

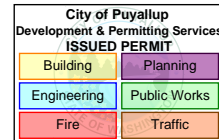
PRCNC20220578

Calculations required to be provided by the Permittee on site for all Inspections

Structural Calculations for

City of Puyallup
Building
REVIEWED
FOR
COMPLIANCE

BSnowden
12/30/2024
7:53:43 AM



SOUTHERN BLEACHER COMPANY

Graham, Texas

Cascade Christian School Grandstands

Puyallup, Washington



Brooks Ransom

ASSOCIATES

7415 N. PALM, STE. 100 | FRESNO, CA 93711
(559) 449-8444 OFFICE | (559) 449-8404 FAX
BROOKSRANSOM.COM

Job No. 22172

2022-04-22

REVISED 2024-01-26



EXPIRES 02/03/2026

DESIGN PARAMETERS:

Puyallup WA

I. GOVERNING CODES:

- 1. IBC 2018 Edition

II. BASIC STRESSES:

1. LT. WT. CONC. (110 PCF).....	F'c =	NA PSI
2. NORM. WT. CONC.....	F'c =	3,000 PSI
3. CMU.....	F'm =	NA PSI
4. REINFORCING STEEL		
a. No. 3 & SMALLER.....	Fy =	40,000 PSI
b. No. 4 & LARGER.....	Fy =	60,000 PSI
5. WF BEAMS.....	Fy =	50,000 PSI
6. STRUCTURAL ANGLES.....	Fy =	50,000 PSI
7. STEEL RODS.....	Fy =	50,000 PSI
8. HSS TUBE STEEL.....	Fy =	46,000 PSI
9. STRUCTURAL BOLTS.....	Gr. =	A307 UNO
10. ANCHOR BOLTS.....	Gr. =	A307 UNO
11. ALUMINUM PLANKING (6063-T6).....	Fy =	25,000 PSI
12. ALUMINUM SHAPES (6061-T6).....	Fy =	35,000 PSI
13. FOUNDATION BEARING CAPACITY.....		0 PSF

III. DESIGN LOAD SUMMARY

1. RISK CATEGORY (ASCE 7-16 TABLE 1.5-1).....	TYPE III
2. GRANDSTAND	
a. DEAD LOADS.....	10 PSF
b. LIVE LOADS.....	100 PSF
c. SEAT BOARDS.....	120 PLF
d. SWAY (PERPENDICULAR).....	10 PLF
e. SWAY (PARALLEL).....	24 PLF
f. GUARDRAIL.....	50 PLF
g. HANDRAIL.....	200 LBS
3. PRESSBOX	
a. ROOF DEAD LOADS.....	15 PSF
b. FLOOR DEAD LOADS.....	10 PSF
c. ROOF LIVE LOADS.....	20 PSF
d. FLOOR LIVE LOADS.....	100 PSF
e. WALL DEAD LOADS.....	10 PSF
4. WIND LOADS	
a. WIND SPEED, V_{ULT}	115 MPH
b. EXPOSURE CATEGORY.....	C
c. WIND FORCE.....	SEE "WIND LOAD PRESSURES"

Search Information

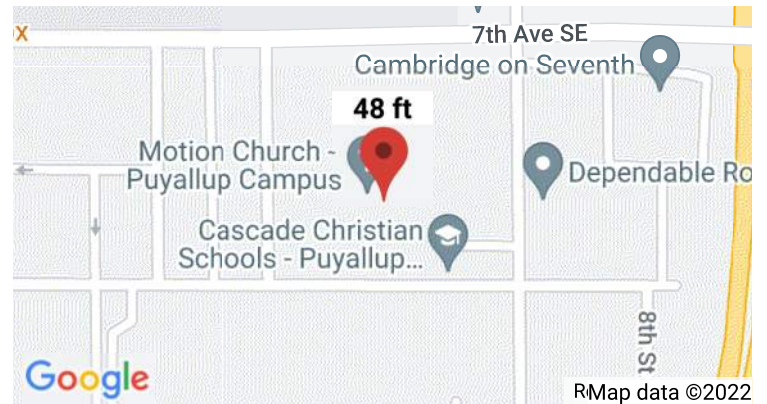
Address: 601 9th Ave SE, Puyallup, WA 98372

Coordinates: 47.1849634, -122.2870963

Elevation: 48 ft

Timestamp: 2022-04-06T16:29:52.624Z

Hazard Type: Snow



ASCE 7-16

Ground Snow Load ----- ⚠️ 18 lb/sqft

The reported ground snow load applies at the query location of 48 feet up to a maximum elevation of 40 feet with a tolerance of 100 feet.

ASCE 7-10

Ground Snow Load --- ⚠️ 15 lb/sqft

The reported ground snow load applies at the query location of 48 feet up to a maximum elevation of 400 feet.

ASCE 7-05

Ground Snow Load ----- ⚠️ 15 lb/sqft

The reported ground snow load applies at the query location of 48 feet up to a maximum elevation of 400 feet.

The results indicated here DO NOT reflect any state or local amendments to the values or any delineation lines made during the building code adoption process. Users should confirm any output obtained from this tool with the local Authority Having Jurisdiction before proceeding with design.

Disclaimer

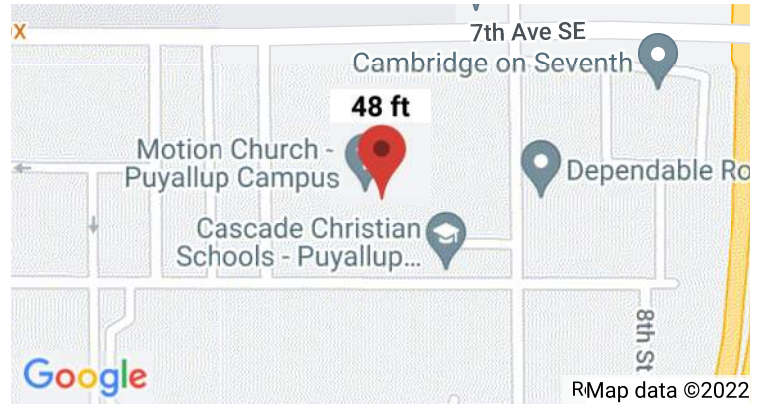
Hazard loads are interpolated from data provided in ASCE 7 and rounded up to the nearest whole integer.

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ATC Hazards by Location

Search Information

Address: 601 9th Ave SE, Puyallup, WA 98372
Coordinates: 47.1849634, -122.2870963
Elevation: 48 ft
Timestamp: 2022-04-06T16:30:33.757Z
Hazard Type: Wind



ASCE 7-16

MRI 10-Year 67 mph
 MRI 25-Year 73 mph
 MRI 50-Year 78 mph
 MRI 100-Year 82 mph
 Risk Category I 92 mph
 Risk Category II 97 mph
 Risk Category III 104 mph
 Risk Category IV 108 mph

ASCE 7-10

MRI 10-Year 72 mph
 MRI 25-Year 79 mph
 MRI 50-Year 85 mph
 MRI 100-Year 91 mph
 Risk Category I 100 mph
 Risk Category II 110 mph
 Risk Category III-IV 115 mph

ASCE 7-05

ASCE 7-05 Wind Speed 85 mph

The results indicated here DO NOT reflect any state or local amendments to the values or any delineation lines made during the building code adoption process. Users should confirm any output obtained from this tool with the local Authority Having Jurisdiction before proceeding with design.

Disclaimer

Hazard loads are interpolated from data provided in ASCE 7 and rounded up to the nearest whole integer. Per ASCE 7, islands and coastal areas outside the last contour should use the last wind speed contour of the coastal area – in some cases, this website will extrapolate past the last wind speed contour and therefore, provide a wind speed that is slightly higher. NOTE: For queries near wind-borne debris region boundaries, the resulting determination is sensitive to rounding which may affect whether or not it is considered to be within a wind-borne debris region.

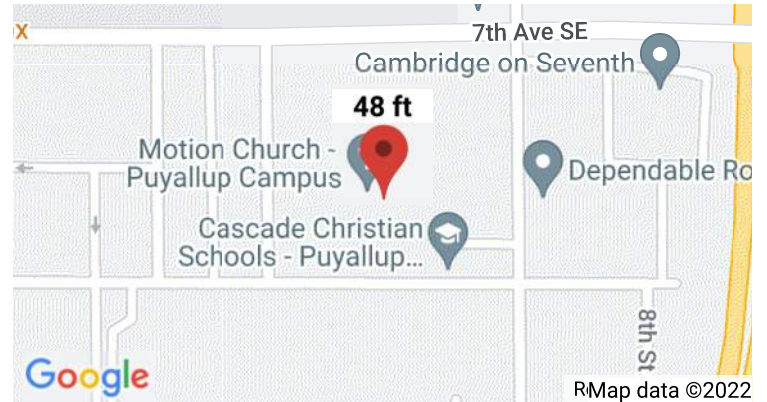
Mountainous terrain, gorges, ocean promontories, and special wind regions shall be examined for unusual wind conditions.

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Search Information

Address:	601 9th Ave SE, Puyallup, WA 98372
Coordinates:	47.1849634, -122.2870963
Elevation:	48 ft
Timestamp:	2022-04-06T16:31:02.635Z
Hazard Type:	Seismic
Reference Document:	ASCE7-16
Risk Category:	III
Site Class:	D-default



Basic Parameters

Name	Value	Description
S_S	1.267	MCE_R ground motion (period=0.2s)
S_1	0.436	MCE_R ground motion (period=1.0s)
S_{MS}	1.521	Site-modified spectral acceleration value
S_{M1}	* null	Site-modified spectral acceleration value
S_{DS}	1.014	Numeric seismic design value at 0.2s SA
S_{D1}	* null	Numeric seismic design value at 1.0s SA

* See Section 11.4.8

Additional Information

Name	Value	Description
SDC	* null	Seismic design category
F_a	1.2	Site amplification factor at 0.2s
F_v	* null	Site amplification factor at 1.0s
CR_S	0.914	Coefficient of risk (0.2s)
CR_1	0.898	Coefficient of risk (1.0s)
PGA	0.5	MCE_G peak ground acceleration
F_{PGA}	1.2	Site amplification factor at PGA
PGA_M	0.6	Site modified peak ground acceleration

T _L	6	Long-period transition period (s)
SsRT	1.267	Probabilistic risk-targeted ground motion (0.2s)
SsUH	1.386	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	1.5	Factored deterministic acceleration value (0.2s)
S1RT	0.436	Probabilistic risk-targeted ground motion (1.0s)
S1UH	0.486	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	0.6	Factored deterministic acceleration value (1.0s)
PGAd	0.5	Factored deterministic acceleration value (PGA)

* See Section 11.4.8

The results indicated here DO NOT reflect any state or local amendments to the values or any delineation lines made during the building code adoption process. Users should confirm any output obtained from this tool with the local Authority Having Jurisdiction before proceeding with design.

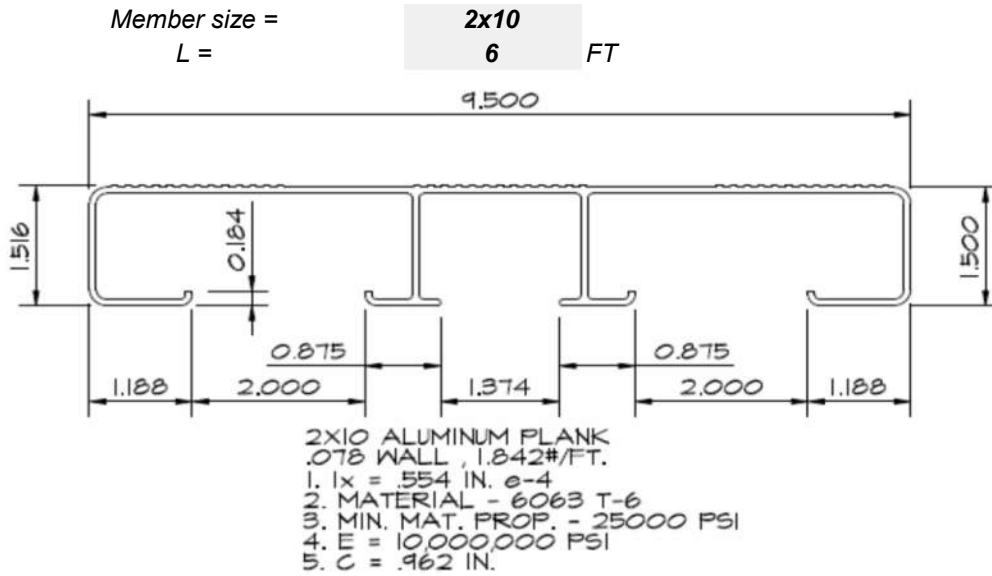
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Hazard loads are provided by the U.S. Geological Survey [Seismic Design Web Services](#).

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CHECK FOOTBOARD (Aluminum Design Manual, 2015)

PLANK PROPERTIES



$S_{x \text{ Top}} =$	1.004	IN^3	$I_x =$	0.554	IN^4
$S_{x \text{ Bottom}} =$	0.578	IN^3	$I_y =$	13.918	IN^4
$S_y =$	2.930	IN^3	$b_1 =$	3.470	IN
$t =$	0.078	IN	$b_2 =$	0.845	IN
Self Weight =	1.842	PLF			

LOADS


Load case is: **4 spans**

$W_{DL} =$	1.84	PLF
Uniform $LL =$	100.00	PSF
$W_{LL} =$	79.17	PLF

MOMENTS

$M_{b+x} =$	283.56	$\# \cdot \text{FT}$
$M_{b-x} =$	351.95	$\# \cdot \text{FT}$

(Maximum moments calculated based on critical skip loading for number of spans indicated above)



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Date:
Job no:

Sheet
Of:

BENDING STRESSES

$f_{b+x top} =$	3.39	KSI (Comp.)
$f_{b+x bot} =$	5.89	KSI (Tens.)
$f_{b-x top} =$	4.21	KSI (Tens.)
$f_{b-x bot} =$	7.31	KSI (Comp.)

ALLOWABLE BENDING STRESS

* BOTH EDGES SUPPORTED

(ADM 2015, Table 2-21, Sec. B5.5.1)

$\lambda_1 =$	34.70
$\lambda_2 =$	93.00

** SUPPORTED ONE EDGE

(ADM 2015, Table 2-21, Sec. B5.4.1)

$\lambda_1 =$	7.30
$\lambda_2 =$	12.60

Top Flange (Compression) *

$\lambda_{top} = b_1 / t =$	44.49	$\lambda_2 > (b/t) > \lambda_1$
$F =$	21.23	KSI (ADM 2015, Table 2-21, Sec. B5.5.1)

Bottom Flange (Compression) **

$\lambda_{bot} = b_2 / t =$	10.83	$\lambda_2 > (b/t) > \lambda_1$
$F =$	13.26	KSI (ADM 2015, Table 2-21, Sec. B5.4.1)

All Flanges (Tension)


$F =$	22.70	KSI (ADM 2015, Table 2-21, Sec. B5.5.1)
-------	--------------	---

STRESS RATIO CHECKS

Stress Ratio (Compression) =	0.55	< 1.00
Stress Ratio (Tension) =	0.30	< 1.00
Max Deflection =	0.31 in.	< L/200

(Section 303.6 ICC 300-2012)

2 x 10 ADEQUATE FOR DESIGN



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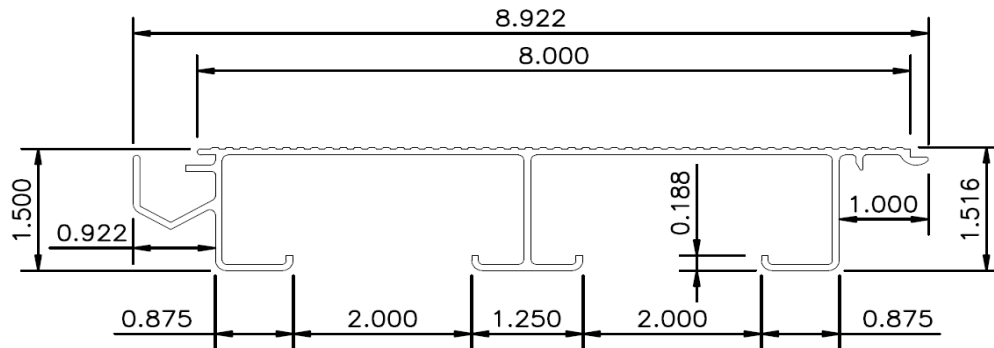
By:
Date:
Job no:

Sheet
Of:

CHECK FOOTBOARD (Aluminum Design Manual, 2015)

PLANK PROPERTIES

Member size = **2x8 INTER**
 L = **6** FT



2X8 ALUMINUM INTERLOCKING DECK PLANK
 .078 WALL, 1.746#/FT.
 1. $I_x = .479 \text{ IN.}^4$
 2. MATERIAL - 6063 T-6
 3. MIN. MAT. PROP. - 25000 PSI
 4. $E = 10,000,000 \text{ PSI}$
 5. $C = .981 \text{ IN.}$

$S_{x \text{ Top}} =$	0.895	IN^3	$I_x =$	0.479	IN^4
$S_{x \text{ Bottom}} =$	0.488	IN^3	$I_y =$	14.117	IN^4
$S_y =$	2.720	IN^3	$b_1 =$	3.259	IN
$t =$	0.078	IN	$b_2 =$	0.625	IN
Self Weight =	1.746	PLF			

LOADS

Load case is: **4 spans**

$W_{DL} =$	1.75	PLF
Uniform $LL =$	100	PSF
$W_{LL} =$	66.67	PLF


MOMENTS

$M_{b+x} =$	239.33	$\# * \text{FT}$
$M_{b-x} =$	297.13	$\# * \text{FT}$

(Maximum moments calculated based on critical skip loading for number of spans indicated above)

BENDING STRESSES

$f_{b+x \text{ top}} =$	3.21	KSI (Comp.)
$f_{b+x \text{ bot}} =$	5.89	KSI (Tens.)
$f_{b-x \text{ top}} =$	3.98	KSI (Tens.)
$f_{b-x \text{ bot}} =$	7.31	KSI (Comp.)



