Preliminary Drainage Report

Puyallup High School Portables

711, 721 & 701 West Main Puyallup, WA 98371

Prepared for

Puyallup School District c/o Studio Meng Strazzara 2001 Western Ave, Suite 200 Seattle, WA 98121 206.587.3797

Prepared by

JMJ Team 905 Main Street, Suite 200 Sumner, WA 98390 206.596.2020 Justin Jones, PE



April 5, 2024

PROJECT ENGINEER'S CERTIFICATION

"I hereby state that this Drainage Control Plan for the Puyallup High School Portables has been prepared by me or under my supervision and meets minimum standard of care and expertise which is usual and customary in this community for professional engineers. I understand that the City of Puyallup does not and will not assume liability for the sufficiency, suitability, or performance of drainage facilities prepared by me."

Justin Jones, PE





TABLE OF CONTENTS

Project Overview and Vicinity Map	1
Existing Conditions Summary	3
Proposed Conditions Summary	3
Summary of Minimum Requirements	5

Appendix A: Site Development Drawings

Appendix B: Maps

Appendix C: WWHM Modeling

Appendix D: Infiltration Report



PROJECT OVERVIEW AND VICINITY MAP

The Puyallup High School Portables project is located at the intersection of West Main and 7th Street SW in the City of Puyallup. The project site includes parcels 5870000231, 5870000190, 5870000200, and 5870000171, with a total lot area of 1.00 AC. The project has a total site area of 0.38 acres. The site is currently developed as a PF – Public Facilities lot. New development on-site includes the construction of 3 portable classroom buildings, open-graded gravel pad, and the construction of permeable asphalt walkways. The stormwater approach is to fully infiltrate runoff on-site.



Vicinity Map



Proposed Site Area Map

EXISTING CONDITIONS SUMMARY

The Puyallup High School Portables project has a lot area of 1.00 acre. The existing site consists of landscaping, asphalt parking lot, and existing portables east of the parking lot. The site is fairly flat and has a slight slope towards the north and west side of the property.

The existing storm system consists of downspout dispersion and gravity pipe conveyance system. Runoff from roof disperses onto parking lot and is captured via Contech Catch Basin Inlet Filter that connects to the City of Puyallup stormwater system along West Main. Runoff is then conveyed to the Puyallup River via gravity pipe conveyance system.

The site is located within Lahar Hazard area.

There are no critical areas within site.

PROPOSED CONDITIONS SUMMARY

The proposed development is located in the landscaped area west of the existing parking lot. New development includes the construction of 3 portable classroom buildings, perforated aluminum landing, and site improvements.

The proposed development will result in an addition of 8,678 SF of new impervious surfaces within the project site area. Total land disturbing activity on-site to be approximately 14,165 SF. Minimum requirements 1-9 will apply to this project. Lot Coverage Table has been provided in the report following.

Site improvements include the construction of permeable open-graded gravel pad, permeable asphalt walkways, landscaping, and stormwater conveyance and infiltration gallery. The portables will also have utility service connections for power and communications.

Stormwater runoff from the new portables will be collected via roof downspouts and conveyed to an infiltration gallery to be fully infiltrated. Runoff from aluminum landing will drain through the perforated surface and be collected on the permeable gravel pad where stormwater will fully infiltrate into native soils. Runoff from permeable asphalt walkways will infiltrate through the porous surface and fully infiltrate into native soils.

Infiltration suitability was evaluated during the wet season (December 1st - April 1st) to determine infiltration rate and groundwater separation. Small PIT tests and groundwater monitoring were performed in accordance with the 2019 Stormwater Management Manual for Western Washington (DOE Manual) to determine infiltration feasibility. The infiltration rate was determined to be 0.64 in/hr (corrected). Infiltration Report has been provided in Appendix D.

LOT COVERAGE

The following tables show the existing and proposed lot coverage for the Puyallup High School Portables project site.

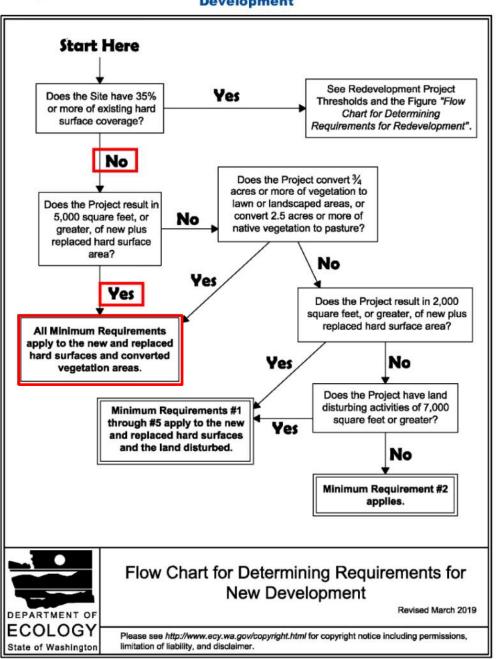
Existing Lot Coverage – 43,574 SF (1.00 AC) Lot Area								
Coverage Area (SF) Area (Acres) % of Site								
Impervious	Impervious							
Roof	1,722	0.04						
Concrete Sidewalk	964	0.03						
Asphalt Parking Lot	6,686	0.15						
Total Site Impervious	9,372	0.22	22.0%					
Pervious								
Landscape	34,202	0.78						
Total Site Pervious	34,202	0.78	78.0%					

Proposed Lot Coverage – 43,574 SF (1.00 AC) Lot Area							
Coverage Area (SF) Area (Acres) % of Site							
Impervious							
Ex. Roof	1,722	0.04					
Ex. Concrete Sidewalk	964	0.03					
Ex. Asphalt Parking Lot	6,686	0.15					
New Roof	5,785	0.12					
New Permeable Asphalt Sidewalk	663	0.02					
New Permeable Gravel Pad	1,570	0.04					
New Perforated Aluminum Landing	660	0.02					
Total New Impervious 8,678 0.20 20.0%							
Total Site Impervious	18,050	0.42	42.0%				
Pervious							
Landscape	25,524	0.58					
Total Site Pervious	25,524	0.58	58.0%				

Thank

SUMMARY OF MINIMUM REQUIREMENTS

The City of Puyallup adopts the 2019 Stormwater Management Manual for Western Washington (DOE Manual). Volume 1 of the DOE Manual describes the minimum requirements for a development project. Using the flowchart below, Minimum Requirements #1-9 applies to the project site.





MINIMUM REQUIREMENT 1: PREPARATION OF STORMWATER SITE PLANS

Stormwater Site Plan drawings have been prepared per the City of Puyallup development codes and the 2019 Stormwater Management Manual for Western Washington (DOE Manual), see Appendix A.

MINIMUM REQUIREMENT 2: CONSTRUCTION STORMWATER POLLUTION PREVENTION

A Temporary Erosion and Sediment Control Plan has been prepared per the City of Puyallup development codes and the 2019 DOE Manual and is included in this report, see Appendix A. Construction Stormwater Pollution Prevention measures may include storm drain inlet protection; construction entrance; silt fence and a sediment trap.

MINIMUM REQUIREMENT 3: SOURCE CONTROL OF POLLUTION

Source control BMPs will be implemented to minimize stormwater contamination and help comply with the DOE Manual. BMP's for the project may include:

- Inspect and clean treatment BMPs, conveyance systems, and catch basins as needed, and determine necessary O & M Improvements.
- Clean catch basins when the depth of deposits reaches 60-percent of the sump depth as measured from the bottom of basin to the invert of the lowest pipe into or out of the basin.
- Clean woody debris in a catch basin as frequently as needed to ensure proper operation of the catch basin.

MINIMUM REQUIREMENT 4: PRESERVATION OF NATURAL DRAINAGE SYSTEMS AND OUTFALLS

Natural drainage for the developed site area surface flows towards the north and west side of the site and infiltrates into native soil. The project proposes to maintain natural drainage patterns and discharge at natural location.

MINIMUM REQUIREMENT 5: ONSITE STORMWATER MANAGEMENT

Per Figure I-3.3 of the 2019 DOE Manual, the Puyallup High School Portables project is required to either meet LID Performance Standards or utilize List #3 to determine appropriate stormwater management BMPs for various surfaces. This project proposes to meet LID Performance Standards.

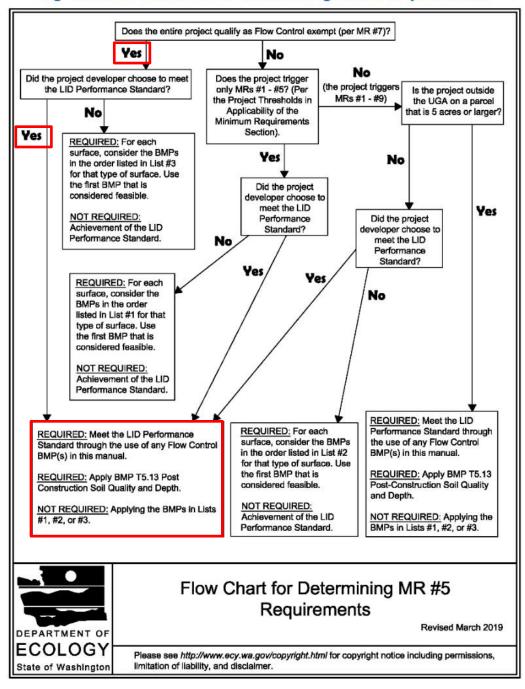


Figure I-3.3: Flow Chart for Determining MR #5 Requirements

To meet LID Performance Standards, stormwater discharges must match developed discharge durations to predeveloped discharge rates from 8% of the 2-year peak flow to the full 50-year flow.

The following BMPs were considered for the site:

- Roofs:
 - <u>Downspout Full Infiltration</u>:

Downspout Full Infiltration was evaluated and was deemed feasible for the site. Runoff from proposed roof areas will be routed to the infiltration gallery and infiltrate 100% of roof runoff into native soils. The infiltration galleries have been sized utilizing the WWHM model for a gravel trench bed based on the following criteria:

- Infiltration rate: 0.64 in/hr
- Drain Rock Basin with a porosity of 0.33.
- 12" Drainage/Storage Layer.
- Minimum 1-foot of separation between the bottom of the infiltration gallery and the seasonal high groundwater level.

A 441 SF gallery was determined to be the minimum area needed to fully infiltrate runoff from a single portable, see Appendix C for WWHM modeling. The project proposes a 1,325 SF gallery to manage runoff from all (3) three portables.

- Other Hard Surfaces:
 - <u>Permeable Pavements:</u>

Permeable Pavements were evaluated for the management of runoff from the gravel pad and asphalt walkway. This BMP was deemed feasible for the project. Runoff will permeate through the open-graded gravel pad and asphalt walkway and fully infiltrate into native soils. The permeable pavements have been sized utilizing the WWHM model based on the following criteria:

Infiltration rate: 0.64 in/hr

- Layers for each surface type:
 - Gravel Pad: 10" Open-Graded Gravel (0.33 porosity)
 - Asphalt Walkways: 4" Porous Asphalt (0.33 porosity)
 6" Permeable Ballast (0.33 porosity)
- Minimum 1-foot of separation between the bottom of the permeable pavement and the seasonal high groundwater level.

The modeling determined that the proposed layers was sufficient to infiltrate 100% of runoff. See Appendix C for WWHM modeling.

- Lawn and Landscaped Areas:
 - This project is required to retain and protect undisturbed soil in areas not being developed and, prior to completion of the project, amend all new, replaced, and disturbed topsoil (including construction lay-down areas) with organic matter in accordance with BMP T5.13 of the 2019 DOE Manual.

This project proposes to infiltrate 100% of influent runoff on-site, resulting in no net gain of stormwater discharge from the developed site; therefore, this project meets or exceeds the LID Performance Threshold.

MINIMUM REQUIREMENT 6: RUNOFF TREATMENT

Per the 2019 DOE Manual, Runoff Treatment is required if the site Threshold Discharge Area (TDA) has a total of 5,000 SF of pollution generating hard surfaces (PGHS) or 3/4 acres of pollution generating pervious surfaces (PGPS). The Puyallup High School Portables project does not meet these thresholds as the site does not propose any PGHS or PGPS; therefore, runoff treatment is not required on-site.

MINIMUM REQUIREMENT 7: FLOW CONTROL

Per 2019 DOE Manual, Flow Control BMPs are required if the site TDA meets any of the following thresholds:

- TDAs that have a total of 10,000 SF or more of effective impervious surfaces, or
- TDAs that convert 3/4 acres or more of native vegetation, pasture, scrub/shrub, or unmaintained nonnative vegetation to lawn or landscape, or convert 2.5 acres or more of native vegetation to pasture, and from which there is a surface discharge in a natural or man-made conveyance system from the TDA, or
- TDAs that through a combination of effective hard surfaces and converted vegetation areas cause a 0.15 cubic feet per second (cfs) or greater increase in the 100-year flow frequency as estimated using an approved continuous simulation model and 15-minute time step.

