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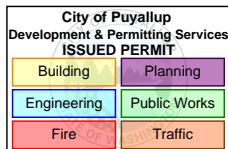
## STRUCTURAL CALCULATIONS

FOR

MARCOE'S CANDY WA STATE FAIR  
110 9<sup>TH</sup> AVE SW  
PUYALLUP, WA 98371

Calculations required to be provided by  
the Permittee on site for all Inspections

PREPARED BY  
PCS STRUCTURAL SOLUTIONS



MAY 8, 2026  
26-304

City of Puyallup  
Building  
REVIEWED  
FOR  
COMPLIANCE

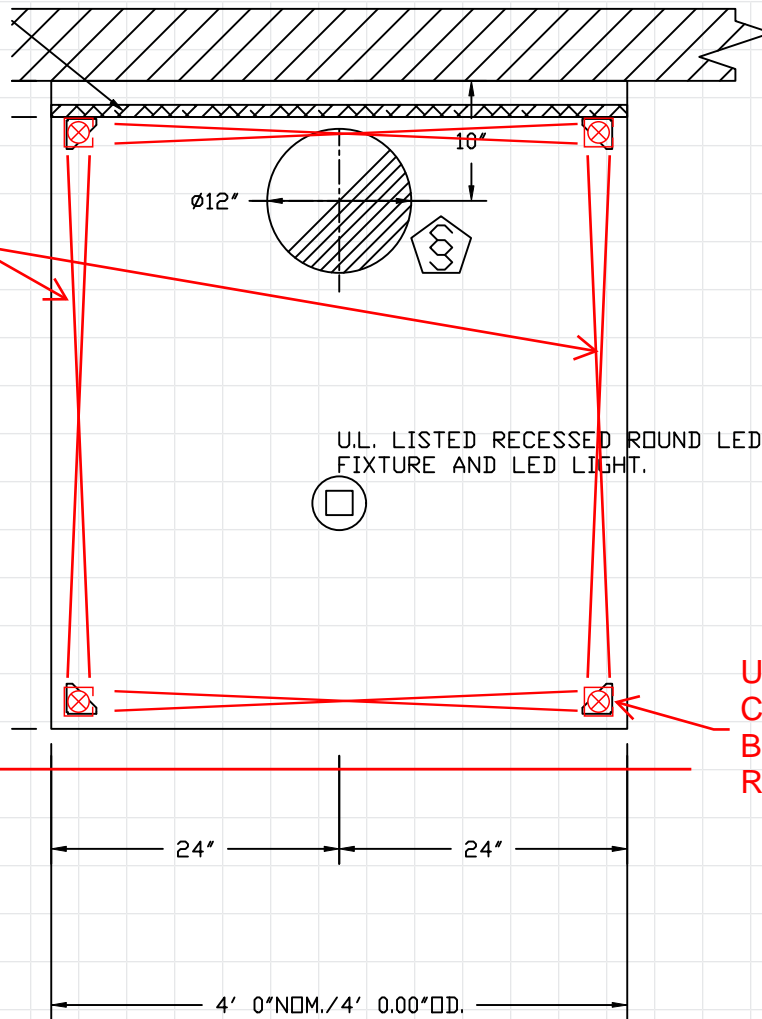
SKinnear  
06/02/2026  
9:51:01 AM



DIAGONAL "X"  
SEISMIC BRACING  
- TYP.




2  
SSK

UNISTRUT  
COMPRESSION  
BRACE & HANGING  
ROD - TYP.



PLAN VIEW - HOOD #1 (KH)  
4' 0.00" LONG 5412ESX-2

NOTES:

1.  INDICATES SEISMIC BRACE CONNECTION - SEE DETAIL 2. (2) MINIMUM REQUIRED IN EACH DIRECTION FOR EACH KITCHED HOOD ((4) TOTAL MIN. PER KITCHEN HOOD). PROVIDE UNISTRUT COMPRESSION BRACE - TYPICAL EACH END OF SEISMIC BRACE - SEE NOTE 3.
2.  INDICATES APPROXIMATE LOCATION OF GRAVITY HANGER CONNECTION - SEE DETAIL 2 FOR FURTHER INFORMATION. LOCATE HANGERS PER MANUFACTURER. FOLLOW HANGING ANGLE ASSEMBLY INSTRUCTIONS BY MANUFACTURER.
3.  INDICATES GRAVITY HANGER W/ UNISTRUT P1000T COMPRESSION BRACE W/ P2485K CLIPS T&B

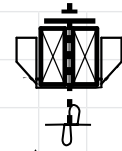
1 SECTION  
SSK NO SCALE

) 2x4 W/ PW.  
SHIM AT HGR

2x4 BRACING  
BEYOND PER  
SECTION A-A

SHT'G

(2) 2x4 W/ PW. SHIM  
BTWN AT ROD



NUT & WASHER

(E) PRE-MFR TRUSS  
U44 EA. END

1/2"φ MIN. SUPPORT  
ROD AT EA. HOOD  
SUPPORT POINT

24" MAX.

