0 0 1

4 0 0 0 0 0 0 0 0 0 0 1
    3
    4
   5
  END PRINT-INFO
  HYDR-PARM1
   RCHRES Flags for each HYDR Section
   # - # VC A1 A2 A3 ODFVFG for each *** ODGTFG for each FUNCT for each FG FG FG possible exit *** possible exit possible exit
           * * *
   1
                                                              2 2 2 2 2
2 1 2 2 2
2 2 2 2 2
2 2 2 2 2
    2
    3
    5
  END HYDR-PARM1
  HYDR-PARM2
  # - # FTABNO LEN DELTH STCOR KS DB50
                                                                        * * *
  <----><----><---->
             1 0.01 0.0 0.0 0.0 0.0
2 0.01 0.0 0.0 0.0 0.0
3 0.01 0.0 0.0 0.0 0.0
4 0.01 0.0 0.0 0.0 0.0
5 0.02 0.0 0.0 0.5 0.0
   1
    2
    3
    5
  END HYDR-PARM2
  HYDR-INIT
   RCHRES Initial conditions for each HYDR section
```

```
# - # *** VOL
                           Initial value of COLIND Initial value of OUT for each possible exit for each possible exit
                                                                     Initial value of OUTDGT
           *** ac-ft
                              <---><---><---><--->
  <---->

      4.0
      5.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
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      0.0
      0.0
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      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0.0
      0
     1
                   Ω
                     0
     3
                     0
                     0
     4
     5
                     0
  END HYDR-INIT
END RCHRES
SPEC-ACTIONS
*** User-Defined Variable Quantity Lines
* * *
*** kwd varnam optyp opn vari s1 s2 s3 tp multiply lc ls ac as agfn ***
  <****> <----> <--> <-> <--> ***
  UVQUAN vol2 RCHRES 2 VOL
                                                        4
                  GLOBAL
                              WORKSP 1
WORKSP 2
  UVQUAN v2m2
  UVQUAN vpo2 GLOBAL WORKSP 2
UVQUAN v2d2 GENER 2 K 1
*** User-Defined Variable Quantity Lines
* * *
                                   addr
* * *
                                  <--->
*** kwd varnam optyp opn vari s1 s2 s3 tp multiply lc ls ac as agfn ***
  <****> <----> <--> <-> <--> ***
                                                 4
  UVQUAN vol4 RCHRES 4 VOL
  UVQUAN v2m4 GLOBAL WORKSP 3
UVQUAN vpo4 GLOBAL WORKSP 4
UVQUAN v2d4 GENER 4 K 1
*** User-Defined Target Variable Names
* * *
                                                                addr or
                         addr or
* * *
                         <--->
                                                                <--->
*** kwd varnam ct vari s1 s2 s3 frac oper
                                                                vari s1 s2 s3 frac oper
  <****> <---><-><-><-><-><->
                                                                <---><-><-><->
  UVNAME v2m2 1 WORKSP 1
                                               1.0 QUAN
  UVNAME vpo2 1 WORKSP 2
UVNAME v2d2 1 K 1
                                        1.0 QUAN
1.0 QUAN
*** User-Defined Target Variable Names
                         addr or
                                                                addr or
* * *
                         <--->
                                                                <--->
                                                            vari sl s2 s3 1100 1
*** kwd varnam ct vari s1 s2 s3 frac oper
  <****> <---><-><-><-><-><-><->
  *** opt foplop dcdts yr mo dy hr mn d t vnam s1 s2 s3 ac quantity tc ts rp
  v2m2
                                                                          = 418.05
*** Compute remaining available pore space
  GENER 2
                                                      vpo2
  GENER
                                                      vpo2
*** Check to see if VPORA goes negative; if so set VPORA = 0.0
IF (vpo2 < 0.0) THEN
  GENER 2
                                                                          = 0.0
                                                      vpo2
END IF
*** Infiltration volume
  GENER 2
                                                      v2d2
                                                                          = vpo2
*** opt foplop dcdts yr mo dy hr mn d t vnam s1 s2 s3 ac quantity tc ts rp
  v2m4
                                                                         = 284.39
*** Compute remaining available pore space
                                                                         = v2m4
                                                      vpo4
                                                                        -= vol4
                                                      vpo4
*** Check to see if VPORA goes negative; if so set VPORA = 0.0
IF (vpo4 < 0.0) THEN
 GENER
                                                      vpo4
                                                                          = 0.0
END IF
*** Infiltration volume
                                                                          = vpo4
  GENER 4
                                                      v2d4
```

END SPEC-ACTIONS FTABLES FTABLE 5 92 Depth Volume Outflow1 Outflow2 Velocity Travel Time\*\*\* Area (ft) (acres) (acre-ft) (cfs) (cfs) (ft/sec) (Minutes) \* \* \* 0.000000 0.044353 0.000000 0.00000 0.00000 0.000000 0.038014 0.044353 0.000488 0.033333 0.066667 0.044353 0.000976 0.00000 0.038014 0.100000 0.044353 0.001464 0.00000 0.038014 0.133333 0.044353 0.001952 0.000000 0.038014 0.044353 0.002439 0.166667 0.000000 0.038014 0.200000 0.044353 0.002927 0.00000 0.038014 0.044353 0.233333 0.003415 0.00000 0.038014 0.266667 0.044353 0.003903 0.00000 0.038014 0.044353 0.00000 0.300000 0.004391 0.038014 0.333333 0.044353 0.004879 0.000000 0.038014 0.00000 0.044353 0.005367 0.038014 0.366667 0.400000 0.044353 0.005855 0.00000 0.038014 0.433333 0.044353 0.006342 0.00000 0.038014 0.044353 0.466667 0.006830 0.000000 0.038014 0.500000 0.044353 0.007318 0.00000 0.038014 0.533333 0.044353 0.007806 0.00000 0.038014 0.044353 0.008294 0.00000 0.566667 0.038014 0.600000 0.044353 0.008782 0.000000 0.038014 0.044353 0.000000 0.633333 0.009270 0.038014 0.00000 0.666667 0.044353 0.009758 0.038014 0.700000 0.044353 0.00000 0.010245 0.038014 0.733333 0.044353 0.010733 0.000000 0.038014 0.766667 0.044353 0.011221 0.000000 0.038014 0.800000 0.044353 0.011709 0.00000 0.038014 0.044353 0.012197 0.00000 0.833333 0.038014 0.866667 0.044353 0.012685 0.00000 0.038014 0.900000 0.044353 0.013173 0.000000 0.038014 0.044353 0.000000 0.933333 0.013661 0.038014 0.044353 0.014148 0.00000 0.038014 0.966667 1.000000 0.044353 0.014636 0.00000 0.038014 0.044353 0.015124 1.033333 0.000000 0.038014 1.066667 0.044353 0.015612 0.00000 0.038014 1.100000 0.044353 0.016100 0.000000 0.038014 0.00000 1.133333 0.044353 0.016588 0.038014 1.166667 0.044353 0.017076 0.00000 0.038014 1.200000 0.044353 0.017564 0.00000 0.038014 1.233333 0.044353 0.018052 0.000000 0.038014 1.266667 0.044353 0.000000 0.018539 0.038014 1.300000 0.044353 0.019027 0.000000 0.038014 1.333333 0.044353 0.019515 0.000000 0.038014 1.366667 0.044353 0.020003 0.00000 0.038014 0.044353 0.020491 0.00000 1.400000 0.038014 1.433333 0.044353 0.020979 0.000000 0.038014 1.466667 0.044353 0.021467 0.00000 0.038014 1.500000 0.044353 0.021955 0.00000 0.038014 1.533333 0.044353 0.022442 0.000000 0.038014 0.044353 0.022930 0.00000 1.566667 0.038014 0.00000 1.600000 0.044353 0.023418 0.038014 1.633333 0.044353 0.023906 0.00000 0.038014 0.044353 0.024394 0.00000 0.038014 1.666667 1.700000 0.044353 0.024882 0.000000 0.038014 0.044353 0.025370 0.000000 0.038014 1.733333 0.025858 1.766667 0.044353 0.00000 0.038014 0.044353 0.026345 0.00000 1.800000 0.038014 1.833333 0.044353 0.026833 0.000000 0.038014 1.866667 0.044353 0.027321 0.000000 0.038014 0.00000 1.900000 0.044353 0.027809 0.038014 0.044353 0.028297 0.00000 1.933333 0.038014 1.966667 0.044353 0.028785 0.00000 0.038014 2.000000 0.044353 0.029273 0.000000 0.038014 2.033333 0.044353 0.029761 0.000000 0.038014 2.066667 0.044353 0.030248 0.00000 0.038014

0.038014

0.000000

0.030736

2.100000

0.044353