Effective impervious surfaces can be defined as those impervious surfaces that are connected via sheet flow or discrete conveyance to a drainage system. Impervious surfaces are considered ineffective if approved runoff modeling methods indicate that the entire runoff file is infiltrated.

The Puyallup High School Portables project is proposing to infiltrate 100% of runoff file using an infiltration gallery and permeable pavements; therefore, all proposed impervious areas are deemed ineffective. Since the project is not proposing any effective impervious, TDA Thresholds stated above are not triggered and Flow Control BMPs are not required.

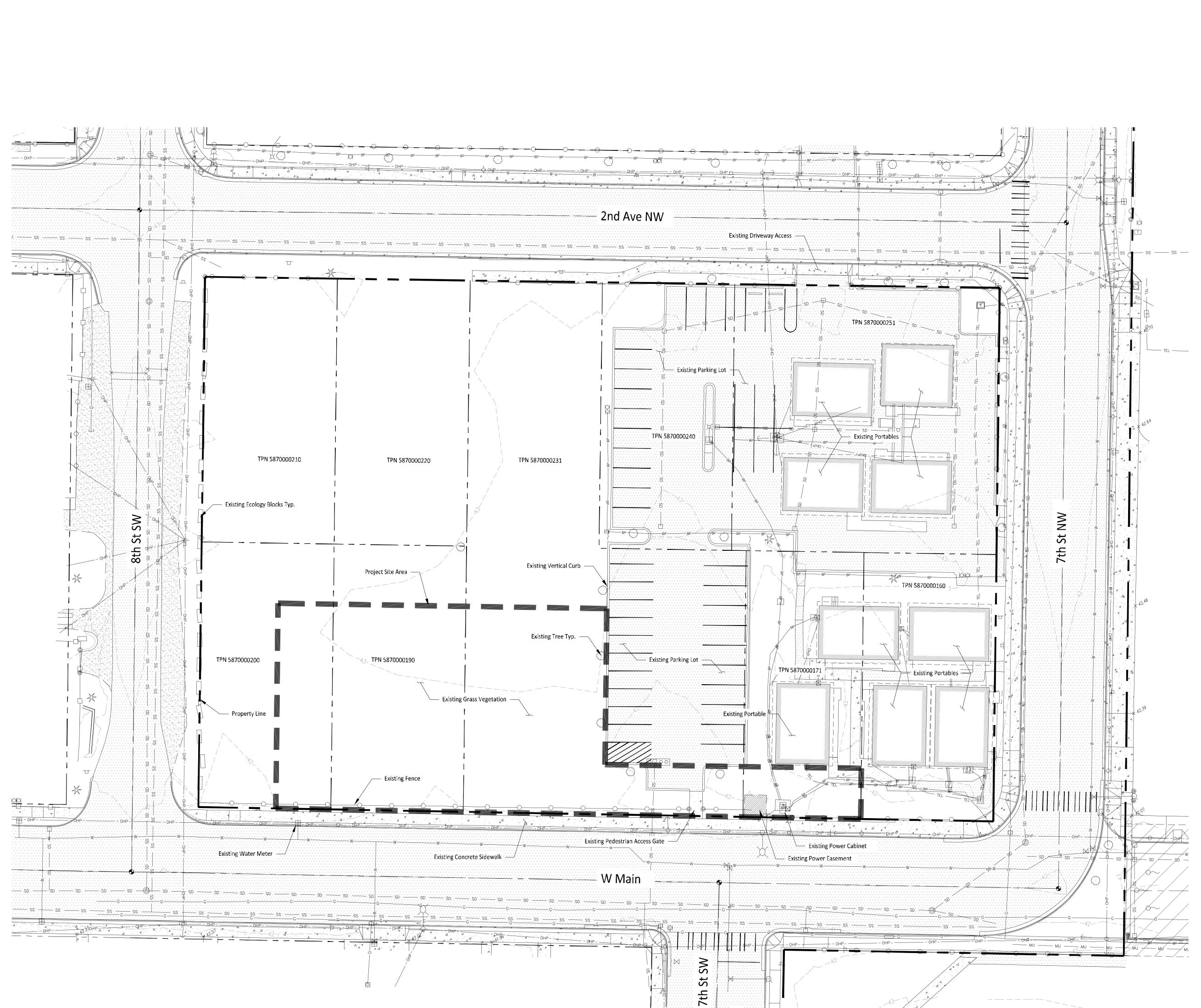
MINIMUM REQUIREMENT 8: WETLAND PROTECTION

This minimum requirement applies only to TDAs whose stormwater discharges to wetlands. This project does not propose to discharge stormwater to wetlands; therefore, this minimum requirement does not apply to the project.

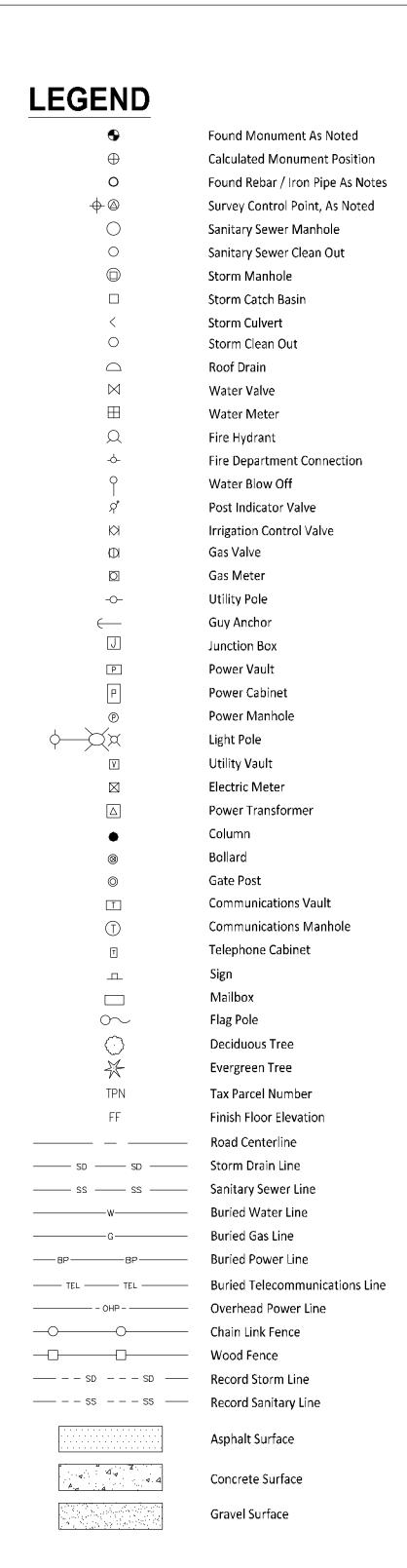
MINIMUM REQUIREMENT 9: OPERATION AND MAINTENANCE

An operation and maintenance manual shall be provided for Stormwater Management BMPs in accordance with the 2019 DOE Manual. This manual will be developed prior to building occupancy.

APPENDIX A







HORIZONTAL DATUM

Washington Plane Coordinate System, South Zone,

NAD 83/2011 Based on GPA observation utilizing the Washington State Reference Network (WSRN) Measured south 88°57'44" east between two found monuments along west main st. at the intersections with 8th st nw and 7th st nw

VERTICAL DATUM

NAVD88

Based on GPS observation utilizing the WSRN with NGS GEOID18 Loaded Temporary Benchmark Elevation = 41.76 Description: Rebar & Control Cap #12 Located at the intersection of West Main & 7th ST NW

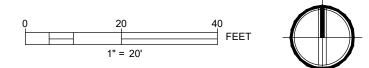
SE of the radial curb line

SITE DATA

- Total Lot Area: 43,574 SF (1.00 AC)
- 16,587 SF (0.38 AC) Total Project Site Area:
- 5870000171, 5870000190, 5870000200, 5870000231 Tax Parcel Numbers:
- PF- Public Facilities Zoning:

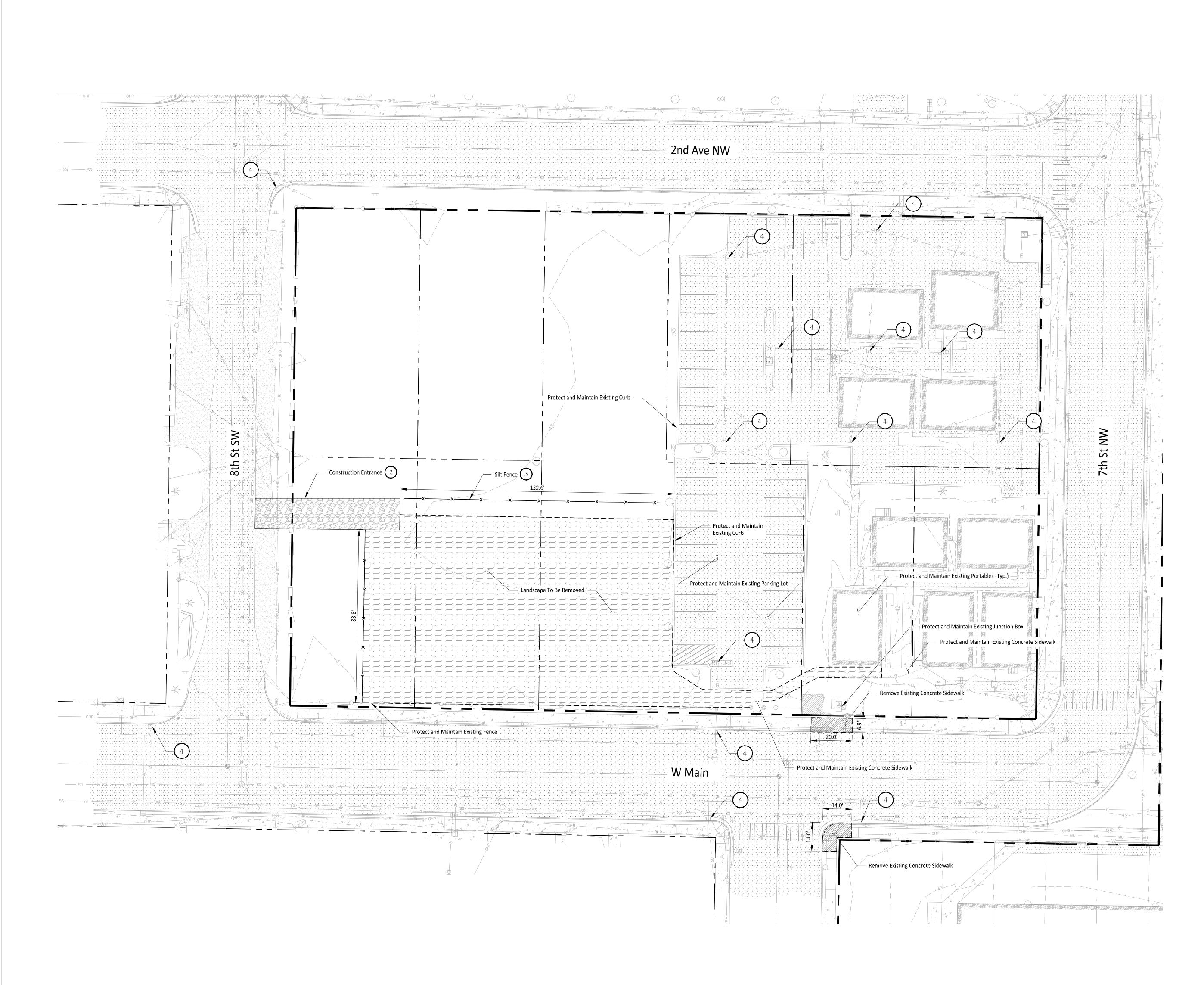
EXISTING LOT COVERAGE

Total Lot Area	43,574 SF	(1.00 AC)	
Coverage	Area (SF)	Area (AC)	% of Site
Impervious			
Roof	1,722	0.04	
Concrete Sidewalk	964	0.03	
Asphalt Parking Lot	6,686	0.15	
Total Site Impervious	9,372	0.22	22.0%
Pervious			
Landscape	34,202	0.78	
Total Site Pervious	34,202	0.78	78.0%





ARCHITECT studicmeng STRAZZARA 2001 WESTERN AVE, STE# 200, SEATTLE, WA 98121 www.studioms.com | P: 206.587.3797 CONSULTANT JMJTEAM JMJ Team 905 Main Street, Suite #200 Sumner, WA 98390 (206) 596-2020 CLIENT/OWNER D PUYALLUP SCHOOL DISTRICT A Trudition of Excellence TITLE PUYALLUP HS NEW PORTABLES 2023 STAMP ALLA. UNAL . 04-05-24 ISSUED: DATE: CONDITIONAL USE PERMITOCT, 11 2023 CUP CC#1 RESPONSE APR, 5 2024 EXISTING SITE PLAN Building Permit #: CUP #: PLCUP20230109 Owner's Project #: 2023106 Architect's Project #: Drawn By МО Checked By JJ C.01