SEISMIC COMPRESSION  
SUPPORT - PROVIDE UNISTRUT  
PI000T FOR LENGTH OF ROD  
W/ P2485K CLIPS AT T&B -  
TYP. AT EA. ROD

6S10 DIAGONAL "X" SEISMIC  
BRACING BY GRIPPLE, INC. -  
SEE DETAIL 2 FOR LOCATION

KITCHEN HOOD

A34 W/ #9x1/2" SDS  
SCREWS EA. SIDE  
& EA. END

SHT'G

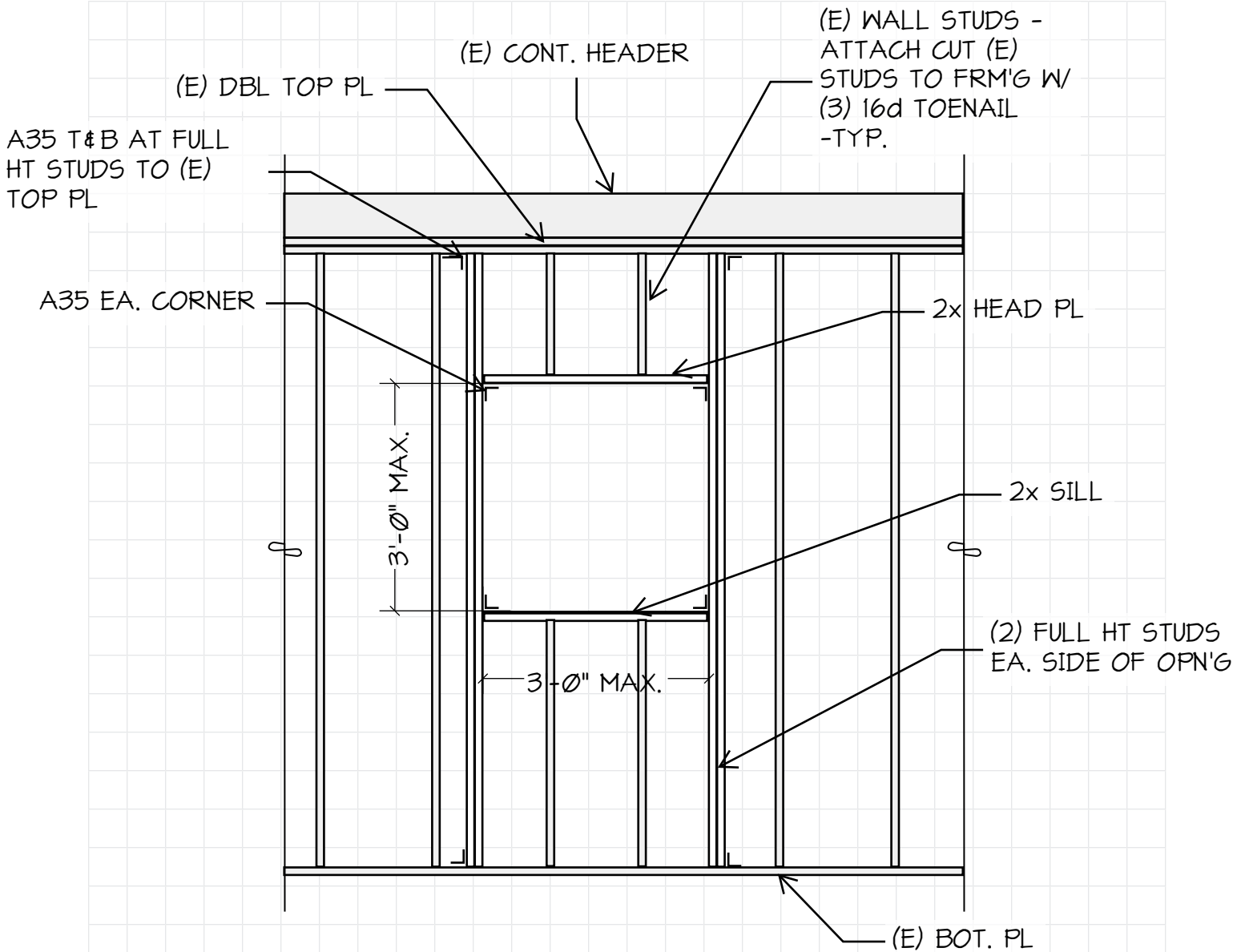
(E) PRE-MFR TRUSS

U44 EA. END

2x4 DIAG. BRACE FROM  
TOP TO BOT. CHORD -  
LOCATE WITHIN 6" OF  
KITCHEN HOOD SUPPORT  
ROD LOCATION

SECTION A-A

**2** SECTION  
SSK NO SCALE



**NOTES:**

1. ATTACH EXISTING SHT'G TO NEW STUDS W/ 10d @ 6" O.C.
2. DEMOLISH AND PATCH WALL FINISHES AS REQUIRED TO INSTALL NEW FRAMING.

NEW LOUVER OPENING (36" MAX. x 36" MAX.)

3  
SSK

**DETAIL**  
NO SCALE

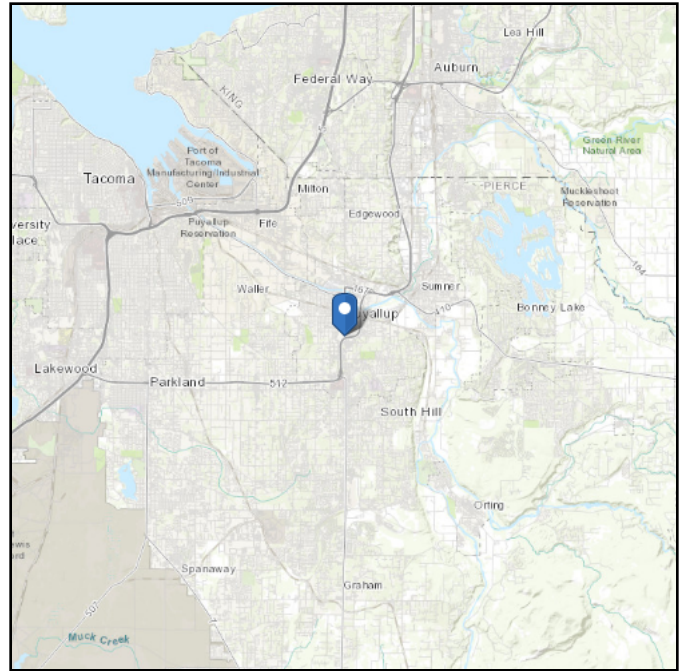
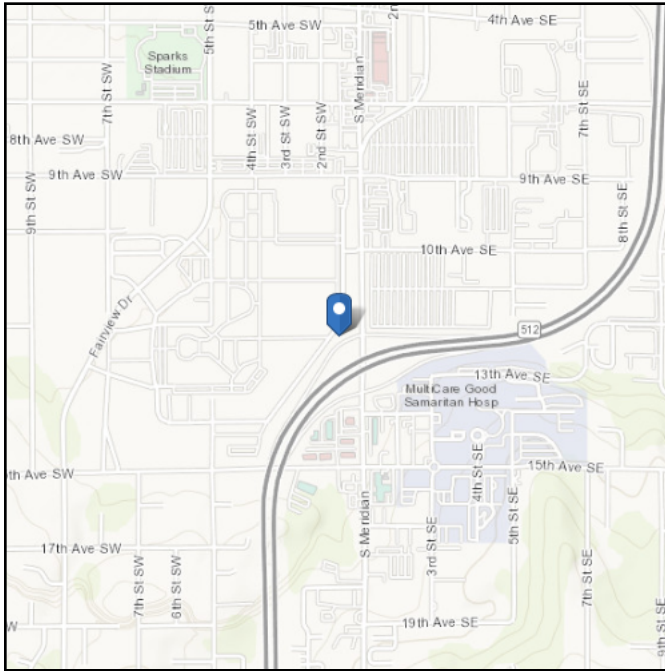


# ASCE Hazards Report

**Address:**  
110 9th Ave SW  
Puyallup, Washington  
98371

**Standard:** ASCE/SEI 7-16  
**Risk Category:** II  
**Soil Class:** D - Stiff Soil

**Latitude:** 47.18057  
**Longitude:** -122.2944  
**Elevation:** 44.38853781479012 ft  
(NAVD 88)



**Site Soil Class:** D - Stiff Soil

**Results:**

$S_s$ :	1.269	$S_{D1}$ :	N/A
$S_1$ :	0.437	$T_L$ :	6
$F_a$ :	1	PGA :	0.5
$F_v$ :	N/A	PGA <sub>M</sub> :	0.55
$S_{MS}$ :	1.269	$F_{PGA}$ :	1.1
$S_{M1}$ :	N/A	$I_e$ :	1
$S_{DS}$ :	0.846	$C_v$ :	1.354

Ground motion hazard analysis may be required. See ASCE/SEI 7-16 Section 11.4.8.

