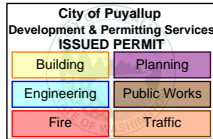
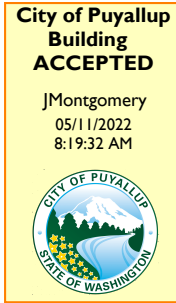


PROJECT: CASCAOE CHRISTIAN OFFICE			SHEET NO. 1/6
BY: CF	DATE: 3/23/22	JOB NO. 22044	



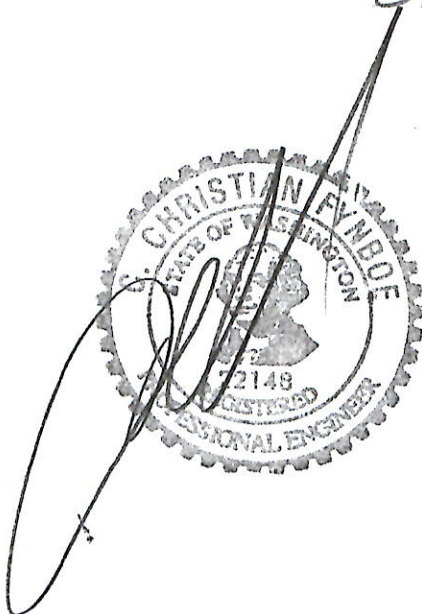
THE APPROVED CONSTRUCTION PLANS, DOCUMENTS AND ALL ENGINEERING MUST BE POSTED ON THE JOB AT ALL INSPECTIONS IN A VISIBLE AND READILY ACCESSIBLE LOCATION.

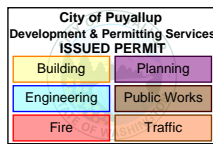
FULL SIZED LEDGIBLE COLOR PLANS ARE REQUIRED TO BE PROVIDED BY THE PERMITEE ON SITE FOR INSPECTION

STRUCTURAL CALCULATIONS  
FOR THE  
CASCAOE CHRISTIAN  
OFFICE ADDITION  
(815 - 2<sup>ND</sup> ST SE)

-JEFF BROWN ARCHITECTURE

DESIGN PARAMETERS: 2018 IBC  
SEE NOTES ON "SLD"



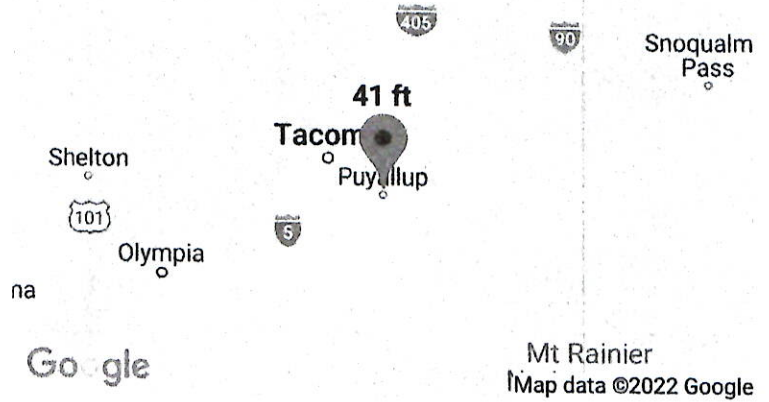


#22044

2/E

**Search Information**

**Address:** Puyallup, WA, USA  
**Coordinates:** 47.1853785, -122.2928974  
**Elevation:** 41 ft  
**Timestamp:** 2022-03-23T15:23:05.377Z  
**Hazard Type:** Seismic  
**Reference Document:** ASCE7-16  
**Risk Category:** II  
**Site Class:** D-default



**Basic Parameters**

Name	Value	Description
$S_S$	1.27	$MCE_R$ ground motion (period=0.2s)
$S_1$	0.437	$MCE_R$ ground motion (period=1.0s)
$S_{MS}$	1.524	Site-modified spectral acceleration value
$S_{M1}$	* null	Site-modified spectral acceleration value
$S_{DS}$	1.016	Numeric seismic design value at 0.2s SA
$S_{D1}$	* null	Numeric seismic design value at 1.0s SA

$$V = 1.02 \frac{W}{6.5} = 1.6W$$

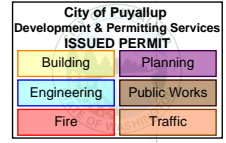
\* See Section 11.4.8

**Additional Information**

Name	Value	Description
SDC	* null	Seismic design category
$F_a$	1.2	Site amplification factor at 0.2s
$F_v$	* null	Site amplification factor at 1.0s
$CR_S$	0.914	Coefficient of risk (0.2s)
$CR_1$	0.898	Coefficient of risk (1.0s)
PGA	0.5	$MCE_G$ peak ground acceleration
$F_{PGA}$	1.2	Site amplification factor at PGA
$PGA_M$	0.6	Site modified peak ground acceleration