LEGEND

	Construction Entrance
	Landscape To Be Removed
	Concrete To Be Removed
	Existing Asphalt Pavement
	Existing Gravel Pavement
	Existing Concrete Pavement
	Property Line
	Parcel Line
xx	Silt Fence
	Existing Overhed Power Line
SS SS	Existing Sewer Line
SD SD	Existing Storm Line
W	Existing Water Line
G	Existing Gas Line
	Existing Building Line
———————	Existing Chainlink Fence Line
\bigcirc	Existing Tree
	Existing Type II Storm Manhole
	Existing Type I Storm Catch Basin
\bigcirc	Existing Sewer Manhole
$\varphi \longrightarrow \swarrow$	Existing Light Pole
-0-	Existing Power Pole

TESC NOTES

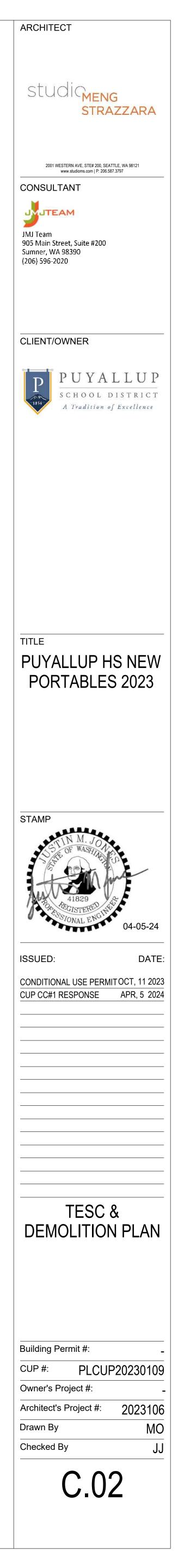
- 1. Contractor to install TESC measures as necessary to ensure stormwater leaving the site is free of settleable solids.
- 2. Install and maintain construction entrance per City of Puyallup Standard Detail 05.01.01 and
- install wheel wash as needed per Washington DOE BMP C106. 3. Install silt fence per City of Puyallup Standard Detail 02.03.02. Silt Fence to mark clearing limits in the field.
- Maintain and Install storm drain inlet protection in all existing catch basins within the project vicinity per WSDOT Standard Plan I-40.20-00 and storm drain barriers per City of Puyallup Standard Details 02.03.05 and 02.03.06.
- 5. Roads shall be cleared thoroughly as needed to protect stormwater infrastructure and downstream water resources. Sediment shall be removed from roads by shoveling or pickup sweeping and be transported to a controlled sediment disposal area.
- 6. Exposed soils shall be watered as necessary to prevent dust from leaving the site.
- 7. Concrete handling and equipment washing in accordance with DOE BMP C151.
- 8. Disturbed soils to be amended per DOE BMP T5.13
- 9. If necessary, alternative sediment control methods shall be submitted by the contractor for review and approval prior to construction.
- 10. A CESCL shall be present on-site or on-call for the duration of construction operations.

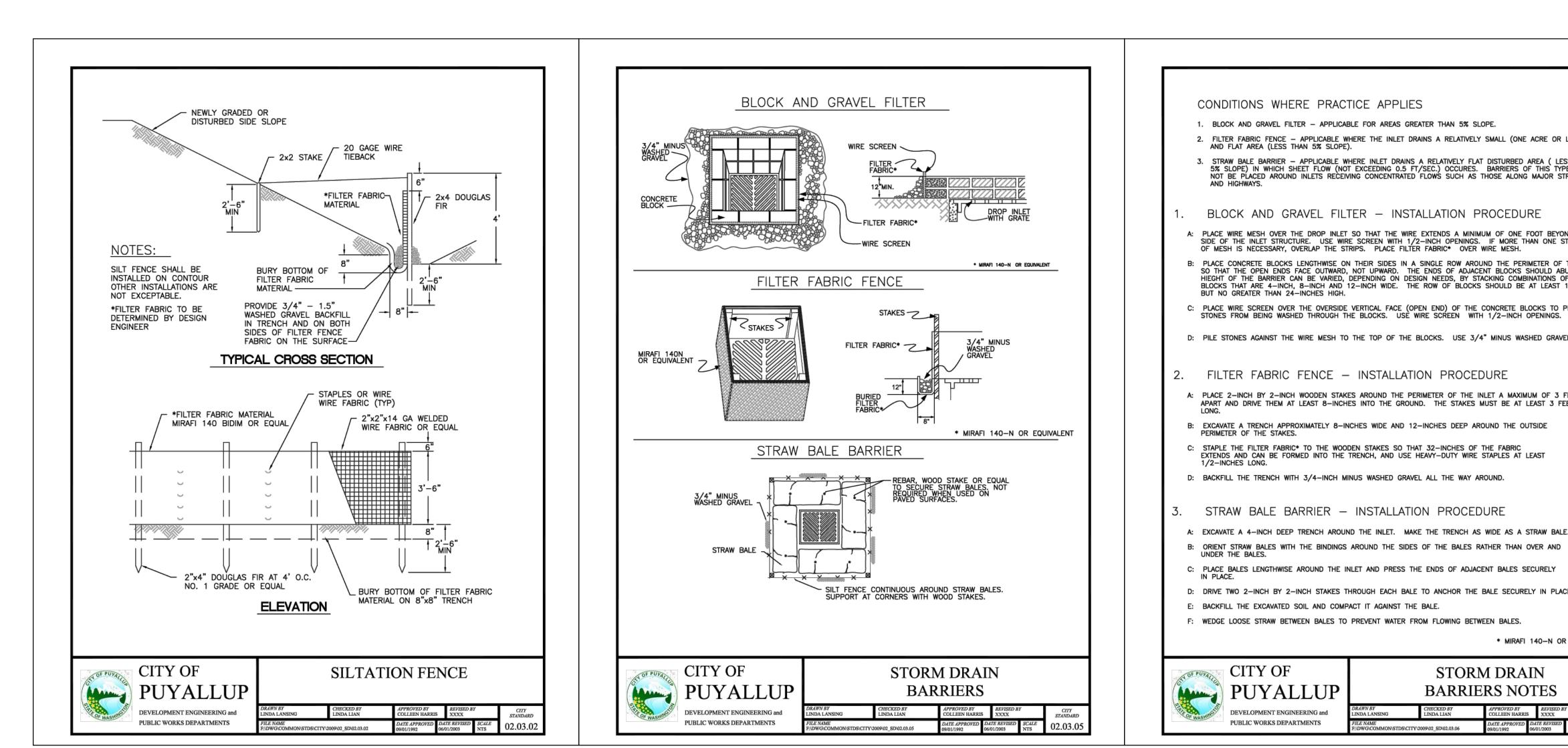
DEMOLITION NOTES

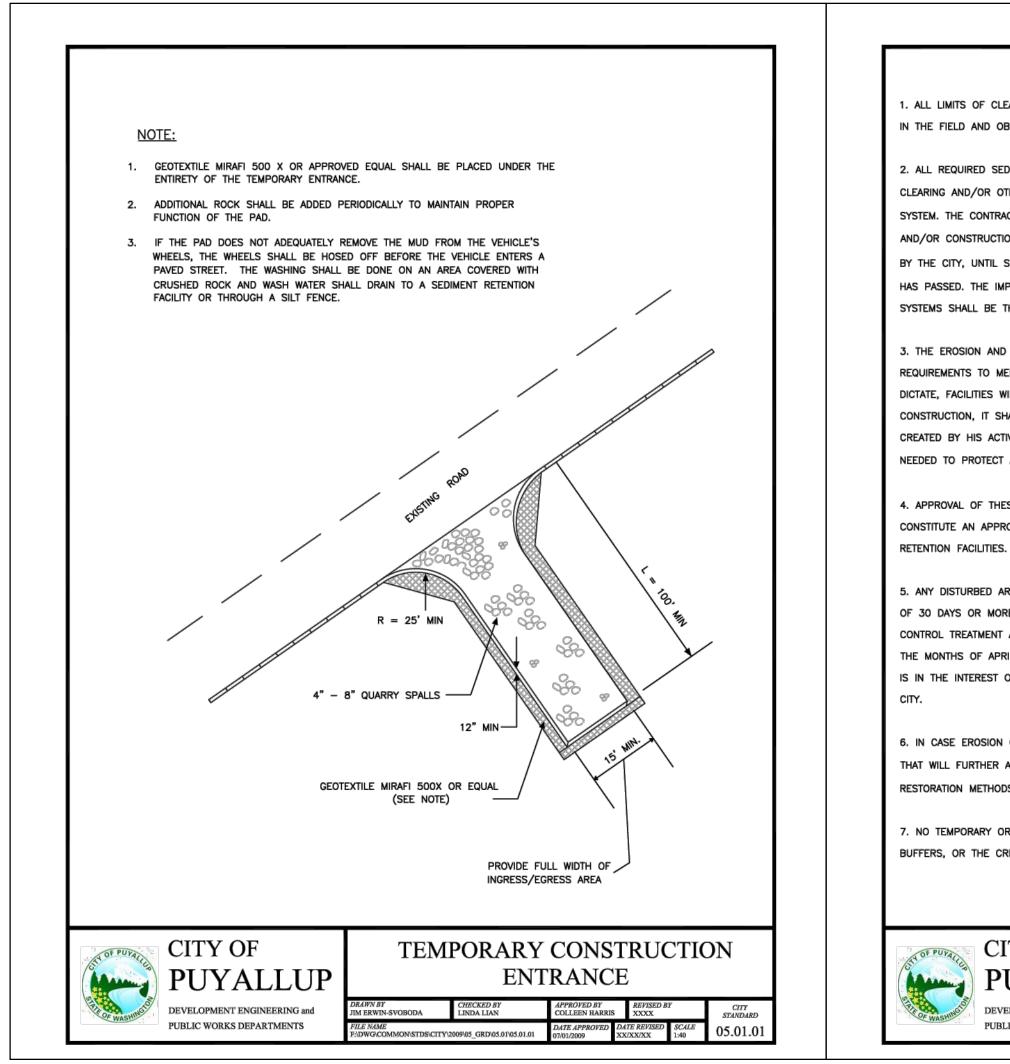
- Landscaping to be Cleared & Grubbed: 14,165 SF
- Concrete to be Removed: 275 SF
- Disturbed Area On-site: 14,165 SF











COPYRIGHT 2023 studio Meng Strazzara

1. ALL LIMITS OF CLEARING AND AREAS OF VEGETATION PRESERVATION AS PRESCRIBED ON THE PLANS SHALL BE CLEARLY FLAGGED IN THE FIELD AND OBSERVED DURING CONSTRUCTION.

2. ALL REQUIRED SEDIMENTATION AND EROSION CONTROL FACILITIES MUST BE CONSTRUCTED AND IN OPERATION PRIOR TO ANY LAND CLEARING AND/OR OTHER CONSTRUCTION TO ENSURE THAT SEDIMENT LADEN WATER DOES NOT ENTER THE NATURAL DRAINAGE SYSTEM. THE CONTRACTOR SHALL SCHEDULE AN INSPECTION OF THE EROSION CONTROL FACILITIES PRIOR TO ANY LAND CLEARING AND/OR CONSTRUCTION. ALL EROSION AND SEDIMENT FACILITIES SHALL BE MAINTAINED IN A SATISFACTIRY CONDITION AS DETERMINED BY THE CITY, UNTIL SUCH TIME THAT CLEARING AND/OR CONSTRUCTION IS COMPLETED AND THE POTENTIAL FOR ON-SITE EROSION HAS PASSED. THE IMPLEMENTATION, MAINTENANCE, REPLACEMENT, AND ADDITIONS TO THE EROSION AND SEDIMENTATION CONTROL SYSTEMS SHALL BE THE RESPONSIBILITY OF THE PERMITEE.

3. THE EROSION AND SEDIMENTATION CONTROL SYSTEM FACILITIES DEPICTED ON THESE PLANS ARE INTENDED TO BE MINIMUM REQUIREMENTS TO MEET ANTICIPATED SITE CONDITIONS. AS CONSTRUCTION PROGRESSES AND UNEXPECTED OR SEASONAL CONDITIONS DICTATE, FACILITIES WILL BE NECESSARY TO ENSURE COMPLETE SILTATION CONTROL ON THE SITE. DURING THE COURSE OF CONSTRUCTION, IT SHALL BE THE OBLIGATION AND RESPONSIBILITY OF THE PERMITEE TO ADDRESS ANY NEW CONDITIONS THAT MAY BE CREATED BY HIS ACTIVITIES AND TO PROVIDE ADDITIONAL FACILITIES, OVER AND ABOVE THE MINIMUM REQUIREMENTS, AS MAY BE NEEDED TO PROTECT ADJACENT PROPERTIES, SENSITIVE AREAS, NATURAL WATER COURSES, AND/OR STORM DRAINAGE SYSTEMS.