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Date: _____

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Sheet

Of: _____

ALLOWABLE BENDING STRESS

*** BOTH EDGES SUPPORTED**

(ADM 2015, Table 2-21, Sec. B5.5.1)

$\lambda_1 =$ **34.70**

$\lambda_2 =$ **93.00**

**** SUPPORTED ONE EDGE**

(ADM 2015, Table 2-21, Sec. B5.4.1)

$\lambda_1 =$ **7.30**

$\lambda_2 =$ **12.60**

Top Flange (Compression) *

$\lambda_{top} = b_1 / t =$ **41.78** $\lambda_2 > (b/t) > \lambda_1$

$F =$ **21.63** KSI (ADM 2015, Table 2-21, Sec. B5.5.1)

Bottom Flange (Compression) **

$\lambda_{bot} = b_2 / t =$ **8.01** $\lambda_2 > (b/t) > \lambda_1$

$F =$ **14.75** KSI (ADM 2015, Table 2-21, Sec. B5.4.1)

Both Flanges (Tension)

$F =$ **22.70** KSI (ADM 2015, Table 2-21, Sec. B5.5.1)

STRESS RATIO CHECKS


Stress Ratio (Compression) = **0.50** < 1.00 (Comp. Stress in Top Flange Governs)

Stress Ratio (Tension) = **0.30** < 1.00

Max Deflection = **0.305 in.** < L/200

(Section 303.6 ICC 300-2012)

2 x 8 INTER ADEQUATE FOR DESIGN



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Of:

Table 2-21
ALLOWABLE STRESSES F/Ω (k/in²) FOR BUILDING-TYPE STRUCTURES (UNWELDED)

<u>Axial Tension</u>	Section	F/Ω	6063 - T6 B221, B241, B429 0.000 to 1.000 in. thick	
axial tension stress on net effective area	D.2b	15.4		
axial tension stress on gross area	D.2a	15.2		
<u>Shear or torsion</u>				
Shear or torsion rupture	G, H.2	9.2	$F_{ty} =$	25 k/in ²
<u>Bearing</u>				
bolts or rivets on holes	J.3.6a, J.4.6	30.8	$F_{cy} =$	25 k/in ²
bolts on slots, pins on holes, flat surfaces	J.3.6b, J.6.5, J.8	20.5	$F_{tw} =$	30 k/in ²
screws in holes	J.5.5.1	20.0	$E =$	10,100 k/in ²
			$k_t =$	1

	λ	F/Ω for $\lambda \leq \lambda_1$	λ_1	F/Ω for $\lambda_1 < \lambda < \lambda_2$	λ_2	F/Ω for $\lambda \geq \lambda_2$
<u>Axial Compression - member buckling</u>	E.2	kL/r	15.2	18.2	$0.00022 \lambda^2 - 0.133\lambda + 17.5$	78
<u>Flexure - lateral-torsional buckling</u>	F.4	see F.4.2	-	see F.4		78
<u>Elements - Uniform Compression</u>						
flat elements supported on one edge in columns whose buckling axis is not an axis of symmetry	B.5.4.1	b/t	15.2	7.3	$19.0 - 0.530 \lambda$	15
flat elements supported on one edge in all other columns and all beams	B.5.4.1	b/t	15.2	7.3	$19.0 - 0.530 \lambda$	12.6
flat elements supported on both edges	B.5.4.2	b/t	15.2	22.8	$19.0 - 0.170\lambda$	39
flat elements supported on both edges and with an intermediate stiffener	B.5.4.4	λ_s	15.2	18.2	$16.7 - 0.088\lambda$	78
round hollow elements	B.5.4.5	R_p/t	15.2	31.2	$18.5 - 0.593 \lambda^{1/2}$	189
flat elements - direct strength method	B.5.4.6	λ_{eq}	15.2	36.5	$19.0 - 0.106\lambda$	63
<u>Elements - Flexural Compression</u>						
flat elements supported on both edges	B.5.5.1	b/t	22.7	34.7	$27.9 - 0.150\lambda$	93
flat elements supported on tension edge, compression edge free	B.5.5.2	b/t	22.7	6.5	$27.9 - 0.810\lambda$	23
flat elements supported on both edges and with a longitudinal stiffener	B.5.5.3	b/t	22.7	77.8	$27.9 - 0.067\lambda$	208
pipes and round tubes	B.5.5.4	R_p/t	$27.7 - 1.70\lambda^{1/2}$	70.0	$18.5 - 0.593\lambda^{1/2}$	189
flat elements - direct strength method	B.5.5.5	λ_{eq}	M_{np}/S_{xz}	36.5	see B.5.5.5	74
<u>Elements - Shear</u>						
flat elements supported on both edges	G.2	b/t	9.1	38.7	$11.5 - 0.062\lambda$	76
flat elements supported on one edge	G.3	b/t	9.1	16.1	$11.5 - 0.150\lambda$	32
pipes and round or oval tubes	G.4	λ_p^*	9.1	72.2	$15.0 - 0.081\lambda$	76
<u>Torsion - pipes and round or oval tubes</u>	H.2.1	λ_p^*	9.1	38.7	$11.5 - 0.062\lambda$	76

* $\lambda_p = 2.9(R_p/t)^{5/8}(L/R_d)^{1/4}$
† $k_n = (1 + \lambda^{12}/35)^{-2}$



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By: _____

Date: _____

Job no: _____

Sheet

6

Of: _____

FOOTBOARD ANGLE

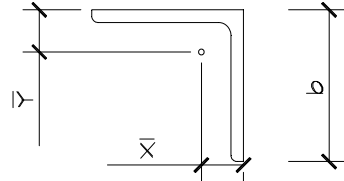
MEMBER SIZE

L2 x 2 x 3/16

$S_N =$	0.188	IN ³
$F_y =$	50000	PSI
$b =$	2	IN
(thickness) $t =$	0.1875	IN
$I_y =$	0.271	IN ⁴
$I_x =$	0.271	IN ⁴
$x =$	0.561	IN
$y =$	0.561	IN
(Unbraced Length) $l =$	30	IN
$C_b =$	1	
$E =$	29000000	PSI
$L =$	30	IN

- | |
|---|
| <p>01. Equal Angle No Restraint Bending Single Axis</p> <p>02. Equal Angle Restraint @ Max Moment Bending Single Axis</p> <p>03. Equal Angle Bending Principle Axis</p> <p>04. Unequal Angle Bending Principle Axis</p> |
|---|

- | |
|---|
| <p>1. Yield</p> <p>2. Lateral Torsional Buckling</p> <p>3. Leg Local Buckling</p> |
|---|



ANGLE FLEXURE CHECKS

Select : Compression Flange

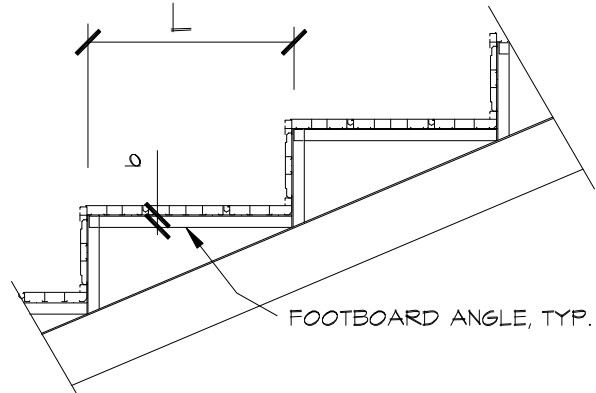
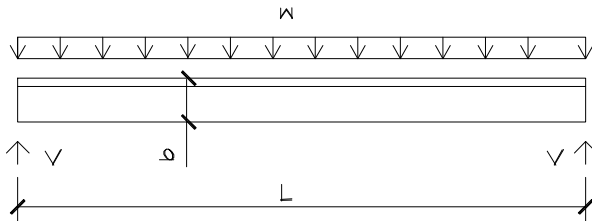
Bending About X Axis

Select: (Angle Type)

Equal Angle

Select: (Angle, Restraint, Bending)

03.



$w =$	630	PLF
$V =$	787.5	#
$M =$	393.75	#*FT ← Moment - Partial End Fixity
$f_b = M / S_N =$	25132.98	PSI

$w_{DL} = 5$ PSF
$w_{LL} = 100$ PSF > 120 PLF for this L
Trib. Width = 6 FT

STRESS CHECK

$M_n = (\text{Smallest of } 1, 2, 3) =$	1148.65	#*FT
$M_n / \Omega_b =$	687.81	#*FT
$F_b = (M_n / \Omega_b) / S_N =$	43903.04	PSI

MEMBER CHECK **0.57** < 1.0 **OK!**

USE: **L2 x 2 x 3/16**

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Sheet
7
Of:

RAIL LOADINGS;

IBC/ICC; 50 PLF UNIFORM LOAD ANY DIRECTION @ TOP
OR
200# POINT LOAD @ ANY LOCATION

STANDARD 1 5/8" Ø HANDRAIL (6063- T6)

$$R_b / t = \frac{0.830}{0.080} = 10.375$$

$$S_1 \text{ MAX} = 33 > 10.375$$

$$F_b = 17.7 \text{ ksi}$$

$$\begin{aligned} \text{MOMENT} &= F_b \times S_x \\ &= 17,700 \times 0.1689 = 2,989.53 \text{ in} \cdot \text{lb} \\ &= 249.13 \text{ ft} \cdot \text{lb} \\ &= 0.249 \text{ k} \cdot \text{ft} \end{aligned}$$

FOR MULTI - SPAN CONDITIONS (2 OR MORE);

$$M_p @ CL = \frac{13 \cdot P \cdot l}{64}$$

$$M_w \text{ CONTINUOUS} = \frac{w \cdot l^2}{8}$$

CODE	MAX L FOR PT.	MAX L FOR w	DESIGN L
IBC/ICC	6.13'	6.31'	6' 1-1/2"

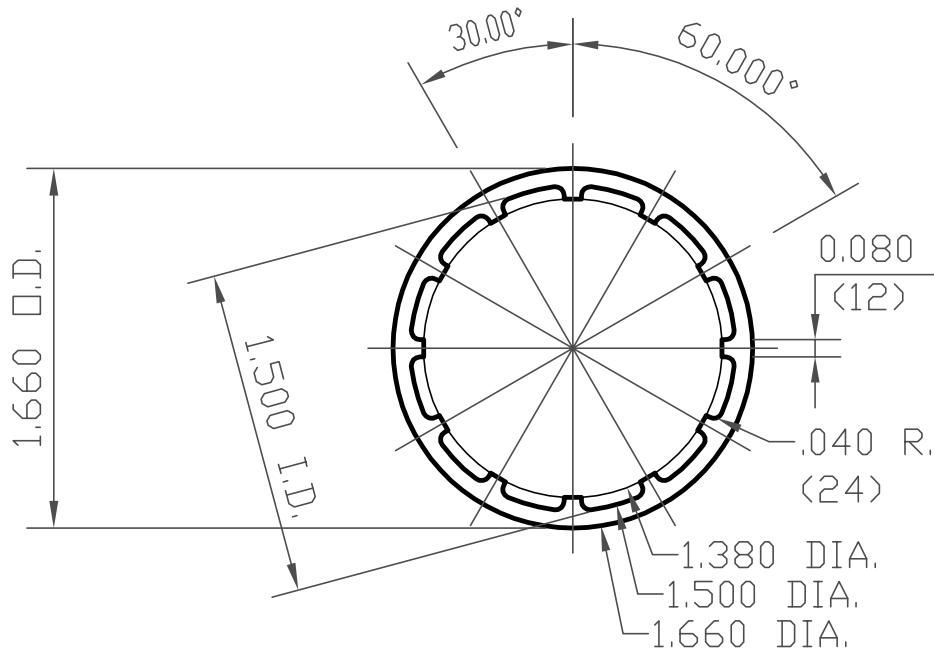
FOR POINT, $P \cdot l = 1225.85$

FOR UNIFORM, $w \cdot l^2 = 1992$



By: _____
Date: _____
Job no. _____

Sheet
8
Of: _____



AREA .465 , .558#/FT.

1. $I_x = .1402 \text{ IN. e-4}$
2. MATERIAL - 6063 T-6
3. MIN. MAT. PROP. - 25000 PSI
4. $E = 10,000,000 \text{ PSI}$
5. $C = 0.830 \text{ IN.}$
6. $S_x = .1689 \text{ IN. e-3}$

1 5/8" O.D. ALUMINUM RAIL DETAIL

NOT TO SCALE

6063 T6



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 CIVIL ENGINEERS
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 FRESNO, CALIFORNIA 93711
 (559)449-8444 FAX: (559)449-8404

By:

Date:

Job no:

Sheet

9

HANDRAIL ANGLE MEMBERS - TO STEEL STRINGERS

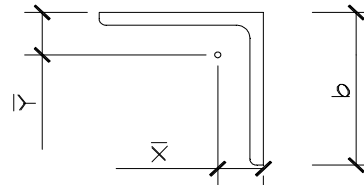
@ FRONT WALK

MEMBER SIZE L 3 x 3 x 1/4

$S_N =$	0.569	IN ³
$F_y =$	50000	PSI
$b =$	3	IN
(thickness) $t =$	0.25	IN
$I_y =$	1.23	IN ⁴
$I_x =$	1.23	IN ⁴
$x =$	0.836	IN
$y =$	0.836	IN
(Unbraced Length) $l =$	42	IN
$C_b =$	1	
$E =$	29000000	PSI
$L =$	42	IN

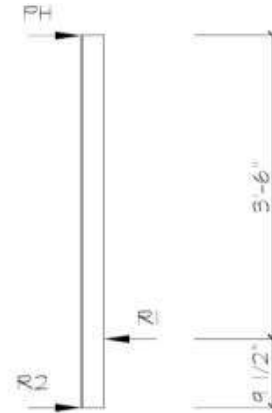
- | | |
|------------|--|
| 01. | Equal Angle No Restraint Bending Single Axis |
| 02. | Equal Angle Restraint @ Max Moment Bending Single Axis |
| 03. | Equal Angle Bending Principle Axis |
| 04. | Unequal Angle Bending Principle Axis |

- | | |
|-----------|----------------------------|
| 1. | Yield |
| 2. | Lateral Torsional Buckling |
| 3. | Leg Local Buckling |



ANGLE FLEXURE CHECKS

Select : Compression Flange	Bending About X Axis
Select: (Angle Type)	Equal Angle
Select: (Angle, Restraint, Bending)	01.



$P =$	300	#
$M = P*L =$	1050	#*FT
$f_b = M / S_N =$	22144.11	PSI

$w_{LL} =$	50	PLF
$P_{LL} =$	200	#
Trib. Width =	6	FT

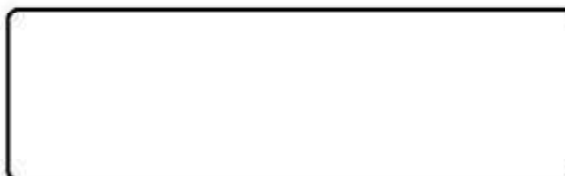
STRESS CHECK

$M_n = (\text{Smallest of 1,2,3}) =$	2557.81	#*FT
$M_n / \Omega_b =$	1531.62	#*FT
$F_b = (M_n / \Omega_b) / S_N =$	32301.36	PSI

MEMBER CHECK **0.69** **LESS THAN 1.0 OK!**

USE: L 3 x 3 x 1/4

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By:
Date:
Job no:

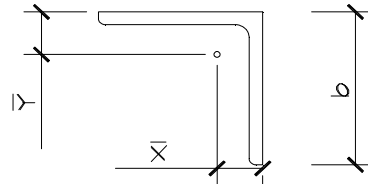
HANDRAIL ANGLE MEMBERS - TO STEEL STRINGERS

@ SIDES

MEMBER SIZE L 3 x 3 x 1/4

$S_N =$	0.569	IN ³
$F_y =$	50000	PSI
$b =$	3	IN
(thickness) $t =$	0.25	IN
$I_y =$	1.23	IN ⁴
$I_x =$	1.23	IN ⁴
$x =$	0.836	IN
$y =$	0.836	IN
(Unbraced Length) $l =$	64	IN
$C_b =$	1	
$E =$	29000000	PSI
$L =$	64	IN

- | |
|--|
| <p>O1. Equal Angle No Restraint Bending Single Axis</p> <p>O2. Equal Angle Restraint @ Max Moment Bending Single Axis</p> <p>O3. Equal Angle Bending Principle Axis</p> <p>O4. Unequal Angle Bending Principle Axis</p>
<p>1. Yield</p> <p>2. Lateral Torsional Buckling</p> <p>3. Leg Local Buckling</p> |
|--|



ANGLE FLEXURE CHECKS

Select : Compression Flange	Bending About X Axis
Select: (Angle Type)	Equal Angle
Select: (Angle, Restraint, Bending)	O1.


$P =$	250	#
$M = P * L =$	1333.33	#*FT
$f_b = M / S_N =$	28119.51	PSI

$w_{LL} =$	50	PLF
$P_{LL} =$	200	#
Trib. Width =	5	FT

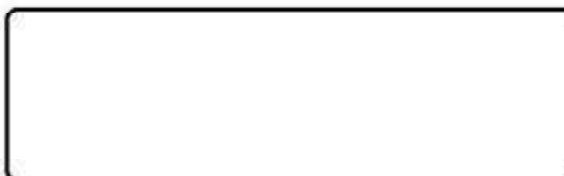
STRESS CHECK

$M_n = (\text{Smallest of } 1, 2, 3) =$	2469.05	#*FT
$M_n / \Omega_b =$	1478.47	#*FT
$F_b = (M_n / \Omega_b) / S_N =$	31180.45	PSI

MEMBER CHECK **0.90** **LESS THAN 1.0 OK!** **USE: L 3 x 3 x 1/4**



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By:
Date:
Job no:

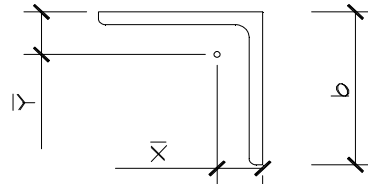
HANDRAIL ANGLE MEMBERS - TO STEEL STRINGERS

@ BACK

MEMBER SIZE **L 3 x 3 x 1/4**

$S_N =$	0.569	IN^3
$F_y =$	50000	PSI
$b =$	3	IN
(thickness) $t =$	0.25	IN
$I_y =$	1.23	IN^4
$I_x =$	1.23	IN^4
$x =$	0.836	IN
$y =$	0.836	IN
(Unbraced Length) $l =$	67	IN
$C_b =$	1	
$E =$	29000000	PSI
$L =$	59	IN

- O1.** Equal Angle No Restraint Bending Single Axis
O2. Equal Angle Restraint @ Max Moment Bending Single Axis
O3. Equal Angle Bending Principle Axis
O4. Unequal Angle Bending Principle Axis
1. Yield
 2. Lateral Torsional Buckling
 3. Leg Local Buckling



ANGLE FLEXURE CHECKS

Select : Compression Flange	Bending About X Axis
Select: (Angle Type)	Equal Angle
Select: (Angle, Restraint, Bending)	O1.