```
2.133333
          0.044353
                     0.031224
                                0.000000
                                           0.038014
                                           0.038014
          0.044353
                     0.031712
                                0.000000
2.166667
2.200000
          0.044353
                     0.032200
                                0.00000
                                           0.038014
2.233333
          0.044353
                     0.032688
                                0.00000
                                           0.038014
          0.044353
                     0.033176
                                0.00000
2.266667
                                           0.038014
2.300000
          0.044353
                     0.033664
                                0.00000
                                           0.038014
2.333333
          0.044353
                                0.000000
                     0.034152
                                           0.038014
          0.044353
                                0.000000
2.366667
                     0.034639
                                           0.038014
2.400000
          0.044353
                     0.035127
                                0.00000
                                           0.038014
2.433333
           0.044353
                     0.035615
                                0.00000
                                           0.038014
2.466667
          0.044353
                     0.036103
                                0.000000
                                           0.038014
          0.044353
2.500000
                     0.036591
                                0.000000
                                           0.038014
2.533333
          0.044353
                     0.037079
                                0.00000
                                           0.038014
          0.044353
2.566667
                     0.037567
                                0.000000
                                           0.038014
2.600000
           0.044353
                     0.038055
                                0.00000
                                           0.038014
          0.044353
                     0.038542
                                0.00000
2.633333
                                           0.038014
                     0.039030
2.666667
          0.044353
                                0.000000
                                           0.038014
2.700000
                                0.00000
          0.044353
                     0.039518
                                           0.038014
2.733333
          0.044353
                     0.040006
                                0.00000
                                           0.038014
2.766667
          0.044353
                     0.040494
                                0.000000
                                           0.038014
          0.044353
                     0.040982
2.800000
                                0.000000
                                           0.038014
                                           0.038014
2.833333
          0.044353
                     0.041470
                                0.00000
2.866667
          0.044353
                     0.041958
                                0.00000
                                           0.038014
2.900000
          0.044353
                     0.042445
                                0.00000
                                           0.038014
2.933333
          0.044353
                     0.042933
                                0.021395
                                           0.038014
          0.044353
                     0.043421
                                0.058227
2.966667
                                           0.038014
3.000000
          0.044353
                     0.043909
                                0.096846
                                           0.038014
          0.044353
                     0.045388
                                0.125736
3.033333
                                           0.038014
END FTABLE
             2
FTABLE
 71
   Depth
                        Volume
                                Outflow1 Velocity
                                                     Travel Time ***
               Area
    (ft)
            (acres)
                    (acre-ft)
                                 (cfs)
                                          (ft/sec)
                                                       (Minutes) * * *
0.000000
          0.015909
                     0.000000
                                0.000000
0.046703
          0.015707
                     0.000016
                                0.00000
0.093407
          0.015367
                     0.000034
                                0.00000
0.140110
          0.015030
                     0.000053
                                0.00000
          0.014697
                     0.000076
0.186813
                                0.00000
0.233516
          0.014368
                     0.000100
                                0.00000
0.280220
          0.014042
                     0.000127
                                0.000000
          0.013720
                     0.000156
0.326923
                                0.000021
0.373626
          0.013401
                     0.000188
                                0.000036
0.420330
          0.013086
                     0.000222
                                0.000056
0.467033
          0.012775
                     0.000260
                                0.000082
                     0.000299
                                0.000114
0.513736
          0.012467
0.560440
          0.012163
                     0.000342
                                0.000153
                     0.000388
0.607143
          0.011862
                                0.000200
0.653846
           0.011565
                     0.000436
                                0.000246
0.700549
          0.011272
                     0.000488
                                0.000254
0.747253
          0.010982
                     0.000543
                                0.000317
0.793956
          0.010696
                     0.000601
                                0.000389
0.840659
          0.010414
                     0.000662
                                0.000470
0.887363
          0.010135
                     0.000727
                                0.000556
          0.009859
                     0.000795
                                0.000560
0.934066
                                0.000598
0.980769
          0.009587
                     0.000867
1.027473
          0.009319
                     0.000942
                                0.000661
1.074176
          0.009055
                     0.001022
                                0.000771
1.120879
          0.008794
                     0.001104
                                0.000892
1.167582
          0.008537
                     0.001191
                                0.001024
1.214286
          0.008283
                     0.001282
                                0.001149
1.260989
          0.008033
                     0.001376
                                0.001167
1.307692
          0.007786
                     0.001475
                                0.001245
          0.007543
1.354396
                     0.001577
                                0.001321
1.401099
          0.007304
                     0.001684
                                0.001488
1.447802
          0.007068
                     0.001796
                                0.001666
1.494505
          0.006836
                     0.001911
                                0.001856
1.541209
           0.006608
                     0.002032
                                0.001928
1.587912
          0.006383
                     0.002156
                                0.002060
1.634615
          0.006162
                     0.002285
                                0.002275
          0.005944
1.681319
                     0.002419
                                0.002301
```