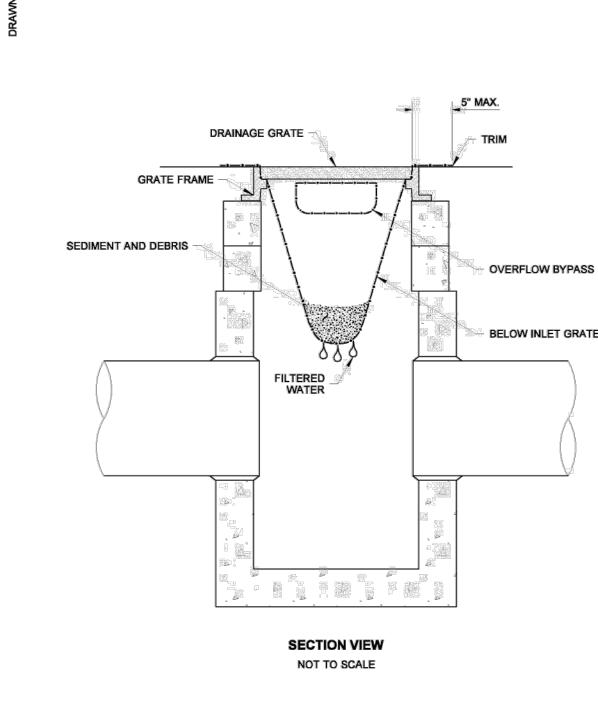
4. APPROVAL OF THESE PLANS IS FOR GRADING, TEMPORARY DRAINAGE, EROSION AND SEDIMENTATION CONTROL ONLY. IT DOES NOT CONSTITUTE AN APPROVAL OF PERMANENT STORM DRAINAGE DESIGN, SIZE OR LOCATION OF PIPES, RESTRICTORS, CHANNELS, OR RETENTION FACILITIES.

5. ANY DISTURBED AREA WHICH HAS BEEN STRIPPED OF VEGETATION AND WHERE NO FURTHER WORK IS ANTICIPATED FOR A PERIOD OF 30 DAYS OR MORE, MUST BE IMMEDIATELY STABILIZED WITH MULCHING, GRASS PLANTING, OR OTHER APPROVED EROSION CONTROL TREATMENT APPLICABLE TO THE TIME OF YEAR IN QUESTION. GRASS SEEDING ALONE WILL BE ACCEPTABLE ONLY DURING THE MONTHS OF APRIL THROUGH SEPTEMBER INCLUSVE. SEEDING MAY PROCEED OUTSIDE THE SPECIFIED TIME PERIOD WHENEVER IT IS IN THE INTEREST OF THE PERMITEE BUT MUST BE AUGMENTED WITH MULCHING, NETTING, OR OTHER TREATMENT APPROVED BY THE

6. IN CASE EROSION OR SEDIMENTATION OCCURS TO ADJACENT PROPERTIES, ALL CONSTRUCTION WORK WITHIN THE DEVELOPMENT THAT WILL FURTHER AGGRAVATE THE SITUATION MUST CEASE, AND THE OWNER/CONTRACTOR WILL IMMEDIATELY COMMENCE RESTORATION METHODS. RESTORATION ACTIVITY WILL CONTINUE UNTIL SUCH TIME AS THE AFFECTED PROPERTY OWNER IS SATISFIED.

7. NO TEMPORARY OR PERMANENT STOCKPILING OF MATERIALS OR EQUIPMENT SHALL OCCUR WITHIN CRITICAL AREAS OR ASSOCIATED BUFFERS, OR THE CRITICAL ROOT ZONE FOR VEGETATION PROPOSED FOR RETENTION.

CITY OF		ADING, E		· ·		
PUYALLUP	SEDIMENTATION CONTROL NOTES					
DEVELOPMENT ENGINEERING and	DRÁWN BY JIM ERWIN-SVOBODA	CHECKED BY LINDA LIAN	APPROVED BY COLLEEN HARRIS	REVISED B. XXXX	Y	CITY STANDARD
PUBLIC WORKS DEPARTMENTS	FILE NAME F:\DWG\COMMON\STDS\CITY\2	009\05_GRD\05.01\05.02.01		DATE REVISED X/XX/XX	SCALE 1:1	05.02.01



OPE.	
SMALL (ONE ACRE OR LESS)	
T DISTURBED AREA (LESS THAN BARRIERS OF THIS TYPE SHOULD THOSE ALONG MAJOR STREETS	
ROCEDURE	
UM OF ONE FOOT BEYOND EACH IF MORE THAN ONE STRIP WIRE MESH.	
UND THE PERIMETER OF THE INLET, ENT BLOCKS SHOULD ABUT. THE ACKING COMBINATIONS OF SHOULD BE AT LEAST 12-INCHES	
CONCRETE BLOCKS TO PREVENT 1 1/2-INCH OPENINGS.	
4" MINUS WASHED GRAVEL.	
DURE	
NLET A MAXIMUM OF 3 FEET MUST BE AT LEAST 3 FEET	
OUND THE OUTSIDE	
THE FABRIC STAPLES AT LEAST	
ROUND.	
URE	
WIDE AS A STRAW BALE.	
ATHER THAN OVER AND	
ENT BALES SECURELY	
BALE SECURELY IN PLACE.	
EN BALES.	
* MIRAFI 140-N OR EQUIVALENT	

CITY STANDARD

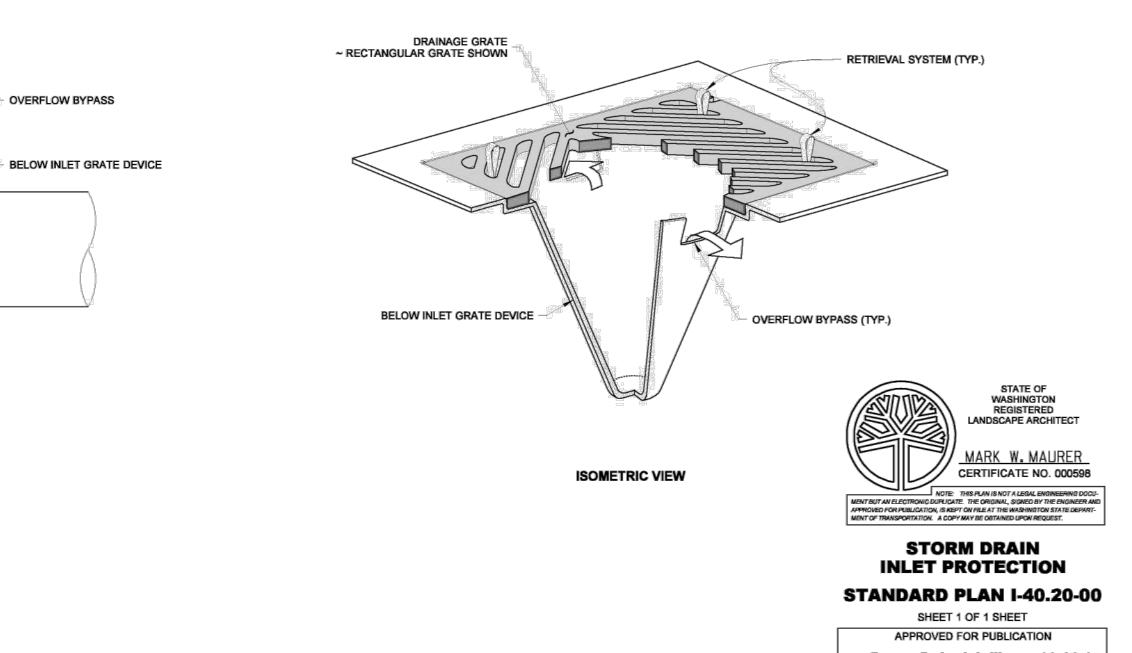
02.03.06

 Size the Below Inlet Grate Device (BIGD) for the storm water structure it will service.

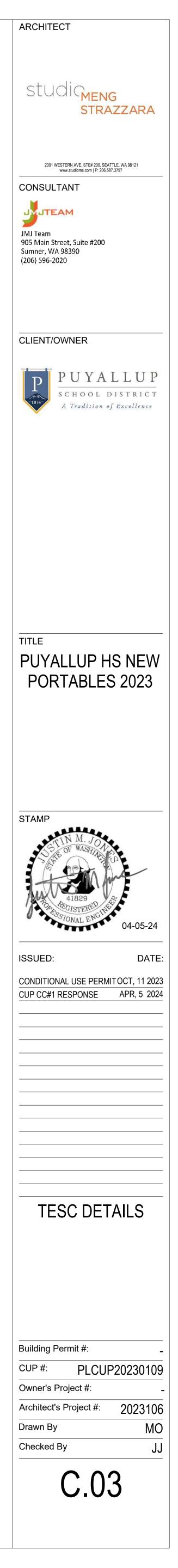
2. The BIGD shall have a built-in high-flow relief system (overflow bypass).

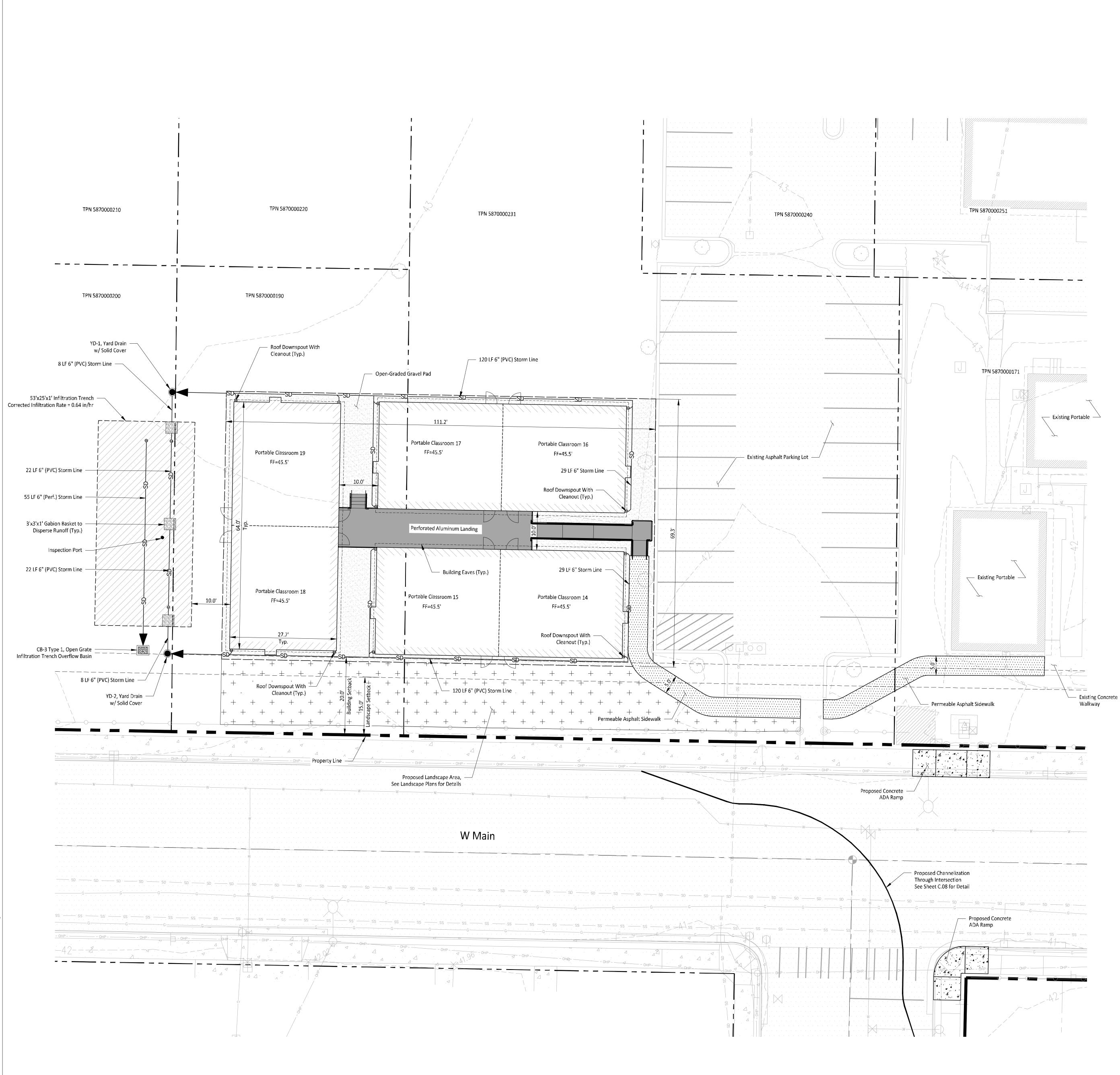
3. The retrieval system must allow removal of the BIGD without spilling the

collected material.
 Perform maintenance in accordance with Standard Specification 8-01.3(15).