$T_L$	6	Long-period transition period (s)
SsRT	1.27	Probabilistic risk-targeted ground motion (0.2s)
SsUH	1.389	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	1.5	Factored deterministic acceleration value (0.2s)
S1RT	0.437	Probabilistic risk-targeted ground motion (1.0s)
S1UH	0.487	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	0.6	Factored deterministic acceleration value (1.0s)
PGAd	0.5	Factored deterministic acceleration value (PGA)

#22044 3/8



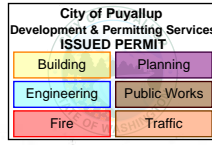
\* See Section 11.4.8

*The results indicated here DO NOT reflect any state or local amendments to the values or any delineation lines made during the building code adoption process. Users should confirm any output obtained from this tool with the local Authority Having Jurisdiction before proceeding with design.*

## Disclaimer

Hazard loads are provided by the U.S. Geological Survey [Seismic Design Web Services](#).

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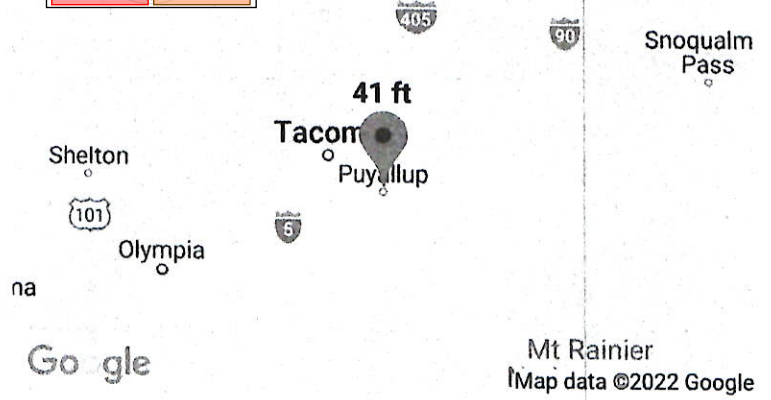


#2044

*[Handwritten signature]*

**Search Information**

**Address:** Puyallup, WA, USA  
**Coordinates:** 47.1853785, -122.2928974  
**Elevation:** 41 ft  
**Timestamp:** 2022-03-23T15:22:48.181Z  
**Hazard Type:** Wind



**ASCE 7-16**

MRI 10-Year 67 mph  
 MRI 25-Year 73 mph  
 MRI 50-Year 78 mph  
 MRI 100-Year 82 mph  
 Risk Category I 92 mph  
 Risk Category II 97 mph  
 Risk Category III 104 mph  
 Risk Category IV 108 mph

**ASCE 7-10**

MRI 10-Year 72 mph  
 MRI 25-Year 79 mph  
 MRI 50-Year 85 mph  
 MRI 100-Year 91 mph  
 Risk Category I 100 mph  
 Risk Category II 110 mph  
 Risk Category III-IV 115 mph

**ASCE 7-05**

ASCE 7-05 Wind Speed 85 mph

*The results indicated here DO NOT reflect any state or local amendments to the values or any delineation lines made during the building code adoption process. Users should confirm any output obtained from this tool with the local Authority Having Jurisdiction before proceeding with design.*

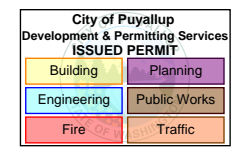
**Disclaimer**

Hazard loads are interpolated from data provided in ASCE 7 and rounded up to the nearest whole integer. Per ASCE 7, islands and coastal areas outside the last contour should use the last wind speed contour of the coastal area – in some cases, this website will extrapolate past the last wind speed contour and therefore, provide a wind speed that is slightly higher. NOTE: For queries near wind-borne debris region boundaries, the resulting determination is sensitive to rounding which may affect whether or not it is considered to be within a wind-borne debris region.

Mountainous terrain, gorges, ocean promontories, and special wind regions shall be examined for unusual wind conditions.