**Data Accessed:** Mon Apr 20 2026

**Date Source:** [USGS Seismic Design Maps](#)

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# **Kitchen Hood Support**

## **Summary**

The purpose of these calculations is to demonstrate that the anchorage and support for (1) kitchen hood, each weighing approximately 300 lb, is structurally adequate.

## **Design Criteria**

Risk Category: II

Building Height:  $H := 12 \cdot ft$

### **Unit Weights**

**Unit Name:**                      **Weight:**  
 Kitchen Hood:                       $W_{p1} := 301 \cdot lbf$

## **Design Forces**

### **Seismic Criteria**

Site Class: D (Default)

Sds:  $S_{DS} := 0.846$

From ASCE 7-16 CH. 13: Air-side HVAC

$a_p := 2.5$                $H = 12 \cdot ft$                $I_p := 1.0$                $S_{DS} = 0.846$   
 $R_p := 6$                $z := 14 \cdot ft$                $\Omega := 2.0$

$$f_p := \frac{0.4 \cdot a_p \cdot S_{DS}}{\left(\frac{R_p}{I_p}\right)} \cdot \left(1 + 2 \cdot \frac{z}{H}\right) = 0.47 \quad (\text{ASCE 13.3-1})$$

$$f_{pmax} := 1.6 \cdot S_{DS} \cdot I_p = 1.35 \quad (\text{ASCE 13.3-2})$$

$$f_{pmin} := 0.3 \cdot S_{DS} \cdot I_p = 0.25 \quad (\text{ASCE 13.3-3})$$

Design Force (Horizontal):  $f_p := \min(f_{pmax}, \max(f_p, f_{pmin})) = 0.47$

Design Force (Vertical):  $f_{pv} := 0.2 \cdot S_{DS} = 0.17$

## **Support Design**

### **Demands:**

Weight:  $W_p := W_{p1} = 301 \text{ lbf}$   
 Seismic Force (Vertical):  $F_{Ev} := f_{pv} \cdot W_p = 50.9 \text{ lbf}$   
 Seismic Force (Horiz):  $F_E := f_p \cdot W_p = 141.5 \text{ lbf}$   
 Allowable Axial Demand:  $P_a := W_p + 0.7 \cdot F_{Ev} = 336.65 \text{ lbf}$   
 Bracing Angle:  $\theta := 30 \cdot \text{deg}$

### **Anchor Rod Design:**

Number of Vertical Supports:  $n_v := 4$   
 Demand:  
 Anchor Rod Axial Demand:  $P_{av} := \frac{P_a}{n_v} = 84.16 \text{ lbf}$

### **Capacity:**

Anchor Rod Diameter:  $D_r := 0.5 \cdot \text{in}$   
 Anchor Rod Area:  $A_r := 0.25 \cdot \pi \cdot D_r^2 = 0.196 \text{ in}^2$   
 Anchor Rod Tensile Strength:  $F_y := 36 \cdot \text{ksi}$   
 Reduction Factor:  $\Omega := 1.67$

Tensile Capacity:  $P_{n\Omega} := \frac{F_y \cdot A_r}{\Omega} = 4232.68 \text{ lbf} > P_{av} = 84.16 \text{ lbf}$  OK

### **Unistrut Compression Strut Design:**

Number of Braces:  $n_b := 2$  (2) Tension only braces in each direction  
 Root Area of 1/2" Rod:  $A_r := 0.126 \cdot \text{in}^2$

Comp Loading:  $C_a := 0.6 \cdot \left( \frac{W_p - F_{Ev}}{n_v} \right) - \frac{F_E \cdot \tan(\theta)}{n_b} = -3.33 \text{ lbf}$

Allowable Compressive Strength of 1/2" Anchor Rod w/ P2485K Cradle Clips @ 21" O.C.

Allowable Rod Stress:  $F_{yAR} := 3745 \cdot \text{psi}$

$C_{aAR} := \frac{F_{yAR} \cdot A_r}{\Omega} = 282.56 \text{ lbf} > |C_a| = 3.33 \text{ lbf}$  OK

**Use 1/2" Anchor Rod w/ P2485K Cradle Clips @ 21" O.C. w/ P1000T**

### **Tension Brace Design:**

Number of Braces:  $n_b = 2$  (2) Tension only braces in each direction

Tension Load:  $T_a := \frac{0.7 F_E}{n_b \cdot \cos(\theta)} = 57.17 \text{ lbf}$

GS10 Gripple Seismic Brace Capacity:  $T_{n\Omega} := 225 \cdot \text{lbf} > |T_a| = 57.17 \text{ lbf}$  OK

### **Supporting Framing**

Hanging rod attached to (2) 2x4 spanning 24" between trusses.

Span:  $l := 24 \cdot \text{in}$

$A := 2 \cdot 1.5 \cdot \text{in} \cdot 3.5 \cdot \text{in} = 10.5 \text{ in}^2$

$S := 2 \cdot \frac{1.5 \cdot \text{in} \cdot (3.5 \cdot \text{in})^2}{6} = 0.51 \text{ ft} \cdot \text{in}^2$

Hanging Point Load:  $P_a := \frac{W_p + 0.7 \cdot F_{Ev}}{n_v} = 84.16 \text{ lbf}$

Moment Demand:  $M_a := \frac{P_a \cdot l}{4} = 42.08 \text{ lbf} \cdot \text{ft}$        $f_b := M_a \cdot S^{-1} = 82.45 \text{ psi}$

Shear Demand:  $V_a := \frac{P_a}{2} = 42.08 \text{ lbf}$        $f_v := \frac{3 \cdot V_a}{2 \cdot A} = 6.01 \text{ psi}$

(2) 2x4 DF #2 OK by inspection

### **Truss Bracing**

2x4 Diag bracing from bot. chord to top chord w/ A34 Ea. End

Axial (ASD):  $P_a := \frac{0.7 \cdot F_E \cdot n_v^{-1} \cdot 2}{\sqrt{2}} = 35.01 \text{ lbf}$

2x4 DF #2 diag brace OK by inspection. A34 w/ #9 screws tension allowable = 170# > 35# OK.

## Existing Truss Framing Check

We have reviewed the existing truss calculation by MiTek USA, Inc dated June 27, 2025 and these calculations appear to include the hood and fan weight demands on the trusses. The combined hood and fan loading is less than the loading to the truss. Our review of the truss calculations is for loading criteria only and does not include the actual analysis of the truss. The design of the truss is per the truss engineer of record.