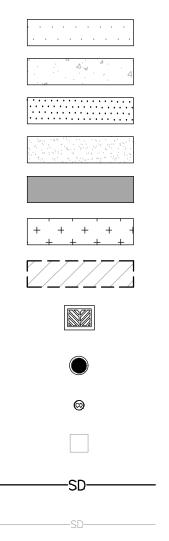
Pasco Bakotich III 09-20-07 STATE DESIGN ENGINEER DATE Washington State Department of Transportation





© COPYRIGHT 2023 studio Meng Strazzari

LEGEND



Existing Asphalt Existing Concrete Proposed Permeable Asphalt Proposed Open-Graded Gravel Proposed Perforated Aluminum Landing Proposed Landscape Area Proposed Infiltration Trench Proposed Catch Basin Type 1, Open Grate Proposed Cleanout Existing Catch Basin

Proposed Storm Drain Line Existing Storm Drain Line

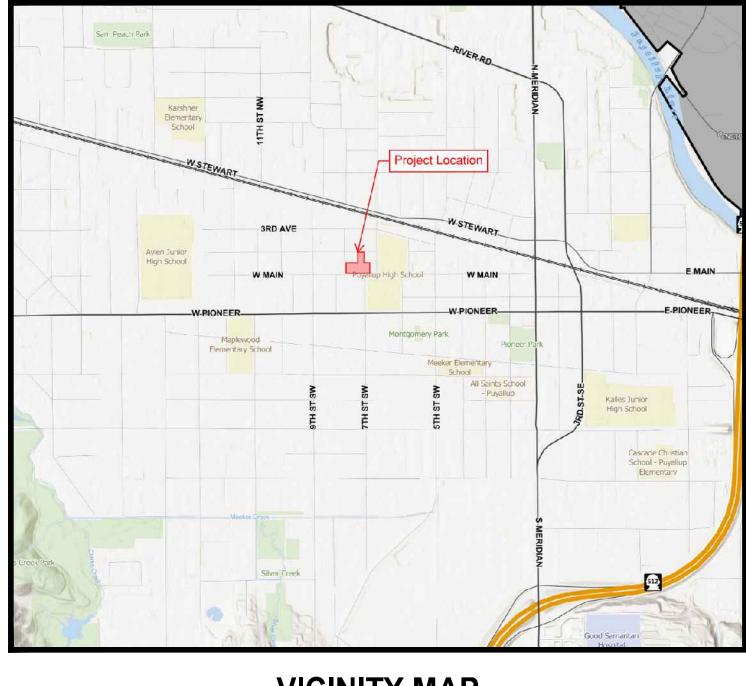
SITE DATA

- Total Lot Area:
 - ea: 43,574 SF (1.00 AC)
- Total Project Site Area:
 Tax Parcel Numbers:
- 16,587 SF (0.38 AC) 5870000171, 5870000190, 587000020
- Zoning:

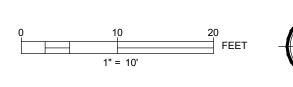
5870000171, 5870000190, 5870000200, 5870000231 PF- Public Facilities

PROPOSED LOT COVERAGE

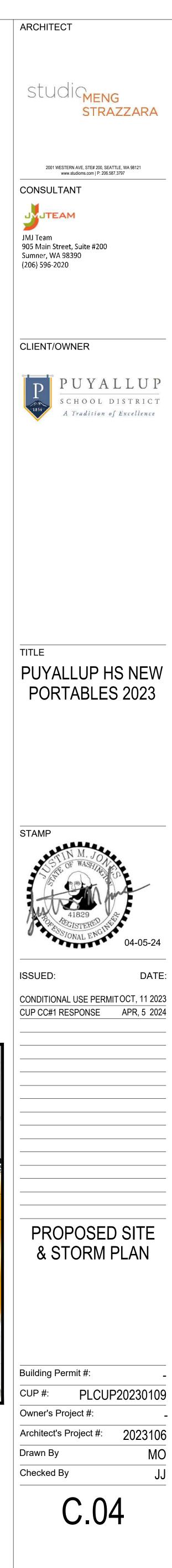
Total Lot Area	43,574 SF (1.00 AC)					
Coverage	Area (SF)	Area (AC)	% of Site			
Impervious						
Ex. Roof	1,722	0.04				
Ex. Concrete Sidewalk	964	0.03				
Ex. Asphalt Parking Lot	6,686	0.15				
New Roof	5,785	0.12				
New Permeable Asphalt Sidewalk	663	0.02				
New Open-Graded Gravel Pad	1,570	0.04				
New Perforated Aluminum Landing	660	0.02				
Total New Impervious	8,678	0.20	20.0%			
Total Site Impervious	18,050	0.42	42.0%			
Pervious						
Landscape	25,524	0.58				
Total Site Pervious	25,524	0.58	58.0%			