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#22034 5/28



**JEFF BROWN ARCHITECTURE**

JEFF BROWN ARCHITECTURE  
12181 C STREET SOUTH  
TACOMA, WA 98444

**PROJECT LEAD**  
JEFFREY E. BROWN  
253406.8324  
jeff@jeffbrownarchitecture.com



PROJECT NAME/ADDRESS

**CASCADE CHRISTIAN SCHOOLS  
DISTRICT OFFICE TI & ADDITION**  
815 21ST STREET SE  
PUYALLUP, WA 98372

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These documents have been prepared specifically for the above named project. They are not suitable for use on other projects or in other locations without the approval and participation of the Architect.

PROJECT NUMBER  
22003

DRAWING TYPE

**PERMIT DOCUMENTS**

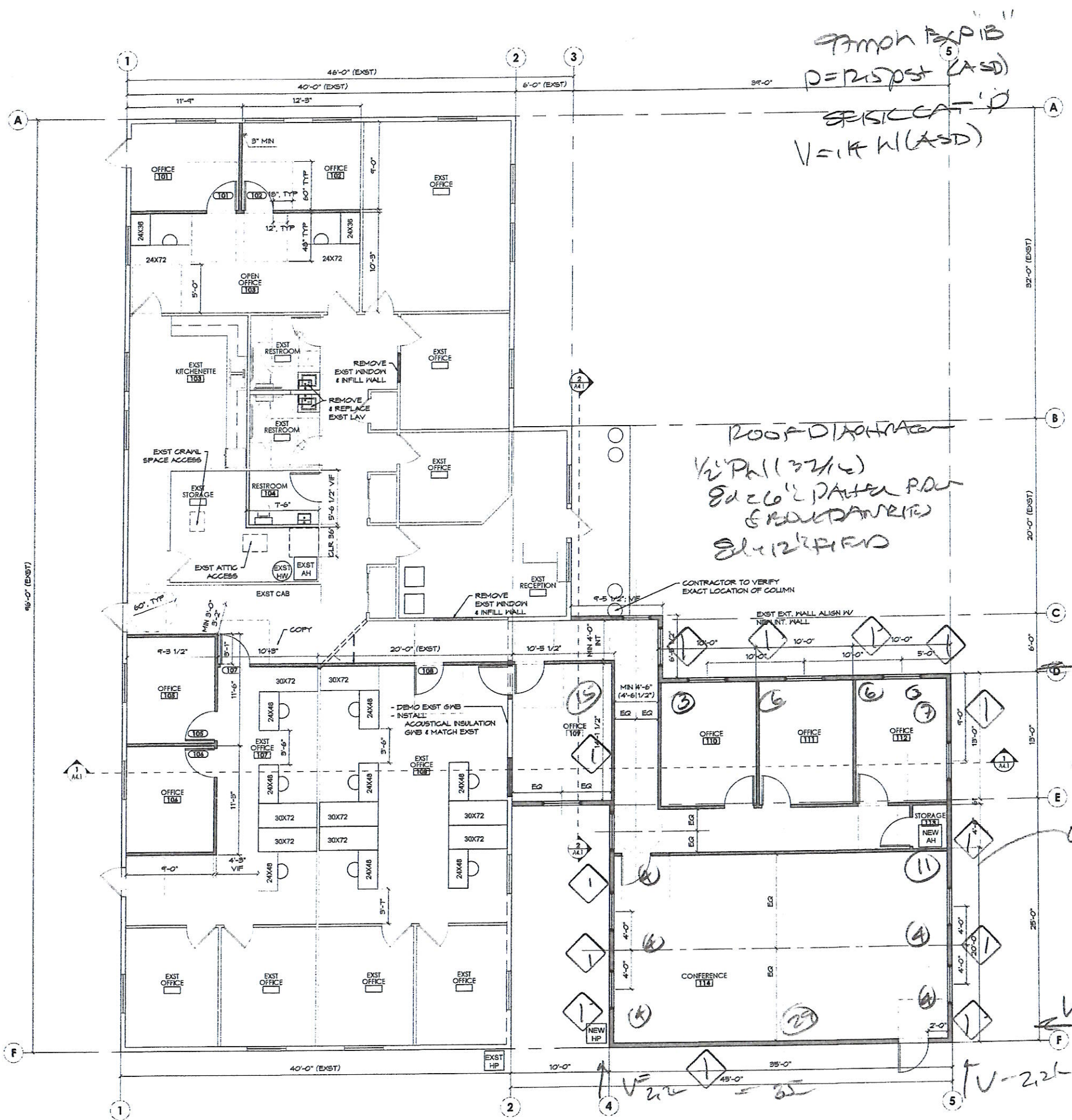
DATE	ISSUE	NO.
03.16.22		

SHEET TITLE

**EXST, DEMO, NEW FLOOR PLAN**

SHEET #

**A2.1**



**EXST, DEMO, AND NEW FLOOR PLAN**  
11X17 SCALE: 3/32" = 1'-0"  
22X34 SCALE: 3/16" = 1'-0"



PROJECT:			SHEET NO.
BY:	DATE:	JOB NO.	6/48
		22044	

City of Puyallup Development & Permitting Services ISSUED PERMIT			
Building	Planning	Engineering	Public Works
Fire	Traffic		