Weight of hood:  $W_p = 301 \text{ lbf}$

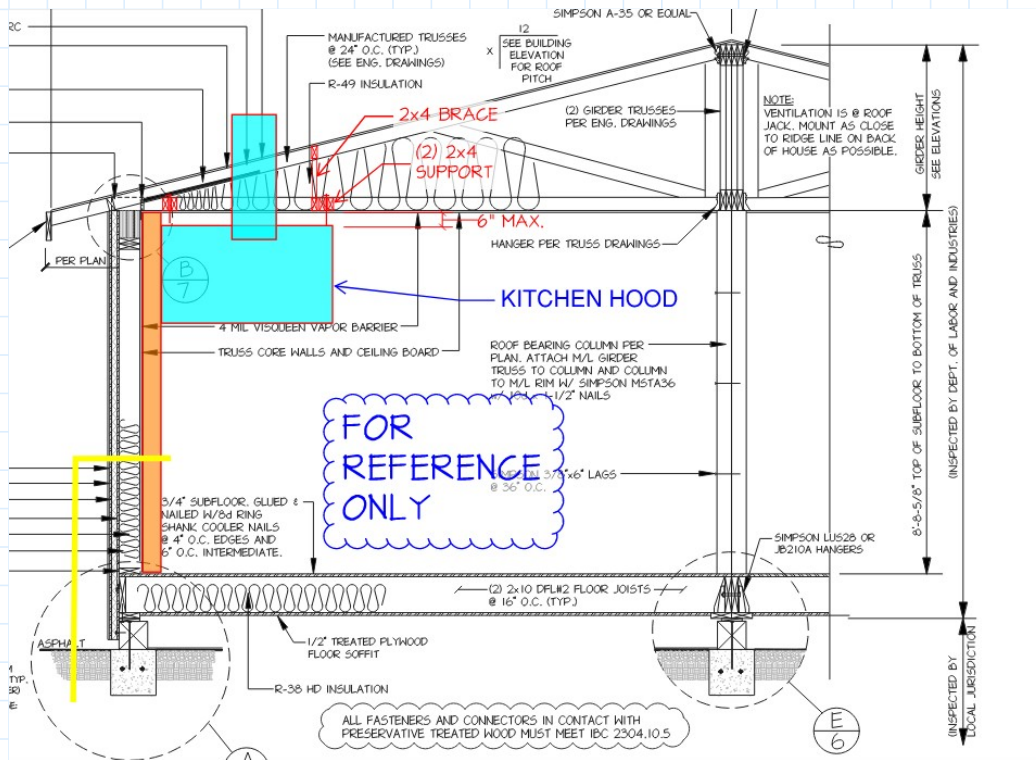
Weight of fan:  $W_f := 71 \cdot \text{lbf}$

Hood Area:  $A := 4 \cdot \text{ft} \cdot 4 \cdot \text{ft} = 16 \text{ ft}^2$

Unit Dead Load:  $DL := \frac{W_p + W_f}{A} = 23.25 \text{ psf}$

Additional Weight included in Truss Calcs:  $30 \text{ psf} > DL = 23.25 \text{ psf}$

The truss calculations for the supporting trusses have been included for reference



## New 36"x36" Louver Check

### Shear Wall Check

Checking the reduction of shear capacity using a perforated shear wall check per SDPWS 2021.

Height:  $h := 8.67 \cdot ft$   
 Length:  $L_1 := 4.17 \cdot ft$   
 $L_2 := 5.75 \cdot ft$   
 $L := L_1 + L_2 = 9.92 \cdot ft$

Opening Area:  $A_o := 3 \cdot ft \cdot 3 \cdot ft$

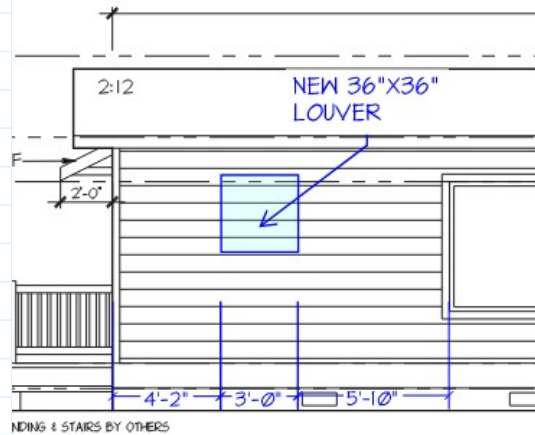
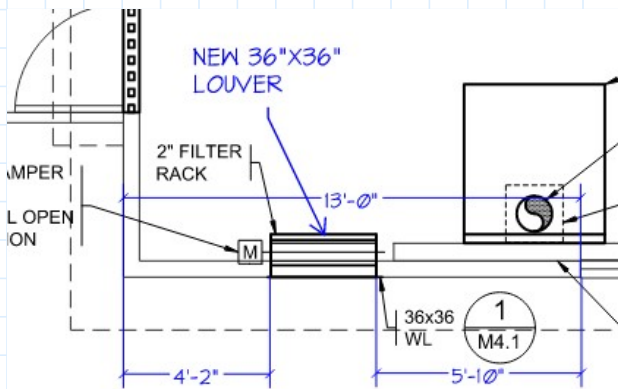
Shear Wall Area:  $A_w := 112 \cdot ft^2$

Sheathed Area:  $A_{fhs} := h \cdot (L_1 + L_2) = 86.01 \cdot ft^2$

$$WSP := \min\left(1, 1.25 - 0.125 \cdot \frac{h}{L_2}\right) = 1 \quad \text{Aspect ratio is OK}$$

(SDPWS Eq. 4.3-5)  $C_o := \frac{A_w}{(3 \cdot A_o + A_{fhs})} = 0.991$

Less than a 1% reduction in shear capacity --> new opening OK by inspection.



### Header Check

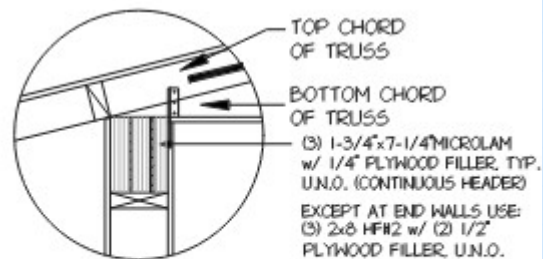
(3) 1-3/4"x7 1/4" SCL Cont. Header

$L := 3 \cdot ft$

$DL := 20 \cdot psf$

$SL := 25 \cdot psf$

$trib := 7.5 \cdot ft$



(B) ———— **DETAIL**

See Enercalc --> existing header OK

## Wood Beam

Project File: Existing Truss Check 2026-04-16.ec6

LIC# : KW-06014122, Build:20.25.04.16

PCS STRUCTURAL SOLUTIONS

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**DESCRIPTION:** Existing Cont. Header