```
1.728022
           0.005730
                     0.002558
                                0.002504
                                0.002746
1.774725
           0.005520
                     0.002688
1.821429
           0.005313
                     0.002823
                                0.002959
1.868132
           0.005109
                     0.002962
                                0.003001
           0.004910
                     0.003106
                                0.003269
1.914835
1.961538
           0.004714
                     0.003255
                                0.003551
                     0.003408
                                0.003737
2.008242
           0.004521
2.054945
                                0.003771
           0.004333
                     0.003566
2.101648
           0.004147
                     0.003729
                                0.005266
2.148352
           0.003966
                     0.003897
                                0.005736
2.195055
           0.003788
                     0.004070
                                0.006250
2.241758
           0.003613
                     0.004248
                                0.006250
                                0.006250
2.288462
           0.003443
                     0.004432
2.335165
           0.003275
                     0.004620
                                0.006250
2.381868
           0.003112
                     0.004814
                                0.006250
           0.002952
                     0.005013
                                0.006250
2.428571
2.475275
           0.002795
                     0.005217
                                0.006250
           0.002643
                     0.005428
                                0.006250
2.521978
2.568681
           0.002493
                     0.005643
                                0.006250
2.615385
           0.002348
                     0.005865
                                0.006250
2.662088
           0.002206
                     0.006092
                                0.006250
2.708791
           0.002068
                     0.006324
                                0.006250
2.755495
           0.001933
                     0.006563
                                0.006250
           0.001802
                     0.006808
                                0.006250
2.802198
2.848901
           0.001674
                     0.007058
                                0.006250
           0.001550
2.895604
                     0.007315
                                0.006250
                                0.006250
2.942308
           0.001430
                     0.007578
2.989011
                     0.007847
                                0.006250
           0.001313
3.035714
           0.001200
                     0.008122
                                0.006250
3.082418
           0.001091
                     0.008404
                                0.006250
           0.000985
                     0.008692
3.129121
                                0.006250
3.175824
           0.000882
                     0.008987
                                0.006250
3.222527
           0.000784
                     0.009288
                                0.006250
3.250000
           0.000689
                     0.009597
                                0.006250
END FTABLE
            2
             1
FTABLE
 23
                                           Outflow2
                                                      Velocity
                                                                 Travel Time***
   Depth
               Area
                        Volume
                                Outflow1
            (acres) (acre-ft)
                                  (cfs)
                                              (cfs)
                                                      (ft/sec)
                                                                   (Minutes) * * *
    (ft)
0.000000
                     0.000000
                                0.00000
                                           0.00000
           0.000689
                                0.00000
0.046703
           0.016255
                     0.000751
                                           0.004167
0.093407
           0.016605
                     0.001518
                                0.00000
                                           0.005121
0.140110
           0.016958
                     0.002302
                                0.00000
                                           0.005250
0.186813
           0.017315
                     0.003102
                                0.000000
                                           0.005380
                     0.003920
                                0.000000
0.233516
           0.017675
                                           0.005510
0.280220
           0.018039
                     0.004754
                                0.000000
                                           0.005640
                     0.005605
0.326923
           0.018407
                                0.000000
                                           0.005769
0.373626
           0.018778
                     0.006473
                                0.00000
                                           0.005899
0.420330
           0.019153
                     0.007359
                                0.00000
                                           0.006029
0.467033
           0.019531
                     0.008262
                                0.000000
                                           0.006158
0.513736
           0.019913
                     0.009183
                                0.011388
                                           0.006288
0.560440
           0.020299
                     0.010122
                                0.104618
                                           0.006418
0.607143
           0.020688
                     0.011079
                                0.242355
                                           0.006548
           0.021081
                     0.012055
                                0.398865
0.653846
                                           0.006677
0.700549
           0.021477
                     0.013048
                                0.549487
                                           0.006807
0.747253
           0.021877
                     0.014061
                                0.672007
                                           0.006937
0.793956
           0.022281
                     0.015092
                                0.754652
                                           0.007067
0.840659
           0.022688
                     0.016142
                                0.817028
                                           0.007196
           0.023099
                     0.017211
                                           0.007326
0.887363
                                0.871236
0.934066
           0.023513
                     0.018300
                                0.922263
                                           0.007456
           0.023931
                                0.970611
                                           0.007585
0.980769
                     0.019408
1.000000
           0.024105
                     0.019869
                                1.016663
                                           0.007639
END FTABLE
            1
             4
FTABLE
 71
   Depth
                       Volume
                                Outflow1 Velocity
                                                     Travel Time***
               Area
    (ft)
            (acres)
                     (acre-ft)
                                  (cfs)
                                          (ft/sec)
                                                       (Minutes) ***
0.00000
                                0.00000
           0.012093
                     0.000000
0.046703
           0.011919
                     0.000005
                                0.00000
                                0.00000
0.093407
           0.011627
                     0.000012
```

2.381868       0.001736       0.003045       0.00208         2.428571       0.001624       0.003187       0.00208         2.475275       0.001516       0.003334       0.00208         2.521978       0.001412       0.003485       0.00208         2.568681       0.001311       0.003641       0.00208         2.615385       0.001213       0.003966       0.00208         2.708791       0.001030       0.004137       0.00208         2.755495       0.000943       0.004312       0.00208         2.802198       0.000860       0.004492       0.00208         2.848901       0.000781       0.004677       0.00208         2.942308       0.000633       0.005063       0.00208         2.989011       0.000565       0.005263       0.00208         3.035714       0.000500       0.005470       0.00208         3.129121       0.000381       0.005898       0.00208         3.175824       0.000327       0.006121       0.00208         3.222527       0.000276       0.006349       0.00208	0.233516 0.280220 0.326923 0.373626 0.4203330 0.467033 0.513736 0.560440 0.607143 0.653846 0.700549 0.747253 0.793956 0.887363 0.9340669 1.074776 1.120879 1.167582 1.214286 1.260989 1.354396 1.401099 1.447802 1.541209 1.587912 1.634615 1.681319 1.728022 1.774725 1.8681329 1.8681329 1.868132 1.914835 1.	0.010773 0.010495 0.010495 0.010221 0.009951 0.009684 0.009421 0.009161 0.008905 0.008653 0.008404 0.007918 0.007918 0.007918 0.007445 0.006544 0.006544 0.006544 0.006544 0.0065701 0.005906 0.005701 0.005906 0.005701 0.005499 0.005301 0.005106 0.004915 0.004728 0.004728 0.004364 0.004364 0.004364 0.004364 0.004364 0.004364 0.004364 0.004364 0.004364 0.004364 0.004364 0.004364 0.003516 0.003516 0.003516 0.003516 0.003516 0.003516 0.003516 0.003516 0.001516	0.000038 0.000050 0.000050 0.000062 0.000077 0.000092 0.000110 0.000129 0.000150 0.000150 0.000254 0.000285 0.000319 0.000355 0.000393 0.000434 0.000477 0.000572 0.000678 0.000678 0.000736 0.000736 0.000796 0.000927 0.001147 0.001227 0.001311 0.001399 0.001490 0.001576 0.001666 0.001760 0.001857	0.00000 0.00000 0.00000 0.00000 0.00000 0.00001 0.00001 0.00005 0.00008 0.00008 0.00010 0.00013 0.00015 0.00018 0.00018 0.00019 0.00022 0.00025 0.00029 0.00034 0.00038 0.00019 0.0004 0.0004 0.0004 0.0004 0.0006 0.00008
1.260989       0.005499       0.000736       0.0003         1.307692       0.005301       0.000796       0.0004         1.354396       0.005106       0.000860       0.0004         1.401099       0.004915       0.000927       0.0004         1.447802       0.004728       0.000997       0.0005         1.494505       0.004544       0.001070       0.0006         1.541209       0.004364       0.001147       0.0006         1.587912       0.004187       0.001227       0.0006         1.634615       0.004014       0.001311       0.0007         1.728022       0.003679       0.001490       0.0008         1.774725       0.003516       0.001576       0.0009         1.868132       0.003203       0.001666       0.0009         1.961538       0.002904       0.001857       0.0010         1.961538       0.002760       0.002062       0.0012         2.054945       0.002619       0.002171       0.0012         2.101648       0.002482       0.002283       0.0017         2.195055       0.002219       0.002520       0.0020         2.241758       0.002093       0.002645       0.0020	0.280220 0.326923 0.373626 0.420330 0.467033 0.513736 0.560440 0.607143 0.653846 0.700549 0.747253 0.793956 0.840659 0.887363 0.934066 0.980769 1.027473 1.074176 1.120879 1.167582	0.010495 0.010221 0.009951 0.009684 0.009421 0.009161 0.008905 0.008653 0.008404 0.008159 0.007918 0.007680 0.007446 0.007215 0.006988 0.006764 0.006544 0.006328 0.006115	0.000050 0.000062 0.000077 0.000092 0.000110 0.000129 0.000150 0.000173 0.000198 0.000225 0.000254 0.000285 0.000319 0.000355 0.000393 0.000434 0.000477 0.000523 0.000572	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001
	1.214286 1.260989 1.307692 1.354396 1.401099 1.447802 1.494505 1.541209 1.587912 1.634615 1.681319 1.728022 1.774725 1.821429 1.868132 1.914835 1.961538 2.0054945 2.101648 2.148352 2.195055 2.241758 2.288462	0.005701 0.005499 0.005301 0.005106 0.004915 0.004728 0.004544 0.004364 0.004187 0.004014 0.003879 0.003516 0.003358 0.003203 0.003051 0.002904 0.002760 0.002619 0.002482 0.002349 0.002219 0.002093 0.001970	0.000678 0.000736 0.000796 0.000860 0.000927 0.001070 0.001147 0.001227 0.001311 0.001399 0.001576 0.001666 0.001760 0.001857 0.001958 0.002062 0.002171 0.002283 0.002400 0.002520 0.002574	0.00038 0.00038 0.00041 0.00049 0.00055 0.00061 0.00068 0.00075 0.00076 0.00083 0.00091 0.00109 0.00109 0.00118 0.00125 0.00175 0.00175 0.00191 0.00208 0.00208

