GEOENGINEERS

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October 31, 2022

Washington State Department of Enterprise Services Division of Engineering & Architectural Services 206 General Administration Building Olympia, Washington 98504-1012

Attention: Dennis Flynn

Subject: Supplemental Groundwater Information Addendum #1 Pierce College Puyallup – Northwest Parking Lot Additions Puyallup, Washington File No. 21342-003-00

INTRODUCTION

This addendum presents additional groundwater monitoring information collected for the Pierce College Puyallup – Parking Lot Additions project in Puyallup, Washington, and is intended to supplement our Geotechnical Engineering Services Report for the same project, dated January 31, 2022 (Geotechnical Report). Our services have been provided in general accordance with our Additional Service Agreement #1 for this project dated December 22, 2021 and our Signed Agreement No. 2020-546 C dated March 16, 2022. Reference to this study should include review and full inclusion of our January 31, 2022 Geotechnical Report. This addendum and our report should be provided and reviewed together for all our geotechnical information, conclusions, and recommendations presented by us on this project.

The City of Puyallup (City) requested, and in general accordance with the Washington State Department of Ecology's 2014 Stormwater Management Manual for Western Washington (SWMMWW), that groundwater monitoring data be collected during the wet season (defined by City as December 21 through April 1) in the vicinity of the former proposed detention pond to be located near the future northwest parking lot. We facilitated drilling and installation of a groundwater monitoring well (MW-1) at the site on January 3, 2022. MW-1 was placed in the vicinity of the former proposed stormwater detention system. The location of the well is shown on the Site Plan, Figure 1. We understand that due to site constraints and other factors, the northwest stormwater facility design was changed to an underground detention pipe system. The underground system will be located beneath the western portion of the proposed northwest parking lot. The bottom of the facility is planned to be between about Elevation 506.5 and 507 feet. As part of the system change, the parking lot layout was elongated toward the west to northwest.

In the following sections, we discuss the subsurface conditions encountered during drilling, present the groundwater monitoring data collected, and provide additional conclusions and recommendations for design of the northwest stormwater facility.



SUBSURFACE CONDITIONS

During drilling for MW-1, we advanced through about 12 inches of forest duff and/or organic-rich soil at the surface. Underlying the forest duff, we encountered what we interpret to be glacial till. The upper approximate 4½ feet was weathered and generally consisted of medium dense silty sand. Beneath the weathered zone, soil generally consisted of dense to very dense silty sand with gravel, very dense gravel with silt and sand, and very stiff to hard silt with varying sand content. A more detailed description of our interpretation of geologic and subsurface conditions at the project site and additional exploration logs are provided in our Geotechnical Report. Our exploration and laboratory testing program and summary exploration log for this study is included in Appendix A.

We encountered groundwater at about 21 feet below ground surface (bgs) during drilling. After constructing the monitoring well, we measured groundwater at about 9³/₄ feet bgs. Based on subsurface soil conditions (soil lithology and soil moisture conditions), followed by the subsequent rise in groundwater level (approximate 11-foot rise after well construction), it is our opinion that artesian groundwater conditions are present in the vicinity of MW-1. It should be noted that our other geotechnical studies in the project vicinity on campus have documented near surface perched groundwater seepage, but it was not interpreted to be a regional groundwater table at the depths noted or an artesian condition.

GROUNDWATER MONITORING

We installed a pressure transducer data logger within MW-1 to record groundwater levels at regular time intervals. The data logger was programmed to collect a groundwater reading once a day at 12:00 between January 4 and May 18, 2022. Groundwater data collected was compiled and correlated to an elevation versus date presented in the Groundwater Hydrograph, Figure 2.

The maximum and average groundwater elevations are presented in Table 1 below.

TABLE 1. GROUNDWATER ELEVATION SUMMARY

Date and Time of Maximum Elevation	Approx. Maximum Elevation (feet, NAVD88 ¹)	Approx. Average Elevation (feet, NAVD88 ¹)
1/17/22 12:00	506.0	504.5

Notes:

¹ The North American Vertical Datum 1988.