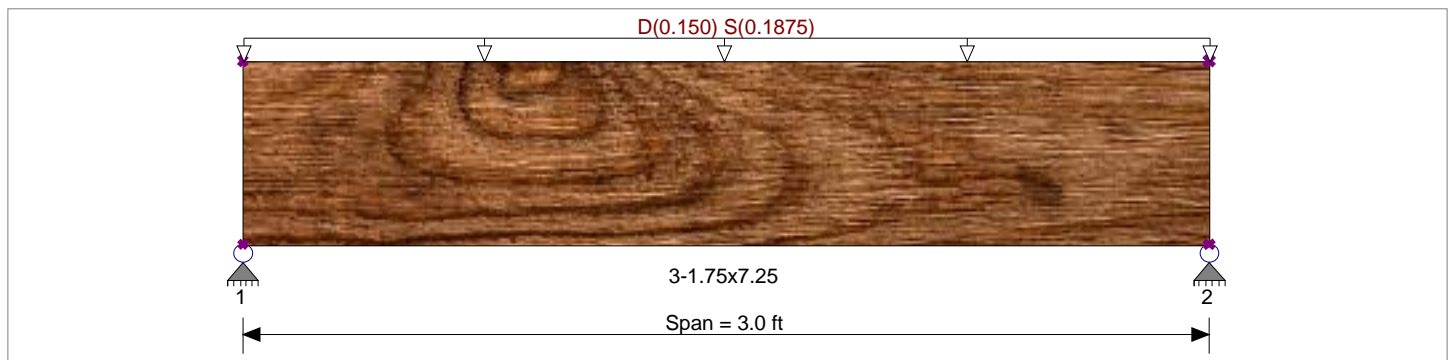
### CODE REFERENCES

Calculations per NDS 2018, IBC 2021

Load Combination Set : ASCE 7-16

### Material Properties

Analysis Method : Allowable Stress Design	Fb +	2600 psi	<i>E : Modulus of Elasticity</i>	
Load Combination : ASCE 7-16	Fb -	2600 psi	Ebend- xx	2000ksi
	Fc - Prll	2510 psi	Eminbend - xx	1016.535ksi
Wood Species : iLevel Truss Joist	Fc - Perp	750 psi		
Wood Grade : MicroLam LVL 2.0 E	Fv	285 psi		
	Ft	1555 psi	Density	42.01 pcf
Beam Bracing : Completely Unbraced				



### Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading

Loads on all spans...

Uniform Load on ALL spans : D = 0.020, S = 0.0250 ksf, Tributary Width = 7.50 ft

### DESIGN SUMMARY

**Design OK**

<b>Maximum Bending Stress Ratio</b>	=	<b>0.032</b> : 1	<b>Maximum Shear Stress Ratio</b>	=	<b>0.038</b> : 1
Section used for this span		<b>3-1.75x7.25</b>	Section used for this span		<b>3-1.75x7.25</b>
fb: Actual	=	102.33psi	fv: Actual	=	12.33 psi
F'b	=	3,193.50psi	F'v	=	327.75 psi
Load Combination		+D+S	Load Combination		+D+S
Location of maximum on span	=	1.500ft	Location of maximum on span	=	0.000 ft
Span # where maximum occurs	=	Span # 1	Span # where maximum occurs	=	Span # 1
<b>Maximum Deflection</b>					
Max Downward Transient Deflection		0.001 in Ratio = <b>34924</b> >=360	Span: 1 : S Only		
Max Upward Transient Deflection		0 in Ratio = <b>0</b> <360	n/a		
Max Downward Total Deflection		0.002 in Ratio = <b>18784</b> >=180	Span: 1 : +D+S		
Max Upward Total Deflection		0 in Ratio = <b>0</b> <180	n/a		

### Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios									Moment Values			Shear Values					
			M	V	CD	CM	C <sub>t</sub>	CLx	C <sub>F</sub>	C <sub>fu</sub>	C <sub>i</sub>	C <sub>r</sub>	M	fb	F'b	V	fv	F'v		
D Only	Length = 3.0 ft	1	0.019	0.022	0.90	1.00	1.00	1.00	1.071	1.00	1.00	1.00	0.18	47.3	2,500.8	0.00	0.00	0.0	0.0	0.0
+D+S	Length = 3.0 ft	1	0.032	0.038	1.15	1.00	1.00	1.00	1.071	1.00	1.00	1.00	0.39	102.3	3,193.5	0.31	12.3	327.8	0.0	0.0
+D+0.750S	Length = 3.0 ft	1	0.028	0.033	1.15	1.00	1.00	1.00	1.071	1.00	1.00	1.00	0.34	88.6	3,193.5	0.27	10.7	327.8	0.00	0.0
+0.60D	Length = 3.0 ft	1	0.006	0.008	1.60	1.00	1.00	1.00	1.071	1.00	1.00	1.00	0.11	28.4	4,438.1	0.09	3.4	456.0	0.00	0.0

Project Title: **Marcoes Candy WA**  
 Engineer: **AOB**  
 Project ID: **26304**  
 Project Descr:

**Wood Beam**

Project File: Existing Truss Check 2026-04-16.ec6

LIC# : KW-06014122, Build:20.25.04.16

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**DESCRIPTION:** Existing Cont. Header

**Overall Maximum Deflections**

Span	Load Combination	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
1	+D+S	0.0019	1.511		0.0000	0.000

**Vertical Reactions**

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	0.523	0.523
Max Upward from Load Combinations	0.523	0.523
Max Upward from Load Cases	0.281	0.281
D Only	0.242	0.242
+D+S	0.523	0.523
+D+0.750S	0.453	0.453
+0.60D	0.145	0.145
S Only	0.281	0.281

Job J25001347-A	Truss A2X	Truss Type Monopitch	Qty 38	Ply 1	7161 MARCOE CANDY Job Reference (optional)	R88936995
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Parr Truss Woodinville #207, Woodinville, WA - 98072,

Run: 8.83 S Jun 11 2025 Print: 8.830 S Jun 11 2025  
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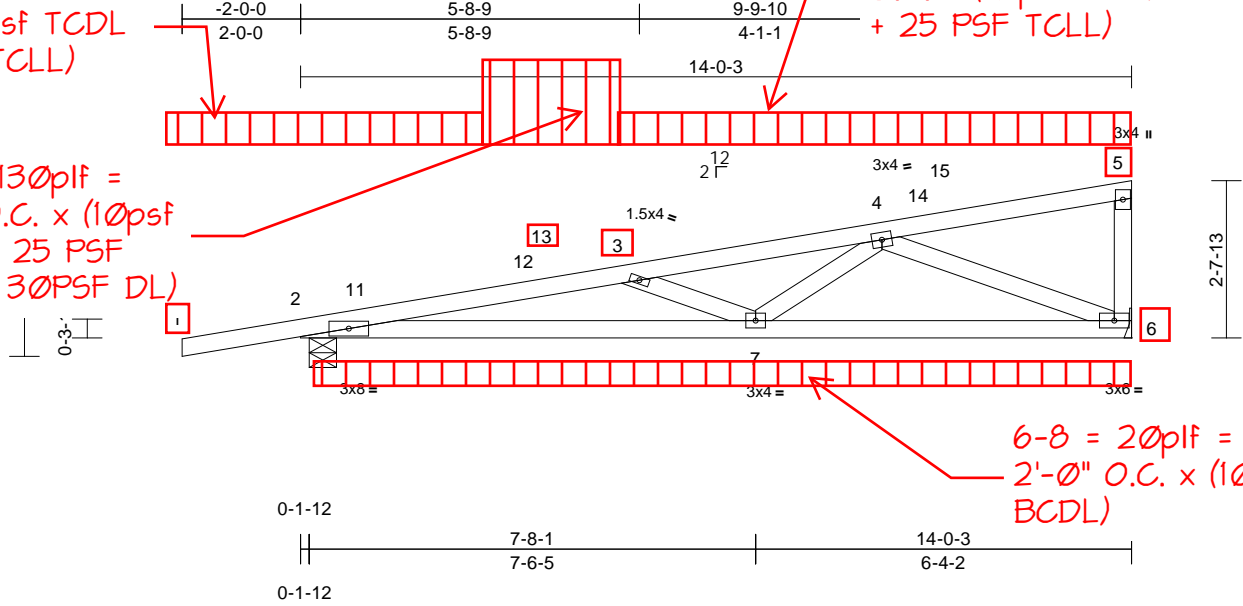
Page: 1