$P =$	300	$\#$
$M = P * L =$	1475.00	$\# * FT$
$f_b = M / S_N =$	31107.21	PSI

$w_{LL} =$	50	PLF
$P_{LL} =$	200	$\#$
Trib. Width =	6	FT

STRESS CHECK

$M_n = (\text{Smallest of } 1, 2, 3) =$	2456.32	$\# * FT$
$M_n / \Omega_b =$	1470.85	$\# * FT$
$F_b = (M_n / \Omega_b) / S_N =$	31019.69	PSI

MEMBER CHECK **1.00** **<= 1.0 OK!** **USE: L 3 x 3 x 1/4**

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By: _____

Date: _____

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HANDRAIL ANGLE MEMBERS - TO STEEL STRINGERS

5/8" DIA. CONNECTION BOLTS

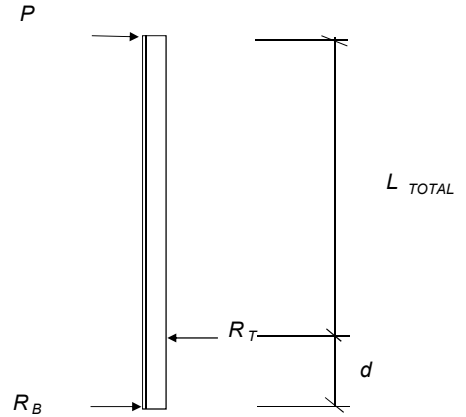
@ BACK

$P = 300 \text{ \#}$
 $L_{TOTAL} = 59 \text{ IN}$
 $d = 8 \text{ IN}$

$R_T = 2212.50 \text{ \#}$

5/8" DIA. A307 BOLT


$T_{ALLOW} = 6900 \text{ \#} \quad OK > R_T$



@ FRONT & SIDE

BY OBSERVATION, LOADS TO BOLTS ARE LESS THAN @ BACK. THEREFORE, OK

USE: 5/8 " DIA. A307 BOLTS


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By: _____
 Date: _____
 Job no: _____

Sheet
13
 Of: _____

WIND LOAD PRESSURES (PARTIALLY ENCLOSED)

Puyallup WA

MWFRS STRINGER LOADING

I. DESIGN PARAMETERS

• RISK CATEGORY	TYPE III
• MEAN STRUCTURE HEIGHT, h	10.00 FT (ASCE 7-16 FIG. 27.4-1)
• PEAK STRUCTURE HEIGHT, Z	20.00 FT (ASCE 7-16 FIG. 27.4-1)
• SLOPE OF GRANDSTAND	16 : 24 (RISE : RUN)
• SLOPE ANGLE OF GRANDSTAND, θ	33.69 DEGREES
• LENGTH OF GRANDSTAND	156.00 FT
• DEPTH OF GRANDSTAND	27.08 FT
• LONGITUDINAL WIND, L/B	5.76 (ASCE 7-16 FIG. 27.4-1)
• TRANSVERSE WIND, L/B	0.17 (ASCE 7-16 FIG. 27.4-1)
• TRANSVERSE WIND, h/L	0.37 (ASCE 7-16 FIG. 27.4-1)

II. WIND LOAD PARAMETERS

• BASIC WIND SPEED, V	115 MPH (ASCE 7-16 FIG. 26.5-1)
• WIND DIRECTIONALITY FACTOR, K_d	0.85 (ASCE 7-16 TABLE 26.6-1)
• EXPOSURE CATEGORY	C (ASCE 7-16 SEC. 26.7.3)
• VELOCITY PRESSURE EXPOSURE COEFFICIENT, K_z	0.90 (ASCE 7-16 TABLE 27.3-1)
• TOPOGRAPHIC FACTOR, K_{zT}	1.00 (ASCE 7-16 FIG. 26.8-1)
• GUST EFFECT FACTOR, G	0.85 (ASCE 7-16 SEC. 26.9)
• INTERNAL PRESSURE COEFFICIENT, GC_{pi}	0.55 \pm (ASCE 7-16 TABLE 26.11-1)

III. VELOCITY PRESSURE

• VELOCITY PRESSURE, $q_z = 0.00256K_zK_{zt}K_dV^2$	25.90 PSF (ASCE 7-16 EQN. 27.3-1)
---	-----------------------------------

IV. EXTERNAL PRESSURE COEFFICIENTS, C_p

• WINDWARD WALL	0.80 (ASCE 7-16 FIG. 27.4-1)
• LEEWARD WALL (LONGITUDINAL WIND)	-0.20 (ASCE 7-16 FIG. 27.4-1)
• LEEWARD WALL (TRANSVERSE WIND)	-0.50 (ASCE 7-16 FIG. 27.4-1)
• WINDWARD ROOF (POSITIVE or NEGATIVE).....	-0.18 (ASCE 7-16 FIG. 27.4-1)
• WINDWARD ROOF (NEGATIVE).....	-0.70 (ASCE 7-16 FIG. 27.4-1)
• LEEWARD ROOF	-0.60 (ASCE 7-16 FIG. 27.4-1)
• FLAT ROOF CASE 1.....	-0.90 (ASCE 7-16 FIG. 27.4-1)
• FLAT ROOF CASE 2	-0.18 (ASCE 7-16 FIG. 27.4-1)

V. DESIGN WIND PRESSURES, $P = qGC_p - q_i(GC_{pi})$ (ASCE 7-16 EQN. 27.4-1)

• WINDWARD WALL	31.86 PSF
• LEEWARD WALL (LONGITUDINAL WIND)	-18.65 PSF
• LEEWARD WALL (TRANSVERSE WIND)	-25.25 PSF
• WINDWARD ROOF (POSITIVE or NEGATIVE).....	-18.21 PSF
• WINDWARD ROOF (NEGATIVE).....	-29.66 PSF
• LEEWARD ROOF	-27.45 PSF
• FLAT ROOF CASE 1.....	-34.06 PSF
• FLAT ROOF CASE 2	-18.21 PSF

WIND LOAD PRESSURES (OPEN)
MWFERS STRINGER LOADING

Puyallup WA

I. DESIGN PARAMETERS

• RISK CATEGORY	TYPE III
• MEAN STRUCTURE HEIGHT, h	31.00 FT (ASCE 7-16 FIG. 27.4-1)
• PEAK STRUCTURE HEIGHT, Z	32.25 FT (ASCE 7-16 FIG. 27.4-1)
• SLOPE OF ROOF COVER	1 : 12 (RISE : RUN)
• SLOPE ANGLE OF ROOF COVER, θ	4.76 DEGREES
• LENGTH OF ROOF COVER	156.00 FT
• DEPTH OF ROOF COVER	26.50 FT
• LONGITUDINAL WIND, L/B	5.89 (ASCE 7-16 FIG. 27.4-1)
• TRANSVERSE WIND, L/B	0.17 (ASCE 7-16 FIG. 27.4-1)
• TRANSVERSE WIND, h/L	1.17 (ASCE 7-16 FIG. 27.4-1)

II. WIND LOAD PARAMETERS

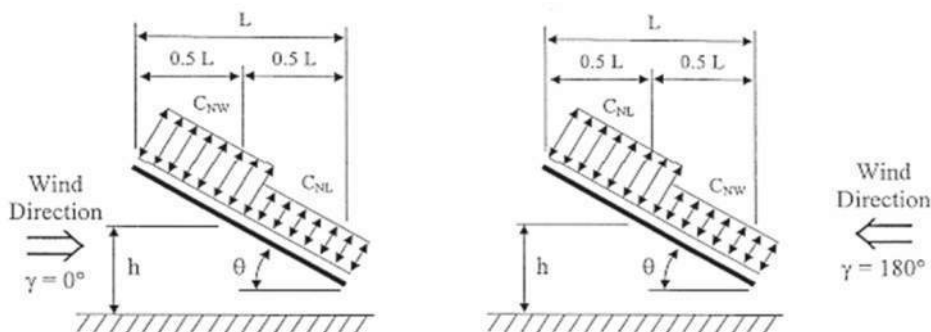
• BASIC WIND SPEED, V	115 MPH (ASCE 7-16 FIG. 26.5-1)
• WIND DIRECTIONALITY FACTOR, K_d	0.85 (ASCE 7-16 TABLE 26.6-1)
• EXPOSURE CATEGORY	C (ASCE 7-16 SEC. 26.7.3)
• VELOCITY PRESSURE EXPOSURE COEFFICIENT, K_z	0.98 (ASCE 7-16 TABLE 27.3-1)
• TOPOGRAPHIC FACTOR, K_{zt}	1.00 (ASCE 7-16 FIG. 26.8-1)
• GUST EFFECT FACTOR, G	0.85 (ASCE 7-16 SEC. 26.9)

III. VELOCITY PRESSURE

• VELOCITY PRESSURE, $q_z = 0.00256K_zK_{zt}K_dV^2$	28.20 PSF (ASCE 7-16 EQN. 27.3-1)
---	-----------------------------------

IV. NET PRESSURE COEFFICIENTS, C_N

	C_{NW}	C_{NL}
• CASE A CLEAR WIND FLOW, $\gamma = 0^\circ$	1.2	0.3
• CASE B CLEAR WIND FLOW, $\gamma = 0^\circ$	-1.1	-0.1
• CASE A CLEAR WIND FLOW, $\gamma = 180^\circ$	1.2	0.3
• CASE B CLEAR WIND FLOW, $\gamma = 180^\circ$	-1.1	-0.1



V. DESIGN WIND PRESSURES, $P = q_hGC_N$ (ASCE 7-16 EQN. 27.4-3)

	C_{NW}	C_{NL}
• CASE A CLEAR WIND FLOW, $\gamma = 0^\circ$	28.77 PSF	7.19 PSF
• CASE B CLEAR WIND FLOW, $\gamma = 0^\circ$	-26.37 PSF	-2.4 PSF
• CASE A CLEAR WIND FLOW, $\gamma = 180^\circ$	28.77 PSF	7.19 PSF
• CASE B CLEAR WIND FLOW, $\gamma = 180^\circ$	-26.37 PSF	-2.4 PSF

WIND LOAD PRESSURES (PARTIALLY ENCLOSED)
MWFRS LOADING

Puyallup WA

I. DESIGN PARAMETERS

• RISK CATEGORY	TYPE III
• MEAN STRUCTURE HEIGHT, h	9.00 FT (ASCE 7-16 FIG. 27.3-1)
• PEAK STRUCTURE HEIGHT, Z (FROM GRADE)	20.00 FT (ASCE 7-16 FIG. 27.3-1)
• ROOF SLOPE	2 : 12 (RISE : RUN)
• ROOF SLOPE ANGLE, θ	9.46 DEGREES
• LENGTH	24.00 FT
• DEPTH	8.00 FT
• LONGITUDINAL WIND, L/B	3.00 (ASCE 7-16 FIG. 27.3-1)
• TRANSVERSE WIND, L/B	0.33 (ASCE 7-16 FIG. 27.3-1)
• TRANSVERSE WIND, h/L	1.13 (ASCE 7-16 FIG. 27.3-1)

II. WIND LOAD PARAMETERS

• BASIC WIND SPEED, V	115 MPH (ASCE 7-16 FIG. 26.5-1)
• WIND DIRECTIONALITY FACTOR, K_d	0.85 (ASCE 7-16 TABLE 26.6-1)
• EXPOSURE CATEGORY	C (ASCE 7-16 SEC. 26.7.3)
• VELOCITY PRESSURE EXPOSURE COEFFICIENT, K_z	0.90 (ASCE 7-16 TABLE 27.3-1)
• TOPOGRAPHIC FACTOR, K_{zT}	1.00 (ASCE 7-16 FIG. 26.8-1)
• GUST EFFECT FACTOR, G	0.85 (ASCE 7-16 SEC. 26.9)
• INTERNAL PRESSURE COEFFICIENT, GC_{pi}	0.55 \pm (ASCE 7-16 TABLE 26.11-1)

III. VELOCITY PRESSURE

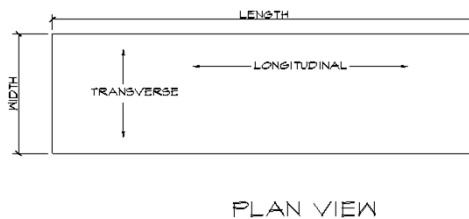
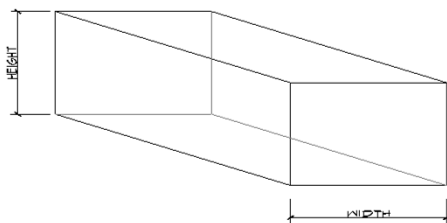
• VELOCITY PRESSURE, $q_z = 0.00256K_zK_{zt}K_dV^2$	25.90 PSF (ASCE 7-16 EQN. 27.3-1)
---	-----------------------------------

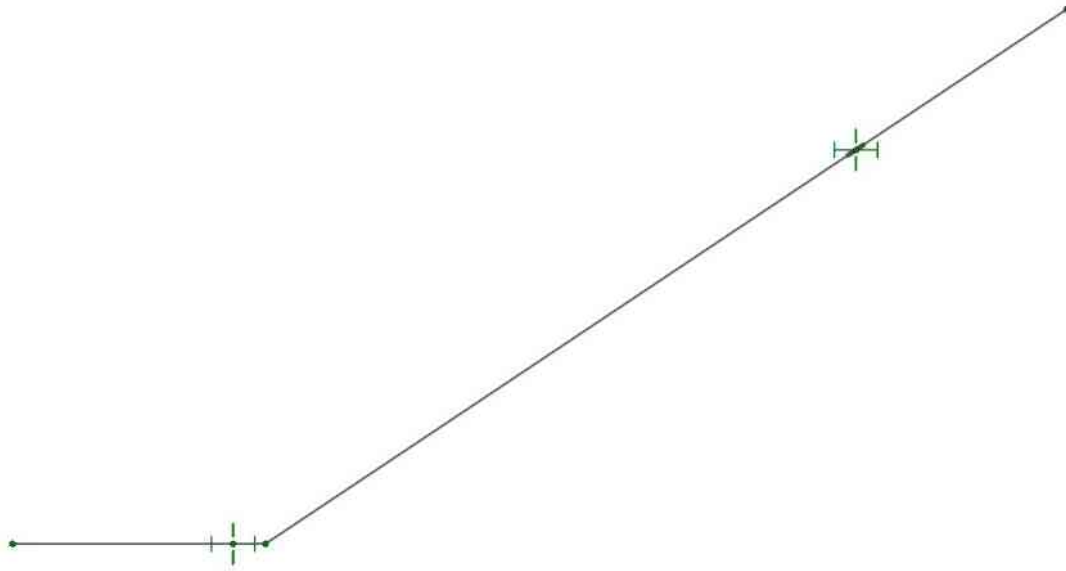
IV. EXTERNAL PRESSURE COEFFICIENTS, C_p

• WINDWARD WALL	0.80 (ASCE 7-16 FIG. 27.3-1)
• LEEWARD WALL (LONGITUDINAL WIND)	-0.20 (ASCE 7-16 FIG. 27.3-1)
• LEEWARD WALL (TRANSVERSE WIND)	-0.50 (ASCE 7-16 FIG. 27.3-1)
• FLAT ROOF (CASE 1).....	-0.90 (ASCE 7-16 FIG. 27.3-1)
• FLAT ROOF (CASE 2).....	-0.18 (ASCE 7-16 FIG. 27.3-1)

V. DESIGN WIND PRESSURES, $P = qGC_p - q_i(GC_{pi})$ (ASCE 7-16 EQN. 27.3-1)

• WINDWARD WALL	31.86 PSF
• LEEWARD WALL (LONGITUDINAL WIND)	-18.65 PSF
• LEEWARD WALL (TRANSVERSE WIND)	-25.25 PSF
• FLAT ROOF (CASE 1).....	-34.06 PSF
• FLAT ROOF (CASE 2).....	-18.21 PSF





Review Loads

Rise =	16	in	} See "Stringer Dead Loads"
Run =	24	in	
Stringer Spacing =	6	ft	

Dead Loads:

$$W_{DL} = 10 \text{ psf} \times \text{Stringer spacing} = \mathbf{0.060 \text{ klf}}$$

Live Loads:

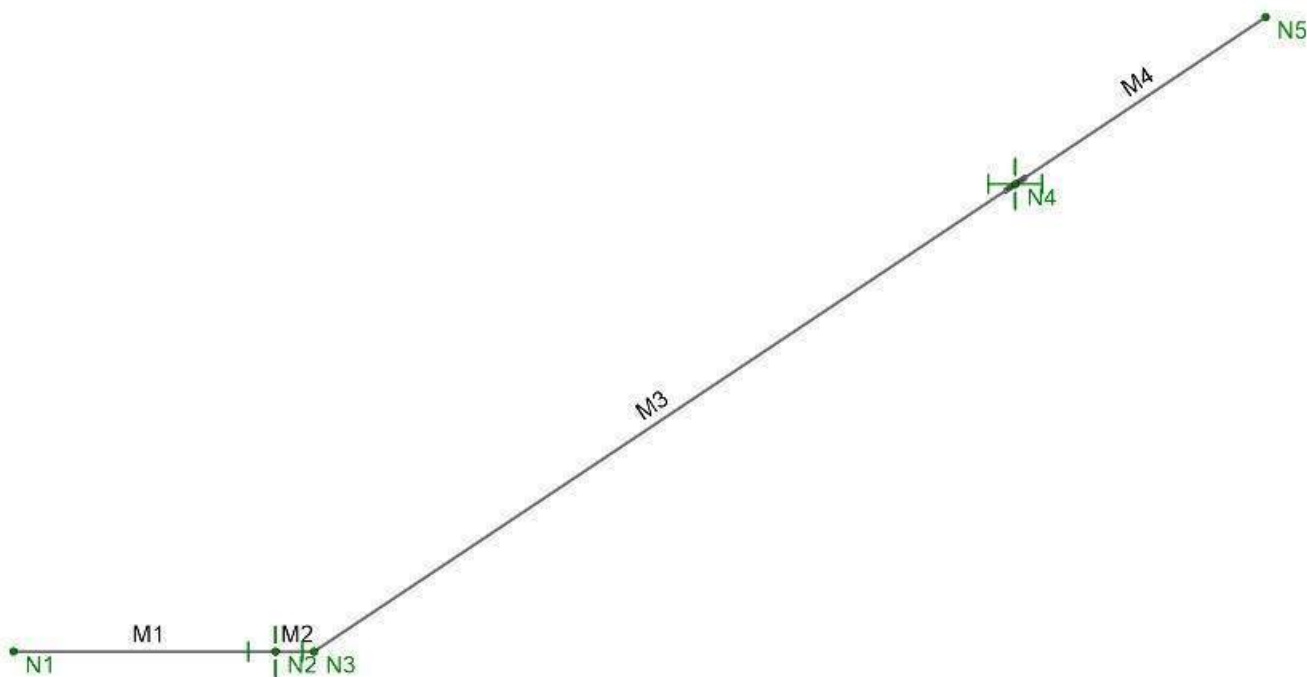
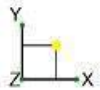
$$W_{LL} = 100 \text{ psf} \times \text{Stringer spacing} = \mathbf{0.600 \text{ klf}}$$

Sway Loads:

$$W_{SWAY (II)} = 24 \text{ plf} \times \text{Stringer spacing} \times (12/\text{Run}) = \mathbf{0.072 \text{ klf}}$$

Wind Loads @ Stringer:

See "Wind Load Pressures"



SK-1
Apr 15, 2022
STRINGERS.r3d

Model Settings

Solution

Members

Number of Reported Sections	5
Number of Internal Sections	100
Member Area Load Mesh Size (in ²)	144
Consider Shear Deformation	Yes
Consider Torsional Warping	Yes

Wall Panels

Approximate Mesh Size (in)	12
Transfer Forces Between Intersecting Wood Walls	Yes
Increase Wood Wall Nailing Capacity for Wind Loads	Yes
Include P-Delta for Walls	Yes
Optimize Masonry and Wood Walls	Yes
Maximum Number of Iterations	3

Processor Core Utilization

Single	No
Multiple (Optimum)	Yes
Maximum	No

Axis

Vertical Global Axis

Global Axis corresponding to vertical direction	Y
Convert Existing Data	Yes

Default Member Orientation

Default Global Plane for z-axis	XZ
---------------------------------	----

Plate Axis

Plate Local Axis Orientation	Nodal
------------------------------	-------

Codes

Hot Rolled Steel	AISC 14th (360-10): ASD
Stiffness Adjustment	Yes (Iterative)
Notional Annex	None
Connections	None
Cold Formed Steel	None
Stiffness Adjustment	Yes (Iterative)
Wood	None
Temperature	< 100F
Concrete	None
Masonry	None
Aluminum	None
Structure Type	Building
Stiffness Adjustment	Yes (Iterative)
Stainless	None
Stiffness Adjustment	Yes (Iterative)

Concrete

Compression Stress Block	Rectangular Stress Block
Analyze using Cracked Sections	Yes
Leave room for horizontal rebar splices (2*d bar spacing)	No

Model Settings (Continued)

List forces which were ignored for design in the Detail Report	Yes
--	-----

Rebar

Column Min Steel	1
Column Max Steel	8
Rebar Material Spec	ASTM A615
Warn if beam-column framing arrangement is not understood	No