```
23
                       Volume Outflow1 Outflow2 Velocity
     Depth
                                                               Travel Time***
                Area
             (acres) (acre-ft)
                                 (cfs)
                                             (cfs)
                                                      (ft/sec)
                                                                (Minutes)***
      (ft)
  0.000000 0.000230 0.000000
                                 0.000000
                                           0.00000
  0.046703
           0.012390 0.000572
                                0.000000
                                           0.001389
  0.093407
            0.012692 0.001157
                                 0.000000 0.001707
            0.012996
                                0.000000 0.001750
  0.140110
                     0.001757
  0.186813
            0.013305
                      0.002371
                                0.000000 0.001793
  0.233516
            0.013617
                      0.003000
                                 0.000000
                                           0.001837
  0.280220
            0.013933
                      0.003643
                                 0.000000
                                           0.001880
                      0.004302
  0.326923
            0.014252
                                0.000000
                                           0.001923
            0.014575
                      0.004975
                                 0.000000
  0.373626
                                           0.001966
  0.420330
            0.014902
                      0.005663
                                0.000000
                                           0.002010
                      0.006367
                                 0.000000
  0.467033
            0.015232
                                           0.002053
  0.513736
            0.015566
                      0.007086
                                0.011388
                                           0.002096
                                           0.002139
            0.015903
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END MASS-LINK