1-13 = 70plf = 2'-0"  
O.C. x (10psf TCDL  
+ 25 PSF TCLL)

3-13 = 130plf =  
2'-0" O.C. x (10psf  
TCDL + 25 PSF  
TCLL + 30PSF DL)

3-5 = 70plf = 2'-0"  
O.C. x (10psf TCDL  
+ 25 PSF TCLL)

6-8 = 20plf =  
2'-0" O.C. x (10psf  
BCDL)



Loading	(psf)	Spacing	2-0-0	CSI	DEFL	in	(loc)	l/defl	L/d	PLATES	GRIP	
TCLL	25.0	Plate Grip DOL	1.15	TC	0.51	Vert(LL)	-0.13	7-10	>999	360	MT20	220/195
(Roof Snow = 25.0)		Lumber DOL	1.15	BC	0.84	Vert(CT)	-0.24	7-10	>695	240		
TCDL	10.0	Rep Stress Incr	NO	WB	0.47	Horz(CT)	0.04	6	n/a	n/a		
BCLL	0.0*	Code	IRC2021/TPI2014	Matrix-MS		Wind(LL)	0.08	7-10	>999	240		
BCDL	10.0										Weight: 56 lb	FT = 20%

- LUMBER**  
 TOP CHORD 2x4 DF No.2  
 BOT CHORD 2x4 DF No.2  
 WEBS 2x4 DF No.2
- BRACING**  
 TOP CHORD Structural wood sheathing directly applied or 3-2-8 oc purlins, except end verticals.  
 BOT CHORD Rigid ceiling directly applied or 7-10-13 oc bracing.
- REACTIONS** (size) 2=0-5-8, 6= Mechanical  
 Max Horiz 2=125 (LC 11)  
 Max Uplift 2=-227 (LC 10), 6=-148 (LC 11)  
 Max Grav 2=909 (LC 19), 6=790 (LC 19)
- FORCES** (lb) - Maximum Compression/Maximum Tension  
 TOP CHORD 1-2=0/39, 2-3=-2925/527, 3-4=-2118/334, 4-5=-72/40, 5-6=-163/72  
 BOT CHORD 2-7=-634/2872, 6-7=-346/1434  
 WEBS 3-7=-882/252, 4-7=-69/790, 4-6=-1508/338

- NOTES**
- Wind: ASCE 7-16; Vult=110mph (3-second gust) Vasd=87mph; TCDL=5.5psf; BCDL=4.0psf; h=25ft; B=45ft; L=24ft; eave=4ft; Cat. II; Exp C; Enclosed; MWFRS (directional) and C-C Exterior(2E) -2-0-0 to 1-0-0, Interior (1) 1-0-0 to 13-10-7 zone; cantilever left and right exposed; end vertical left and right exposed; C-C for members and forces & MWFRS for reactions shown; Lumber DOL=1.60 plate grip DOL=1.60
  - TCLL: ASCE 7-16; Pf=25.0 psf (Lum DOL = 1.15 Plate DOL = 1.15); Is=1.0; Rough Cat C; Partially Exp.; Ce=1.0; Cs=1.00; Ct=1.00
  - Unbalanced snow loads have been considered for this design.
  - This truss has been designed for greater of min roof live load of 20.0 psf or 2.00 times flat roof load of 25.0 psf on overhangs non-concurrent with other live loads.

- As requested, plates have not been designed to provide for placement tolerances or rough handling and erection conditions. It is the responsibility of the fabricator to increase plate sizes to account for these factors.
- Plates checked for a plus or minus 20 degree rotation about its center.
- This truss has been designed for a 10.0 psf bottom chord live load nonconcurrent with any other live loads.
- \* This truss has been designed for a live load of 20.0psf on the bottom chord in all areas where a rectangle 3-06-00 tall by 2-00-00 wide will fit between the bottom chord and any other members.
- Refer to girder(s) for truss to truss connections.
- Provide mechanical connection (by others) of truss to bearing plate capable of withstanding 148 lb uplift at joint 6 and 227 lb uplift at joint 2.
- In the LOAD CASE(S) section, loads applied to the face of the truss are noted as front (F) or back (B).

- LOAD CASE(S)** Standard
- Dead + Snow (balanced): Lumber Increase=1.15, Plate Increase=1.15  
 Uniform Loads (lb/ft)  
 Vert: 1-13=-70, 3-13=-130 (F=-60), 3-5=-70, 6-8=-20

FOR  
REFERENCE  
ONLY

3-13 = 130plf =  
2'-0" O.C. x (10psf  
TCDL + 25 PSF  
TCLL + 30PSF DL)

WEIGHT OF UNIT & FAN =  
24 PSF --> OK



June 27, 2025

**WARNING - Verify design parameters and READ NOTES ON THIS AND INCLUDED MITEK REFERENCE PAGE MII-7473 rev. 1/2/2023 BEFORE USE.**

Design valid for use only with MiTek® connectors. This design is based only upon parameters shown, and is for an individual building component, not a truss system. Before use, the building designer must verify the applicability of design parameters and properly incorporate this design into the overall building design. Bracing indicated is to prevent buckling of individual truss web and/or chord members only. Additional temporary and permanent bracing is always required for stability and to prevent collapse with possible personal injury and property damage. For general guidance regarding the fabrication, storage, delivery, erection and bracing of trusses and truss systems, see ANSITPI1 Quality Criteria and DSB-22 available from Truss Plate Institute (www.tpinst.org) and BCSI Building Component Safety Information available from the Structural Building Component Association (www.sbcsccomponents.com)

**MiTek®**

400 Sunrise Ave., Suite 270  
Roseville, CA 95661  
916.755.3571 / MiTek-US.com

FOR QUESTIONS, CALL THE  
 Seattle Office  
 REGGIN BS  
 PHONE: (425) 212 - 5996  
 EMAIL: reg85@econair.com