Shear Reinforcement

Number of Shear Regions	4
Region 2 & 3 Spacing Increase Increment (in)	4

Seismic

RISA-3D Seismic Load Options

Code	ASCE 7-16
Risk Category	III
Drift Cat	Other
Base Elevation (ft)	
Include the weight of the structure in base shear calcs	Yes

Site Parameters

S_1 (g)	1
SD_1 (g)	1
SD_s (g)	1
T_1 (sec)	5

Structure Characteristics

T Z (sec)	
T X (sec)	
$C_d X$	0.02
$C_{Exp. Z}$	0.75
$C_{Exp. X}$	0.75
R Z	3
R X	3
$\Omega_0 Z$	1
$\Omega_0 X$	1
$C_d Z$	1
$C_d X$	1
ρZ	1
ρX	1

Hot Rolled Steel Properties

	Label	E [ksi]	G [ksi]	Nu	Therm. Coeff. [$1e^{-5}F^{-1}$]	Density [k/ft ³]	Yield [ksi]	Ry	Fu [ksi]	Rt
1	A36 Gr.36	29000	11154	0.3	0.65	0.49	36	1.5	58	1.2
2	A572 Gr.50	29000	11154	0.3	0.65	0.49	50	1.1	65	1.1
3	A992	29000	11154	0.3	0.65	0.49	50	1.1	65	1.1
4	A500 Gr.42	29000	11154	0.3	0.65	0.49	42	1.4	58	1.3
5	A500 Gr.46	29000	11154	0.3	0.65	0.49	46	1.4	58	1.3

Hot Rolled Steel Section Sets

	Label	Shape	Type	Design List	Material	Design Rule	Area [in ²]	Iyy [in ⁴]	Izz [in ⁴]	J [in ⁴]
1	STRINGERS	W10X12	Beam	Wide Flange	A992	Typical	3.54	2.18	53.8	0.055

Node Coordinates

	Label	X [ft]	Y [ft]	Z [ft]	Detach From Diaphragm
1	N1	0	4	0	
2	N2	5.6667	4	0	
3	N3	6.5	4	0	
4	N4	21.667	14.11133	0	
5	N5	27.08333	17.7224	0	

Node Boundary Conditions

	Node Label	X [k/in]	Y [k/in]	Z [k/in]	X Rot [k-ft/rad]
1	N2	Reaction	Reaction	Reaction	Fixed
2	N4		Reaction	Reaction	Fixed

Member Primary Data

	Label	I Node	J Node	Section/Shape	Type	Design List	Material	Design Rule
1	M1	N1	N2	STRINGERS	Beam	Wide Flange	A992	Typical
2	M2	N2	N3	STRINGERS	Beam	Wide Flange	A992	Typical
3	M3	N3	N4	STRINGERS	Beam	Wide Flange	A992	Typical
4	M4	N4	N5	STRINGERS	Beam	Wide Flange	A992	Typical

Hot Rolled Steel Design Parameters

	Label	Shape	Length [ft]	Lb y-y [ft]	Lcomp top [ft]	Lcomp bot [ft]	K y-y	K z-z	Function
1	M1	STRINGERS	5.667	3.5	3.5		2.1	2.1	Lateral
2	M2	STRINGERS	0.833	3.5	3.5		1	1	Lateral
3	M3	STRINGERS	18.228	3.5	3.5	9	1	1	Lateral
4	M4	STRINGERS	6.51	3.5	3.5		2.1	2.1	Lateral

Member Distributed Loads (BLC 1 : DEAD LOADS)

	Member Label	Direction	Start Magnitude [k/ft, F, ksf, k-ft/ft]	End Magnitude [k/ft, F, ksf, k-ft/ft]	Start Location [(ft, %)]	End Location [(ft, %)]
1	M1	PY	-0.06	-0.06	0	%100
2	M2	PY	-0.06	-0.06	0	%100
3	M3	PY	-0.06	-0.06	0	%100
4	M4	PY	-0.06	-0.06	0	%100

Member Distributed Loads (BLC 2 : LIVE LOADS(UNIFORM))

Member Label	Direction	Start Magnitude [k/ft, F, ksf, k-ft/ft]	End Magnitude [k/ft, F, ksf, k-ft/ft]	Start Location [(ft, %)]	End Location [(ft, %)]
1	M1	PY	-0.6	-0.6	0 %100
2	M2	PY	-0.6	-0.6	0 %100
3	M3	PY	-0.6	-0.6	0 %100
4	M4	PY	-0.6	-0.6	0 %100

Member Distributed Loads (BLC 3 : SWAY LOADS)

Member Label	Direction	Start Magnitude [k/ft, F, ksf, k-ft/ft]	End Magnitude [k/ft, F, ksf, k-ft/ft]	Start Location [(ft, %)]	End Location [(ft, %)]
1	M1	Z	0.072	0.072	0 %100
2	M2	Z	0.072	0.072	0 %100
3	M3	Z	0.072	0.072	0 %100
4	M4	Z	0.072	0.072	0 %100

Member Distributed Loads (BLC 4 : WIND LOADS FTB)

Member Label	Direction	Start Magnitude [k/ft, F, ksf, k-ft/ft]	End Magnitude [k/ft, F, ksf, k-ft/ft]	Start Location [(ft, %)]	End Location [(ft, %)]
1	M3	PX	0.178	0.178	0 %100
2	M4	PX	0.178	0.178	0 %100

Member Distributed Loads (BLC 5 : WIND LOADS UPLIFT)

Member Label	Direction	Start Magnitude [k/ft, F, ksf, k-ft/ft]	End Magnitude [k/ft, F, ksf, k-ft/ft]	Start Location [(ft, %)]	End Location [(ft, %)]
1	M1	y	0.165	0.165	0 %100
2	M2	y	0.165	0.165	0 %100
3	M3	y	0.165	0.165	0 %100
4	M4	y	0.165	0.165	0 %100

Basic Load Cases

	BLC Description	Category	Distributed
1	DEAD LOADS	DL	4
2	LIVE LOADS(UNIFORM)	LL	4
3	SWAY LOADS	OL1	4
4	WIND LOADS FTB	WLX	2
5	WIND LOADS UPLIFT	WL-X	4

Load Combinations

	Description	Solve	P-Delta	BLC	Factor	BLC	Factor	BLC	Factor
1	DL								
2		Yes	Y	DL	1				
3									
4	DL + LL								
5		Yes	Y	DL	1	LL	1		
6									
7	DL + LL + SWAYZ								
8		Yes	Y	DL	1	OL1	0.75	LL	0.75
9									
10									
11	DL + LL + WLFTB								
12		Yes	Y	DL	1	WLX	0.45	LL	0.75
13									
14	DL + WLFTB								

Load Combinations (Continued)

Description	Solve	P-Delta	BLC	Factor	BLC	Factor	BLC	Factor
15	Yes	Y	DL	1	WLX	0.6		
16	Yes	Y	DL	0.6	WLX	0.6		
17								
18	DL + LL- WLFTB							
19	Yes	Y	DL	1	WLX	-0.45	LL	0.75
20								
21	DL - WLFTB							
22	Yes	Y	DL	1	WLX	-0.6		
23	Yes	Y	DL	0.6	WLX	-0.6		
24								
25	DL + LL + WLUP							
26	Yes	Y	DL	1	WL-X	0.45	LL	0.75
27								
28	DL + WLUP							
29	Yes	Y	DL	1	WL-X	0.6		
30	Yes	Y	DL	0.6	WL-X	0.6		
31								
32		Y	DL	1				
33		Y	LL	1				
34		Y	OL1	1				
35		Y	WLX	1				
36		Y	WL-X	1				

Envelope Node Reactions

Node Label	X [k]	LC	Y [k]	LC	Z [k]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N2	max	1.436	23	9.079	5	0	30	NC	NC	0	30
2		min	-1.436	15	-0.3	30	-0.816	8	NC	NC	0	2
3	N4	max	0	30	8.521	5	0	30	NC	NC	0	30
4		min	0	2	-1.375	30	-0.844	8	NC	NC	0	2
5	Totals:	max	1.436	23	17.6	5	0	30				
6		min	-1.436	15	-1.675	30	-1.66	8				

Envelope AISC 14TH (360-10): ASD Member Steel Code Checks

Member	Shape	Code Check	Loc[ft]	LC	Shear	Check	Loc[ft]	Dir	LC	Pnc/om [k]	Pnt/om [k]	Mnyy/om [k-ft]	Mnzz/om [k-ft]	Cb	Eqn
1	M1	W10X12	0.464	5.667	8	0.1	5.667	y	5	42.085	105.988	4.296	31.207	2.326	H1-1b
2	M2	W10X12	0.541	0	8	0.142	0	y	5	80.467	105.988	4.296	31.207	1.195	H1-1b
3	M3	W10X12	0.668	17.978	8	0.113	17.978	y	5	30.32	105.988	4.296	15.74	1	H1-1b
4	M4	W10X12	0.462	0	8	0.076	0	y	5	42.085	105.988	4.296	31.207	2.328	H1-1b

Load Combinations

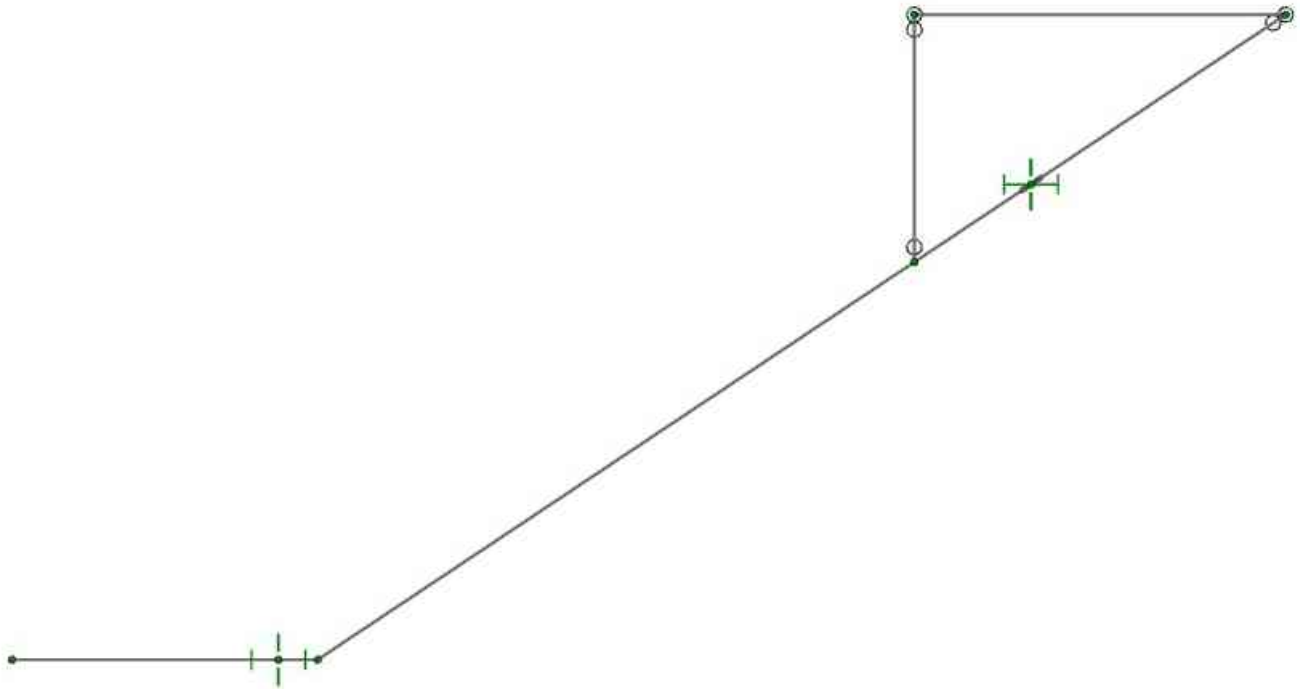
	Description	Solve	P-Delta	BLC	Factor	BLC	Factor	BLC	Factor
1	DL								
2			Y	DL	1				
3									
4	DL + LL								
5			Y	DL	1	LL	1		
6									
7	DL + LL + SWAYZ								
8			Y	DL	1	OL1	0.75	LL	0.75
9									
10									
11	DL + LL+ WLFTB								
12			Y	DL	1	WLX	0.45	LL	0.75
13									
14	DL + WLFTB								
15			Y	DL	1	WLX	0.6		
16			Y	DL	0.6	WLX	0.6		
17									
18	DL + LL- WLFTB								
19			Y	DL	1	WLX	-0.45	LL	0.75
20									
21	DL - WLFTB								
22			Y	DL	1	WLX	-0.6		
23			Y	DL	0.6	WLX	-0.6		
24									
25	DL + LL + WLUP								
26			Y	DL	1	WL-X	0.45	LL	0.75
27									
28	DL + WLUP								
29			Y	DL	1	WL-X	0.6		
30			Y	DL	0.6	WL-X	0.6		
31									
32	DL	Yes	Y	DL	1				
33	LL	Yes	Y	LL	1				
34	SWAY	Yes	Y	OL1	1				
35	WLFTB	Yes	Y	WLX	1				
36	WLUP	Yes	Y	WL-X	1				

Node Reactions

	LC	Node Label	X [k]	Y [k]	Z [k]	MX [k-ft]	MY [k-ft]	MZ [k-ft]
1	32	N2	0	0.825	0	NC	0	0
2	32	N4	0	0.775	0	NC	0	0
3	32	Totals:	0	1.6	0			
4	32	COG (ft):	X: 13.427	Y: 9.146	Z: 0			
5	33	N2	0	8.254	0	NC	0	0
6	33	N4	0	7.747	0	NC	0	0
7	33	Totals:	0	16	0			
8	33	COG (ft):	X: 13.427	Y: 9.146	Z: 0			
9	34	N2	0	0	-1.081	NC	0	0
10	34	N4	0	0	-1.132	NC	0	0
11	34	Totals:	0	0	-2.213			
12	34	COG (ft):	NC	NC	NC			
13	35	N2	-2.393	-1.016	0	NC	0	0
14	35	N4	0	1.016	0	NC	0	0
15	35	Totals:	-2.393	0	0			

Node Reactions (Continued)

LC	Node Label	X [k]	Y [k]	Z [k]	MX [k-ft]	MY [k-ft]	MZ [k-ft]
16	35	COG (ft):	NC	NC	NC		
17	36	N2	2.214	-1.325	0	0	0
18	36	N4	0	-3.067	0	0	0
19	36	Totals:	2.214	-4.392	0		
20	36	COG (ft):	X: 13.415	Y: 9.138	Z: 0		



Review Loads

Rise =	16	in	} See "Stringer Dead Loads"
Run =	24	in	
Stringer Spacing =	6	ft	
Pressbox Length =	24.00	ft	} See "Wind Load Pressures"
Pressbox Width =	8.00	ft	
Pressbox Height =	9.00	ft	
Pressbox Roof Weight =	15	psf	} See "Design Load Summary"
Pressbox Wall Weight =	10	psf	
Pressbox Floor Weight =	10	psf	

Review Loads Cont.

Dead Loads:

$W_{DL(Grand.)} =$	10	psf x Stringer spacing =	0.060	klf
$P_{DL(PB Roof)} =$	15	psf x Stringer spacing x PB Width / 2 =	0.360	Kips
$P_{DL(PB Floor)} =$	10	psf x Stringer spacing x PB Width / 2 =	0.240	Kips

Live Loads:

$W_{LL(Grand.)} =$	100	psf x Stringer spacing =	0.600	klf
$P_{LL(PB Roof)} =$	20	psf x Stringer spacing x PB Width / 2 =	0.480	Kips
$P_{LL(PB Floor)} =$	100	psf x Stringer spacing x PB Width / 2 =	2.400	Kips

Sway Loads:

$W_{SWAY(II)} =$	24	plf x Stringer spacing x (12/Run) =	0.072	klf
$W_{SWAY(L)} =$	10	plf x Stringer spacing x (12/Run) =	0.030	klf

Wind Loads @ Stringer:

See "Wind Load Pressures"

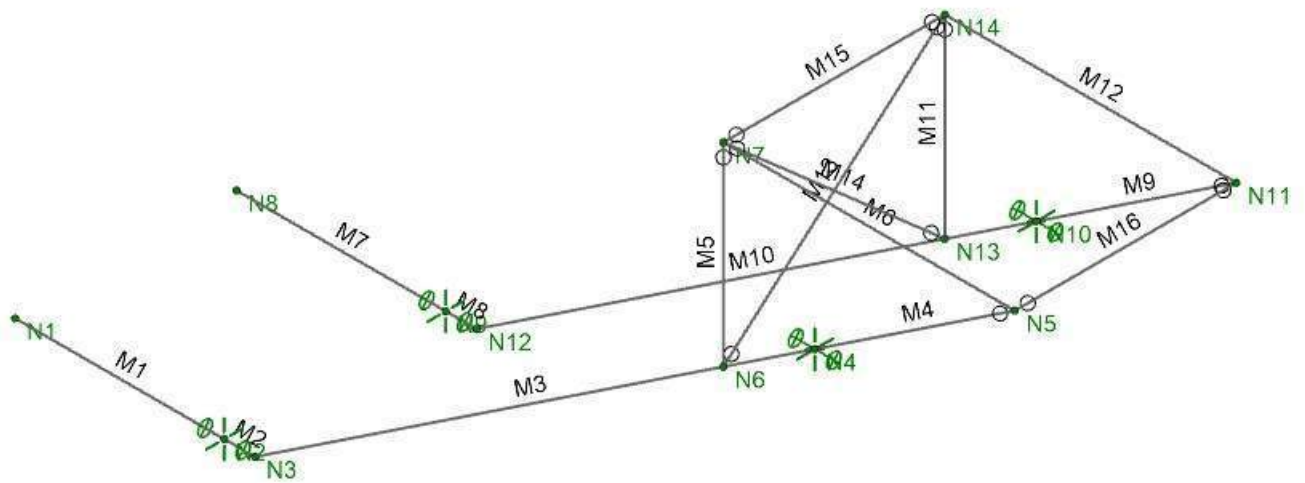
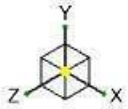
Wind Loads @ Pressbox (MWFRS):

Windward case 1&2

$P_{WL(Roof)} =$	57.11	psf x PB Length/2 x PB Height/2 =	3.084	Kips
$P_{WL(End Flr.)} =$	57.11	psf x Stringer Spacing/2 x PB Height/2 =	0.771	Kips
$P_{WL(Total End)} =$			3.855	Kips
$P_{WL(Int. Flr.)} =$	57.11	psf x Stringer Spacing x PB Height/2 =	1.542	Kips
$T = C = (P_{WL(Roof)} \times PB Height/2) / (PB Width/2) =$			3.469	Kips

Leeward (Lateral Wall Loading):

$P_{WL(Roof)} =$	57.11	psf x PB Length/2 x PB Height/2 =	3.084	Kips
$P_{WL(End Flr.)} =$	57.11	psf x Stringer Spacing/2 x PB Height/2 =	0.771	Kips
$P_{WL(Total End)} =$			3.855	Kips
$P_{WL(Int. Flr.)} =$	57.11	psf x Stringer Spacing x PB Height/2 =	1.542	Kips
$T = C = (P_{WL(Roof)} \times PB Height/2) / (PB Width/2) =$			3.469	Kips



SK-1

Apr 15, 2022

STRINGERS@PB.r3d

Model Settings

Solution

Members

Number of Reported Sections	5
Number of Internal Sections	100
Member Area Load Mesh Size (in ²)	144
Consider Shear Deformation	Yes
Consider Torsional Warping	Yes