END RUN

# Predeveloped HSPF Message File

# Mitigated HSPF Message File

## Disclaimer

## Legal Notice

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# **APPENDIX E**

## #2 - Maintenance Checklist for Infiltration Basins and Trenches:

Drainage System Feature	Defect or Problem	Condition When Maintenance Is Needed	Results Expected When Maintenance Is Performed
General	Trash and Debris	Any trash and debris which exceed five cubic feet per 1,000 square feet. If less than threshold, all trash and debris will be removed as part of next scheduled maintenance.	Trash and debris cleared from site.
General	Poisonous Vegetation and Noxious Weeds	Any poisonous or nuisance vegetation which may constitute a hazard to maintenance personnel or the public. Any evidence of noxious weeds as defined in the Pierce County Noxious Weeds List. (Apply requirements of adopted integrated pest management policies for the use of herbicides.)	No danger of poisonous vegetation where maintenance personnel or the public might normally be. (Coordinate with Tacoma-Pierce County Health Department) Complete eradication of noxious weeds may not be possible. Compliance with state or local eradication policies required.
General	Contaminants and Pollution	Any evidence of oil, gasoline, contaminants or other pollutants.	No contaminants or pollutants present. (Coordinate removal/cleanup with Pierce County Surface Water Management 253-798-2725 and/or Dept. of Ecology Spill Response 800- 424-8802.)
General	Rodent Holes	If the facility is constructed with a dam or berm, look for rodent holes or any evidence of water piping through the dam or berm.	Rodents removed and dam or berm repaired. (Coordinate with Tacoma-Pierce County Health Department; coordinate with Ecology Dam Safety Office if pond exceeds 10 acre-feet.)
General	Beaver Dams	Beaver dam results in an adverse change in the functioning of the facility.	Facility returned to design function. (Contact WDFW Region 6 to identify the appropriate Nuisance Wildlife Control Operator)
General	Insects	When insects such as wasps and hornets interfere with maintenance activities.	Insects destroyed or removed from site. Apply insecticides in compliance with adopted integrated pest management policies.
General	Performance	Check crest gauge against design expectations (see Maintenance and Source Control Manual).	Crest gauge results reflect design performance expectations. Reading recorded. County notified if not meeting design performance.
Crest Gauge	Crest Gauge Missing/ Broken	Crest gauge is not functioning properly, has been vandalized, or is missing.	Crest gauge present and functioning. Repair/replace crest gauge if missing or broken.
Storage Area	Water Not Infiltrating	Water ponding in infiltration basin after rainfall ceases and appropriate time allowed for infiltration. Treatment basins should infiltrate Water Quality Design Storm Volume within 48 hours, and empty within 24 hours after cessation of most rain events. (A percolation test pit or test of facility indicates facility is only working at 90 percent of its designed capabilities. If 2 inches or more sediment is present, remove).	Facility infiltrates as designed. Sediment is removed and/or facility is cleaned so that infiltration system works according to design.