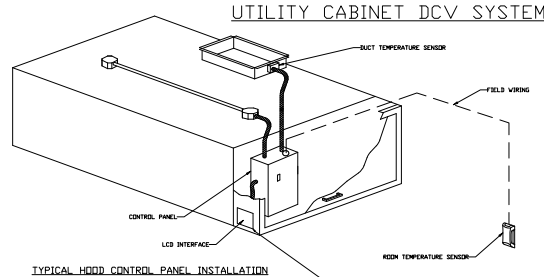
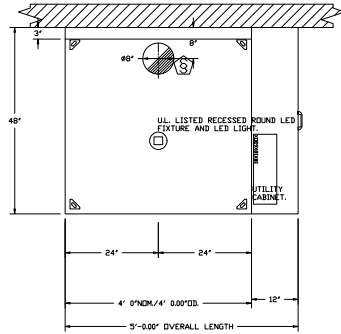
PATENT NUMBERS  
 EXHAUST HOODS ND-2/BD-2/SND-2 (CANADA) - CA PATENT 2520435 C.

**HOOD INFORMATION - JOB#8622463**

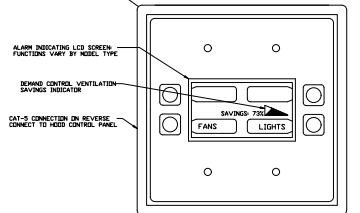
HOOD NO	TAG	MODEL	MANUFACTURER	LENGTH	MAX. COOKING TEMP.	TYPE	APPLIANCE DUTY	DESIGN CFM/FT	TOTAL EXH CFM	EXHAUST FLOW (DISCHARGE)				HOOD CONSTRUCTION	HOOD CLEARANCE				
										WIDTH	HEIGHT	DIA	VEL		SP	END TO END	RDW		
1		4824 EX-2	ECON-AIR	4' 0"	600 DEG	I	HEAVY	200	800			4'	8"	800	2292	-0.882"	430 SS WHERE EXPOSED	ALONE	ALONE

**HOOD INFORMATION**

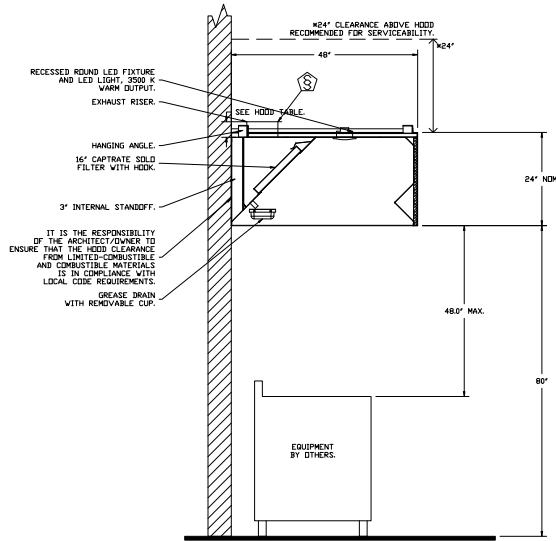
HOOD NO	TAG	FILTERS				LIGHTS				UTILITY CABINETS				FIRE SYSTEM PIPING	HOOD HANGING WEIGHT		
		TYPE	QTY	HEIGHT	LENGTH	EFFICIENCY @ 7 MICRONS	QTY	TYPE	WIRE GUARD	LOCATION	SIZE	TYPE	SIZE			MODEL #	QUANTITY
1		CAPTRATE SOLD FILTER	2	16"	20"	85% SEE FILTER SPEC	1	RECESSED ROUND	NO	RIGHT	12"x48"x24"			SC-11011000	1 LIGHT 1 FAN	NO	301 LBS



TYPICAL HOOD CONTROL PANEL INSTALLATION



FOR REFERENCE ONLY



SECTION VIEW - MODEL 4824EX-2  
 HOOD - #1

**SPECIFICATION: CAPTRATE™ GREASE-STOP™ SOLD FILTER**

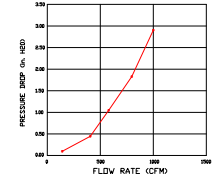
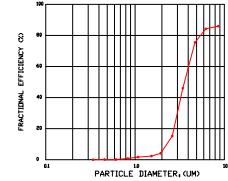
THE CAPTRATE GREASE-STOP SOLD FILTER IS A SINGLE-STAGE FILTER FEATURING A UNIQUE S-Baffle DESIGN IN CONJUNCTION WITH A SPLITTED REAR Baffle DESIGN, TO DELIVER EXCEPTIONAL FILTRATION EFFICIENCY.

FILTER IS STAINLESS STEEL CONSTRUCTION, AND SIZED TO FIT INTO STANDARD 2-INCH DEEP HOOD CHANNEL(S).

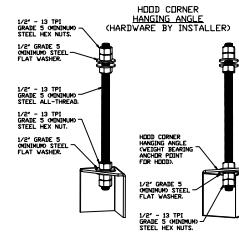
UNITS SHALL INCLUDE STAINLESS STEEL HANDLES AND A FASTENING DEVICE TO SECURE THE TWO COMPONENTS WHEN ASSEMBLED.

GREASE EXTRACTION EFFICIENCY PERFORMANCE SHALL REMOVE AT LEAST 75% OF GREASE PARTICLES FIVE MICRONS IN SIZE, AND 85% GREASE PARTICLES SEVEN MICRONS IN SIZE AND LARGER, WITH A CORRESPONDING PRESSURE DROP NOT TO EXCEED 1.0 INCHES OF WATER GAUGE. THE CAPTRATE GREASE-STOP SOLD WAS TESTED TO ASTM STANDARD ASTM F2519-05. MANUFACTURER APPROVED FOR USE IN SOLID FUEL APPLICATIONS AS A SPARK ARRESTER.

EFFICIENCY VS. PARTICLE DIAMETER



CAPTRATE FILTERS ARE IN COMPLIANCE WITH:  
 NFPA #96,  
 NSF STANDARD #2,  
 UL STANDARD #1046,  
 INT. MECH. CODE (CMC),  
 ULC-3649.



HANGING ANGLE MUST BE SUPPORTED WITH 1/2" - 13 TPI GRADE 5 (MINIMUM) ALL-THREAD SANDWICH HANGING ANGLES AND CEILING ANCHOR POINTS WITH 1/2" GRADE 5 (MINIMUM) STEEL FLAT WASHERS AND 1/2" - 13 TPI GRADE 5 (MINIMUM) HEX NUTS AS SHOWN. MUST USE DOUBLED HEX NUT CONFIGURATION BENEATH HOOD HANGING ANGLES AND ABOVE CEILING ANCHORS. MAINTAIN 1/4" OF EXPOSED THREADS BENEATH BOTTOM HEX NUT. TORQUE ALL HEX NUTS TO 57 FT-LBS.