CONCLUSIONS AND RECOMMENDATION

Design Considerations

- We recommend that Elevation 506 feet be considered the limiting elevation for the bottom of the stormwater system for storage considerations.
- Buoyancy effects should be considered as a part of the detention system design. As such, we suggest that an initial and assumed groundwater elevation of 508 feet (NAVD88) be considered as a target groundwater elevation for buoyancy calculation checks. This is somewhat conservative. If



it is found that buoyancy effects at this groundwater elevation is a concern, we should be contacted and provided an opportunity to review and assist with the design.

- Total soil unit weight (above groundwater) may be considered to be 125 pounds per cubic foot (pcf).
- Effective soil unit weight (below groundwater) may be considered to be 62.6 pcf.
- Follow detention pipe system manufacturer recommendations for mitigating buoyancy effects.

Construction Considerations

Based on proposed design elevations, expect to encounter water below about Elevation 506 feet during excavation and construction. This will occur from either near surface seepage and/or artesian conditions, as described above. Artesian conditions may temporarily cause the base of the excavation to "float" and/or become unstable and/or disturbed. We expect that artesian conditions should subside shortly after excavation and just be wet. If the excavation takes place in mid- to late-summer, we expect the upward artesian seepage to be less prominent and the basal soils could potentially be dryer and less difficult to manage.

Subgrade stabilization below the bottom of the stormwater system may be necessary during construction. As such, we recommend budgeting and planning for at least 12 inches of subgrade over-excavation and replacement with quarry spalls (Washington State Department of Transportation [WSDOT] Standard Specification 9-13.1(5)), aside from any design base materials already in the project plans and specifications. Ultimately, base and subgrade conditions will have to be observed during excavation to determine if this, or other means of stabilization, are necessary.

LIMITATIONS

We have prepared this letter for the exclusive use of the Washington State Department of Enterprise Services (DES) and their authorized agents for the Pierce College Puyallup – Parking Lot Additions project located in Puyallup, Washington.

Within the limitations of scope, schedule and budget, our services have been executed in accordance with generally accepted practices for geotechnical engineering in this area at the time this letter was prepared. The conclusions, recommendations, and opinions presented in this letter are based on our professional knowledge, judgment, and experience. No warranty, express or implied, applies to the services or this letter.

Except for described and modified herein, the conclusions and recommendations and limitations presented in our January 31, 2022 Geotechnical Report remain unchanged and still apply to this project. Please refer to Appendix A titled "Report Limitations and Guidelines for Use" in our Geotechnical Report for additional information pertaining to use of this letter.



We trust that this letter meets your needs. If you have any questions regarding this letter, please contact us.

Sincerely, GeoEngineers, Inc.



Dennis (D.J.) Thompson, PE

Associate Geotechnical Engineer

Christopher R. Newton, PE Geotechnical Engineer

CRN:DJT:leh

Attachments: Figure 1. Site Plan Figure 2. Groundwater Hydrograph Appendix A. Subsurface Explorations and Laboratory Testing Figure A-1 – Key to Exploration Logs Figure A-2 – Log of Monitoring Well Figures A-3 and A-4 – Sieve Analysis Results