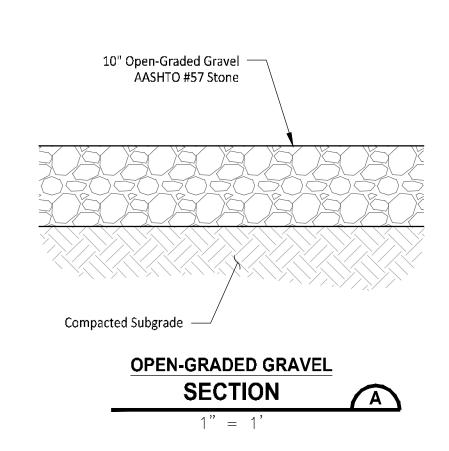


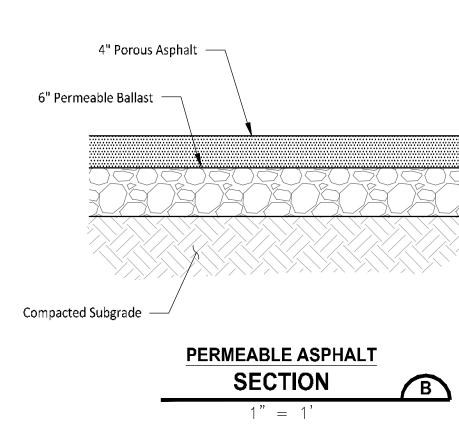
VICINITY MAP

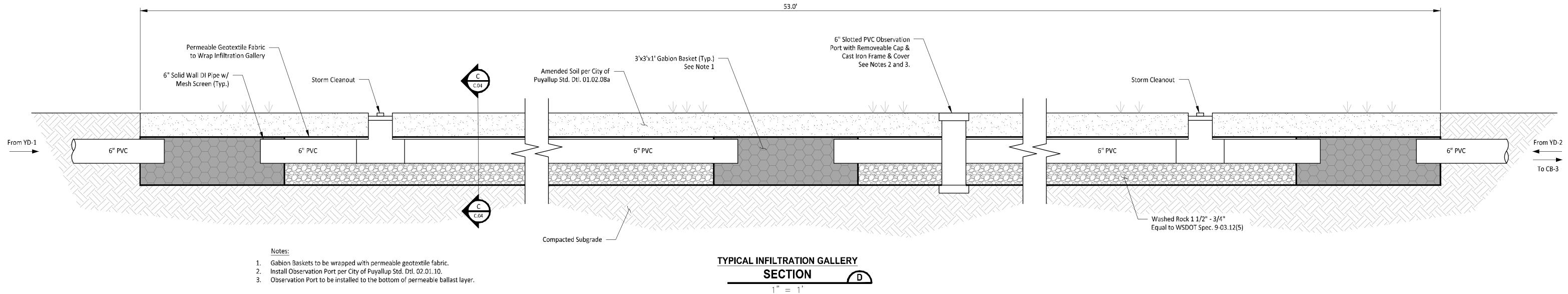


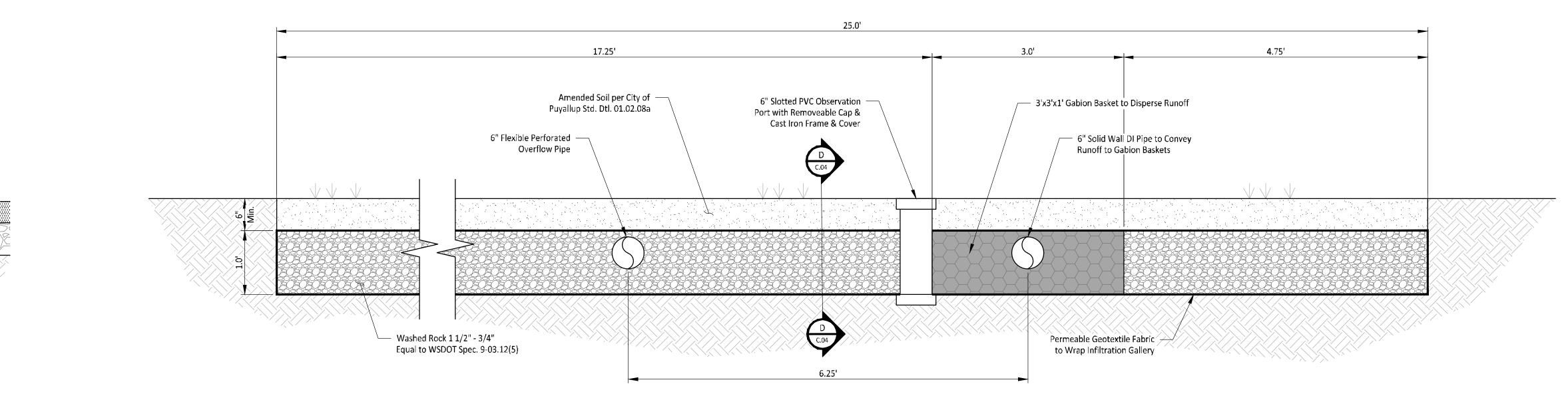


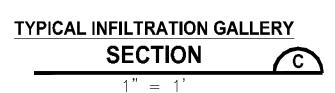


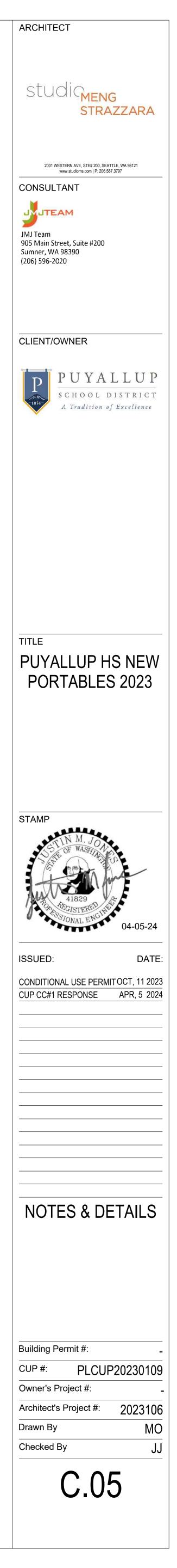


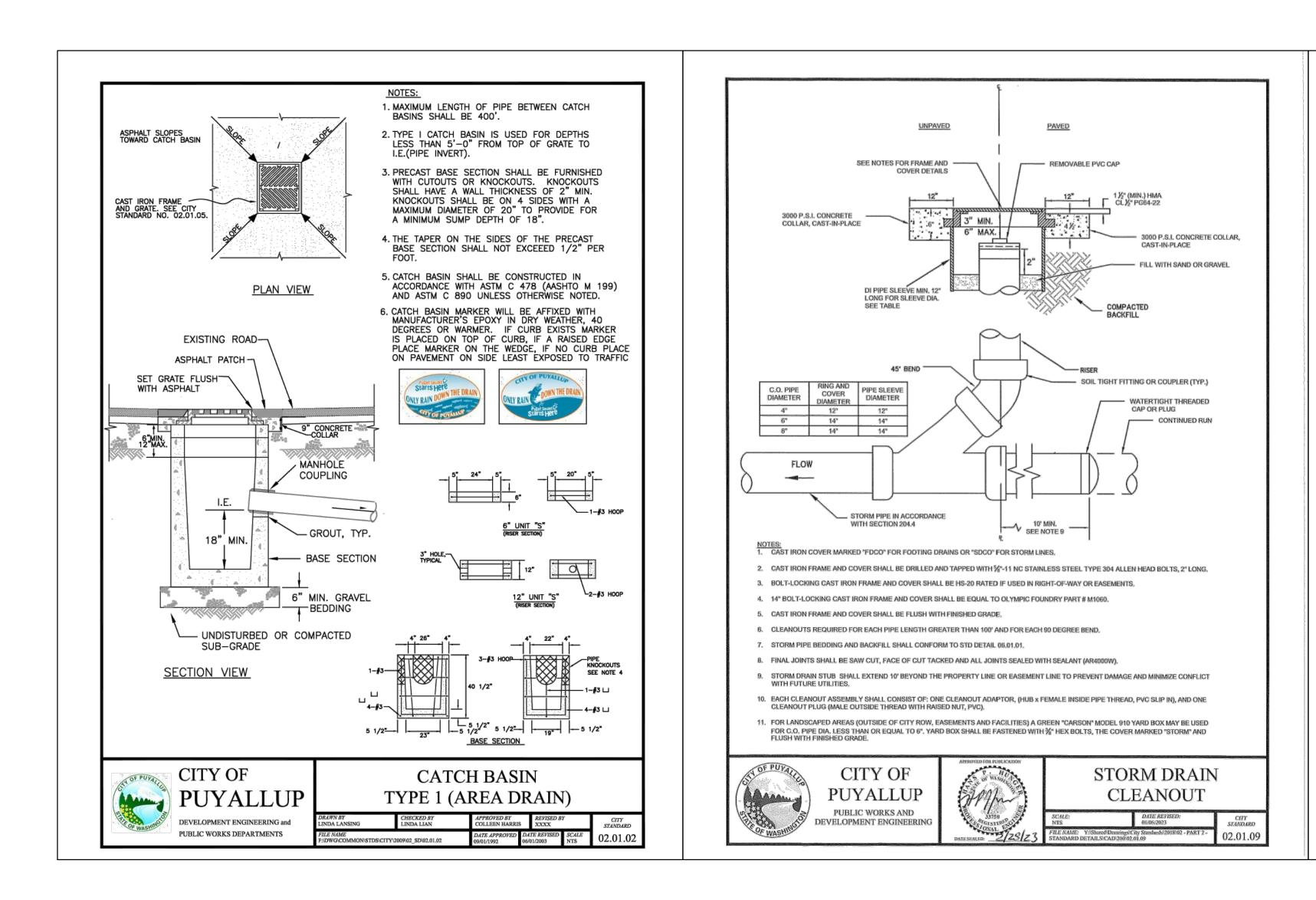


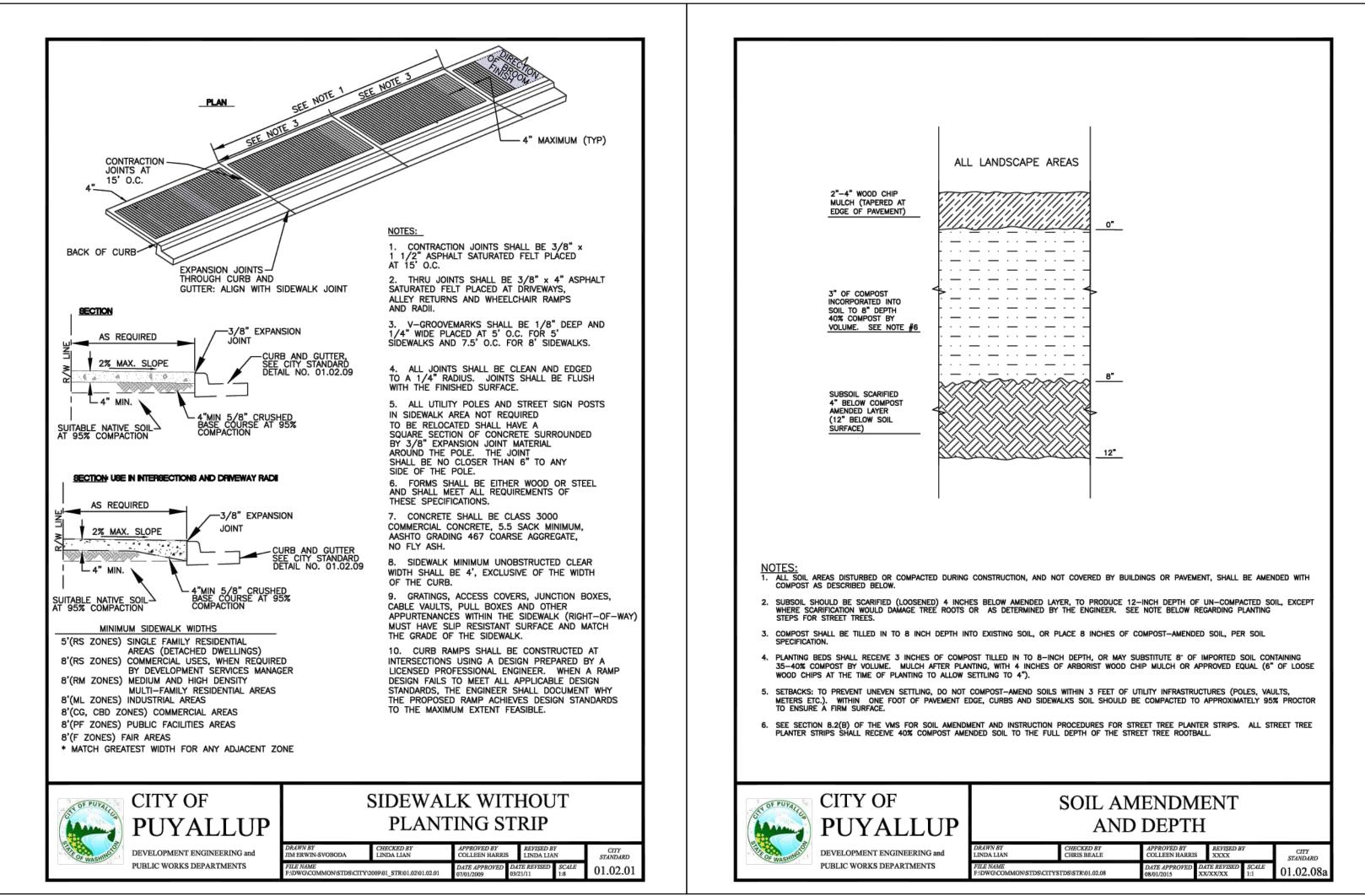


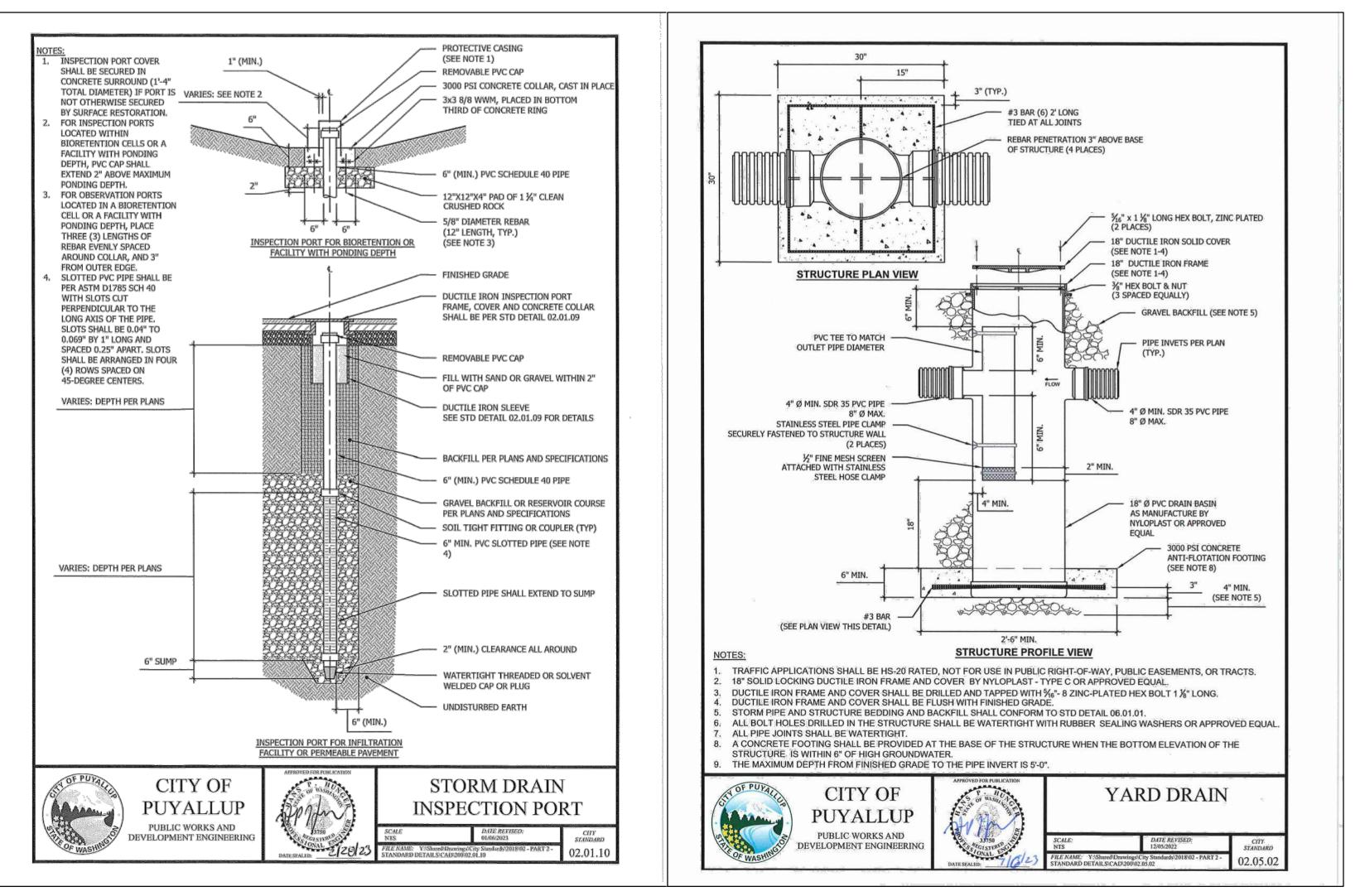




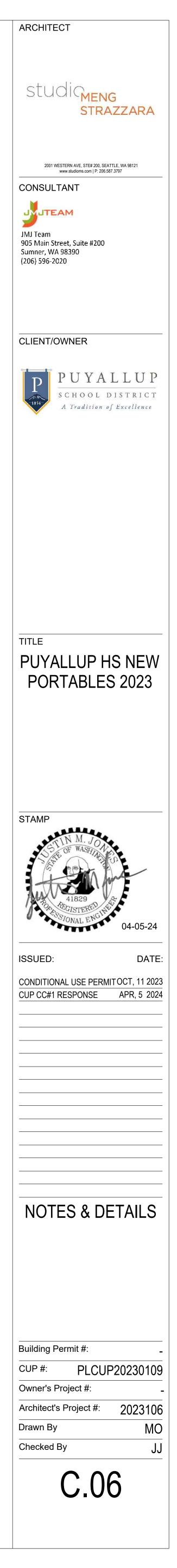


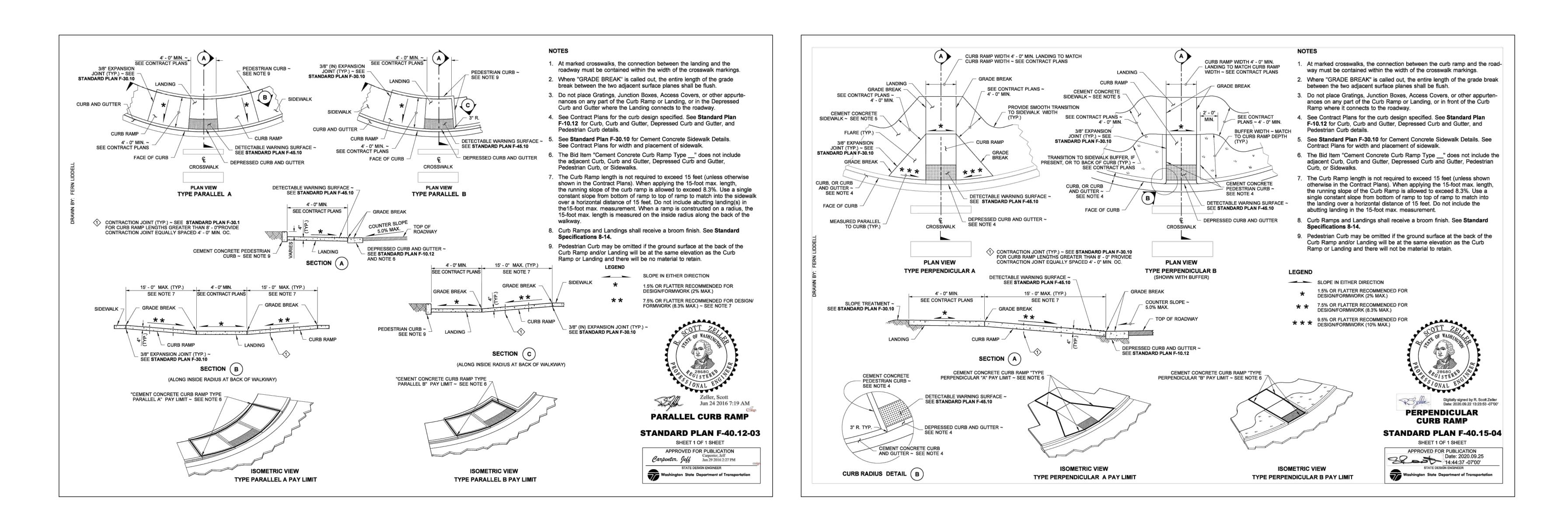


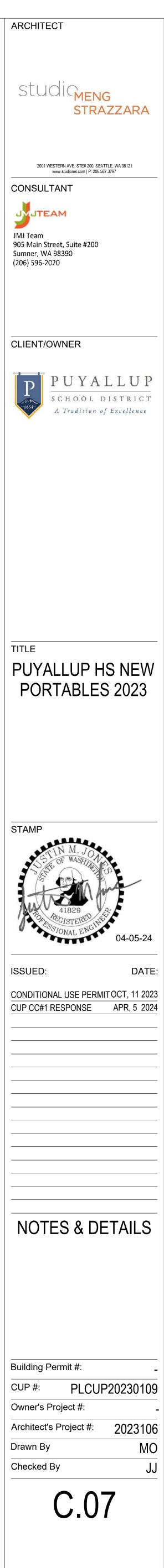


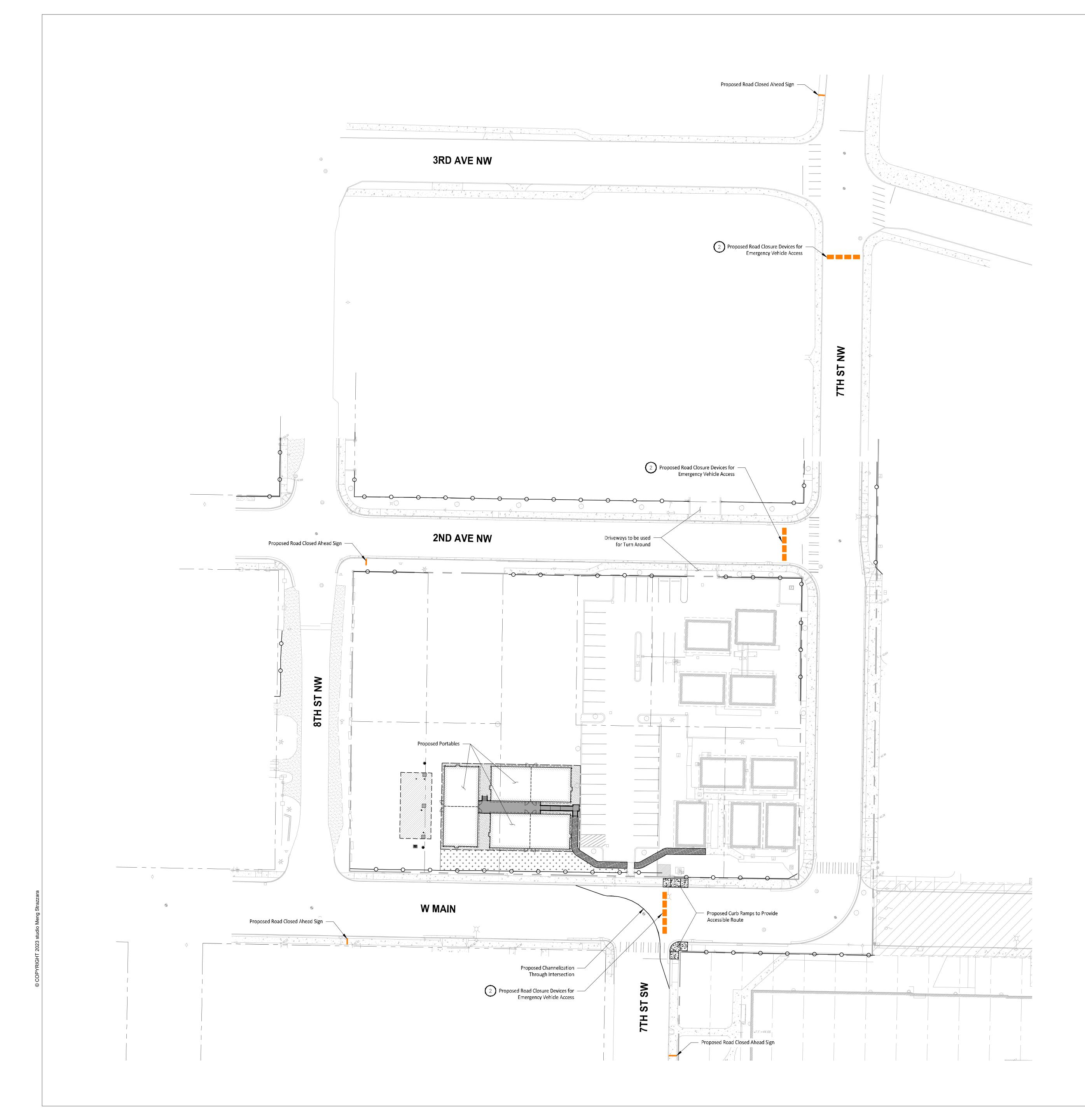


N. I.	CITY OF PUYALLUP	SOIL AMENDMENT AND DEPTH					
NO	DEVELOPMENT ENGINEERING and	DRAWN BY LINDA LIAN	CHECKED BY CHRIS BEALE	APPROVED BY COLLEEN HARRIS	REVISED B XXXX	Y	CHTY STANDARD
80	PUBLIC WORKS DEPARTMENTS	FILE NAME F:\DWG\COMMON\STDS\CITYS	TDS\STR\01.02.08	DATE APPROVED 12 08/01/2015 2	DATE REVISED XX/XX/XX	SCALE 1:1	01.02.08a







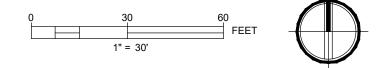


GENERAL NOTE

