### GENERAL

- ALL MATERIALS AND WORK SHALL CONFORM TO THE REQUIREMENTS OF THE WASHINGTON STATE BUILDING CODE REF. 2021 INTERNATIONAL BUILDING CODE (IBC).
- CONSTRUCTION METHODS AND PROJECT SAFETY: DRAWINGS AND SPECIFICATIONS REPRESENT THE FINISHED STRUCTURE AND DO NOT INDICATE METHODS, PROCEDURES, OR SEQUENCE OF CONSTRUCTION. TAKE NECESSARY PRECAUTIONS TO MAINTAIN AND ENSURE THE INTEGRITY OF THE STRUCTURE DURING CONSTRUCTION. THE EOR WILL NOT ENFORCE SAFETY MEASURES OR REGULATIONS. THE CONTRACTOR SHALL DESIGN, CONSTRUCT, AND MAINTAIN ALL SAFETY DEVICES AND SHALL BE SOLELY RESPONSIBLE FOR CONFORMING TO ALL LOCAL, STATE, AND FEDERAL SAFETY AND
- HEALTH STANDARDS, LAWS, AND REGULATIONS. VERIFY ALL DIMENSIONS, ELEVATIONS AND SITE CONDITIONS PRIOR TO THE START OF CONSTRUCTION AND NOTIFY THE ENGINEER IMMEDIATELY OF ANY DISCREPANCIES OR INCONSISTENCIES THAT ARE FOUND. NOTED DIMENSIONS TAKE PRECEDENCE OVER SCALED
- DIMENSIONS. DO NOT SCALE DRAWINGS. ALL OMISSIONS AND/OR CONFLICTS BETWEEN THE VARIOUS ELEMENTS OF THE WORKING DRAWINGS AND SPECIFICATIONS SHALL BE BROUGHT TO THE ATTENTION OF THE ENGINEER AND FIELD INSPECTOR. THE ENGINEER SHALL PROVIDE A SOLUTION PRIOR TO PROCEEDING WITH ANY WORK AFFECTED BY THE CONFLICT OR
- OMISSION. WHERE NO CONSTRUCTION DETAILS ARE SHOWN OR NOTED FOR ANY PART OF THE WORK, USE THOSE FOR OTHER SIMILAR WORK. WHEN A DETAIL IS IDENTIFIED AS TYPICAL, APPLY IN ESTIMATING AND CONSTRUCTION TO EVERY LIKE CONDITION WHETHER OR NOT THE
- REFERENCE IS REPEATED IN EVERY INSTANCE. CHANGES TO THE DRAWINGS: OBTAIN PRIOR WRITTEN APPROVAL. WORK PERFORMED IN CONFLICT WITH THE DRAWINGS OR APPLICABLE BUILDING CODE REQUIREMENTS SHALL BE CORRECTED AT THE EXPENSE OF THE CONTRACTOR.

### DESIGN CRITERIA

- STRUCTURE IS DESIGNED IN ACCORDANCE WITH ASCE 7-16: MINIMUM DESIGN LOADS FOR BUILDINGS AND OTHER STRUCTURES. WIND LOAD:
- BASIC WIND SPEED,  $V_{ULT} = 100$  MPH MAXIMUM RISK CATEGORY: II EXPOSURE: C SNOW LOAD: IMPORTANCE FACTOR,  $I_5 = 1.0$ SURFACE ROUGHNESS: C EXPOSURE: C
- 20 PSF MAXIMUM. GROUND ROOF --- PSF . ROOF LIVE LOAD: PSF