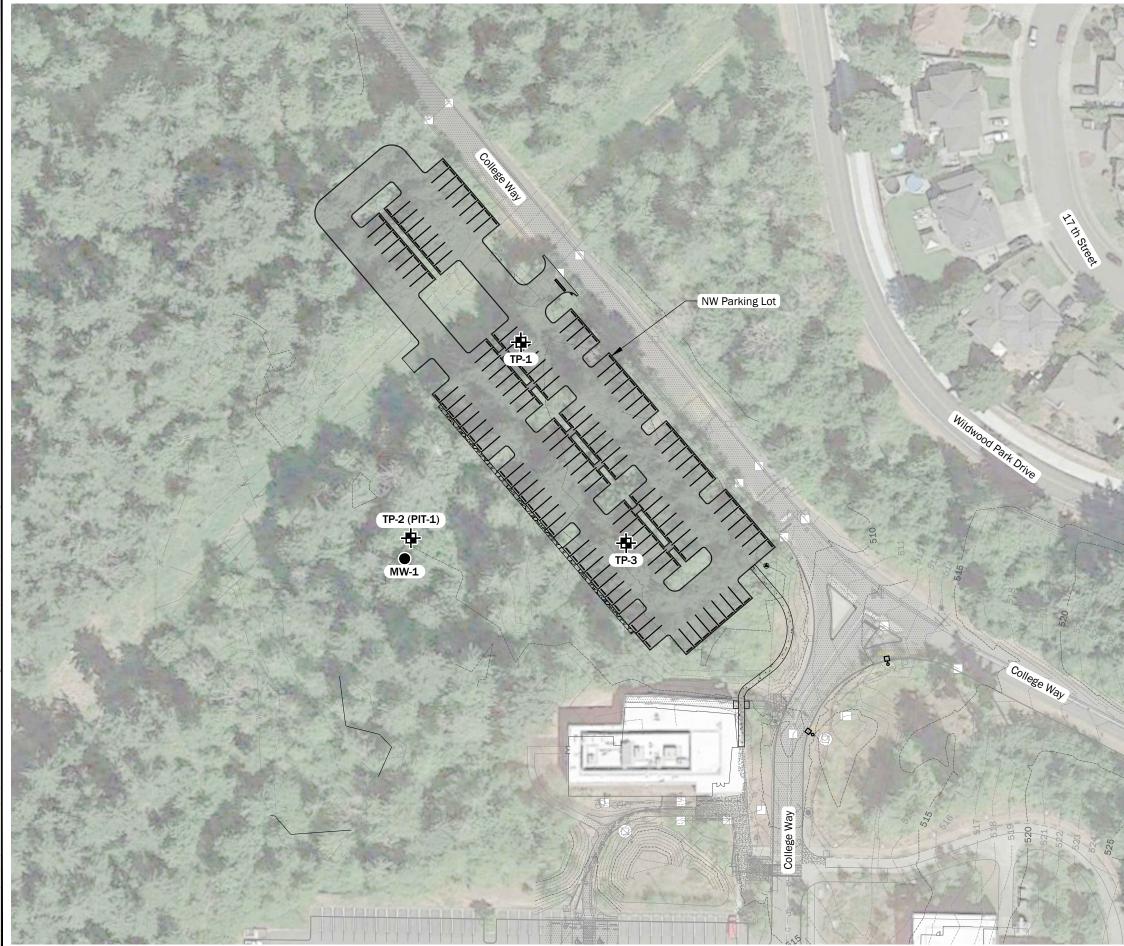
1 copy submitted electronically

Disclaimer: Any electronic form, facsimile or hard copy of the original document (email, text, table, and/or figure), if provided, and any attachments are only a copy of the original document. The original document is stored by GeoEngineers, Inc. and will serve as the official document of record.









Legend

MW-1 Monitoring Well by GeoEngineers, Inc., 2022

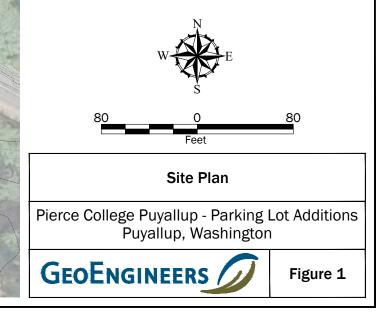
TP-1 🖶 Test Pit by GeoEngineers, Inc., 2021