Wall Panels

Approximate Mesh Size (in)	12
Transfer Forces Between Intersecting Wood Walls	Yes
Increase Wood Wall Nailing Capacity for Wind Loads	Yes
Include P-Delta for Walls	Yes
Optimize Masonry and Wood Walls	Yes
Maximum Number of Iterations	3

Processor Core Utilization

Single	No
Multiple (Optimum)	Yes
Maximum	No

Axis

Vertical Global Axis

Global Axis corresponding to vertical direction	Y
Convert Existing Data	Yes

Default Member Orientation

Default Global Plane for z-axis	XZ
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Plate Axis

Plate Local Axis Orientation	Nodal
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Codes

Hot Rolled Steel	AISC 14th (360-10): ASD
Stiffness Adjustment	Yes (Iterative)
Notional Annex	None
Connections	None
Cold Formed Steel	None
Stiffness Adjustment	Yes (Iterative)
Wood	None
Temperature	< 100F
Concrete	None
Masonry	None
Aluminum	None
Structure Type	Building
Stiffness Adjustment	Yes (Iterative)
Stainless	None
Stiffness Adjustment	Yes (Iterative)

Concrete

Compression Stress Block	Rectangular Stress Block
Analyze using Cracked Sections	Yes
Leave room for horizontal rebar splices (2*d bar spacing)	No

Model Settings (Continued)

List forces which were ignored for design in the Detail Report	Yes
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Rebar

Column Min Steel	1
Column Max Steel	8
Rebar Material Spec	ASTM A615
Warn if beam-column framing arrangement is not understood	No

Shear Reinforcement

Number of Shear Regions	4
Region 2 & 3 Spacing Increase Increment (in)	4

Seismic

RISA-3D Seismic Load Options

Code	ASCE 7-16
Risk Category	III
Drift Cat	Other
Base Elevation (ft)	
Include the weight of the structure in base shear calcs	Yes

Site Parameters

S_1 (g)	1
SD_1 (g)	1
SD_s (g)	1
T_1 (sec)	5

Structure Characteristics

T Z (sec)	
T X (sec)	
C_x	0.02
$C_{Exp. Z}$	0.75
$C_{Exp. X}$	0.75
R Z	3
R X	3
$\Omega_0 Z$	1
$\Omega_0 X$	1
$C_d Z$	1
$C_d X$	1
ρZ	1
ρX	1

Hot Rolled Steel Properties

	Label	E [ksi]	G [ksi]	Nu	Therm. Coeff. [$1e^{-5}F^{-1}$]	Density [k/ft ³]	Yield [ksi]	Ry	Fu [ksi]	Rt
1	A36 Gr.36	29000	11154	0.3	0.65	0.49	36	1.5	58	1.2
2	A572 Gr.50	29000	11154	0.3	0.65	0.49	50	1.1	65	1.1
3	A992	29000	11154	0.3	0.65	0.49	50	1.1	65	1.1
4	A500 Gr.42	29000	11154	0.3	0.65	0.49	42	1.4	58	1.3
5	A500 Gr.46	29000	11154	0.3	0.65	0.49	46	1.4	58	1.3

Hot Rolled Steel Section Sets

	Label	Shape	Type	Design List	Material	Design Rule	Area [in ²]	Iyy [in ⁴]	Izz [in ⁴]	J [in ⁴]
1	STRINGERS	W10X12	Beam	Wide Flange	A992	Typical	3.54	2.18	53.8	0.055
2	vert	W10X12	Column	Wide Flange	A992	Typical	3.54	2.18	53.8	0.055
3	crossbracing	L2x2x3	VBrace	Single Angle	A992	Typical	0.722	0.271	0.271	0.009
4	channel	C8X11.5	Beam	Channel	A992	Typical	3.37	1.31	32.5	0.13

Node Coordinates

	Label	X [ft]	Y [ft]	Z [ft]	Detach From Diaphragm
1	N1	0	4	0	
2	N2	5.6667	4	0	
3	N3	6.5	4	0	
4	N4	21.667	14.11133	0	
5	N5	27.08333	17.7224	0	
6	N6	19.188768	12.459176	0	
7	N7	19.188768	17.7224	0	
8	N8	0	4	-6	
9	N9	5.6667	4	-6	
10	N10	21.667	14.11133	-6	
11	N11	27.08333	17.7224	-6	
12	N12	6.5	4	-6	
13	N13	19.188768	12.459176	-6	
14	N14	19.188768	17.7224	-6	

Node Boundary Conditions

	Node Label	X [k/in]	Y [k/in]	Z [k/in]	X Rot [k-ft/rad]
1	N2	Reaction	Reaction	Reaction	Fixed
2	N4		Reaction	Reaction	Fixed
3	N9	Reaction	Reaction	Reaction	Fixed
4	N10		Reaction	Reaction	Fixed

Member Primary Data

	Label	I Node	J Node	Section/Shape	Type	Design List	Material	Design Rule
1	M1	N1	N2	STRINGERS	Beam	Wide Flange	A992	Typical
2	M2	N2	N3	STRINGERS	Beam	Wide Flange	A992	Typical
3	M3	N3	N4	STRINGERS	Beam	Wide Flange	A992	Typical
4	M4	N4	N5	STRINGERS	Beam	Wide Flange	A992	Typical
5	M5	N6	N7	vert	Column	Wide Flange	A992	Typical
6	M6	N7	N5	STRINGERS	Beam	Wide Flange	A992	Typical
7	M7	N8	N9	STRINGERS	Beam	Wide Flange	A992	Typical
8	M8	N9	N12	STRINGERS	Beam	Wide Flange	A992	Typical
9	M9	N10	N11	STRINGERS	Beam	Wide Flange	A992	Typical
10	M10	N12	N10	STRINGERS	Beam	Wide Flange	A992	Typical

Member Primary Data (Continued)

	Label	I Node	J Node	Section/Shape	Type	Design List	Material	Design Rule
11	M11	N13	N14	vert	Column	Wide Flange	A992	Typical
12	M12	N14	N11	STRINGERS	Beam	Wide Flange	A992	Typical
13	M13	N6	N14	crossbracing	VBrace	Single Angle	A992	Typical
14	M14	N7	N13	crossbracing	VBrace	Single Angle	A992	Typical
15	M15	N7	N14	channel	Beam	Channel	A992	Typical
16	M16	N11	N5	channel	Beam	Channel	A992	Typical

Hot Rolled Steel Design Parameters

	Label	Shape	Length [ft]	Lb y-y [ft]	Lcomp top [ft]	Lcomp bot [ft]	K y-y	K z-z	Function
1	M1	STRINGERS	5.667	3.5	3.5		2.1	2.1	Lateral
2	M2	STRINGERS	0.833	3.5	3.5		1	1	Lateral
3	M3	STRINGERS	18.228	3.5	3.5	6	1	1	Lateral
4	M4	STRINGERS	6.51	3.5	3.5		2.1	2.1	Lateral
5	M5	vert	5.263		Lbyy		1	1	Lateral
6	M6	STRINGERS	7.895		Lbyy		1	1	Lateral
7	M7	STRINGERS	5.667	3.5	3.5		2.1	2.1	Lateral
8	M8	STRINGERS	0.833	3.5	3.5		1	1	Lateral
9	M9	STRINGERS	6.51	3.5	3.5		2.1	2.1	Lateral
10	M10	STRINGERS	18.228	3.5	3.5	6	1	1	Lateral
11	M11	vert	5.263		Lbyy		1	1	Lateral
12	M12	STRINGERS	7.895		Lbyy		1	1	Lateral
13	M13	crossbracing	7.981		Lbyy		1	1	Lateral
14	M14	crossbracing	7.981		Lbyy		1	1	Lateral
15	M15	channel	6		Lbyy		1	1	Lateral
16	M16	channel	6		Lbyy		1	1	Lateral

Member Distributed Loads (BLC 1 : DEAD LOADS)

	Member Label	Direction	Start Magnitude [k/ft, F, ksf, k-ft/ft]	End Magnitude [k/ft, F, ksf, k-ft/ft]	Start Location [(ft, %)]	End Location [(ft, %)]
1	M1	PY	-0.06	-0.06	0	%100
2	M2	PY	-0.06	-0.06	0	%100
3	M3	PY	-0.06	-0.06	0	15.25
4	M6	PY	-0.06	-0.06	0	%100
5	M7	PY	-0.06	-0.06	0	%100
6	M8	PY	-0.06	-0.06	0	%100
7	M10	PY	-0.06	-0.06	0	15.25
8	M12	PY	-0.06	-0.06	0	%100

Member Distributed Loads (BLC 2 : LIVE LOADS(UNIFORM))

	Member Label	Direction	Start Magnitude [k/ft, F, ksf, k-ft/ft]	End Magnitude [k/ft, F, ksf, k-ft/ft]	Start Location [(ft, %)]	End Location [(ft, %)]
1	M1	PY	-0.6	-0.6	0	%100
2	M2	PY	-0.6	-0.6	0	%100
3	M3	PY	-0.6	-0.6	0	15.25
4	M6	PY	-0.6	-0.6	0	%100
5	M7	PY	-0.6	-0.6	0	%100
6	M8	PY	-0.6	-0.6	0	%100
7	M10	PY	-0.6	-0.6	0	15.25
8	M12	PY	-0.6	-0.6	0	%100

Member Distributed Loads (BLC 3 : SWAY LOADS)

Member Label	Direction	Start Magnitude [k/ft, F, ksf, k-ft/ft]	End Magnitude [k/ft, F, ksf, k-ft/ft]	Start Location [(ft, %)]	End Location [(ft, %)]
1	M1	Z	0.072	0.072	0 %100
2	M2	Z	0.072	0.072	0 %100
3	M3	Z	0.072	0.072	0 15.25
4	M7	Z	0.072	0.072	0 %100
5	M8	Z	0.072	0.072	0 %100
6	M10	Z	0.072	0.072	0 15.25

Member Distributed Loads (BLC 4 : WIND LOADS FTB)

Member Label	Direction	Start Magnitude [k/ft, F, ksf, k-ft/ft]	End Magnitude [k/ft, F, ksf, k-ft/ft]	Start Location [(ft, %)]	End Location [(ft, %)]
1	M3	PX	0.178	0.178	0 15.25
2	M5	PX	0.178	0.178	0 %100
3	M10	PX	0.178	0.178	0 15.25
4	M11	PX	0.178	0.178	0 %100

Member Distributed Loads (BLC 5 : WIND LOADS UPLIFT)

Member Label	Direction	Start Magnitude [k/ft, F, ksf, k-ft/ft]	End Magnitude [k/ft, F, ksf, k-ft/ft]	Start Location [(ft, %)]	End Location [(ft, %)]
1	M1	y	0.165	0.165	0 %100
2	M2	y	0.165	0.165	0 %100
3	M3	y	0.165	0.165	0 %100
4	M4	y	0.165	0.165	0 %100
5	M7	y	0.165	0.165	0 %100
6	M8	y	0.165	0.165	0 %100
7	M9	y	0.165	0.165	0 %100
8	M10	y	0.165	0.165	0 %100

Node Loads and Enforced Displacements (BLC 1 : DEAD LOADS)

Node Label	L, D, M	Direction	Magnitude [(k, k-ft), (in, rad), (k*s ² /ft, k*s ² *ft)]
1	N5	L	Y -0.36
2	N7	L	Y -0.36
3	N11	L	Y -0.36
4	N14	L	Y -0.36

Node Loads and Enforced Displacements (BLC 2 : LIVE LOADS(UNIFORM))

Node Label	L, D, M	Direction	Magnitude [(k, k-ft), (in, rad), (k*s ² /ft, k*s ² *ft)]
1	N5	L	Y -0.48
2	N7	L	Y -0.48
3	N11	L	Y -0.48
4	N14	L	Y -0.48

Node Loads and Enforced Displacements (BLC 4 : WIND LOADS FTB)

Node Label	L, D, M	Direction	Magnitude [(k, k-ft), (in, rad), (k*s ² /ft, k*s ² *ft)]
1	N5	L	Y -3.469
2	N7	L	Y 3.469
3	N7	L	X 0.771
4	N7	L	X 3.084
5	N14	L	X 1.542

Node Loads and Enforced Displacements (BLC 5 : WIND LOADS UPLIFT)

	Node Label	L, D, M	Direction	Magnitude [(k, k-ft), (in, rad), (k*s ² /ft, k*s ² *ft)]
1	N5	L	Y	3.469
2	N7	L	Y	-3.469
3	N7	L	X	-0.771
4	N7	L	X	-3.084
5	N14	L	X	-1.542

Basic Load Cases

	BLC Description	Category	Nodal	Distributed
1	DEAD LOADS	DL	4	8
2	LIVE LOADS(UNIFORM)	LL	4	8
3	SWAY LOADS	OL1		6
4	WIND LOADS FTB	WLX	5	4
5	WIND LOADS UPLIFT	WL-X	5	8

Load Combinations

	Description	Solve	P-Delta	BLC	Factor	BLC	Factor	BLC	Factor
1	DL	Yes	Y	DL	1				
2									
3	DL + LL	Yes	Y	DL	1	LL	1		
4									
5	DL + LL + SWAYZ	Yes	Y	DL	1	OL1	0.75	LL	0.75
6									
7	DL + LL + SWAYZ	Yes	Y	DL	1	WLX	0.45	LL	0.75
8									
9	DL + WLFTB	Yes	Y	DL	1	WLX	0.6		
10		Yes	Y	DL	0.6	WLX	0.6		
11									
12	DL + LL- WLFTB	Yes	Y	DL	1	WLX	-0.45	LL	0.75
13									
14	DL - WLFTB	Yes	Y	DL	1	WLX	-0.6		
15		Yes	Y	DL	0.6	WLX	-0.6		
16									
17	DL + LL + WLUP	Yes	Y	DL	1	WL-X	0.45	LL	0.75
18									
19	DL + WLUP	Yes	Y	DL	1	WL-X	0.6		
20		Yes	Y	DL	0.6	WL-X	0.6		
21									
22	DL		Y	DL	1				
23	LL		Y	LL	1				
24	SWAY		Y	OL1	1				
25	WLFTB		Y	WLX	1				
26	WLUP		Y	WL-X	1				

Envelope Node Reactions

	Node Label		X [k]	LC	Y [k]	LC	Z [k]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N2	max	3.778	15	9.625	12	0.003	12	NC	NC	0	20	0	20
2		min	-3.778	9	-3.19	10	-0.844	5	NC	NC	0	1	0	1
3	N4	max	0	20	11.111	7	0.022	17	NC	NC	0	20	0	20
4		min	0	1	-3.885	20	-0.215	5	NC	NC	0	1	0	1
5	N9	max	2.391	14	8.923	3	0.001	12	NC	NC	0	20	0	20
6		min	-2.391	10	-0.973	10	-0.854	5	NC	NC	0	1	0	1

Envelope Node Reactions (Continued)

Node Label	X [k]	LC	Y [k]	LC	Z [k]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
7 N10 max	0	20	10.632	3	0.005	7	NC	NC	0	20	0	20
8 min	0	1	-1.695	20	-0.436	5	NC	NC	0	1	0	1
9 Totals: max	6.169	14	39.11	3	0	7						
10 min	-6.169	9	-2.457	20	-2.349	5						

Envelope AISC 14TH (360-10): ASD Member Steel Code Checks

Member	Shape	Code Check	Loc[ft]	LC	Shear Check	Loc[ft]	Dir	LC	Pnc/om [k]	Pnt/om [k]	Mnyy/om [k-ft]	Mnzz/om [k-ft]	Cb	Eqn	
1	M1	W10X12	0.464	5.667	5	0.1	5.667	y	3	42.085	105.988	4.296	31.207	2.326	H1-1b
2	M2	W10X12	0.539	0	5	0.181	0	y	12	80.467	105.988	4.296	31.207	1.186	H1-1b
3	M3	W10X12	0.93	15.169	9	0.191	15.357	y	7	30.32	105.988	4.296	23.856	1	H1-1b
4	M4	W10X12	0.584	0	7	0.07	6.26	y	7	42.085	105.988	4.296	31.207	1.667	H1-1b
5	M5	W10X12	0.643	0	7	0.106	0	y	7	64.782	105.988	4.296	31.207	1.694	H1-1b
6	M6	W10X12	0.241	3.947	3	0.069	7.895	y	3	36.511	105.988	4.296	22.053	1.136	H1-1b
7	M7	W10X12	0.464	5.667	5	0.1	5.667	y	3	42.085	105.988	4.296	31.207	2.326	H1-1b
8	M8	W10X12	0.538	0	5	0.138	0	y	3	80.467	105.988	4.296	31.207	1.188	H1-1b
9	M9	W10X12	0.419	0	3	0.05	6.26	y	3	42.085	105.988	4.296	31.207	1.667	H1-1b
10	M10	W10X12	0.681	8.802	5	0.185	17.978	y	3	30.32	105.988	4.296	29.727	1	H1-1b
11	M11	W10X12	0.336	0	7	0.056	0	y	7	64.782	105.988	4.296	31.207	1.722	H1-1b
12	M12	W10X12	0.241	3.947	3	0.069	7.895	y	3	36.511	105.988	4.296	22.053	1.136	H1-1b
13	M13	L2x2x3	0.011	7.981	5	0.007	7.981	y	5	1.79	21.617	0.515	0.678	1	H2-1*
14	M14	L2x2x3	0.002	7.981	17	0.01	7.981	y	9	1.79	21.617	0.515	0.678	1	H2-1*
15	M15	C8X11.5	0.002	6	5	0.043	6	y	19	37.983	100.898	3.098	17.546	1	H1-1b*
16	M16	C8X11.5	0	6	5	0.043	6	y	19	37.983	100.898	3.098	17.546	1	H1-1b*

Load Combinations

	Description	Solve	P-Delta	BLC	Factor	BLC	Factor	BLC	Factor
1	DL		Y	DL	1				
2									
3	DL + LL		Y	DL	1	LL	1		
4									
5	DL + LL + SWAYZ		Y	DL	1	OL1	0.75	LL	0.75
6									
7	DL + LL + SWAYZ		Y	DL	1	WLX	0.45	LL	0.75
8									
9	DL + WLFTB		Y	DL	1	WLX	0.6		
10			Y	DL	0.6	WLX	0.6		
11									
12	DL + LL - WLFTB		Y	DL	1	WLX	-0.45	LL	0.75
13									
14	DL - WLFTB		Y	DL	1	WLX	-0.6		
15			Y	DL	0.6	WLX	-0.6		
16									
17	DL + LL + WLUP		Y	DL	1	WL-X	0.45	LL	0.75
18									
19	DL + WLUP		Y	DL	1	WL-X	0.6		
20			Y	DL	0.6	WL-X	0.6		
21									
22	DL	Yes	Y	DL	1				
23	LL	Yes	Y	LL	1				
24	SWAY	Yes	Y	OL1	1				
25	WLFTB	Yes	Y	WLX	1				
26	WLUP	Yes	Y	WL-X	1				