## #2 - Maintenance Checklist for Infiltration Basins and Trenches:

Drainage System Feature	Defect or Problem	Condition When Maintenance Is Needed	Results Expected When Maintenance Is Performed
Filter Bags (if applicable)	Filled with Sediment and Debris	Sediment and debris fill bag more than one-half full.	Filter bag less than one-half full. Filter bag is replaced or system is redesigned.
Rock Filters	Sediment and Debris	By visual inspection, little or no water flows through filter during heavy rain storms.	Water flows through filter. Replace gravel in rock filter if needed.
Trenches	Observation Well (Use Surface of Trench if Well is Not Present)	Water ponds at surface during storm events. Less than 90 percent of design infiltration rate.	Remove and replace/clean rock and geomembrane.
Ponds	Vegetation	Exceeds 18 inches.	Grass or groundcover mowed to a height no greater than 6 inches.
Ponds	Vegetation	Bare spots.	No bare spots. Revegetate and stabilize immediately.
Side Slopes of Pond	Erosion	Erosion damage over 2 inches deep where cause of damage is still present or where there is potential for continued erosion.	Slopes stabilized using appropriate erosion control measure(s); e.g., rock reinforcement, planting of grass, compaction.  If erosion is occurring on compacted slope, a professional engineer should be consulted to resolve source of erosion.
Pond Berms (Dikes)	Settlements	Any part of berm which has settled 4 inches lower than the design elevation. If settlement is apparent, measure berm to determine amount of settlement. Settling can be an indication of more severe problems with the berm or outlet works.	Dike is built back to the design elevation.  If settlement is significant, a professional engineer should be consulted to determine the cause of the settlement.
Pond Berms (Dikes)	Piping	Discernable water flow through pond berm. Ongoing erosion with potential for erosion to continue.	No water flow through pond berm. Piping eliminated. Erosion potential eliminated. Recommend a geotechnical engineer be called in to inspect and evaluate condition and recommend repair of condition.
General	Hazard Trees	If dead, diseased, or dying trees are identified.	Hazard trees removed. (Use a certified Arborist to determine health of tree or removal requirements).
General	Tree Growth and Dense Vegetation	Tree growth and dense vegetation which impedes inspection, maintenance access or interferes with maintenance activity (i.e., slope mowing, silt removal, vactoring, or equipment movements).	Trees and vegetation do not hinder inspection or maintenance activities. Harvested trees should be recycled into mulch or other beneficial uses (e.g., alders for firewood).

## #2 - Maintenance Checklist for Infiltration Basins and Trenches:

Drainage System Feature	Defect or Problem	Condition When Maintenance Is Needed	Results Expected When Maintenance Is Performed
Pond Berms (Dikes)	Tree Growth	Tree growth on berms over 4 feet in height may lead to piping through the berm which could lead to failure of the berm.	Trees on berms removed.  If root system is small (base less than 4 inches) the root system may be left in place. Otherwise the roots should be removed and the berm restored. A professional engineer should be consulted for proper berm/spillway restoration.
Emergency Overflow/ Spillway	Tree Growth	Tree growth on emergency spillways creates blockage problems and may cause failure of the berm due to uncontrolled overtopping.	Trees on emergency spillways removed.  If root system is small (base less than 4 inches) the root system may be left in place. Otherwise the roots should be removed and the berm restored. A professional engineer should be consulted for proper berm/spillway restoration.
Emergency Overflow/ Spillway	Rock Missing	Only one layer of rock exists above native soil in area five square feet or larger, or any exposure of native soil at the top of outflow path of spillway.	Rocks and pad depth restored to design standards. (Riprap on inside slopes need not be replaced.)
Emergency Overflow/ Spillway	Erosion	Erosion damage over 2 inches deep where cause of damage is still present or where there is potential for continued erosion.  Any erosion observed on a compacted berm embankment.	Slopes stabilized using appropriate erosion control measure(s); e.g., rock reinforcement, planting of grass, compaction.  If erosion is occurring on compacted berms a professional engineer should be consulted to resolve source of erosion.
Presettling Ponds and Vaults	Facility or sump filled with Sediment and/or Debris	6 inches or designed sediment trap depth of sediment.	No sediment present in presettling pond or vault. Sediment is removed.
Drain Rock	Water Ponding	If water enters the facility from the surface, inspect to see if water is ponding at the surface during storm events.  If buried drain rock, observe drawdown through observation port or cleanout.	No water ponding on surface during storm events.  Clear piping through facility when ponding occurs. Replace rock material/sand reservoirs as necessary. Tilling of subgrade below reservoir may be necessary (for trenches) prior to backfill.

If you are unsure whether a problem exists, contact a professional engineer.