- STEEL SHAPES SHALL CONFORM TO THE FOLLOWING (U.N.O.): ASTM A500, GR C Fy=46 KSI MIN. RND. HSS SQ./RECT. HSS ASTM A500. GR C Fy=50 KSI MIN. THREADED ROD ASTM A36 Fy=36 KSI MIN. STEEL PLATE ASTM A36 Fy=36 KSI MIN. ANGLE & CHANNEL ASTM A36 Fy=36 KSI MIN. ASTM A53, GR B STD. PIPE Fy=35 KSI MIN. STRUCT. PIPE ASTM A252, GR 3  $F_y=45$  KSI MIN.
- WIDE FLANGE ASTM A992 Fy=50 KSI MIN. MACHINE BOLTS SPECIFIED AS "A307" SHALL CONFORM TO ASTM A307 w/ NUTS PER ASTM A563A \$ WASHERS PER ASTM F844 (U.N.O.). THREADED PARTS, NUTS, AND WASHERS SHALL BE HDG OR
- ZP AS DEFINED HEREIN. STRUCTURAL BOLTS SHALL CONFORM TO ASTM F3 | 25 GRADES A325 OR A490 AS SPECIFIED ("A325" OR "A490") w/ NUTS PER ASTM A563DH & WASHERS PER ASTM F436. A. WHERE DESIGNATED AS "-X", CARE MUST BE TAKEN TO ENSURE THREADS ARE EXCLUDED FROM THE SHEAR PLANE(S). B. WHERE DESIGNATED AS "-N" OR IF NO DESIGNATION IS NOTED,
- THREADS MAY BE INCLUDED IN THE SHEAR PLANE(S). C. WHERE SPECIFIED, "A325" MAY BE HDG OR ZP AS DEFINED
- D. GRADE "A490" SHALL NOT BE HDG OR ZP AS DEFINED HEREIN. ANCHORS CAST IN CONCRETE SHALL CONFORM TO ASTM F1554 GR. 36 (U.N.O.) w/ NUTS TO ASTM A563 AND WASHERS TO ASTM F436. PARTS SHALL BE HOT-DIP GALVANIZED (HDG) OR ZINC (MECHANICAL) PLATED (ZP). PARTS EMBEDDED ENTIRELY IN
- CONCRETE MAY BE PLAIN STEEL. WHERE SPECIFIED FOR STEEL THREADED PARTS, NUTS, AND WASHERS, HOT-DIP GALVANIZING (HDG) SHALL CONFORM TO ASTM F2329 AND ZINC (MECHANICAL) PLATING (ZP) TO CLASS 55 PER ASTM B695.
- PLAIN STEEL FASTENERS ARE NOT TO BE USED UNLESS SPECIFIED. ZINC ELECTRO-PLATED FASTENERS PER ASTM F 1941 MAY BE SUBSTITUTED FOR INTERIOR APPLICATIONS, BUT ARE OTHERWISE NOT TO BE USED UNLESS SPECIFIED.
- NUTS AND WASHERS SHALL HAVE THE SAME COATING AS THE CORRESPONDING THREADED PART. WHERE SPECIFIED, IRON AND STEEL HARDWARE SHALL BE HOT-DIP GALVANIZED PER ASTM A 153.
- D. STAINLESS STEEL (SS) BOLTS, STUDS, AND THREADED ROD SHALL CONFORM TO ASTM F593 AND BE ALLOY 304 OR 316 W/ NUTS TO ASTM F594. NUTS AND WASHERS SHALL MATCH THE ALLOY OF THE THREADED PART.
- . WELDING: A. WELD STRUCTURAL STEEL IN COMPLIANCE WITH ANSI/AWS DI.I AND AISC SPECIFICATION, CHAPTER J. WELDERS SHALL BE CERTIFIED AS REQUIRED BY THE LOCAL BUILDING AUTHORITY. WELDING SHALL BE DONE BY ELECTRIC ARC PROCESS USING LOW-HYDROGEN ELECTRODES WITH SPECIFIED TENSILE STRENGTH NOT LESS THAN 70 KSI UNLESS NOTED OTHERWISE.
- B. UNLESS A LARGER WELD SIZE IS INDICATED, PROVIDE MINIMUM SIZE WELD PER AISC SPECIFICATION, SECTION J2, TABLE J2.4.

## ALUMINUM

- FABRICATE AND ERECT ALUMINUM IN COMPLIANCE WITH THE 2020 ALUMINUM DESIGN MANUAL (ADM I), THE SPECIFICATIONS FOR ALUMINUM SHEET METAL WORK (ASM35), AND CHAPTER 20 OF THE BUILDING CODE.
- ALUMINUM SHAPES SHALL CONFORM TO THE FOLLOWING: 6061-T6 ASTM B429 Fy=35 KSI MIN. STRUCT. PROFILES 6061-T6 ASTM B308 Fy=35 KSI MIN. SHEET # PLATE 6061-T6 ASTM B209 Fy=35 KSI MIN.

- STAPLE TUBE 6063-T5 ASTM B221 Fy=16 KSI MIN. ALL SHOP AND FIELD WELDS SHALL BE PERFORMED BY AN AISC QUALITY CERTIFIED FABRICATOR.
- UNLESS A LARGER WELD SIZE IS INDICATED, PROVIDE MINIMUM SIZE
- WELD PER ADM 1. FILLER SHALL BE 5556 ALLOY REGARDLESS OF MEMBER THICKNESS. NO OTHER FILLER ALLOY SHALL BE USED UNLESS NOTED OTHERWISE.

### CONCRETE & REINFORCEMENT

- MINIMUM 28-DAY COMPRESSIVE STRENGTH (fc) SHALL BE 2,500 PSI.
- REINFORCEMENT TO BE ASTM AG 15 GR 60, Fy=60 KSI UNO. CALCIUM CHLORIDE OR ADDED CHLORIDE IS NOT PERMITTED.
- 4. ALL REINFORCED CONCRETE SHALL BE CONSOLIDATED WITH MECHANICAL VIBRATORS.
- MINIMUM CONCRETE COVER: CAST AGAINST & EXPOSED TO EARTH EXPOSED TO EARTH OR WEATHER
- CHAIRS AND SPACERS: AS REQUIRED TO MAINTAIN COVER. GROUT SHALL BE NON-SHRINK AND NON-METALLIC WITH A MINIMUM COMPRESSIVE STRENGTH OF 5,000 PSI AT (1) DAY. MIX AND PLACE IN ACCORDANCE WITH MANUFACTURER INSTRUCTIONS.

### FOUNDATIONS

DESIGN BEARING PRESSURES ARE PER IBC CLASS 5 PRESUMPTIVE ' VALUES (NO SPECIAL INSPECTION REQUIRED): LATERAL BEARING: 100 PSF/FT