REVISIONS

NO.	DESCRIPTION	DATE



Morcoe Candy Company - Puyallup, WA St. Fair Revit  
 110 9th Avenue Southwest,  
 Puyallup, WA, 98371

DATE: 4/17/2026

DWG.#: 8622463

DRAWN BY:

SCALE: 3/4" = 1'-0"

MASTER DRAWING

SHEET NO.

**EXHAUST FAN INFORMATION - JOB#8622463**

FAN UNIT NO.	TAG	QTY	FAN UNIT MODEL #	MANUFACTURER	CFM	ESP	RPM	MOTOR ENCL.	HP	BHP	PHASE	VOLT	FLA	DISCHARGE VELOCITY	WEIGHT (LBS)	ONES
1	KEF	1	EADU3H	ECDN-AIR	800	0.650	1452	TEAD-ECM	0.333	0.2020	1	208	2.5	396 FPM	71	14.6

**FAN ACCESSORIES**

FAN UNIT NO.	TAG	EXHAUST			SUPPLY			
		GREASE CUP	GRAVITY DAMPER	WALL MOUNT	SIDE DISCHARGE	GRAVITY DAMPER	MOTORIZED DAMPER	WALL MOUNT
1	KEF	YES						

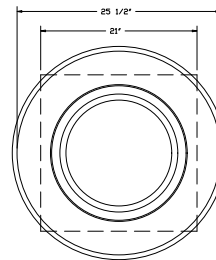
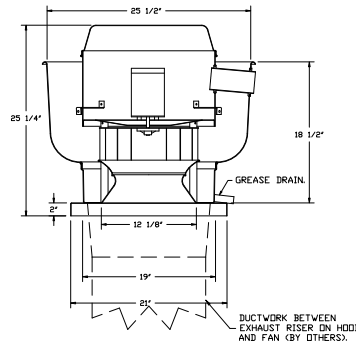
**CURB ASSEMBLIES**

NO.	IN FAN	TAG	WEIGHT	ITEM	SIZE
1	# 1	KEF	31 LBS	CURB	19.500"W X 19.500"L X 20.000"H 2.000:12.000 PITCH ALONG LENGTH, RIGHT VENTED HINGED.

**FAN OPTIONS**

FAN UNIT NO.	TAG	QTY	DESCRIPTION
1	KEF	1	GREASE BOX
		1	FAN BASE CERAMIC SEAL - DU/DR30/33HFA - INSTALLED AT PLANT - FOR GREASE DUCTS
		1	ECM WIRING PACKAGE - PWM SIGNAL FROM ECMPD3 PREWIRE (TELCD MOTOR), CCW ROTATION
		1	2 YEAR PARTS WARRANTY

FAN #1 EADU3H - EXHAUST FAN (KEF)



**FEATURES:**

- DIRECT DRIVE CONSTRUCTION (NO BELTS/PULLEYS).
- ROOF MOUNTED FANS.
- RESTAURANT MODEL.
- UL705 AND UL742 AND ULC-S645
- VARIABLE SPEED CONTROL.
- INTERNAL WIRING.
- THERMAL OVERLOAD PROTECTION (SINGLE PHASE).
- HIGH HEAT OPERATION 300°F (149°C).
- GREASE CLASSIFICATION TESTING.
- NEMA 3R SAFETY DISCONNECT SWITCH.

**NORMAL TEMPERATURE TEST:**

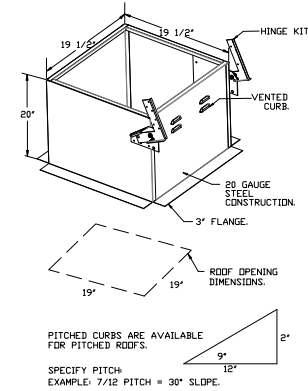
EXHAUST FAN MUST OPERATE CONTINUOUSLY WHILE EXHAUSTING AIR AT 300°F (149°C) UNTIL ALL FAN PARTS HAVE REACHED THERMAL EQUILIBRIUM, AND WITHOUT ANY DETERIORATING EFFECTS TO THE FAN WHICH WOULD CAUSE UNSAFE OPERATION.

**ABNORMAL FLAME-UP TEST:**

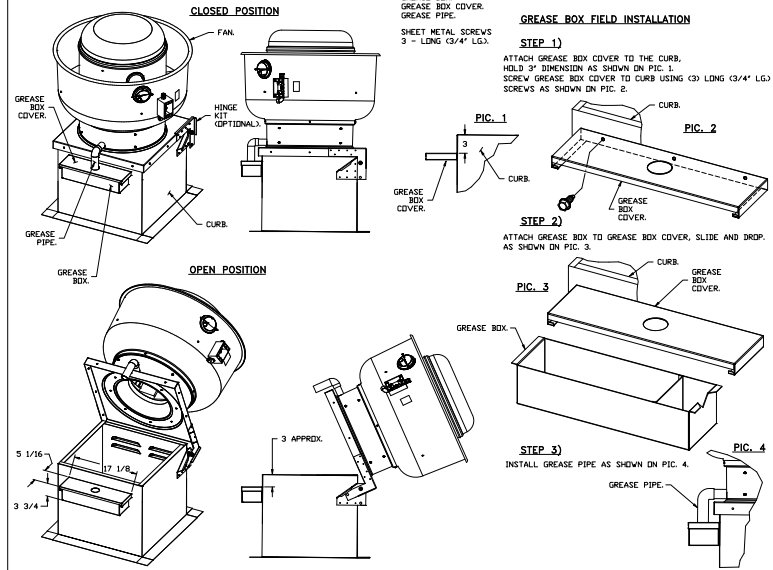
EXHAUST FAN MUST OPERATE CONTINUOUSLY WHILE EXHAUSTING BURNING GREASE VAPORS AT 600°F (316°C) FOR A PERIOD OF 15 MINUTES WITHOUT THE FAN BECOMING DAMAGED TO ANY EXTENT THAT COULD CAUSE AN UNSAFE CONDITION.

**OPTIONS:**

- GREASE BOX.
- FAN BASE CERAMIC SEAL - DU/DR30/33HFA - INSTALLED AT PLANT - FOR GREASE DUCTS.
- ECM WIRING PACKAGE - PWM SIGNAL FROM ECMPD3 PREWIRE (TELCD MOTOR), CCW ROTATION.
- 2 YEAR PARTS WARRANTY.



**GREASE BOX INSTALLATION**



\*NOTE: UL 705 INSTALL.

**FOR REFERENCE ONLY**

**REVISIONS**

NO.	DESCRIPTION	DATE

**econ·air**  
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www.econair.com

Morcoe Candy Company - Puyallup, WA St. Fair Rev1  
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**DRAWN BY:**  
**SCALE:** 3/4" = 1'-0"  
**MASTER DRAWING**

**SHEET NO.**  
2