## **#5 – Maintenance Checklist for Catch Basins:**

Drainage System Feature	Defect or Problem	Condition When Maintenance Is Needed	Results Expected When Maintenance Is Performed
General	"Dump no pollutants" (or similar) stencil or stamp not visible	Stencil or stamp should be visible and easily read.	Warning signs (e.g., "Dump No Waste- Drains to Stream" or "Only rain down the drain"/ "Puget Sound starts here") painted or embossed on or adjacent to all storm drain inlets.
General	Trash and Debris	Trash or debris which is located immediately in front of the catch basin opening or is blocking inlet capacity by more than 10 percent.	No trash or debris located immediately in front of catch basin or on grate opening.
General	Trash and Debris	Trash or debris (in the basin) that exceeds 60 percent of the sump depth as measured from the bottom of basin to invert of the lowest pipe into or out of the basin, but in no case less than a minimum of 6 inches clearance from the debris surface to the invert of the lowest pipe.	No trash or debris in the catch basin.
General	Trash and Debris	Trash or debris in any inlet or outlet pipe blocking more than one-third of its height.	Inlet and outlet pipes free of trash or debris.
General	Trash and Debris	Dead animals or vegetation that could generate odors that could cause complaints or dangerous gases (e.g., methane).	No dead animals or vegetation present within the catch basin.
General	Sediment	Sediment (in the basin) that exceeds 60 percent of the sump depth as measured from the bottom of basin to invert of the lowest pipe into or out of the basin, but in no case less than a minimum of 6 inches clearance from the sediment surface to the invert of the lowest pipe.	No sediment in the catch basin.
General	Structure Damage to Frame and/or Top Slab	Top slab has holes larger than 2 square inches or cracks wider than one-fourth inch.	No holes and cracks in the top slab allowing material to run into the basin.
General	Structure Damage to Frame and/or Top Slab	Frame not sitting flush on top slab, i.e., separation of more than three-fourth inch of the frame from the top slab. Frame not securely attached.	Frame is sitting flush on the riser rings or top slab and firmly attached.
General	Fractures or Cracks in Basin Walls/ Bottom	Maintenance person judges that structure is unsound.	Basin replaced or repaired to design standards.
General	Fractures or Cracks in Basin Walls/ Bottom	Grout fillet has separated or cracked wider than one-half-inch and longer than 1 foot at the joint of any inlet/outlet pipe or any evidence of soil particles entering catch basin through cracks.	Pipe is regrouted and secure at basin wall.
General	Settlement/ Misalignment	If failure of basin has created a safety, function, or design problem.	Basin replaced or repaired to design standards.
General	Vegetation	Vegetation growing across and blocking more than 10 percent of the basin opening.	No vegetation blocking opening to basin.

## **#5 – Maintenance Checklist for Catch Basins:**

Drainage System Feature	Defect or Problem	Condition When Maintenance Is Needed	Results Expected When Maintenance Is Performed
General	Vegetation	Vegetation growing in inlet/outlet pipe joints that is more than 6 inches tall and less than 6 inches apart.	No vegetation or root growth present.
General	Contamination and Pollution	Any evidence of oil, gasoline, contaminants or other pollutants.	No contaminants or pollutants present. (Coordinate removal/cleanup with Pierce County Surface Water Management 253-798-2725 and/or Dept. of Ecology Spill Response 800-424-8802.)
Catch Basin Cover	Cover Not in Place	Cover is missing or only partially in place. Any open catch basin requires maintenance.	Catch basin cover is in place and secured.
Catch Basin Cover	Locking Mechanism Not Working	Mechanism cannot be opened by one maintenance person with proper tools. Bolts into frame have less than one-half-inch of thread.	Mechanism opens with proper tools.
Catch Basin Cover	Cover Difficult to Remove	One maintenance person cannot remove lid after applying normal lifting pressure. (Intent is keep cover from sealing off access to maintenance.)	Cover can be removed by one maintenance person.
Ladder	Ladder Rungs Unsafe	Ladder is unsafe due to missing rungs, not securely attached to basin wall, misalignment, rust, cracks, or sharp edges.	Ladder meets design standards and allows maintenance person safe access.
Grates	Grate Opening Unsafe	Grate with opening wider than seveneighths of an inch.	Grate opening meets design standards.
Grates	Trash and Debris	Trash and debris that is blocking more than 20 percent of grate surface inletting capacity.	Grate free of trash and debris.
Grates	Damaged or Missing	Grate missing or broken member(s) of the grate.	Grate is in place and meets design standards.

If you are unsure whether a problem exists, contact a professional engineer.

## #22 – Maintenance Checklist for Conveyance Systems (Pipes and Ditches):

Drainage System Feature	Defect or Problem	Condition When Maintenance Is Needed	Results Expected When Maintenance Is Performed
Pipes	Sediment & Debris	Accumulated sediment that exceeds 20 percent of the diameter of the pipe.	Pipe cleaned of all sediment and debris.
Pipes	Vegetation	Vegetation that reduces free movement of water though pipes.	Vegetation does not impede free movement of water through pipes.  Prohibit use of sand and sealant application and protect from construction runoff.
Pipes	Damaged (Rusted, Bent or Crushed)	Protective coating is damaged: rust is causing more than 50 percent deterioration to any part of pipe.	Pipe repaired or replaced.
Pipes	Damaged (Rusted, Bent or Crushed)	Any dent that significantly impedes flow (i.e. decreases the cross section area of pipe by more than 20 percent).	Pipe repaired or replaced.
Pipes	Damaged (Rusted, Bent or Crushed)	Pipe has major cracks or tears allowing groundwater leakage.	Pipe repaired or replaced.
Open Ditches	Trash & Debris	Dumping of yard wastes such as grass clippings and branches. Unsightly accumulation of non-degradable materials such as glass, plastic, metal, foam, and coated paper.	No trash or debris present. Trash and debris removed and disposed of as prescribed by the County.
Open Ditches	Sediment Buildup	Accumulated sediment that exceeds 20 percent of the design depth.	Ditch cleaned of all sediment and debris so that it matches design.
Open Ditches	Vegetation	Vegetation (e.g. weedy shrubs or saplings) that reduces free movements of water through ditches.	Water flows freely though ditches. Grassy vegetation should be left alone.
Open Ditches	Erosion Damage to Slopes	Erosion damage over 2 inches deep where cause of damage is still present or where there is potential for continued erosion.	No erosion damage present. Slopes stabilized using appropriate erosion control measure(s); e.g., rock reinforcement, planting of grass, compaction.
Open Ditches	Erosion Damage to Slopes	Any erosion observed on a compacted berm embankment.	If erosion is occurring on compacted berms a professional engineer should be consulted to resolve source of erosion.
Open Ditches	Rock Lining Out of Place or Missing (If Applicable)	Native soil is exposed beneath the rock lining.	Rocks replaced to design standards.