### 1,500 PSF VERTICAL BEARING:

### EXISTING CONDITIONS

- ENGINEER WILL NOT BE PERFORMING ON-SITE INSPECTIONS OR VERIFICATIONS. IT IS THE RESPONSIBILITY OF THE INSTALLER AND OWNER(S) TO IDENTIFY EXISTING CONDITIONS AND CONTACT
- ENGINEER WITH ANY DISCREPANCIES OR CONCERNS. EXISTING INFORMATION HAS BEEN FURNISHED BY THE ENTITY WHOM THIS DOCUMENT WAS PREPARED FOR. ENGINEER IN NO WAY CERTIFIES THIS INFORMATION AS "AS-BUILT".
- FEATURES OF WORK ANNOTATED AS "VERIFY" (OR SIMILAR) MUST BE INSPECTED, VERIFIED AS SUCH, AND DOCUMENTED PRIOR TO FABRICATION AND INSTALLATION.
- IF THERE IS ANY REASON TO BELIEVE THE EXISTING CONDITIONS DETAILED HEREIN ARE NOT ACCURATE, CONTRACTOR SHALL CEASE WORK AND NOTIFY ENGINEER IMMEDIATELY.
- CONTRACTOR SHALL INSPECT AND CONFIRM THE QUALITY OF EXISTING STRUCTURE AS "IN GOOD REPAIR". STRUCTURE SHALL BE FREE OF CORROSION, DECAY, AND ANY OTHER MATERIAL, FABRICATION, ASSEMBLY, OR INSTALLATION DEFECT. IF THERE ARE ANY INDICATIONS THAT THIS IS NOT THE CASE, CONTRACTOR SHALL CEASE WORK IMMEDIATELY AND NOTIFY ENGINEER.

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www.reverenceengineering.com (619) 354-1152 501 W BROADWAY, STE 425 SAN DIEGO. CA 92101

PREPARED FOR:

PERSONA SIGNS

PROJECT #:

2509136

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No: Issue/Revision:	Date:
Initial Submittal	9-24-2025
Updated Soil Class \$ Pier Depth	11-10-2025
2	
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4	



		10-Nov-25
T TITLE	:	
	STRUCTURAL	

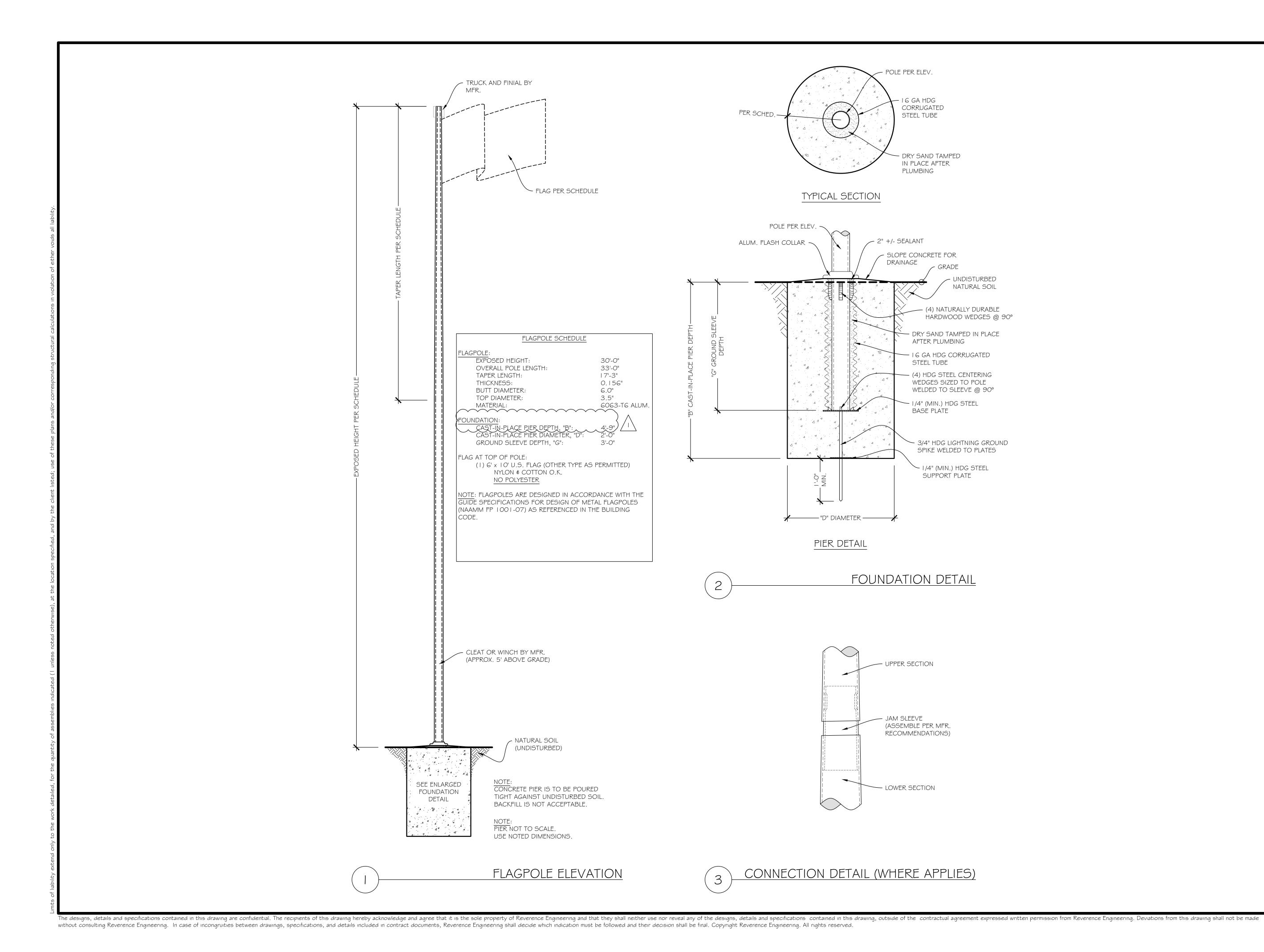
ORIGINAL SHEET SIZE: 24x36

EVALUATION REPORT SCHEDULE

ANCHORS, FASTENERS, AND OTHER PRODUCTS SHALL CONFORM TO AND BE INSTALLED PER THEIR RESPECTIVE EVALUATION REPORT(S) AS FOLLOWS (NOT ALL APPLICABLE THIS PROJECT):