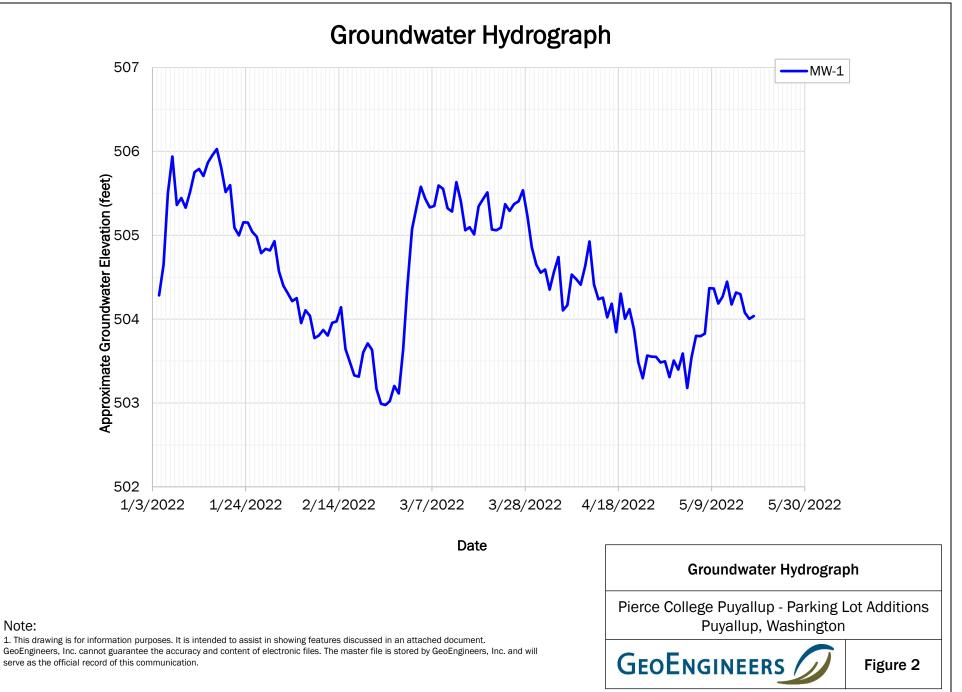
Notes:

- The locations of all features shown are approximate.
 This drawing is for information purposes. It is intended to assist in showing features discussed in an attached document. GeoEngineers, Inc. cannot guarantee the accuracy and content of electronic files. The master file is stored by GeoEngineers, Inc. and will serve as the official record of this communication.

Data Source: Background from AHBL, Inc., received on 10/06/2022. Aerial from Google Earth Pro dated 08/14/2020.

Projection: Washington State Plane, South Zone, NAD83, US Foot





APPENDIX A Subsurface Explorations and Laboratory Testing

APPENDIX A SUBSURFACE EXPLORATIONS AND LABORATORY TESTING

Subsurface Explorations

Subsurface conditions were explored by advancing one hollow-stem auger boring on January 3, 2022. Subsurface exploratory services were provided by Holocene Drilling, Inc. under subcontract to GeoEngineers, Inc. The boring was advanced to a nominal depth of about 25¹/₄ feet below surrounding site grade. A groundwater monitoring well was installed with a pressure transducer at this boring.

The boring was located in the field using an electronic tablet equipped with a global positioning system (GPS) software application. The exploration coordinates were approximated using publicly available aerial imagery and coordinate software. The exploration location is included on the Site Plan, Figure 1. The location and elevation of the exploration should be considered approximate.

Our field representative collected samples, classified the soils, maintained a detailed log of the exploration, and observed groundwater conditions. The samples were obtained with a standard split spoon sampler in general accordance with ASTM International (ASTM) D 1586. Field blow counts are presented on the logs. The soils were classified visually in general accordance with the system described in Figure A-1, which includes a key to the exploration logs. A summary log of the exploration is included as Figure A-2.

Laboratory Testing

Soil samples obtained from the boring were transported to GeoEngineers laboratory. Representative soil samples were selected for laboratory tests to evaluate the pertinent geotechnical engineering characteristics of the site soils and to confirm our field classification.

Our testing program consisted of the following:

- Five Particle-size distribution analyses (sieve analyses (SA))
- One Moisture content determination (MC)

Tests were performed in general accordance with test methods of ASTM or other applicable procedures. The following sections provide a general description of the tests performed.

Sieve Analysis

Particle-size analyses were completed on selected samples in general accordance with ASTM Test Method C 136. This test method determines quantitatively the distribution of particle sizes in soils. Typically, the distribution of particle sizes larger than 75 micrometers (μ m) is determined by sieving. The results of the tests were used to verify field soil classifications and determine pertinent engineering characteristics. Figures A-3 and A-4 present the results of our sieve analyses.