If you are unsure whether a problem exists, contact a professional engineer.

## #32 - Maintenance Checklist for Permeable Pavement:

Drainage System Feature	Defect or Problem	Condition When Maintenance Is Needed	Results Expected When Maintenance Is Performed
Facility – General Requirements	Unstable Adjacent Area	Runoff from adjacent pervious areas deposits soil, mulch, or sediment on pavement.	No deposited soil or other materials on permeable pavement or other adjacent surfacing. All exposed soils that may erode to pavement surface mulched and/or planted.
Facility – General Requirements	Wearing Course Covered by Adjacent Vegetation	Vegetation growing beyond facility edge onto sidewalks, paths, and street edge.	Vegetation does not impede function of adjacent facilities or pose as safety hazard. Groundcovers and shrubs trimmed to avoid overreaching the sidewalks, paths and street edge.
Porous asphalt or pervious cement concrete	NA	None. Maintenance to prevent clogging with fine sediment.	Conventional street sweepers equipped with vacuums, water, and brushes or pressure washer used to restore permeability. Vacuum or pressure wash the pavement two to three times annually.
Porous asphalt or pervious cement concrete	NA	None. Maintenance to prevent clogging with fine sediment.	Use of sand and sealant application prohibited. Protect from construction runoff.
Porous asphalt or pervious cement concrete	Cracks	Major cracks or trip hazards.	Potholes or small cracks filled with patching mixes. Large cracks and settlement addressed by cutting and replacing the pavement section.
Porous asphalt or pervious cement concrete	NA	Utility cuts.	Any damage or change due to utility cuts replaced in kind.
All Pavement Types	Leaf and Debris Accumulation	Fallen leaves or debris.	Removed/disposed.
Interlocking concrete paver blocks	Missing or Damaged Paver Block	Interlocking paver block missing or damaged.	Individual damaged paver blocks removed and replaced or repaired per manufacturer's recommendations.
Interlocking concrete paver blocks	Settlement	Settlement of surface. When deviation from original grade impedes function.	Original grade re-established. May require resetting.
All pavement types	All Pavement Types	Sediment or debris accumulation between paver blocks, on surface of pavement, or in grid voids.	Sediment at surface does not inhibit infiltration. Remove/dispose of sediment.
Interlocking concrete paver blocks	Void material is missing or low	Loss of aggregate material between paver blocks.	Refill per manufacturer's recommendations.
Open-celled paving grid with gravel	Loss of Aggregate Material in Paving Grid	Loss of aggregate material in grid.	Aggregate gravel level maintained at the same level as the plastic rings or no more than 0.25 inch above the top of rings. Refill per manufacturer's recommendations.

## **#32 – Maintenance Checklist for Permeable Pavement:**

Drainage System Feature	Defect or Problem	Condition When Maintenance Is Needed	Results Expected When Maintenance Is Performed
Open-celled paving grid with grass	Lack of Grass Coverage	Loss of soil and/or grass material in grid.	Refill and/or replant per manufacturer's recommendations. Growing medium restored, facility aerated and reseeded or planted, and vegetated area amended as needed.
Inlet/outlet pipe	Pipe is Damaged	Pipe is damaged.	Pipe is repaired/replaced.
Inlet/outlet pipe	Pipe is Clogged	Pipe is clogged.	Roots or debris is removed.
Inlet/outlet pipe	Erosion	Native soil exposed or other signs of erosion damage present.	No eroded or scoured areas Cause of erosion or scour is addressed.
Underdrain pipe	Blocked Underdrain	Plant roots, sediment or debris reducing capacity of underdrain (may cause prolonged drawdown period).	Underdrains and orifice free of sediment and debris. Jet clean or rotary cut debris/roots from underdrain(s). If underdrains are equipped with a flow restrictor (e.g., orifice) to attenuate flows, the orifice must be cleaned regularly.
Spill Prevention and Response	NA	Storage or use of potential contaminants in the vicinity of facility.	Spill prevention measures exercised whenever handling or storing potential contaminants.
Spill Prevention and Response	Release of Pollutants	Any evidence of contaminants such as oil, gasoline, concrete slurries, paint, etc.	Spills are cleaned up as soon as possible to prevent contamination of stormwater. No contaminants or pollutants present. (Coordinate source control, removal, and/or cleanup with Pierce County Surface Water Management 253-798-2725 and/or Dept. of Ecology Spill Response 800-424-8802.)

If you are unsure whether a problem exists, contact a professional engineer.

#### **Log Sheet**

Use copies of this log sheet to keep track of when maintenance checks occur and what items, if any, are repaired or altered. The completed sheets will serve as a record of past maintenance activities and will provide valuable information on how your facilities are operating. This information will be useful for future requirements regarding the types of facilities that are installed. It helps to keep all log sheets in a designated area so that others can easily access them.

Date Checked:// Checked By: Name:			
Position:			
Address:	City:	_ State:	_ Zip:
Phone Number: ()			

Part of Facility Checked	Observations (List things that should be done)	Follow-up Actions Taken	Date Action Taken