Node Reactions

	LC	Node Label	X [k]	Y [k]	Z [k]	MX [k-ft]	MY [k-ft]	MZ [k-ft]
1	22	N2	0	0.759	0	NC	0	0
2	22	N4	0	1.586	0	NC	0	0
3	22	N9	0	0.759	0	NC	0	0
4	22	N10	0	1.586	0	NC	0	0
5	22	Totals:	0	4.69	0			
6	22	COG (ft):	X: 16.487	Y: 12.358	Z: -3			
7	23	N2	0	8.165	0	NC	0	0
8	23	N4	0	9.045	0	NC	0	0
9	23	N9	0	8.165	0	NC	0	0
10	23	N10	0	9.045	0	NC	0	0
11	23	Totals:	0	34.42	0			
12	23	COG (ft):	X: 14.077	Y: 10.413	Z: -3			
13	24	N2	0	-0.001	-1.144	NC	0	0
14	24	N4	0	-0.005	-0.418	NC	0	0
15	24	N9	0	0.001	-1.144	NC	0	0
16	24	N10	0	0.005	-0.426	NC	0	0
17	24	Totals:	0	0	-3.132			
18	24	COG (ft):	NC	NC	NC			
19	25	N2	-6.296	-6.075	0.004	NC	0	0
20	25	N4	0	6.118	0.049	NC	0	0
21	25	N9	-3.985	-2.383	-0.003	NC	0	0
22	25	N10	0	2.341	-0.051	NC	0	0
23	25	Totals:	-10.281	0	0			
24	25	COG (ft):	NC	NC	NC			
25	26	N2	6.068	3.679	0.001	NC	0	0



Company :
 Designer :
 Job Number :
 Model Name :

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 Checked By : _____

Node Reactions (Continued)

LC	Node Label	X [k]	Y [k]	Z [k]	MX [k-ft]	MY [k-ft]	MZ [k-ft]	
26	26	N4	0	-8.037	0.057	NC	0	0
27	26	N9	3.758	-0.002	-0.003	NC	0	0
28	26	N10	0	-4.424	-0.054	NC	0	0
29	26	Totals:	9.826	-8.784	0			
30	26	COG (ft):	X: 16.538	Y: 9.142	Z: -3			

Horizontal Beams -

$V_{\rightarrow WL1} =$ 6.296 kips per stringer (from Risa Reactions @ thrust Row)

$V_{\rightarrow WL2} =$ 3.985 kips per stringer (from Risa Reactions @ thrust Row)

$V_{\rightarrow WL3} =$ 2.393 kips per stringer (from Risa Reactions @ thrust Row)

@ PB

Row	W shape	I_{y-y}	ratio of lateral thrust to W shape	portion of $V_{\rightarrow WL1}$ to W shape	portion of $V_{\rightarrow WL2}$ to W shape
A	W14x43	45.20 in ⁴	0.500	3.15 kips	1.99 kips
B	W14x43	45.20 in ⁴	0.500	3.15 kips	1.99 kips
		0.00 in ⁴	0.000	0.00 kips	0.00 kips
		0.00 in ⁴	0.000	0.00 kips	0.00 kips
		$\Sigma I_{y-y} = 90.40$ in ⁴			

NOT @ PB

Row	W shape	I_{y-y}	ratio of lateral thrust to W shape	portion of $V_{\rightarrow WL3}$ to W shape
A	W14x30	19.60 in ⁴	0.500	1.20 kips
B	W14x30	19.60 in ⁴	0.500	1.20 kips
		0.00 in ⁴	0.000	0.00 kips
		0.00 in ⁴	0.000	0.00 kips
		$\Sigma I_{y-y} = 39.20$ in ⁴		



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By:

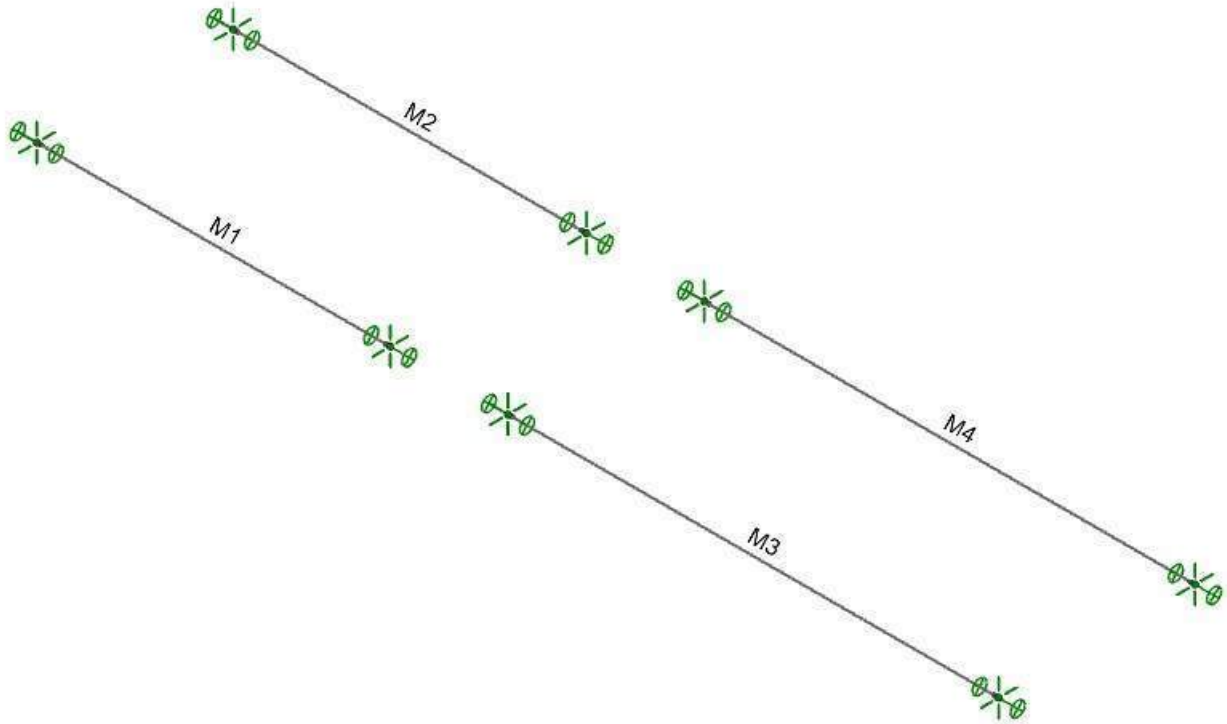
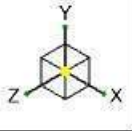
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38

Of:



BRA

SK-4

Apr 15, 2022

HORIZ BEAMS A B.r3d

Model Settings

Solution

Members

Number of Reported Sections	5
Number of Internal Sections	100
Member Area Load Mesh Size (in ²)	144
Consider Shear Deformation	Yes
Consider Torsional Warping	Yes

Wall Panels

Approximate Mesh Size (in)	12
Transfer Forces Between Intersecting Wood Walls	Yes
Increase Wood Wall Nailing Capacity for Wind Loads	Yes
Include P-Delta for Walls	Yes
Optimize Masonry and Wood Walls	Yes
Maximum Number of Iterations	3

Processor Core Utilization

Single	No
Multiple (Optimum)	Yes
Maximum	No

Axis

Vertical Global Axis

Global Axis corresponding to vertical direction	Y
Convert Existing Data	Yes

Default Member Orientation

Default Global Plane for z-axis	XZ
---------------------------------	----

Plate Axis

Plate Local Axis Orientation	Nodal
------------------------------	-------

Codes

Hot Rolled Steel	AISC 14th (360-10): ASD
Stiffness Adjustment	Yes (Iterative)
Notional Annex	None
Connections	AISC 14th (360-10): ASD
Cold Formed Steel	None
Stiffness Adjustment	Yes (Iterative)
Wood	None
Temperature	< 100F
Concrete	None
Masonry	None
Aluminum	None
Structure Type	Building
Stiffness Adjustment	Yes (Iterative)
Stainless	None
Stiffness Adjustment	Yes (Iterative)

Concrete

Compression Stress Block	Rectangular Stress Block
Analyze using Cracked Sections	Yes
Leave room for horizontal rebar splices (2*d bar spacing)	No

Model Settings (Continued)

List forces which were ignored for design in the Detail Report	Yes
--	-----

Rebar

Column Min Steel	1
Column Max Steel	8
Rebar Material Spec	ASTM A615
Warn if beam-column framing arrangement is not understood	No

Shear Reinforcement

Number of Shear Regions	4
Region 2 & 3 Spacing Increase Increment (in)	4

Seismic

RISA-3D Seismic Load Options

Code	ASCE 7-10
Risk Category	I or II
Drift Cat	Other
Base Elevation (ft)	
Include the weight of the structure in base shear calcs	Yes

Site Parameters

S_1 (g)	0
SD_1 (g)	1
SD_s (g)	0
T_L (sec)	-1

Structure Characteristics

T Z (sec)	
T X (sec)	
$C_d X$	0.035
$C_{Exp. Z}$	0
$C_{Exp. X}$	0
R Z	1
R X	1
$\Omega_0 Z$	1
$\Omega_0 X$	1
$C_d Z$	1
$C_d X$	1
ρZ	1
ρX	1

Hot Rolled Steel Properties

	Label	E [ksi]	G [ksi]	Nu	Therm. Coeff. [$1e^{-5}F^{-1}$]	Density [k/ft ³]	Yield [ksi]	Ry	Fu [ksi]	Rt
1	A36 Gr.36	29000	11154	0.3	0.65	0.49	36	1.5	58	1.2
2	A572 Gr.50	29000	11154	0.3	0.65	0.49	50	1.1	58	1.2
3	A992	29000	11154	0.3	0.65	0.49	50	1.1	58	1.2
4	A500 Gr.42	29000	11154	0.3	0.65	0.49	42	1.3	58	1.1
5	A500 Gr.46	29000	11154	0.3	0.65	0.49	46	1.2	58	1.1

Hot Rolled Steel Section Sets

	Label	Shape	Type	Design List	Material	Design Rule	Area [in ²]	Iyy [in ⁴]	Izz [in ⁴]	J [in ⁴]
1	HORIZ ROW A	W14X30	Beam	Wide Flange	A572 Gr.50	Typical	8.85	19.6	291	0.38
2	HORIZ ROW B	W14X30	Beam	Wide Flange	A572 Gr.50	Typical	8.85	19.6	291	0.38
3	HORIZ ROWA@PB	W14X43	Beam	Wide Flange	A572 Gr.50	Typical	12.6	45.2	428	1.05
4	HORIZ ROWB@PB	W14X43	Beam	Wide Flange	A572 Gr.50	Typical	12.6	45.2	428	1.05

Node Coordinates

	Label	X [ft]	Y [ft]	Z [ft]	Detach From Diaphragm
1	N1	0	0	0	
2	N2	18	0	0	
3	N3	0	0	-10	
4	N4	18	0	-10	
5	N5	24	0	0	
6	N6	49	0	0	
7	N7	24	0	-10	
8	N8	49	0	-10	

Node Boundary Conditions

	Node Label	X [k/in]	Y [k/in]	Z [k/in]	X Rot [k-ft/rad]
1	N1	Reaction	Reaction	Reaction	Fixed
2	N2		Reaction	Reaction	Fixed
3	N3	Reaction	Reaction	Reaction	Fixed
4	N4		Reaction	Reaction	Fixed
5	N5	Reaction	Reaction	Reaction	Fixed
6	N6		Reaction	Reaction	Fixed
7	N7	Reaction	Reaction	Reaction	Fixed
8	N8		Reaction	Reaction	Fixed

Member Primary Data

	Label	I Node	J Node	Section/Shape	Type	Design List	Material	Design Rule
1	M1	N1	N2	HORIZ ROW A	Beam	Wide Flange	A572 Gr.50	Typical
2	M2	N3	N4	HORIZ ROW B	Beam	Wide Flange	A572 Gr.50	Typical
3	M3	N5	N6	HORIZ ROWA@PB	Beam	Wide Flange	A572 Gr.50	Typical
4	M4	N7	N8	HORIZ ROWB@PB	Beam	Wide Flange	A572 Gr.50	Typical

Hot Rolled Steel Design Parameters

	Label	Shape	Length [ft]	Lb y-y [ft]	Lcomp top [ft]	Lcomp bot [ft]	K y-y	K z-z	Function
1	M1	HORIZ ROW A	18	6	Lbyy	6	1	1	Lateral
2	M2	HORIZ ROW B	18	6	Lbyy	6	1	1	Lateral
3	M3	HORIZ ROWA@PB	25	6	Lbyy	6	1	1	Lateral
4	M4	HORIZ ROWB@PB	25	6	Lbyy	6	1	1	Lateral

Node Loads and Enforced Displacements (BLC 1 : DEAD LOADS)

	Node Label	L, D, M	Direction	Magnitude [(k, k-ft), (in, rad), (k*s ² /ft, k*s ² *ft)]
1	N1	L	Y	-0.825
2	N2	L	Y	-0.825
3	N3	L	Y	-0.775
4	N4	L	Y	-0.775
5	N5	L	Y	-0.759
6	N6	L	Y	-0.759
7	N7	L	Y	-1.586
8	N8	L	Y	-1.586

Node Loads and Enforced Displacements (BLC 2 : LIVE LOADS)

	Node Label	L, D, M	Direction	Magnitude [(k, k-ft), (in, rad), (k*s ² /ft, k*s ² *ft)]
1	N1	L	Y	-8.253
2	N2	L	Y	-8.253
3	N3	L	Y	-7.747
4	N4	L	Y	-7.747
5	N5	L	Y	-8.165
6	N6	L	Y	-8.165
7	N7	L	Y	-9.045
8	N8	L	Y	-9.045

Node Loads and Enforced Displacements (BLC 3 : WIND LOADS)

	Node Label	L, D, M	Direction	Magnitude [(k, k-ft), (in, rad), (k*s ² /ft, k*s ² *ft)]
1	N1	L	Y	1.325
2	N1	L	Z	1.197
3	N2	L	Y	1.325
4	N2	L	Z	1.197
5	N3	L	Y	3.067
6	N3	L	Z	1.197
7	N4	L	Z	1.197
8	N4	L	Y	3.067
9	N5	L	Z	3.149
10	N5	L	Y	6.087
11	N6	L	Z	3.149
12	N6	L	Y	6.087
13	N7	L	Y	8.071
14	N7	L	Z	3.149
15	N8	L	Z	3.149
16	N8	L	Y	8.071

Member Point Loads (BLC 1 : DEAD LOADS)

	Member Label	Direction	Magnitude [k, k-ft]	Location [(ft, %)]
1	M1	Y	-0.825	6
2	M1	Y	-0.825	12
3	M2	Y	-0.775	6
4	M2	Y	-0.775	12
5	M3	Y	-0.759	18
6	M3	Y	-0.759	6
7	M3	Y	-0.759	12
8	M4	Y	-1.586	18
9	M4	Y	-1.586	12
10	M4	Y	-1.586	6

Member Point Loads (BLC 2 : LIVE LOADS)

	Member Label	Direction	Magnitude [k, k-ft]	Location [(ft, %)]
1	M1	Y	-8.253	12
2	M1	Y	-8.253	6
3	M2	Y	-7.747	6
4	M2	Y	-7.747	12
5	M3	Y	-8.165	12
6	M3	Y	-8.165	6
7	M3	Y	-8.165	18
8	M4	Y	-9.045	6
9	M4	Y	-9.045	12
10	M4	Y	-9.045	18

Member Point Loads (BLC 3 : WIND LOADS)

	Member Label	Direction	Magnitude [k, k-ft]	Location [(ft, %)]
1	M1	Z	1.197	12
2	M1	Z	1.197	6
3	M1	Y	1.325	6
4	M1	Y	1.325	12
5	M2	Z	1.197	12
6	M2	Z	1.197	6
7	M2	Y	3.067	12
8	M2	Y	3.067	6
9	M3	Y	2.383	6
10	M3	Y	2.383	12
11	M3	Y	2.383	18
12	M3	Z	1.99	6
13	M3	Z	1.99	12
14	M3	Z	1.99	18
15	M4	Y	4.424	6
16	M4	Y	4.424	12
17	M4	Y	4.424	18
18	M4	Z	1.99	6
19	M4	Z	1.99	12
20	M4	Z	1.99	18

Basic Load Cases

	BLC Description	Category	Y Gravity	Nodal	Point
1	DEAD LOADS	DL	-1	8	10
2	LIVE LOADS	LL		8	10
3	WIND LOADS	WL		16	20

Load Combinations

	Description	Solve	P-Delta	BLC	Factor	BLC	Factor	BLC	Factor
1	DL + LL	Yes	Y	DL	1	LL	1		
2	DL+0.75LL+0.75WL	Yes	Y	DL	1	LL	0.75	WL	0.45
3	0.6DL+1.0WL	Yes	Y	DL	0.6	WL	0.6		
4	1.0DL+1.0WL	Yes	Y	DL	1	WL	0.6		

Envelope Node Reactions

Node Label	X [k]	LC	Y [k]	LC	Z [k]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC		
1	N1	max	0	4	18.42	1	0	1	NC	NC	0	4	0	4
2		min	0	1	-0.442	3	-1.436	3	NC	NC	0	1	0	1
3	N2	max	0	4	18.42	1	0	1	NC	NC	0	4	0	4
4		min	0	1	-0.442	3	-1.436	3	NC	NC	0	1	0	1
5	N3	max	0	4	17.308	1	0	1	NC	NC	0	4	0	4
6		min	0	1	-2.592	3	-1.436	3	NC	NC	0	1	0	1
7	N4	max	0	4	17.308	1	0	1	NC	NC	0	4	0	4
8		min	0	1	-2.592	3	-1.436	3	NC	NC	0	1	0	1
9	N5	max	0	4	23.371	1	0	1	NC	NC	0	4	0	4
10		min	0	1	-4.402	3	-3.752	3	NC	NC	0	1	0	1
11	N6	max	0	4	22.3	1	0	1	NC	NC	0	4	0	4
12		min	0	1	-4.285	3	-3.609	3	NC	NC	0	1	0	1
13	N7	max	0	4	27.741	1	0	1	NC	NC	0	4	0	4
14		min	0	1	-6.232	3	-3.752	3	NC	NC	0	1	0	1
15	N8	max	0	4	26.465	1	0	1	NC	NC	0	4	0	4
16		min	0	1	-6.028	3	-3.609	3	NC	NC	0	1	0	1
17	Totals:	max	0	4	171.33	1	0	1						
18		min	0	1	-27.015	3	-20.465	3						

Envelope AISC 14TH (360-10): ASD Member Steel Code Checks

Member	Shape	Code Check	Loc[ft]	LC	Shear	Check	Loc[ft]	Dir	LC	Pnc/om [k]	Pnt/om [k]	Mny/om [k-ft]	Mnzz/om [k-ft]	Cb	Eqn
1	M1	W14X30	0.491	8.75	2	0.125	17.5	y	1	135.198	264.97	22.43	114.57	1	H1-1b
2	M2	W14X30	0.457	8.75	1	0.118	17.5	y	1	135.198	264.97	22.43	114.57	1	H1-1b
3	M3	W14X43	0.708	11.74	2	0.173	0	y	1	217.47	377.246	43.164	173.653	1	H1-1b
4	M4	W14X43	0.798	11.74	1	0.205	0	y	1	217.47	377.246	43.164	173.653	1	H1-1b

ROOF FRAMING

ZEE PURLINS

@ 3'-0" BAY O.C. SPAN = 18'-0" MAX

$$W_{DL} = 10 \text{ PSF} (3') = 30 \text{ PLF}$$

$$W_{Lr} = 20 \text{ PSF} (3') = 60 \text{ PLF}$$

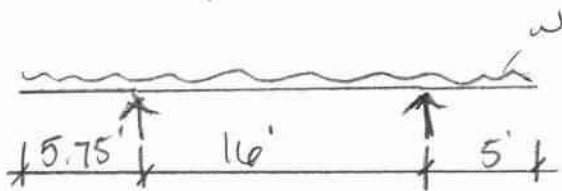
$$\Sigma W = 90 \text{ PLF}$$

\therefore USE $\angle 8 \times 2\frac{1}{2} \times 14 \text{ GA}$

$$GF = 151 \text{ PLF} \checkmark$$

ROOF BEAMS

@ 18' BAY O.C.