ı	, , , , , , , , , , , , , , , , , , ,	
	ANCHOR TYPE	REPORT #
ı	HILTI KB-TZ2 (CS \$ SS) ANCHORS IN CONCRETE	ICC-ESR-4266
ı	HILTI KB-TZ2 (CS \$ SS) ANCHORS IN MASONRY	ICC-ESR-4561
ı	HILTI KH-EZ (CS \$ SS) ANCHORS IN CONCRETE	ICC-ESR-3027
ı	HILTI KH-EZ (CS \$ SS) ANCHORS IN MASONRY	ICC-ESR-3056
ı	HILTI HIT-HY 200 ADHESIVE IN CONCRETE	ICC-ESR-3187
ı	HILTI HIT-HY 200 ADHESIVE IN MASONRY	ICC-ESR-3963
ı	SIMPSON TITEN HD (CS) ANCHORS IN CONCRETE	ICC-ESR-2713
ı	SIMPSON TITEN HD (CS & SS) ANCHORS IN MASONRY	ICC-ESR-1056
ı	SIMPSON TITEN HD (SS) ANCHORS IN CONCRETE	UES-ER-493
ı	TAPCON ANCHORS IN MASONRY	ICC-ESR-1671
ı	TAPCON ANCHORS IN CONCRETE	ICC-ESR-2202
ı	TAPCON+ SCREW ANCHORS IN CONCRETE	ICC-ESR-3699
	ITW BUILDEX TEKS SDS	ICC-ESR-1976
	i e	

ABBR	EVIATIONS		
ABV. ADD'L. AFF ALT. ALUM.	ABOVE ADDITIONAL ABOVE FINISHED FLOOR ALTERNATE ALUMINUM	HDG HOR. O.C. LOC.	GENERAL CONTRACTOR HOT DIP GALVANIZED HORIZONTAL ON CENTER LOCATION MAXIMUM MINIMUM NEW NOT TO EXCEED OVER OUTSIDE DIAMETER OPTIONAL PENETRATION REINFORCEMENT
 FAB. FDN. FRM'G. FTG.	DETAIL EXISTING EXISTING EACH EACH WAY ELEVATION . EMBEDMENT ENGINEER OF RECORD FABRICATOR/FABRICATION FOUNDATION FRAMING FOOTING FIELD VERIFY	U.N.O.	UNLESS NOTED OTHERWISE





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PREPARED FOR:

PERSONA SIGNS

PROJECT #:

2509136

1CDONALDS 43903

No: I	ssue/Revision:	Date:
	nitial Submittal	9-24-2025
L	Jpdated Soil Class \$ Pier Depth	11-10-2025
2		
3		
4		



10-Nov-25

SHEET TITLE:

STRUCTURAL

5.2

ORIGINAL SHEET SIZE: 24x36



STRUCTURAL CALCULATIONS

for

McDonalds 43903 Flagpole

2902 E Pioneer
Puyallup, WA 98372
Prepared for:
Persona Signs

Package Type:

# **Revised Package**

### **DESIGN SPECIFICATIONS**

- 1 Washington State Building Code, ref. 2021 IBC
- 2 ASCE 7-16: Minimum Design Loads for Buildings and Other Structures
- 3 ACI 318-14: Building Code Requirements for Structural Concrete
- 4 ANSI/AISC 360-16: Specification for Structural Steel Buildings 5 Aluminum Design Manual (ADM-1) 2015

Project #:

2509136

DESIGN CRITERA

V<sub>ult</sub> = 100 mph

Exposure: C ::Ground Snow Load::

g = 20 psf

::Solis:: Per

::Wind::

Per Building Code Presumptive Class 5
Allowable Lateral Bearing:

Allowable Vertical Bearing: 1500 psf

# Date Signed: 10/11/2025

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PREPARED FOR:

PERSONA SIGNS

PROJECT #:

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CDONALDS 43903 FLAGPOLE

 No:
 Issue/Revision:
 Date:

 ---- Initial Submittal
 9-24-2025

 Updated Soil Class \$ Pier Depth
 11-10-2025

 2
 3



10-Nov-25

SHEET TITLE:

