

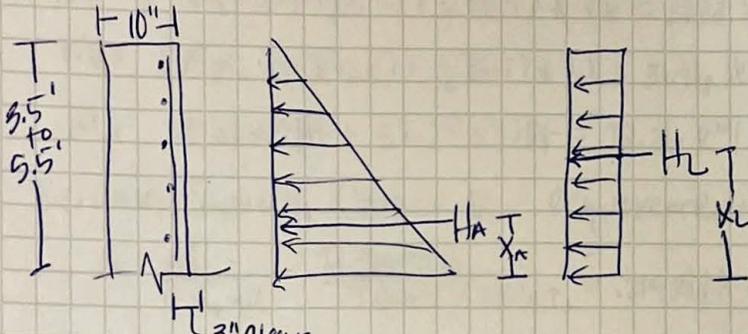


Subject: Reinforcement Schedule WBR 25028

These calculations must be on site and made available by the Permittee for all inspections.

PRPO20251253

Project Parameters:



Assume: 2' surcharge  
 $H = 1.6$  (lateral earth pressure per ASCE 7-16)  
 $f'_c = 4500$  psi  
 $f_y = 60,000$  psi (Grade 60)

$d = 10" - 3" = 7"$  (3" clear cover)

assume  $\phi = .9$  assume  $jd = 0.875d$

3.5" wall or a span wall

$M_n = \frac{1}{2}(65 \times 3.5)(3.5) \times 1.3(3.5) \times 1.6 = 743.16 \text{ lbs} = 8.92 \text{ kN}$   
 $M_q = (65 \times 2) \times 3.5 + \frac{1}{2}(3.5) \times 1.6 = 1274 \text{ lbs} = 15.29 \text{ kN}$   
 $M_u = 8.92 + 15.29 = 24.21 \text{ kN}$

Bending Capacity (vertical bar requirement)

$A_s = \frac{M_u}{\phi f_y j d} = \frac{24.21 \text{ kN}}{.9(60 \text{ ksi})(0.875)(7)} = .073 \text{ in}^2/\text{ft of wall section}$

$a = \frac{A_s f_y}{.85 f'_c b w} = \frac{(.073 \text{ in}^2)(60 \text{ ksi})}{.85(4.5 \text{ ksi})(12")}$   
 $\checkmark j = 7" - \frac{(9.5)/2}{7} = .931$

$A_s = \frac{24.21 \text{ kN}}{.9(60 \text{ ksi})(.931)(7)} = .069 \text{ in}^2/\text{ft} \Rightarrow \underline{.07 \text{ in}^2/\text{ft of wall section}}$

$a = \frac{(.069 \text{ in}^2)(60 \text{ ksi})}{.85(4.5 \text{ ksi})(12")} = \underline{.902}$   
 $\checkmark j = 7" - \frac{(1.902)/2}{7} = .936$

#4 @ 1'-6"  $\Rightarrow .2 (12/18) = \underline{.13} > .07 \text{ okay}$

$A_s \text{ Min} = .00012 \checkmark \text{ OK}$

confirm  $\phi$  in tension  $\Rightarrow \phi = .9 \quad \beta = 0.85 - \frac{0.05(f'_c - 4000)}{1000} = \frac{0.85(4500 - 4000)}{1000} = .825$

$c = \frac{a}{\beta} = \frac{.9}{.825} = 1.09" \quad \epsilon_c = 0.003 \left( \frac{d_c - c}{c} \right) = 0.003 \left( \frac{7" - 1.09"}{1.09"} \right) =$

$.016 > .005 \therefore \phi = .9$

City of Puyallup  
 Building  
 REVIEWED  
 FOR  
 COMPLIANCE  
 BSnowden  
 10/03/2025  
 11:17:45 AM

City of Puyallup  
 Development & Permitting Services  
 ISSUED PERMIT

Building	Planning
Engineering	Public Works
Fire	Traffic



Subject: Reinforcement Schedule (cont)

5.5' Wall

$$M_n = \frac{1}{2} (65 \text{ psi} \times 5.5)(5.5) + \frac{1}{3} (5.5) \times 1.4 = 2883.83 \text{ HS/ft} = 34.61 \text{ kNm/ft}$$

$$M_p = (65 \text{ psi} \times 2')(5.5) + \frac{1}{2} (5.5) \times 1.6 = 31.96 \text{ HS/ft} = 37.75 \text{ kNm/ft}$$

$$M_u = 34.61 \text{ kNm/ft} + 37.75 \text{ kNm/ft} = 72.36 \text{ kNm/ft}$$

Bending Capacity (Vertical Bar Requirement)

$$A_s = \frac{M_u}{\phi f_y d} = \frac{72.36 \text{ kNm/ft}}{.9 (60 \text{ ksi}) (.875)(7)} = .219 \text{ in}^2/\text{ft of wall}$$

$$a = \frac{A_s f_y}{0.085 f_c b_w} = \frac{.219 \text{ in}^2/\text{ft} (60 \text{ ksi})}{0.085 (4.5 \text{ ksi}) (12")} = 286" \quad v_j = \frac{7 - (286/2)}{7} = .796$$

$$A_s = \frac{M_u}{\phi f_y d} = \frac{72.36 \text{ kNm/ft}}{.9 (60 \text{ ksi}) (.796)(7)} = .210 \text{ in}^2/\text{ft}$$

$$a = \frac{A_s f_y}{0.085 f_c b_w} = \frac{.210 \text{ in}^2/\text{ft} (60 \text{ ksi})}{0.085 (4.5 \text{ ksi}) (12")} = 3.14" \quad v_j = \frac{7 - (3.14/2)}{7} = .776$$

$$A_s = \frac{M_u}{\phi f_y d} = \frac{72.63 \text{ kNm/ft}}{.9 (60 \text{ ksi}) (.776)(7)} = .217 \text{ in}^2/\text{ft of wall}$$

$$a = \frac{A_s f_y}{0.085 f_c b_w} = \frac{(.217 \text{ in}^2/\text{ft}) (60 \text{ ksi})}{0.085 (4.5) (12)} = 3.23" \quad v_j = \frac{7 - (3.23/2)}{7} = .769$$

$$A_s = \frac{M_u}{\phi f_y d} = \frac{72.63 \text{ kNm/ft}}{.9 (60 \text{ ksi}) (.769)(7)} = \boxed{.219 \text{ in}^2/\text{ft of wall}} = \boxed{.25 \text{ in}^2/\text{ft}}$$

$$a = \frac{A_s f_y}{0.085 f_c b_w} = \frac{.25 \text{ in}^2/\text{ft}}{0.085 (4.5 \text{ psi}) (12")} = \boxed{3.25"} \quad v_j = \frac{7 - (3.25/2)}{7} = .768 \checkmark$$

Vertical Bar Requirement  $\Rightarrow .25 \text{ in}^2/\text{ft}$

#4 @ MAX 8" = .2 (12/8) = .3 in<sup>2</sup>/ft OK