Moisture Content

The moisture content of a selected sample was determined in general accordance with ASTM Test Method D 2216. The test results are used to aid in soil classification and correlation with other pertinent engineering soil properties. The test results are shown on the exploration log at the respective sample depth.



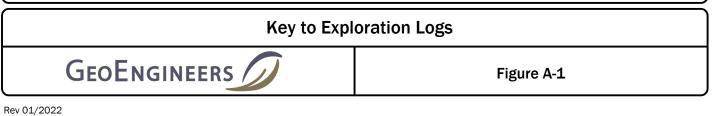
			SYM	BOLS	TYPICAL	
	MAJOR DIVIS	0113	GRAPH	LETTER	DESCRIPTIONS	G
COARSE GRAINED SOILS MORE THAN 50% OF COARSE FRACTION RETAINED ON NO. 4 SIEVE SAND SAND SANDY SOILS	CLEAN GRAVELS		GW	WELL-GRADED GRAVELS, GRAVEL - SAND MIXTURES		
	GRAVELLY	(LITTLE OR NO FINES)		GP	POORLY-GRADED GRAVELS, GRAVEL - SAND MIXTURES	
		GRAVELS WITH FINES		GM	SILTY GRAVELS, GRAVEL - SAND - SILT MIXTURES	
	FRACTION RETAINED	(APPRECIABLE AMOUNT OF FINES)		GC	CLAYEY GRAVELS, GRAVEL - SAND - CLAY MIXTURES	
	CAND	CLEAN SANDS (LITTLE OR NO FINES)		SW	WELL-GRADED SANDS, GRAVELLY SANDS	<u>//</u> ``
	AND			SP	POORLY-GRADED SANDS, GRAVELLY SAND	
	MORE THAN 50% OF COARSE FRACTION PASSING	SANDS WITH FINES		SM	SILTY SANDS, SAND - SILT MIXTURES	
	ON NO. 4 SIEVE	(APPRECIABLE AMOUNT OF FINES)		SC	CLAYEY SANDS, SAND - CLAY MIXTURES	
		LIQUID LIMIT LESS THAN 50		ML	INORGANIC SILTS, ROCK FLOUR, CLAYEY SILTS WITH SLIGHT PLASTICITY	
FINE GRAINED	SILTS AND CLAYS			CL	INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY, GRAVELLY CLAYS, SANDY CLAYS, SILTY CLAYS, LEAN CLAYS	
SOILS				OL	ORGANIC SILTS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY	
IORE THAN 50% PASSING NO. 200 SIEVE		LIQUID LIMIT GREATER THAN 50		МН	INORGANIC SILTS, MICACEOUS OR DIATOMACEOUS SILTY SOILS	/
SILTS AND CLAYS				СН	INORGANIC CLAYS OF HIGH PLASTICITY	
			OH	ORGANIC CLAYS AND SILTS OF MEDIUM TO HIGH PLASTICITY		
HIGHLY ORGANIC SOILS		·····	PT	PEAT, HUMUS, SWAMP SOILS WITH HIGH ORGANIC CONTENTS	%F	
bl Sc "F	2.4- Star She She Pist Dire Dire Con lowcount is re ows required ee exploration "indicates s	ect-Push < or grab tinuous Coring ecorded for dri to advance sa n log for hamn	barrel / D tion Test (tion Samp ampler 12 ner weigh d using th	ames & (SPT) elers as t inches t and dru e weight	Moore (D&M) he number of (or distance noted). op. t of the drill rig.	ALA CPS DDS A CD big MD MO CP PI PP SA X CUU VS NS
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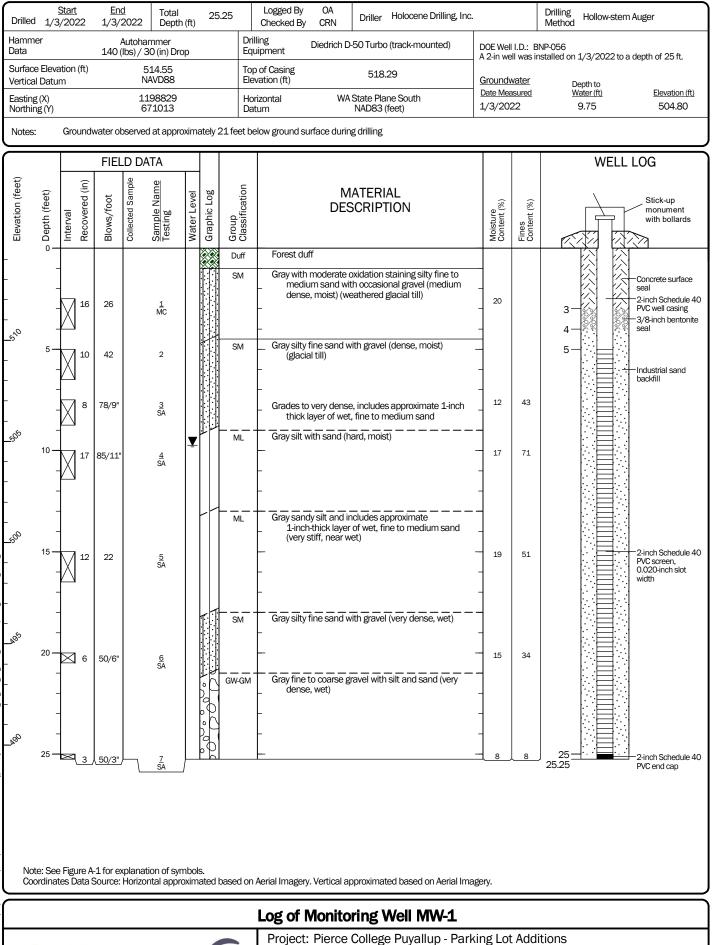
TIONAL MATERIAL SYMBOLS