STRUCTURAL

5.3

1 of 2

2509136

# McDonalds 43903 Flagpole

2902 E Pioneer, Puyallup, WA 98372

# REVERENCE ENGINEERING

h = 30 $T = 17.25$ $S = 12.7$	ft 5 ft 75 ft	Exposed Tapered Straight F	Height	ght	$d_b = d_t = t = 0$		in in in	Butt dian Top dian Pole thic	neter			V = G = m =	1.14			ind Speed ect factor ope
POLE WIND LO	OADS															
Sect. z (ft)		d (in)	A (ft <sup>2</sup> )	$C_h$		V x d	$C_d$	Р	$W_p$	M (k-ft)						
1 12.7	75 6.375	6	6.375	0.86		50	0.7979	20.025	101.85	0.6493						
2 15	13.875	5.837	1.0944			48.641	0.827									
3 18	16.5	5.4565	1.3641	0.8661		45.471	0.9027	22.816	28.095	0.4636						
4 21	19.5	5.0217				41.848	1.0056	26.327		0.6481						
5 24	22.5	-	1.1467			38.225	1.1	29.68								
6 27	25.5	4.1522	1.038	0.9492		34.601	1.1	30.472	34.794	0.8873						
7 30	28.5	3.7174	0.9293	0.9717		30.978	1.1	31.194	31.889	0.9088						
8													Base	Bending	Moment:	4.66 k-ft
9														Bas	se Shear:	286.09 lb
10																
11																
12																
13																
14																
Type: Nylon $b = 6$	ft L	Flag heig			b =	Polyeste 0	r ft	Flag heig			+	+	Base	•	Moment:	
b = 6 w = 10	ft ft 60 ft <sup>2</sup>	Flag heig Flag widt Flag area	th		• •	0	r ft ft ft <sup>2</sup>	Flag heig Flag widt Flag area	th		+	+	Base	•	Moment: se Shear:	
$b = 6$ $w = 10$ $A_F = 6$ $C_h = 0.982$	ft ft 60 ft <sup>2</sup> 23 -	Flag widt	th a	ıht	b = w = A <sub>F</sub> = C <sub>h</sub> =	0 0 0 0.86	ft ft ft <sup>2</sup> -	Flag wid	th a	ght		+		Bas		86.737 lb 0 k-ft
$b = 6$ $w = 10$ $A_F = 6$	ft ft 60 ft <sup>2</sup> 23 -	Flag widt	th a nt of heig	ıht	b = w = A <sub>F</sub> =	0 0 0 0.86	ft ft ft <sup>2</sup> -	Flag wid	th a ent of heig Flag				Base	Bas Bending Bas	se Shear:  Moment: se Shear:	86.737 lb 0 k-ft 0 lb
$b = 6$ $w = 10$ $A_F = 6$ $C_h = 0.982$	ft ft 60 ft <sup>2</sup> 23 -	Flag widt Flag area Coefficie	th a nt of heig	ht	b = w = A <sub>F</sub> = C <sub>h</sub> =	0 0 0 0.86	ft ft ft <sup>2</sup> -	Flag widt Flag area Coefficie	th a ent of heig				Base	Bending Base Bending	Moment: Se Shear: Moment: Moment:	86.737 lb 0 k-ft 0 lb 7.00 k-ft
$b = 6$ $w = 10$ $A_F = 6$ $C_h = 0.982$	ft ft 60 ft <sup>2</sup> 23 -	Flag widt Flag area Coefficie	th a nt of heig	ht	b = w = A <sub>F</sub> = C <sub>h</sub> =	0 0 0 0.86	ft ft ft <sup>2</sup> -	Flag widt Flag area Coefficie	th a ent of heig Flag				Base	Bending Base Bending	se Shear:  Moment: se Shear:	86.737 lb 0 k-ft 0 lb 7.00 k-ft
$b = 6 \\ w = 10 \\ A_F = 6 \\ C_h = 0.982 \\ W_F = 86.73$	ft ft 60 ft <sup>2</sup> 23 - 37 lb	Flag widt Flag area Coefficie	th a nt of heig		b = w = A <sub>F</sub> = C <sub>h</sub> = W <sub>F</sub> =	0 0 0 0.86 0	ft ft ft <sup>2</sup> - Ib	Flag widt Flag area Coefficie Force on	th a ent of heig Flag				Base	Bending Base Bending	Moment: Se Shear: Moment: Moment:	86.737 lb 0 k-ft 0 lb 7.00 k-ft
$b = \frac{6}{4}$ $w = \frac{10}{10}$ $A_{F} = \frac{6}{4}$ $C_{h} = 0.982$ $W_{F} = 86.73$ POLE CHECK	ft ft 60 ft <sup>2</sup> 23 - 37 lb	Flag widt Flag area Coefficie	th a nt of heig	ht Alloy:	$b = W = A_F = C_h = W_F = 6063$	0 0 0 0.86 0	ft ft ft <sup>2</sup> -	Flag widt Flag area Coefficie Force on	th a ent of heig Flag TOTAL			+	Base	Bending Base Bending	Moment: Se Shear: Moment: Moment:	86.737 lb 0 k-ft 0 lb 7.00 k-ft
$b = \begin{array}{c} 6 \\ w = 10 \\ A_F = 6 \\ C_h = 0.982 \\ W_F = 86.73 \\ \end{array}$	ft ft 60 ft <sup>2</sup> 23 - 37 lb	Flag widt Flag area Coefficie	th a nt of heig Flag	Alloy:	$b = W = A_F = C_h = W_F = 6063$	0 0 0 0.86 0	ft ft <sup>2</sup> - lb Temper:	Flag widt Flag area Coefficie Force on T6	th a ent of heig Flag TOTAL		+	+	Base	Bending Base Bending	Moment: Se Shear: Moment: Moment:	86.737 lb 0 k-ft