$$W_{DL} = 15 \text{ PSF} (18') = 270 \text{ PLF}$$

$$W_{Lr} = 20 \text{ PSF} (18') = 360 \text{ PLF}$$

$$W_{WIND} = 26.37 \text{ PSF} (18') = 474.66 \text{ PLF}$$

\therefore USE $W12 \times 19$



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46

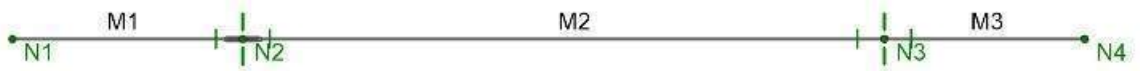
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FLEXOSPAN - CEE AND ZEE LOAD TABLES

Allowable Uniform Loads in Pounds Per Lineal Foot

CEE		Simple Span						ZEE						3 or More Spans, Std. Lap					
		16 Gauge		14 Gauge		12 Gauge		16 Gauge		14 Gauge		12 Gauge		16 Gauge		14 Gauge		12 Gauge	
Section	Bay	2 1/2" Fl.	3 1/2" Fl.	2 1/2" Fl.	3 1/2" Fl.	2 1/2" Fl.	3 1/2" Fl.	2 1/2" Fl.	3 1/2" Fl.	2 1/2" Fl.	3 1/2" Fl.	2 1/2" Fl.	3 1/2" Fl.	2 1/2" Fl.	3 1/2" Fl.	2 1/2" Fl.	3 1/2" Fl.	2 1/2" Fl.	3 1/2" Fl.
6" Web	10 ft	251	-	331	-	480	-	10 ft	254	-	331	-	489	-	-	-	-	-	-
	12 ft	174	-	230	-	333	-	12 ft	126	-	230	-	346	-	-	-	-	-	-
	14 ft	128	-	169	-	244	-	14 ft	129	-	169	-	254	-	-	-	-	-	-
	15 ft	111	-	147	-	213	-	15 ft	113	-	147	-	221	-	235	-	357	-	-
	18 ft	77	-	102	-	148	-	18 ft	78	-	102	-	154	-	176	-	238	-	-
	20 ft	62	-	82	-	120	-	20 ft	63	-	82	-	124	-	94	-	124	-	-
	22 ft	51	-	68	-	99	-	22 ft	52	-	68	-	103	-	76	-	101	-	-
	24 ft	43	-	57	-	83	-	24 ft	44	-	57	-	86	-	63	-	84	-	-
	25 ft	40	-	53	-	76	-	25 ft	40	-	53	-	79	-	58	-	76	-	-
	28 ft	32	-	42	-	61	-	28 ft	32	-	42	-	63	-	46	-	60	-	91
8" Web	12 ft	260	269	341	365	493	545	12 ft	260	265	340	364	510	545	-	-	-	-	-
	14 ft	191	198	250	268	362	400	14 ft	191	195	250	267	374	401	-	-	-	-	-
	15 ft	166	172	218	233	315	349	15 ft	166	169	218	233	326	349	-	-	-	-	-
	18 ft	115	119	151	162	219	242	18 ft	115	117	151	161	226	242	156	158	222	235	345
	20 ft	93	97	122	131	177	196	20 ft	93	95	122	131	183	196	127	129	178	188	275
	22 ft	77	80	101	108	146	162	22 ft	77	78	101	108	151	162	105	107	145	154	223
	24 ft	65	67	85	91	123	136	24 ft	65	66	85	91	127	136	88	90	121	129	185
	25 ft	60	62	78	84	113	125	25 ft	59	61	78	83	117	125	81	83	111	118	170
	28 ft	47	49	62	67	90	100	28 ft	47	48	62	66	93	100	65	66	93	133	142
	30 ft	41	43	54	58	78	87	30 ft	41	42	54	58	81	87	56	57	76	81	115
10" Web	20 ft	115	-	168	173	243	266	20 ft	115	119	168	-	250	266	131	133	217	-	365
	22 ft	95	-	139	143	200	220	22 ft	80	82	116	-	173	185	96	97	154	-	248
	24 ft	80	-	116	120	168	185	24 ft	74	76	107	-	160	170	89	91	142	-	228
	25 ft	74	-	107	111	155	170	25 ft	59	60	85	-	127	136	72	74	114	-	179
	28 ft	59	-	85	88	124	136	28 ft	51	52	74	-	111	118	64	65	99	-	155
	30 ft	51	-	74	77	108	118	30 ft	45	46	65	-	97	104	56	58	87	-	135
	32 ft	45	-	65	67	94	104	32 ft	37	38	54	-	81	87	48	49	73	-	112
	34 ft	40	-	58	60	84	92	34 ft	32	33	46	-	69	73	41	42	61	-	94
	35 ft	37	-	54	56	79	87	35 ft	32	33	46	-	69	73	41	42	61	-	94
	38 ft	32	-	46	48	67	73	38 ft	20 ft	-	183	203	301	345	345	210	220	418	463
12" Web	20 ft	-	-	185	206	293	344	20 ft	-	-	127	141	209	239	-	-	153	162	289
	24 ft	-	-	128	143	203	239	24 ft	-	-	117	130	192	220	-	-	142	151	265
	25 ft	-	-	118	132	187	220	25 ft	-	-	93	103	153	176	-	-	116	124	210
	28 ft	-	-	94	105	149	175	28 ft	-	-	81	90	133	153	-	-	102	109	183
	30 ft	-	-	82	91	130	153	30 ft	-	-	71	79	117	134	-	-	90	97	160
	32 ft	-	-	72	80	114	134	32 ft	-	-	59	66	98	112	-	-	76	82	133
	34 ft	-	-	64	71	101	119	34 ft	-	-	53	59	88	100	-	-	68	74	119
	35 ft	-	-	60	67	95	112	35 ft	-	-	45	50	75	86	-	-	59	64	101
	38 ft	-	-	51	57	81	95	38 ft	-	-	46	51	73	86	-	-	59	64	101
	40 ft	-	-	46	51	73	86	40 ft	-	-	46	51	73	86	-	-	59	64	101

Notes: 1. The weight of the section has not been subtracted from these values. 2. Both flanges of member must be fully braced. 3. These loads are based on the transfer of the support loads directly to the web of the section by the use of clips or plates. For flanges bearing directly on structural, contact factory for section selection. 4. See back page for weights per lineal foot of members shown here. 5. Loads shown are stress governing. When deflection limits are specified, contact factory. 6. These sample calculations are very basic. Many different variables can affect loading. For instance: drift loading, building height, geographic location, etc. Please consult Flexospan if special conditions exist. 7. The selection of sections for your application is subject to final approval by your design professional. 8. Capacity values have been calculated in accordance with the AISI 2001 design manual. 9. Values shown in the load tables for three or more spans are based on uniform bay spacings. If non-uniform bay spacings exist, contact factory. UNCONTROLLED COPY



SK-5

Apr 15, 2022

ROOFBEAM.r3d

Model Settings

Solution

Members

Number of Reported Sections	5
Number of Internal Sections	100
Member Area Load Mesh Size (in ²)	144
Consider Shear Deformation	Yes
Consider Torsional Warping	Yes

Wall Panels

Approximate Mesh Size (in)	12
Transfer Forces Between Intersecting Wood Walls	Yes
Increase Wood Wall Nailing Capacity for Wind Loads	Yes
Include P-Delta for Walls	Yes
Optimize Masonry and Wood Walls	Yes
Maximum Number of Iterations	3

Processor Core Utilization

Single	No
Multiple (Optimum)	Yes
Maximum	No

Axis

Vertical Global Axis

Global Axis corresponding to vertical direction	Y
Convert Existing Data	Yes

Default Member Orientation

Default Global Plane for z-axis	XZ
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Plate Axis

Plate Local Axis Orientation	Nodal
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Codes

Hot Rolled Steel	AISC 14th (360-10): ASD
Stiffness Adjustment	Yes (Iterative)
Notional Annex	None
Connections	AISC 14th (360-10): ASD
Cold Formed Steel	None
Stiffness Adjustment	Yes (Iterative)
Wood	None
Temperature	< 100F
Concrete	None
Masonry	None
Aluminum	None
Structure Type	Building
Stiffness Adjustment	Yes (Iterative)
Stainless	None
Stiffness Adjustment	Yes (Iterative)

Concrete

Compression Stress Block	Rectangular Stress Block
Analyze using Cracked Sections	Yes
Leave room for horizontal rebar splices (2*d bar spacing)	No

Model Settings (Continued)

List forces which were ignored for design in the Detail Report	Yes
--	-----

Rebar

Column Min Steel	1
Column Max Steel	8
Rebar Material Spec	ASTM A615
Warn if beam-column framing arrangement is not understood	No

Shear Reinforcement

Number of Shear Regions	4
Region 2 & 3 Spacing Increase Increment (in)	4

Seismic

RISA-3D Seismic Load Options

Code	ASCE 7-16
Risk Category	I or II
Drift Cat	Other
Base Elevation (ft)	
Include the weight of the structure in base shear calcs	Yes

Site Parameters

S_1 (g)	1
SD_1 (g)	1
SD_s (g)	1
T_1 (sec)	5

Structure Characteristics

T Z (sec)	
T X (sec)	
$C_d X$	0.02
$C_{Exp. Z}$	0.75
$C_{Exp. X}$	0.75
R Z	3
R X	3
$\Omega_0 Z$	1
$\Omega_0 X$	1
$C_d Z$	1
$C_d X$	1
ρZ	1
ρX	1

Hot Rolled Steel Properties

	Label	E [ksi]	G [ksi]	Nu	Therm. Coeff. [$1e^{-5}F^{-1}$]	Density [k/ft ³]	Yield [ksi]	Ry	Fu [ksi]	Rt
1	A36 Gr.36	29000	11154	0.3	0.65	0.49	36	1.5	58	1.2
2	A572 Gr.50	29000	11154	0.3	0.65	0.49	50	1.1	65	1.1
3	A992	29000	11154	0.3	0.65	0.49	50	1.1	65	1.1
4	A500 Gr.42	29000	11154	0.3	0.65	0.49	42	1.4	58	1.3
5	A500 Gr.46	29000	11154	0.3	0.65	0.49	46	1.4	58	1.3

Hot Rolled Steel Section Sets

	Label	Shape	Type	Design List	Material	Design Rule	Area [in ²]	Iyy [in ⁴]	Izz [in ⁴]	J [in ⁴]
1	ROOFBEAM	W12X19	Beam	Wide Flange	A992	Typical	5.57	3.76	130	0.18

Node Coordinates

	Label	X [ft]	Y [ft]	Z [ft]	Detach From Diaphragm
1	N1	0	0	0	
2	N2	5.75	0	0	
3	N3	21.75	0	0	
4	N4	26.75	0	0	

Node Boundary Conditions

	Node Label	X [k/in]	Y [k/in]	Z [k/in]	X Rot [k-ft/rad]
1	N2	Reaction	Reaction	Reaction	Fixed
2	N3		Reaction	Reaction	Fixed

Member Primary Data

	Label	I Node	J Node	Section/Shape	Type	Design List	Material	Design Rule
1	M1	N1	N2	ROOFBEAM	Beam	Wide Flange	A992	Typical
2	M2	N2	N3	ROOFBEAM	Beam	Wide Flange	A992	Typical
3	M3	N3	N4	ROOFBEAM	Beam	Wide Flange	A992	Typical

Hot Rolled Steel Design Parameters

	Label	Shape	Length [ft]	Lb y-y [ft]	Lcomp top [ft]	Lcomp bot [ft]	K y-y	K z-z	Function
1	M1	ROOFBEAM	5.75	3	3	6.33	2.1	2.1	Lateral
2	M2	ROOFBEAM	16	3	3	6.25	1	1	Lateral
3	M3	ROOFBEAM	5	3	3		2.1	2.1	Lateral

Member Distributed Loads (BLC 1 : DEAD LOADS)

	Member Label	Direction	Start Magnitude [k/ft, F, ksf, k-ft/ft]	End Magnitude [k/ft, F, ksf, k-ft/ft]	Start Location [(ft, %)]	End Location [(ft, %)]
1	M1	Y	-0.27	-0.27	0	%100
2	M2	Y	-0.27	-0.27	0	%100
3	M3	Y	-0.27	-0.27	0	%100

Member Distributed Loads (BLC 2 : LIVE LOADS(FULL))

	Member Label	Direction	Start Magnitude [k/ft, F, ksf, k-ft/ft]	End Magnitude [k/ft, F, ksf, k-ft/ft]	Start Location [(ft, %)]	End Location [(ft, %)]
1	M1	Y	-0.36	-0.36	0	%100
2	M2	Y	-0.36	-0.36	0	%100
3	M3	Y	-0.36	-0.36	0	%100

Member Distributed Loads (BLC 3 : LIVE LOADS(ON/OFF))

Member Label	Direction	Start Magnitude [k/ft, F, ksf, k-ft/ft]	End Magnitude [k/ft, F, ksf, k-ft/ft]	Start Location [(ft, %)]	End Location [(ft, %)]
1 M1	Y	-0.36	-0.36	0	%100
2 M3	Y	-0.36	-0.36	0	%100

Member Distributed Loads (BLC 4 : LIVE LOADS(OFF/ON))

Member Label	Direction	Start Magnitude [k/ft, F, ksf, k-ft/ft]	End Magnitude [k/ft, F, ksf, k-ft/ft]	Start Location [(ft, %)]	End Location [(ft, %)]
1 M2	Y	-0.36	-0.36	0	%100

Member Distributed Loads (BLC 5 : WIND UPLIFT LOADS)

Member Label	Direction	Start Magnitude [k/ft, F, ksf, k-ft/ft]	End Magnitude [k/ft, F, ksf, k-ft/ft]	Start Location [(ft, %)]	End Location [(ft, %)]
1 M1	Y	0.475	0.475	0	%100
2 M2	Y	0.475	0.475	0	%100
3 M3	Y	0.475	0.475	0	%100

Basic Load Cases

	BLC Description	Category	Distributed
1	DEAD LOADS	None	3
2	LIVE LOADS(FULL)	None	3
3	LIVE LOADS(ON/OFF)	None	2
4	LIVE LOADS(OFF/ON)	None	1
5	WIND UPLIFT LOADS	None	3

Load Combinations

	Description	Solve	P-Delta	BLC	Factor	BLC	Factor
1	DL+LL(FULL)	Yes	Y	1	1	2	1
2	DL+LL(ON/OFF)	Yes	Y	1	1	3	1
3	DL+LL(OFF/ON)	Yes	Y	1	1	4	1
4	0.6DL+WLUP	Yes	Y	1	0.6	5	0.6
5							
6	DL		Y	1	1		
7	LL		Y	2	1		
8	WLUP		Y	5	1		

Envelope Node Reactions

Node Label		X [k]	LC	Y [k]	LC	Z [k]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1 N2	max	0	4	8.296	1	0	4	NC	NC	0	4	0	4
2	min	0	1	-1.62	4	0	1	NC	NC	0	1	0	1
3 N3	max	0	4	8.031	1	0	4	NC	NC	0	4	0	4
4	min	0	1	-1.568	4	0	1	NC	NC	0	1	0	1
5 Totals:	max	0	4	16.327	1	0	4						
6	min	0	1	-3.188	4	0	1						

Envelope AISC 14TH (360-10): ASD Member Steel Code Checks

Member	Shape	Code Check	Loc[ft]	LC	Shear Check	Loc[ft]	Dir	LC	Pnc/om [k]	Pnt/om [k]	Mnyy/om [k-ft]	Mnzz/om [k-ft]	Cb	Eqn
1 M1	W12X19	0.191	5.333	2	0.059	5.333	y	2	89.697	166.766	7.435	46.981	1	H1-1b
2 M2	W12X19	0.265	7.629	3	0.087	15.583	y	3	66.47	166.766	7.435	61.208	1	H1-1b
3 M3	W12X19	0.128	0	2	0.055	0	y	1	89.697	166.766	7.435	61.627	2.326	H1-1b

Load Combinations

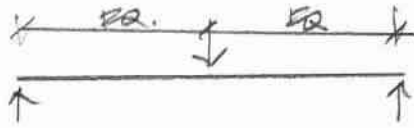
	Description	Solve	P-Delta	BLC	Factor	BLC	Factor
1	DL+LL(FULL)		Y	1	1	2	1
2	DL+LL(ON/OFF)		Y	1	1	3	1
3	DL+LL(OFF/ON)		Y	1	1	4	1
4	0.6DL+WLUP		Y	1	0.6	5	0.6
5							
6	DL	Yes	Y	1	1		
7	LL	Yes	Y	2	1		
8	WLUP	Yes	Y	5	1		

Node Reactions

	LC	Node Label	X [k]	Y [k]	Z [k]	MX [k-ft]	MY [k-ft]	MZ [k-ft]
1	6	N2	0	3.556	0	NC	0	0
2	6	N3	0	3.442	0	NC	0	0
3	6	Totals:	0	6.997	0			
4	6	COG (ft):	X: 13.62	Y: 0	Z: 0			
5	7	N2	0	4.741	0	NC	0	0
6	7	N3	0	4.589	0	NC	0	0
7	7	Totals:	0	9.33	0			
8	7	COG (ft):	X: 13.62	Y: 0	Z: 0			
9	8	N2	0	-6.255	0	NC	0	0
10	8	N3	0	-6.055	0	NC	0	0
11	8	Totals:	0	-12.31	0			
12	8	COG (ft):	X: 13.62	Y: 0	Z: 0			

HEADER BEAM 1

SPAN = 36'-0"



$$P_{DL} = 3.556 \text{ k}$$
$$P_{Lr} = 4.741 \text{ k}$$
$$P_{WR} = -6.255 \text{ k}$$

∴ USE W18x46

HEADER BEAM 2

SPAN = 25'-0"



$$P_{DL} = 3.556 \text{ k} \left(\frac{12.5}{18} \right) = 2.47 \text{ k}$$
$$P_{Lr} = 4.741 \text{ k} \left(\frac{12.5}{18} \right) = 3.293 \text{ k}$$
$$P_{WR} = -6.255 \text{ k} \left(\frac{12.5}{18} \right) = 4.344 \text{ k}$$