- Intersection and Advanced Signage for road closure to meet Manual on Uniform Traffic Control Devices (MUTCD) and City of Puyallup Standards as part of future ROW and Civil Plans.
- 2. Road Closure Device to be Reflective Water Filled Barrier(s) or another MUTCD compliant feature as requested by the City of Puyallup.



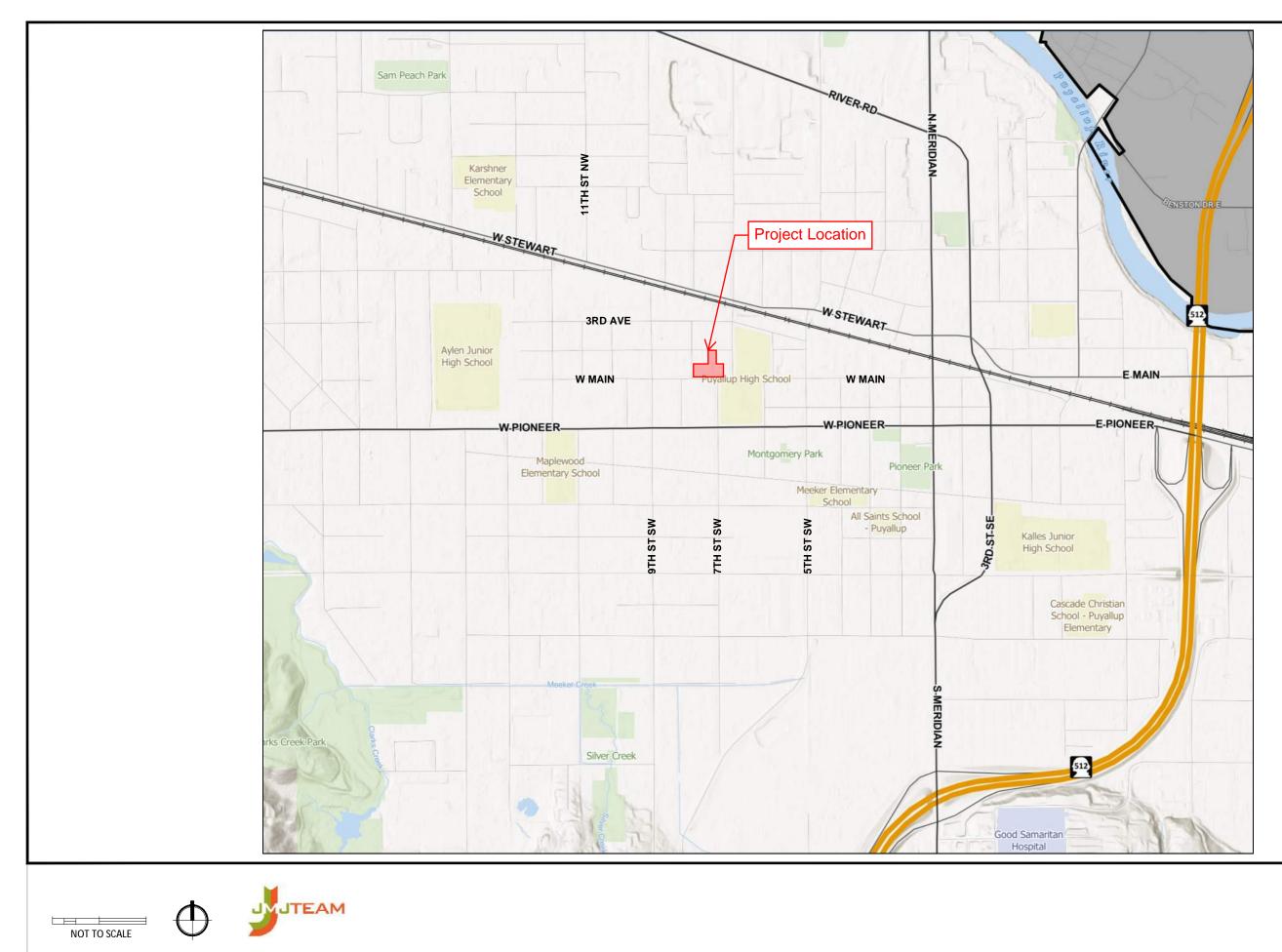
PLASTIC WATER FILLED BARRIER EXAMPLE A NOT TO SCALE





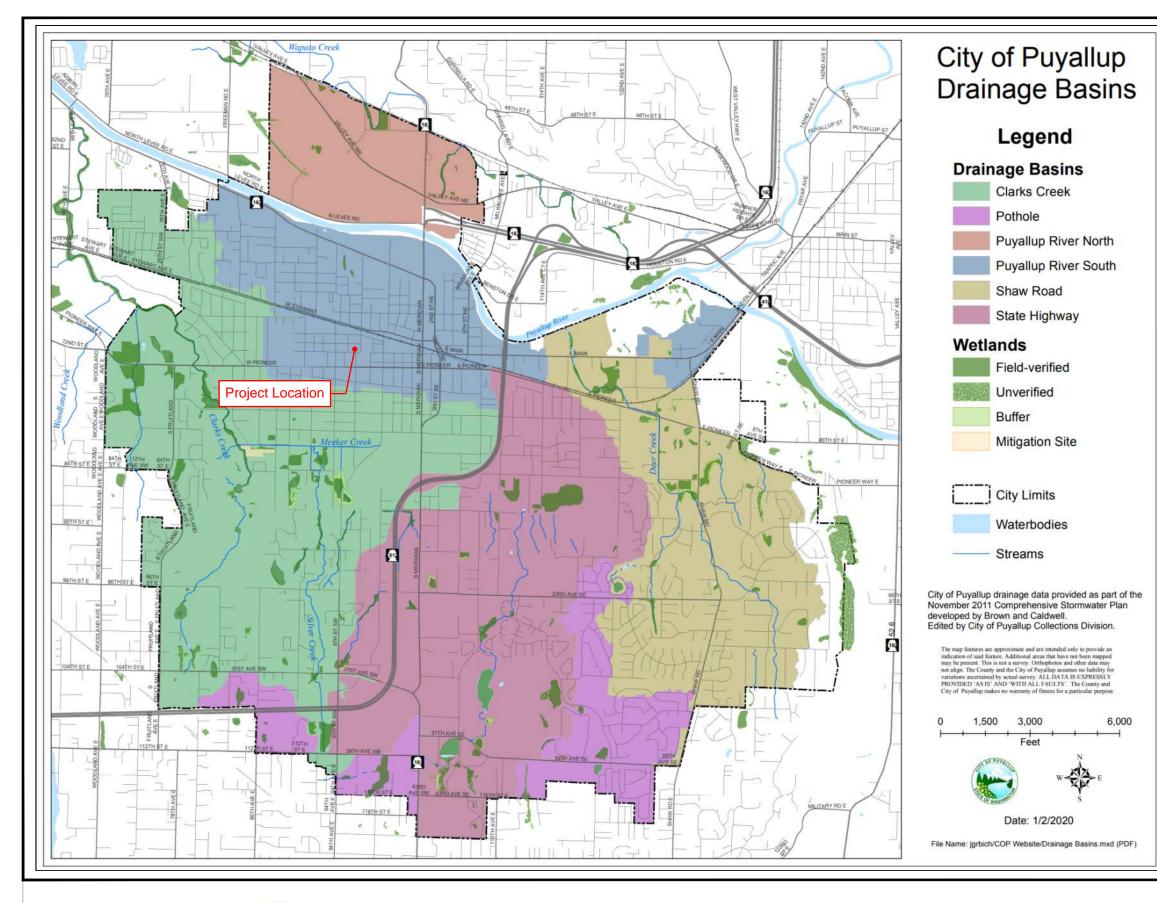
ARCHITECT studicmeng STRAZZARA 2001 WESTERN AVE, STE# 200, SEATTLE, WA 98121 www.studioms.com | P: 206.587.3797 CONSULTANT JUTEAM JMJ Team 905 Main Street, Suite #200 Sumner, WA 98390 (206) 596-2020 CLIENT/OWNER PUYALLUP D SCHOOL DISTRICT A Tradition of Excellence TITLE PUYALLUP HS NEW PORTABLES 2023 STAMP ALLA. A DIVAL 04-05-24 ISSUED: DATE: CONDITIONAL USE PERMITOCT, 11 2023 CUP CC#1 RESPONSE APR, 5 2024 7TH STREET SW ROAD CLOSURE PLAN Building Permit #: CUP #: PLCUP20230109 Owner's Project #: 2023106 Architect's Project #: МО Drawn By Checked By JJ **C.08**