$b = \frac{6}{4}$ $w = \frac{10}{10}$ $A_{F} = \frac{6}{4}$ $C_{h} = 0.982$ $W_{F} = 86.73$ POLE CHECK	ft ft 60 ft <sup>2</sup> 23 - 37 lb	Flag widt Flag area Coefficie Force on	th a nt of heig Flag	Alloy:	$b = W = A_F = C_h = W_F = 6063$	0 0 0 0.86 0	ft ft ft <sup>2</sup> - Ib Temper:	Flag widt Flag area Coefficie Force on T6	th a ent of heig Flag TOTAL	LOADS  Rupture	k <sub>t</sub> =	+	Base	Bending Bas Bending Bas	Moment: Se Shear: Moment: Moment:	86.737 lb 0 k-ft 0 lb 7.00 k-ft
$b = 6 \\ w = 10 \\ A_F = 6 \\ C_h = 0.982 \\ W_F = 86.73$ $POLE CHECK \\ M_u = 7.0$	ft ft 50 ft <sup>2</sup> 23 - 37 lb AT BASE 00 k-ft	Flag widt Flag area Coefficie Force on	th a nt of heig Flag F <sub>tu</sub> =	Alloy: 30	$b = W = A_F = C_h = W_F = 6063$	0 0 0.86 0	ft ft ft² - lb  Temper: $F_{ty} =$ Yielding	Flag widt Flag area Coefficie Force on T6	th a ent of heig Flag TOTAL I	Rupture 0.75	k <sub>t</sub> =	+ 	Base	Bending Bas Bending Bas	Moment: Se Shear: Moment: Moment:	86.737 lb 0 k-ft 0 lb 7.00 k-ft
$b = 6 \\ w = 10 \\ A_{F} = 6 \\ C_{h} = 0.982 \\ W_{F} = 86.73 \\ $ $POLE CHECK \\ M_{u} = 7.0 \\ d_{b} = 6$	ft ft 50 ft <sup>2</sup> 23 - 37 lb AT BASE 00 k-ft	Flag widt Flag area Coefficie Force on	th a nt of heig Flag F <sub>tu</sub> = 5.4461	Alloy: 30	b = w = A <sub>F</sub> = C <sub>h</sub> = W <sub>F</sub> =	0 0 0.86 0	ft ft ft² - lb  Temper: $F_{ty} =$ Yielding 0.9	Flag widt Flag area Coefficie Force on T6	th a ant of heig r Flag <b>TOTAL</b> I	Rupture 0.75	k <sub>t</sub> =	+ = 1 φM <sub>n</sub> =	Base Base	Bending Bas Bending Bas	Moment: Se Shear: Moment: Moment:	86.737 lb 0 k-ft 0 lb 7.00 k-ft
$b = 6 \\ w = 10 \\ A_{F} = 6 \\ C_{h} = 0.982 \\ W_{F} = 86.73 \\ $ $POLE CHECK \\ M_{u} = 7.0 \\ d_{b} = 6$	ft ft 50 ft <sup>2</sup> 23 - 37 lb AT BASE 00 k-ft in 3 in	Flag widt Flag area Coefficie Force on Z = S =	th a nt of heig Flag F <sub>tu</sub> = 5.4461	Alloy: 30	b = w = A <sub>F</sub> = C <sub>h</sub> = W <sub>F</sub> =	0 0 0.86 0	ft ft ft² - lb  Temper: $F_{ty} =$ Yielding 0.9	Flag widt Flag area Coefficie Force on T6	th a ant of heig r Flag <b>TOTAL</b> I	Rupture 0.75	k <sub>t</sub> =	+ = 1 φM <sub>n</sub> =	Base Base	Bending Bas Bending Bas	Moment: Se Shear: Moment: Moment:	86.737 lb 0 k-ft 0 lb 7.00 k-ft
$b = 6 \\ w = 10 \\ A_{F} = 6 \\ C_{h} = 0.982 \\ W_{F} = 86.73$ $Del{eq:bolder} M_{u} = 7.0 \\ d_{b} = 6 \\ t = 0.156$	ft ft 50 ft <sup>2</sup> 23 - 37 lb AT BASE 00 k-ft in 3 in	Flag widt Flag area Coefficie Force on Z = S =	th a nt of heig Flag F <sub>tu</sub> = 5.4461	Alloy: 30	b = w = A <sub>F</sub> = C <sub>h</sub> = W <sub>F</sub> =	0 0 0.86 0	ft ft ft² - lb  Temper: $F_{ty} =$ Yielding 0.9	Flag widt Flag area Coefficie Force on T6	th a ant of heig r Flag <b>TOTAL</b> I	Rupture 0.75	k <sub>t</sub> =	+ = 1 φM <sub>n</sub> =	Base Base	Bending Bas Bending Bas	se Shear:  Moment: se Shear: Moment: se Shear:	86.737 lb  0 k-ft 0 lb  7.00 k-ft 0.3728 kip
$b = 6 \\ w = 10 \\ A_{F} = 6 \\ C_{h} = 0.982 \\ W_{F} = 86.73$ $Del{eq:bolder} M_{u} = 7.0 \\ d_{b} = 6 \\ t = 0.156$	ft ft 50 ft <sup>2</sup> 23 - 37 lb AT BASE 00 k-ft in 3 in	Flag widt Flag area Coefficie Force on Z = S =	th a nt of heig Flag Flag 5.4461 4.0845	Alloy: 30 in <sup>3</sup>	b = w = A <sub>F</sub> = C <sub>h</sub> = W <sub>F</sub> =	0 0 0.86 0	ft ft ft² - lb  Temper: $F_{ty} =$ Yielding 0.9	Flag widt Flag area Coefficie Force on T6	th a ant of heig r Flag <b>TOTAL</b> I	Rupture 0.75	k <sub>t</sub> =	+ = 1 φM <sub>n</sub> =	Base Base	Bending Bas Bending Bas	Moment: Se Shear: Moment: Moment:	86.737 lb 0 k-ft 0 lb 7.00 k-ft 0.3728 kip