∴ USE W18x35



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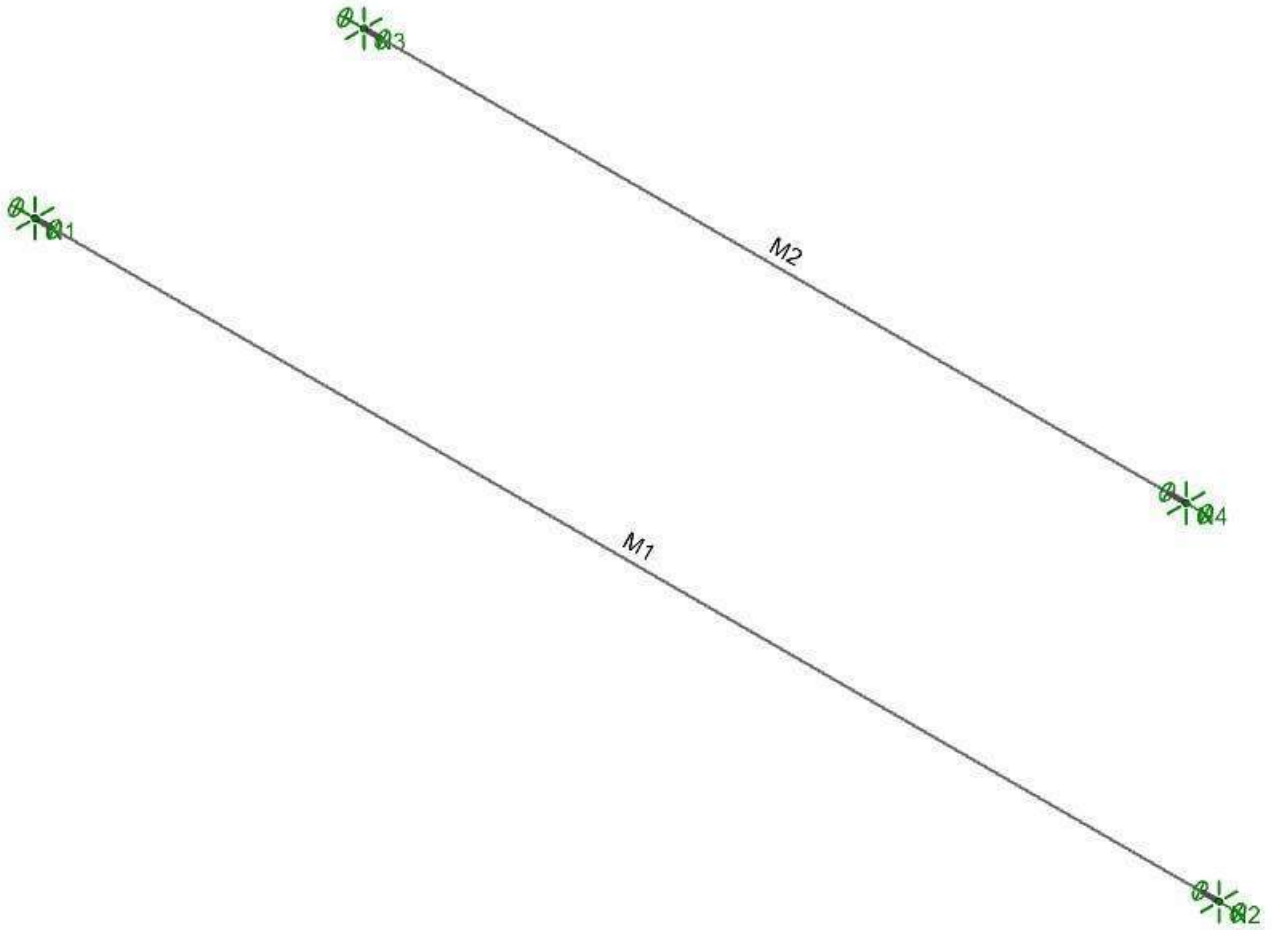
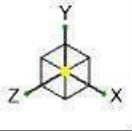
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54

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SK-6

Apr 15, 2022

ROOFHEADERBEAM.r3d

Model Settings

Solution

Members

Number of Reported Sections	5
Number of Internal Sections	100
Member Area Load Mesh Size (in ²)	144
Consider Shear Deformation	Yes
Consider Torsional Warping	Yes

Wall Panels

Approximate Mesh Size (in)	12
Transfer Forces Between Intersecting Wood Walls	Yes
Increase Wood Wall Nailing Capacity for Wind Loads	Yes
Include P-Delta for Walls	Yes
Optimize Masonry and Wood Walls	Yes
Maximum Number of Iterations	3

Processor Core Utilization

Single	No
Multiple (Optimum)	Yes
Maximum	No

Axis

Vertical Global Axis

Global Axis corresponding to vertical direction	Y
Convert Existing Data	Yes

Default Member Orientation

Default Global Plane for z-axis	XZ
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Plate Axis

Plate Local Axis Orientation	Nodal
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Codes

Hot Rolled Steel	AISC 14th (360-10): ASD
Stiffness Adjustment	Yes (Iterative)
Notional Annex	None
Connections	AISC 14th (360-10): ASD
Cold Formed Steel	AISI S100-10: ASD
Stiffness Adjustment	Yes (Iterative)
Wood	AWC NDS-12: ASD
Temperature	< 100F
Concrete	ACI 318-11
Masonry	ACI 530-11: ASD
Aluminum	AA ADM1-10: ASD
Structure Type	Building
Stiffness Adjustment	Yes (Iterative)
Stainless	None
Stiffness Adjustment	Yes (Iterative)

Concrete

Column Design

Analysis Methodology	Exact Integration Method
Parame Beta Factor	0.65

Model Settings (Continued)

Compression Stress Block	Rectangular Stress Block
Analyze using Cracked Sections	Yes
Leave room for horizontal rebar splices (2*d bar spacing)	No
List forces which were ignored for design in the Detail Report	Yes

Rebar

Column Min Steel	1
Column Max Steel	8
Rebar Material Spec	ASTM A615
Warn if beam-column framing arrangement is not understood	No

Shear Reinforcement

Number of Shear Regions	4
Region 2 & 3 Spacing Increase Increment (in)	4

Seismic

RISA-3D Seismic Load Options

Code	ASCE 7-10
Risk Category	I or II
Drift Cat	Other
Base Elevation (ft)	
Include the weight of the structure in base shear calcs	Yes

Site Parameters

S ₁ (g)	1
SD ₁ (g)	1
SD _s (g)	1
T _L (sec)	5

Structure Characteristics

T Z (sec)	
T X (sec)	
C ₁ X	0.02
C ₁ Exp. Z	0.75
C ₁ Exp. X	0.75
R Z	3
R X	3
Ω _g Z	1
Ω _g X	1
C ₂ Z	1
C ₂ X	1
ρ Z	1
ρ X	1

Hot Rolled Steel Properties

	Label	E [ksi]	G [ksi]	Nu	Therm. Coeff. [$1e^{-5}F^{-1}$]	Density [k/ft ³]	Yield [ksi]	Ry	Fu [ksi]	Rt
1	A36 Gr.36	29000	11154	0.3	0.65	0.49	36	1.5	58	1.2
2	A572 Gr.50	29000	11154	0.3	0.65	0.49	50	1.1	65	1.1
3	A992	29000	11154	0.3	0.65	0.49	50	1.1	65	1.1
4	A500 Gr.42	29000	11154	0.3	0.65	0.49	42	1.4	58	1.3
5	A500 Gr.46	29000	11154	0.3	0.65	0.49	46	1.4	58	1.3

Hot Rolled Steel Section Sets

	Label	Shape	Type	Design List	Material	Design Rule	Area [in ²]	Iyy [in ⁴]	Izz [in ⁴]	J [in ⁴]
1	ROOFHEADER1	W18X46	Beam	Wide Flange	A992	Typical	13.5	22.5	712	1.22
2	ROOFHEADER2	W18X35	Beam	Wide Flange	A992	Typical	10.3	15.3	510	0.506

Node Coordinates

	Label	X [ft]	Y [ft]	Z [ft]	Detach From Diaphragm
1	N1	0	0	0	
2	N2	36	0	0	
3	N3	0	0	-10	
4	N4	25	0	-10	

Node Boundary Conditions

	Node Label	X [k/in]	Y [k/in]	Z [k/in]	X Rot [k-ft/rad]
1	N1	Reaction	Reaction	Reaction	Fixed
2	N2		Reaction	Reaction	Fixed
3	N3	Reaction	Reaction	Reaction	Fixed
4	N4		Reaction	Reaction	Fixed

Member Primary Data

	Label	I Node	J Node	Section/Shape	Type	Design List	Material	Design Rule
1	M1	N1	N2	ROOFHEADER1	Beam	Wide Flange	A992	Typical
2	M2	N3	N4	ROOFHEADER2	Beam	Wide Flange	A992	Typical

Hot Rolled Steel Design Parameters

	Label	Shape	Length [ft]	Lb y-y [ft]	Lcomp top [ft]	Lcomp bot [ft]	K y-y	K z-z	Function
1	M1	ROOFHEADER1	36	18	18	18	1	1	Lateral
2	M2	ROOFHEADER2	25	12.5	12.5	12.5	1	1	Lateral

Member Point Loads (BLC 1 : DEAD LOADS)

	Member Label	Direction	Magnitude [k, k-ft]	Location [(ft, %)]
1	M1	Y	-3.556	18
2	M2	Y	-2.468	12.5

Member Point Loads (BLC 2 : LIVE LOADS)

	Member Label	Direction	Magnitude [k, k-ft]	Location [(ft, %)]
1	M1	Y	-4.741	18
2	M2	Y	-3.29	12.5

Member Point Loads (BLC 3 : WIND UPLIFT LOADS)

	Member Label	Direction	Magnitude [k, k-ft]	Location [(ft, %)]
1	M1	Y	6.255	18
2	M2	Y	4.341	12.5

Basic Load Cases

	BLC Description	Category	Point
1	DEAD LOADS	None	2
2	LIVE LOADS	None	2
3	WIND UPLIFT LOADS	None	2

Load Combinations

	Description	Solve	P-Delta	BLC	Factor	BLC	Factor
1	DL+LL	Yes	Y	1	1	2	1
2	0.6DL+WLUP	Yes	Y	1	0.6	3	0.6
3							
4	DL		Y	1	1		
5	LL		Y	2	1		
6	WLUP		Y	3	1		

Envelope Node Reactions

	Node Label		X [k]	LC	Y [k]	LC	Z [k]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N1	max	0	2	4.148	1	0	2	NC	NC	0	2	0	2
2		min	0	1	-0.81	2	0	1	NC	NC	0	1	0	1
3	N2	max	0	2	4.148	1	0	2	NC	NC	0	2	0	2
4		min	0	1	-0.81	2	0	1	NC	NC	0	1	0	1
5	N3	max	0	2	2.879	1	0	2	NC	NC	0	2	0	2
6		min	0	1	-0.562	2	0	1	NC	NC	0	1	0	1
7	N4	max	0	2	2.879	1	0	2	NC	NC	0	2	0	2
8		min	0	1	-0.562	2	0	1	NC	NC	0	1	0	1
9	Totals:	max	0	2	14.055	1	0	2						
10		min	0	1	-2.743	2	0	1						

Envelope AISC 14TH (360-10): ASD Member Steel Code Checks

Member	Shape	Code Check	Loc[ft]	LC	Shear	Check	Loc[ft]	Dir	LC	Pnc/om [k]	Pnt/om [k]	Mny/om [k-ft]	Mnz/om [k-ft]	Cb	Eqn
1	M1	W18X46	0.819	17.5	1	0.032	35	y	1	72.486	404.192	29.192	91.131	1	H1-1b
2	M2	W18X35	0.364	12	1	0.027	24	y	1	98.623	308.383	20.11	98.811	1	H1-1b

Load Combinations

	Description	Solve	P-Delta	BLC	Factor	BLC	Factor
1	DL+LL		Y	1	1	2	1
2	0.6DL+WLUP		Y	1	0.6	3	0.6
3							
4	DL	Yes	Y	1	1		
5	LL	Yes	Y	2	1		
6	WLUP	Yes	Y	3	1		

Node Reactions

	LC	Node Label	X [k]	Y [k]	Z [k]	MX [k-ft]	MY [k-ft]	MZ [k-ft]
1	4	N1	0	1.778	0	NC	0	0
2	4	N2	0	1.778	0	NC	0	0
3	4	N3	0	1.234	0	NC	0	0
4	4	N4	0	1.234	0	NC	0	0
5	4	Totals:	0	6.024	0			
6	4	COG (ft):	X: 15.747	Y: 0	Z: -4.097			
7	5	N1	0	2.37	0	NC	0	0
8	5	N2	0	2.37	0	NC	0	0
9	5	N3	0	1.645	0	NC	0	0
10	5	N4	0	1.645	0	NC	0	0
11	5	Totals:	0	8.031	0			
12	5	COG (ft):	X: 15.747	Y: 0	Z: -4.097			
13	6	N1	0	-3.127	0	NC	0	0
14	6	N2	0	-3.127	0	NC	0	0
15	6	N3	0	-2.17	0	NC	0	0
16	6	N4	0	-2.17	0	NC	0	0
17	6	Totals:	0	-10.596	0			
18	6	COG (ft):	X: 15.747	Y: 0	Z: -4.097			

COLUMNS

$$H = 28.0'$$

e STAND

$$P_{DL} = 6.399^k$$

$$P_U = 38.649^k$$

$$P_{WUP} = -21.106^k$$

LRFD

e ROOF

$$P_{DL} = 3.012^k$$

$$P_U = 4.015^k$$

$$P_{WUP} = -5.297^k$$

LRFD

$$\Sigma P_{DL} = 9.411^k$$

$$\Sigma P_U = 42.664^k$$

$$\Sigma P_{WUP} = -26.403^k$$

LRFD

$$T = C = 5.943^k \left(\frac{14'}{18'} \right) = 4.622^k$$

DUE TO SWAY

$$\Sigma R_{MN} \text{ DL+U+T} = 56.697^k$$

TRY HSS 8x8x1/4

$$K L/r = \frac{(1.0)(28)(12)}{3.15} = 106.67 \quad \therefore P_{allow} = 92.5^k \checkmark$$

\(\therefore\) USE HSS 8x8x1/4 \rightarrow e 'B' ROW

†

HSS 8x8x3/8 \rightarrow e 'A' ROW



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Sheet

61

Of:

WIND BRACE @ 'B' ROW

$$V_{w, \text{STAND}} = 57.11 \text{ PSF} (8' \times 9') = 4.112^k$$

$$V_{w, \text{ROOF}} = 28.77 \text{ PSF} (4' \times 26.50'/2) = 1.525^k$$

$$V_{w, \text{TOTAL}} = 5.64^k$$

ASD LEVEL

$$\text{OR } V_{w, \text{STAND}} = \frac{0.844^k}{6} (169')$$
$$= 23.773^k = 5.943^k$$

4 BAYS
BRAISED
MIN

CONTROLS

BRACES:

$$\alpha = \frac{\sqrt{14^2 + 18^2}}{18} = 1.267$$

$$F = 5.943^k (1.267) = 7.53^k$$

$$L3 \times 3 \times \frac{1}{4} \text{ TENSION ONLY} \rightarrow \frac{P_n}{\phi_t} = 31.0^k > F \therefore \text{OK}$$

USE L3x3x1/4



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Of:

62

FOUNDATIONS

$$Q_s = 1.50 \text{ KSF}$$

@ Row A

@ Non-ROOF COL.

$$R_{xH \text{ DTLU}} = 18.42^k (2) = 36.84^k$$

$$R_{xH \text{ WLP}} = 0.442^k (2) = 0.884^k$$

$$V_{WL \rightarrow} = 1.436^k (3) = 4.308^k$$

\therefore USE 5'-9" SQ. x 18" THK. w/ 20" SOIL
w/ 7 #5's E.W.

@ ROOF COL. TRA

$$R_{xH \text{ DTLU}} = 36.84^k + 4.148^k (2) = 45.136^k$$

$$R_{xH \text{ WLP}} = 0.884^k + 0.81^k (2) = 2.504^k$$

$$V_{WL \rightarrow} = 4.308^k + \underbrace{(0.6)(28.77 \text{ PSF})(4' \times 36')}_{2.486^k} = 6.794^k$$

\therefore USE 6'-3" SQ. x 18" THK. w/ 20" SOIL
w/ 8 #5's E.W.

@ ROOF WL. PB AREA

$$R_{xH \text{ DTLU}} = 41.791^k + 4.148^k + 2.879^k = 48.818^k$$

$$R_{xH \text{ WLP}} = 5.136^k + 0.81^k + 0.562^k = 6.508^k$$

$$V_{WL \rightarrow} = 3.778^k + 2.391^k (2) + 1.436^k = 9.996^k$$

\therefore USE 7'-3" SQ x 18" THK w/ 20" SOIL
w/ 9 #5's E.W.



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Of:

63

@ Row B

$$R_{XNDLTL} = 9.411^k + 42.664^k = 52.075^k$$

$$W_{L\uparrow} = 0.6(-26.403^k) = -15.844^k$$

$$V_{SWAY} = 5.943^k$$

$$T=C = 4.622^k$$

∴ USE 6'-3" SQ. x 18" THK. + 18" SOIL
w/ 8 #5's EM.

@ Row B @ PB AREA

$$R_{XNDLTL} = 45.049^k + 8.296^k = 53.345^k$$

$$W_{L\uparrow} = 8.824^k + 1.62^k = 10.444^k$$

$$V_{SWAY} = 5.943^k$$

$$T=C = 4.622^k$$

∴ USE 6'-3" SQ. x 18" THK. x 18" SOIL
w/ 8 #5's EM.



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67


SPREAD FOOTING TEMPLATE
FOR
SOUTHERN BLEACHER COMPANY

ROW B

REACTION DOWN (KIPS)	52.075
REACTION UPLIFT (KIPS)	-4.622
REACTION SHEAR (KIPS)	5.943
THICKNESS OF FOOTING (INCHES)	18
SOIL OVER FOOTING (INCHES)	18
DIAMETER OF CONCRETE PIER (IN)	24
HEIGHT OF PIER ABOVE SOIL (INCHES)	6
ALLOWABLE SOIL BEARING (PSF)	1500
ALLOWABLE FRICTION (PSF)	100 <--
SOIL UNITS WEIGHT (PCF)	110
OVERTURNING ARM (FEET)	3.5
OTM (KIP FEET)	20.8005
FOOTING WIDTH TO TRY (FT)	6.25

<u>ELEMENT</u>	<u>ARM</u>	<u>WT</u>	<u>MR</u>
UPLIFT	3.13	-4.62	-14.44
PIER	3.13	0.94	2.94
FTG	3.13	8.79	27.47
SOIL	3.13	10.28	32.13
FRICTION 1	4.17	0.94	3.91
FRICTION 2	6.25	0.94	5.86

TOTAL MR (KIP FEET)	57.863
F.S. OVERTURN	2.78 <--
TOTAL FOOTING WEIGHT (KIPS)	17.266
RESULTANT (FT)	2.147
e (FT)	0.978
FOOTING Sx (FT^3)	40.690104
P/A (KSF)	0.442
P*e/Sx	0.415
DL+LL PRESSURE (KSF)	1.333 <--
OVERTURN PRESSURE #1 (KSF)	0.857 <--
OVERTURN PRESSURE #2 (KSF)	0.027 <--
PRESSURE IF #2 IS NEGATIVE	0.858 <--



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SPREAD FOOTING TEMPLATE
FOR
SOUTHERN BLEACHER COMPANY

ROW B PB

REACTION DOWN (KIPS)	53.345
REACTION UPLIFT (KIPS)	-4.622
REACTION SHEAR (KIPS)	5.943
THICKNESS OF FOOTING (INCHES)	18
SOIL OVER FOOTING (INCHES)	18
DIAMETER OF CONCRETE PIER (IN)	24
HEIGHT OF PIER ABOVE SOIL (INCHES)	6
ALLOWABLE SOIL BEARING (PSF)	1500
ALLOWABLE FRICTION (PSF)	100 <--
SOIL UNITS WEIGHT (PCF)	110
OVERTURNING ARM (FEET)	3.5
OTM (KIP FEET)	20.8005
FOOTING WIDTH TO TRY (FT)	6.25

<u>ELEMENT</u>	<u>ARM</u>	<u>WT</u>	<u>MR</u>
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P/A (KSF)	0.442
P*e/Sx	0.415
DL+LL PRESSURE (KSF)	1.366 <--
OVERTURN PRESSURE #1 (KSF)	0.857 <--
OVERTURN PRESSURE #2 (KSF)	0.027 <--
PRESSURE IF #2 IS NEGATIVE	0.858 <--



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