SYMBOLS		TYPICAL	
GRAPH	LETTER	DESCRIPTIONS	
	AC	Asphalt Concrete	
	сс	Cement Concrete	
	CR	Crushed Rock/ Quarry Spalls	
	SOD	Sod/Forest Duff	
	TS	Topsoil	

SILTY SANDS, SAND - SILT MIXTURES	Groundwater Contact
CLAYEY SANDS, SAND - CLAY MIXTURES	Measured groundwater level in exploration, well, or piezometer
NORGANIC SILTS, ROCK FLOUR, CLAYEY SILTS WITH SLIGHT PLASTICITY	Measured free product in well or piezometer
NORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY, GRAVELLY CLAYS, SANDY CLAYS, SILTY CLAYS, LEAN CLAYS	Graphic Log Contact
DRGANIC SILTS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY	Distinct contact between soil strata
NORGANIC SILTS, MICACEOUS OR DIATOMACEOUS SILTY SOILS	Approximate contact between soil strata
DIATOMACEOUS SILTY SOILS	Material Description Contact
NORGANIC CLAYS OF HIGH PLASTICITY	Contact between geologic units
DRGANIC CLAYS AND SILTS OF MEDIUM TO HIGH PLASTICITY	Contact between soil of the same geologic unit
PEAT, HUMUS, SWAMP SOILS WITH HIGH ORGANIC CONTENTS	Laboratory / Field Tests
assifications	%F Percent fines %G Percent gravel AL Atterberg limits CA Chemical analysis CP Laboratory compaction test
loore (D&M) e number of r distance noted). J.	CS Consolidation test DD Dry density DS Direct shear HA Hydrometer analysis MC Moisture content MD Moisture content and dry density Mohs Mohs hardness scale OC Organic content PM Permeability or hydraulic conductivity PI Plasticity index PL Point lead test PP Pocket penetrometer SA Sieve analysis TX Triaxial compression UC Unconfined compression UU Unconsolidated undrained triaxial compression VS Vane shear
of the drill rig.	Sheen Classification
tht of the	NS No Visible Sheen SS Slight Sheen MS Moderate Sheen HS Heavy Sheen

understanding of subsurface conditions. vere made; they are not warranted to be





Project Location: Puyallup, Washington

Project Number: 21342-003-00

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Figure A-2 Sheet 1 of 1