$b = \begin{array}{c} b = 6 \\ w = 10 \\ A_F = 6 \\ C_h = 0.982 \\ W_F = 86.73 \\ \hline \\ POLE CHECK \\ M_u = 7.0 \\ d_b = 6 \\ t = 0.156 \\ \hline \\ CAST-IN-PLACE \\ \hline \\ CAST-IN-PLACE \\ \hline \\ \\ CAST-IN-PLACE \\ \hline \\ \\ CAST-IN-PLACE \\ \hline \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ $	ft ft 50 ft² 23 - 37 lb  AT BASE 00 k-ft  in 3 in	Flag widt Flag area Coefficie Force on Z = S =	th a nt of heig Flag Flu = 5.4461 4.0845	Alloy: 30 in <sup>3</sup>	b = w = A <sub>F</sub> = C <sub>h</sub> = W <sub>F</sub> =	0 0 0.86 0 Φ <sub>b</sub> = M <sub>np</sub> =	ft ft ft² - lb  Temper: F <sub>ty</sub> = Yielding 0.9 11.346	Flag width Flag area Coefficien Force on T6  T6  25 - k-ft Shear a	th a ent of heig Flag TOTAL I ksi φ <sub>b</sub> = M <sub>nu</sub> =	Rupture 0.75 - 13.615	k <sub>t</sub> =	+ φM <sub>n</sub> = D/C:	Base Base 10.211 0.6857	Bending Bas Bending Bas	se Shear:  Moment: se Shear: Moment: se Shear:	86.737 lb  0 k-ft 0 lb  7.00 k-ft 0.3728 kip
$b = \begin{array}{c} b = 6 \\ w = 10 \\ A_F = 6 \\ C_h = 0.982 \\ W_F = 86.73 \\ \hline \\ POLE CHECK \\ M_u = 7.0 \\ d_b = 6 \\ t = 0.156 \\ \hline \\ CAST-IN-PLAC \\ \\ b = 2 \\ M_u = 7.00 \\ \hline \\ \end{array}$	ft ft 50 ft² 23 - 37 lb  AT BASE 00 k-ft  in 3 in	Flag widt Flag area Coefficie Force on Z = S = ESIGN	th a nt of heig Flag Flu = 5.4461 4.0845 diameter* at grade	Alloy: 30 in <sup>3</sup>	b = w = A <sub>F</sub> = C <sub>h</sub> = W <sub>F</sub> =	0 0 0.86 0 Φ <sub>b</sub> = M <sub>np</sub> =	ft ft ft ft² - lb  Temper: F <sub>ty</sub> = Yielding 0.9 11.346	Flag width Flag area Coefficien Force on T6  T6  25 - k-ft Shear a	th a ent of heig Flag TOTAL I ksi φ <sub>b</sub> = M <sub>nu</sub> =	Rupture 0.75 - 13.615	- k-ft	+ - 1 φM <sub>n</sub> = D/C:	Base Base 10.211 0.6857	Bending Bas Bending Bas  Bending Bas  Control	Moment: se Shear: Moment: se Shear: oil Class:	86.737 lb  0 k-ft 0 lb  7.00 k-ft 0.3728 kip
$b = \begin{array}{c} 6 \\ w = 10 \\ A_F = 6 \\ C_h = 0.982 \\ W_F = 86.73 \\ \hline \\ POLE CHECK \\ M_u = 7.0 \\ d_b = 6 \\ t = 0.156 \\ \hline \\ CAST-IN-PLAC \\ \\ D = 2 \\ M_u = 7.00 \\ M_s = 4.201 \\ \hline \\ M_s = 4.201 \\ \hline \\ D = 10 \\ $	ft ft 50 ft² 23 - 37 lb  AT BASE 00 k-ft  in 3 in  EE PIER DI ft k-ft	Flag widt Flag area Coefficie Force on  Z = S =  ESIGN  Footing of Moment a	th a nt of heig Flag Flu = 5.4461 4.0845 diameter* at grade M (0.6*M	Alloy: 30 in i	b = w = A <sub>F</sub> = C <sub>h</sub> = W <sub>F</sub> = 6063	0 0 0.86 0 0 φ <sub>b</sub> = M <sub>np</sub> =	ft ft ft ft² - lb  Temper: F <sub>ty</sub> = Yielding 0.9 11.346	Flag width Flag area Coefficien Force on T6  T6  25 - k-ft Shear a	th a ent of heig Flag TOTAL I ksi φ <sub>b</sub> = M <sub>nu</sub> =	Rupture 0.75 - 13.615	k <sub>t</sub> = - k-ft	+ - - ΦM <sub>n</sub> = D/C:	Base Base 10.211 0.6857	Bending Bas Bending Bas  Bending Bas  Control	Moment: se Shear: Moment: se Shear: Moment: se Shear:	86.737 lb  0 k-ft 0 lb  7.00 k-ft 0.3728 kip