Mark (shear capacity)	Wall Type (3)	Panel Edge Nailing (1), (2)	Intermediate Nailing (2)	Bottom Plate Anchor Bolting or Nailing (5)
1 (200 lb/ft.)	½" CDX Plywood or OSB, one side	8d @ 6" o.c.	8d @ 12" o.c.	½" A.B. @ 4'-0" o.c. or 16d @ 7½" o.c.
2 (350 lb/ft.)	½" CDX Plywood or OSB, one side	8d @ 4" o.c.	8d @ 12" o.c.	5/8" A.B. @ 3'-4" o.c. or 16d @ 4" o.c.
3 (700 lb/ft.)	½" CDX Plywood or OSB, both sides	8d @ 4" o.c. (4)	8d @ 12" o.c.	3/4" A.B. @ 2'-0" o.c. or 16d @ 2" o.c.
11 (200 lb/ft.)	½" GWB, both sides	5d cooler nails @ 7" o.c.	5d cooler nails @ 7" o.c.	½" A.B. @ 4'-0" o.c. or 16d @ 8" o.c.

Notes:

1. Block all panel edges.
2. Common or box nails.
3. 2x studs shall be H.F. #2 or better, kiln-dried.
4. Use 3x studs and plates @ panel edges, wall type 3 only.
5. Anchor bolts shall have minimum 3" by 3" by ¼" thick plate washers.

PROJECT:		City of Puyallup Development & Permitting Services		SHEET NO. 7/c
ISSUED PERMIT		Building	Planning	
BY:	Engineering	Public Works	JOB NO. 22044	
	Fire	Traffic		

SHEAR WALL (HEAVY VALUES)

①  $1\frac{5}{32}$ " STRUCT I Ed @  $6\frac{1}{2}$ "  $280(.82) = 230$   
 $\frac{1}{2}$ "  $\phi$  AB @  $4'0"$   $600(1.6) = 240$  lb/ft  
 $16d$  @  $7\frac{1}{2}$ "  $91(1.6)1\frac{3}{4} = 233$  lb/ft  
200 lb/ft

②  $1\frac{5}{32}$ " STRUCT I Ed @  $4\frac{1}{4}$ "  $430(.82) = 353$   
 $\frac{5}{8}$ "  $\phi$  AB @  $3'4"$   $860(1.6) = 413$  lb/ft  
 $16d$  @  $4\frac{1}{4}$ "  $91(1.6)1\frac{3}{4} = 437$  lb/ft  
350 lb/ft

③  $1\frac{7}{32}$ " STRUCT I Ed @  $4\frac{1}{2}$ "  $353(.82) = 706$  lb/ft  
 $\frac{3}{4}$ "  $\phi$  AB @  $2'0"$   $1150(1.6) = 944$  lb/ft  
 $16d$  @  $2"$   $91(1.6)1\frac{3}{4} = 873$  lb/ft  
700 lb/ft

PROJECT:			SHEET NO.
BY:	DATE:	JOB NO.	8/18
		22044	

City of Puyallup Development & Permitting Services	
ISSUED PERMIT	
Building	Planning
Engineering	Public Works
Fire	Traffic

ROOF FRAMING

$l = 8' \text{ HOR}$

$W = 1.045(17.5) = 18.8 \text{ lb}$

$M = 18.8 \frac{(8')^2}{8} = 96.8 \text{ k-in}$

$S_{REQD} = \frac{96.8}{1.965(4.13)} = 76.10 \text{ in}^3$

4x12DF#2

FLOOR FRAMING

$l = 5'$

$W = (1.05 + 0.1 + 0.02)10 = 0.8 \text{ k/ft}$

$M = 0.8 \frac{(5')^2}{8} = 30 \text{ k-in}$

$S_{REQD} = \frac{30}{1.105} = 28.6 \text{ in}^3$

4x10DF#2