$b = \begin{array}{c} 6 \\ w = 10 \\ A_F = 6 \\ C_h = 0.982 \\ W_F = 86.73 \\ \hline \\ POLE CHECK \\ M_u = 7.0 \\ d_b = 6 \\ t = 0.156 \\ \hline \\ CAST-IN-PLAC \\ \\ D = 2 \\ M_u = 7.00 \\ M_s = 4.201 \\ s = 10 \\ \hline \\ S = 10 \\ \hline \\ \\ S = 10 \\ \hline \\ \\ \\ S = 10 \\ \hline \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ $	ft ft 50 ft² 23 - 37 lb  AT BASE 00 k-ft  in 3 in  EE PIER DI  k-ft   k-ft   2 k-ft	Flag widt Flag area Coefficie Force on  Z = S =  ESIGN  Footing of Moment at Service M	th a nt of height of heigh	Alloy: 30 in of the second of	$b = W = A_F = C_h = W_F = 6063$ $V_u = V_s = ble 1806$	0 0 0.86 0 0 φ <sub>b</sub> = M <sub>np</sub> =	ft ft ft ft² - lb  Temper: F <sub>ty</sub> = Yielding 0.9 11.346	Flag width Flag area Coefficien Force on T6  T6  25 - k-ft Shear a	th a ent of heig Flag TOTAL I ksi φ <sub>b</sub> = M <sub>nu</sub> =	Rupture 0.75 - 13.615	k <sub>t</sub> = - k-ft	+ - - ΦM <sub>n</sub> = D/C:	Base Base 10.211 0.6857	Bending Bas Bending Bas  Bending Bas  Control	Moment: se Shear: Moment: se Shear: Moment: se Shear:	86.737 lb  0 k-ft 0 lb  7.00 k-ft 0.3728 kip
$b = \begin{array}{c} 6 \\ w = 10 \\ A_F = 6 \\ C_h = 0.982 \\ W_F = 86.73 \\ \hline \\ POLE CHECK \\ M_u = 7.0 \\ d_b = 6 \\ t = 0.156 \\ \hline \\ CAST-IN-PLAC \\ \\ D = 2 \\ M_u = 7.00 \\ M_s = 4.201 \\ S = 10 \\ S' = 26 \\ \hline \\ CAST = 10 \\ S' = 26 \\ S' = 26 \\ \hline \\ CAST = 10 \\ S' = 26 \\ $	ft ft 50 ft² 23 - 37 lb  AT BASE 00 k-ft  in 3 in  EE PIER DI  k-ft   k-ft   00 psf/ft	Flag widt Flag area Coefficie Force on  Z = S =  ESIGN  Footing of Moment at Service M Lateral B Increased	th a nt of height of heigh	Alloy: 30 in of the second of	$b = W = A_F = C_h = W_F = 6063$ $V_u = V_s = ble 1806$	0 0 0.86 0 0 φ <sub>b</sub> = M <sub>np</sub> =	ft ft ft ft² - lb  Temper: F <sub>ty</sub> = Yielding 0.9 11.346	Flag widt Flag area Coefficie Force on T6 25 - k-ft Shear a Service	th a ent of heig Flag TOTAL I ksi φ <sub>b</sub> = M <sub>nu</sub> =	Rupture 0.75 - 13.615	k <sub>t</sub> = - k-ft	+ - - ΦM <sub>n</sub> = D/C:	Base Base 10.211 0.6857	Bending Bas Bending Bas  Bending Bas  Control	Moment: se Shear: Moment: se Shear: Moment: se Shear:	86.737 lb  0 k-ft 0 lb  7.00 k-ft 0.3728 kip
$b = \begin{array}{c} 6 \\ w = \begin{array}{c} 10 \\ \text{A}_{F} = \begin{array}{c} 6 \\ \text{C}_{h} = \begin{array}{c} 0.982 \\ \text{W}_{F} = \begin{array}{c} 86.73 \\ \text{A}_{S} = \begin{array}{c} 6 \\ \text{CAST-IN-PLAC} \\ \text{CAST-IN-PLAC} \\ \text{A}_{S} = \begin{array}{c} 4.201 \\ \text{S}_{S} = \begin{array}{c} 26 \\ \text{CAST-IN-PLAC} \\ CAST-IN-PL$	ft ft 50 ft² 23 - 37 lb  AT BASE 00 k-ft  in 3 in  EE PIER DI  k-ft   k-ft   00 psf/ft   57 psf/ft	Flag widt Flag area Coefficie Force on  Z = S =  ESIGN  Footing of Moment at Service M Lateral B Increased IBC 1807	th a nt of height of heigh	Alloy: 30 in of the second of	b = w = A <sub>F</sub> = C <sub>h</sub> = W <sub>F</sub> = 6063 ksi V <sub>u</sub> = V <sub>s</sub> = ble 1806 1806.3	0 0 0.86 0 0 φ <sub>b</sub> = M <sub>np</sub> =	ft ft ft ft² - lb  Temper: F <sub>ty</sub> = Yielding 0.9 11.346	Flag widt Flag area Coefficie Force on  T6  25  - k-ft  Shear a Service	th a ant of height Flag TOTAL I  ksi  φ <sub>b</sub> =  M <sub>nu</sub> =  at grade V (0.6*\	Rupture 0.75 - 13.615	k <sub>t</sub> = - k-ft EPTH:	+ φM <sub>n</sub> = D/C: = 1.3 = 290.8	Base Base 10.211 0.6857	Bending Bas Bending Bas Bending Bas  Reft OK Sc Per IB Latera	Moment: se Shear: Moment: se Shear: Moment: se Shear:	86.737 lb  0 k-ft 0 lb  7.00 k-ft 0.3728 kip

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PERSONA SIGNS

PROJECT #:

2509136

ACDONALDS 43903 FLAGPOLE

No: Issue/Revision:	Date:
Initial Submittal	9-24-2025
Updated Soil Class \$ Pier Depth	11-10-2025
2	
3	
4	



SHEET TITLE:

ORIGINAL SHEET SIZE: 24x36

STRUCTURAL

5.4