APPENDIX B





PHS Portables Vicinity Map Figure 1

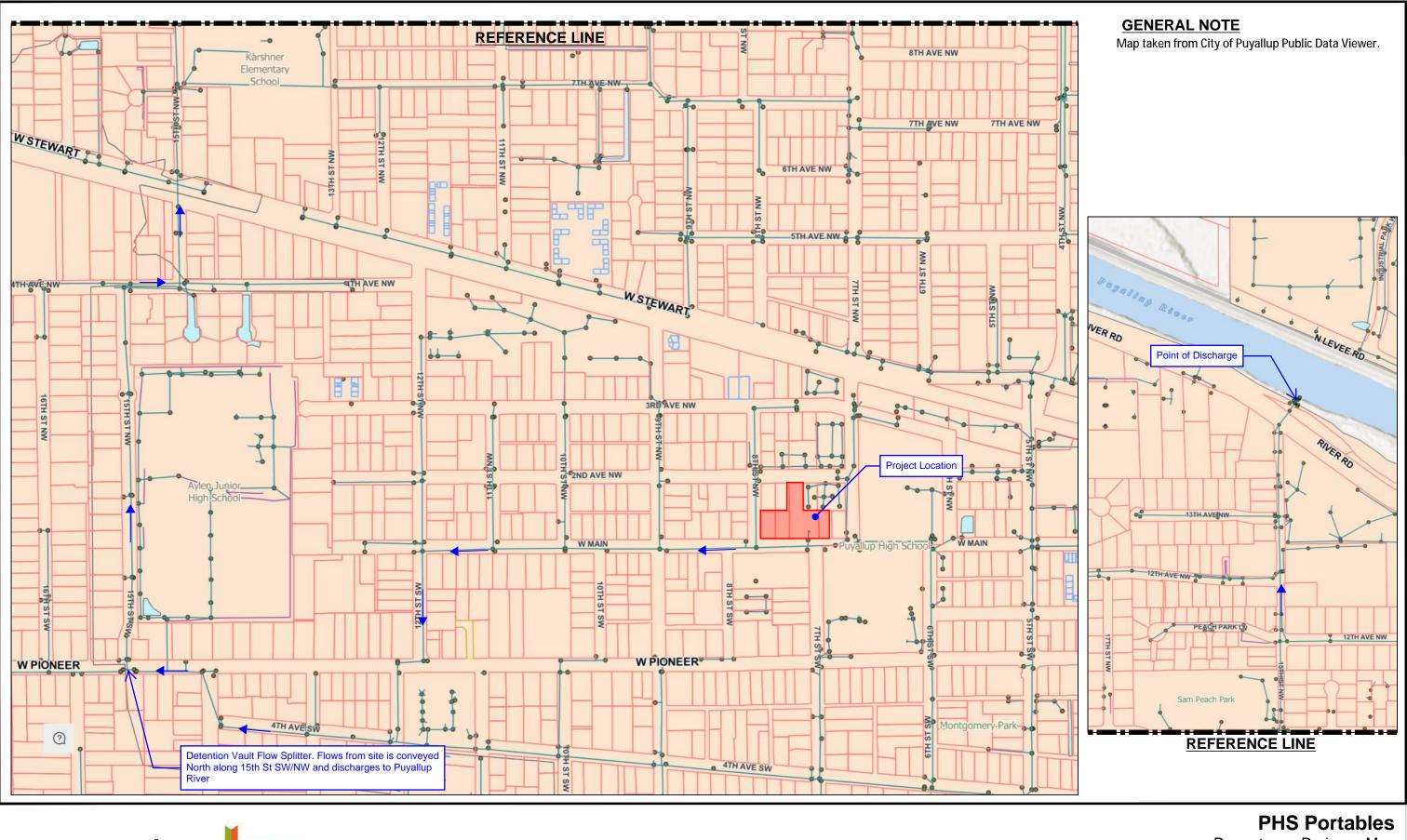


 \oplus

NOT TO SCALE

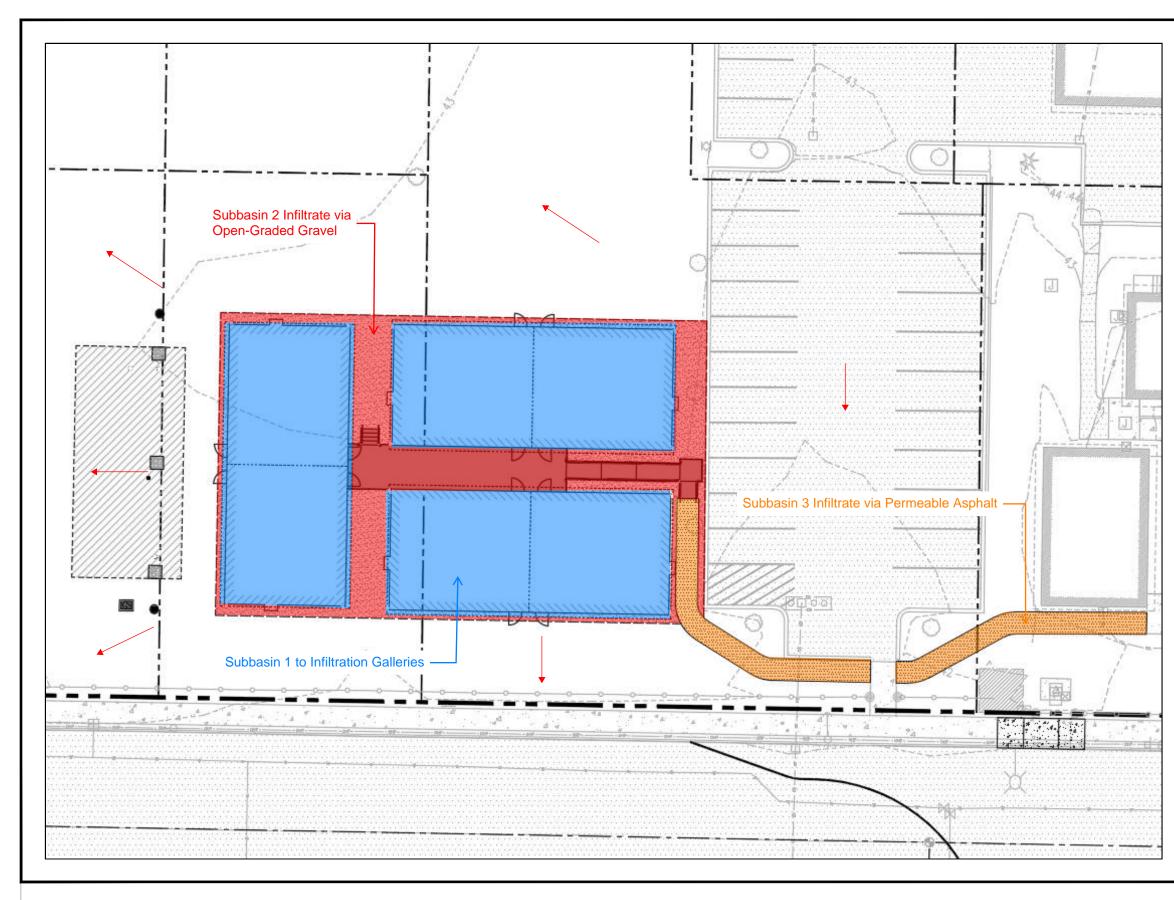
PHS Portables Drainage Basin Map

Figure 2

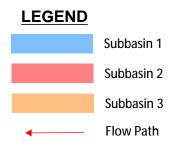


NOT TO SCALE

Downstream Drainage Map Figure 3







PROPOSED BASINS

Subbasin 1:		
Impervious:		
Roof:	5,785 SF	
Total:	5,785 SF	(0.12 AC)
Subbasin 2:		
Impervious:		
Perm. Gravel:	1,570 SF	
Landing:	660 SF	
Total:	2,230 SF	(0.05 AC)
Subbasin 3:		
Impervious:		
Perm. Asphalt:	663 SF	
Total:	663 SF	(0.02 AC)

PHS Portables

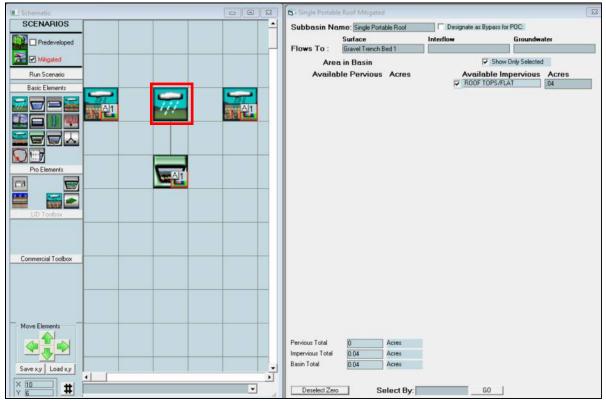
Proposed Basin Map . Figure 4

APPENDIX C

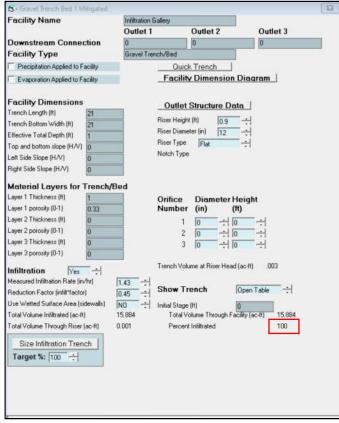
WWHM MODELING

1.0 DOWNSPOUT INFILTRATION:

1.1 Schematic and Basin Areas



1.2 Infiltration Gallery Element

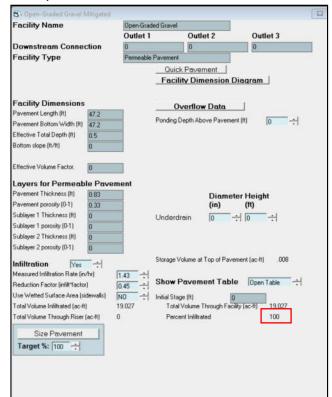


2.0 OPEN-GRADED GRAVEL:

2.1 Schematic



2.2 Open-Graded Gravel Element



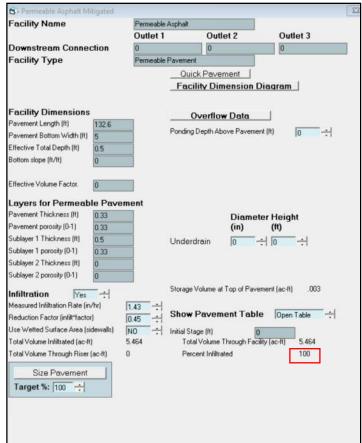
Element area includes gravel pad and landing as runoff from perforated landing will drain through slots and infiltrate into open-graded gravel pad.

3.0 PERMEABLE ASPHALT WALKWAY:

3.1 Schematic



3.2 Permeable Asphalt Element



APPENDIX D

Infiltration Testing Report

Puyallup High School Portables

711, 721 & 701 West Main Puyallup, WA

Prepared for

Puyallup School District c/o Studio Meng Strazzara 2001 Western Ave, Suite 200 Seattle, WA 98121 206.587.3797

Prepared by

JMJ TEAM 905 Main St, Suite 200 Sumner, WA 98390 206.596.2020 Justin Jones, PE



PROJECT ENGINEER'S CERTIFICATION

I hereby certify that this Infiltration Testing Report for Puyallup High School Portables has been prepared by me or under my supervision and meets minimum standards of the Department of Ecology Stormwater Management Manual for Western Washington.

Justin Jones, PE





TABLE OF CONTENTS

Summary	1
nfiltration Test Procedures	3
Findings and Recommendations	4
Test Pit Photo Documentation	7

Appendix A: Data Collection Sheets

Appendix B: Pressure Transducer Specification Sheet

Appendix C: Department of Ecology PIT Procedure

Appendix D: Department of Ecology Factor of Safety Guidelines



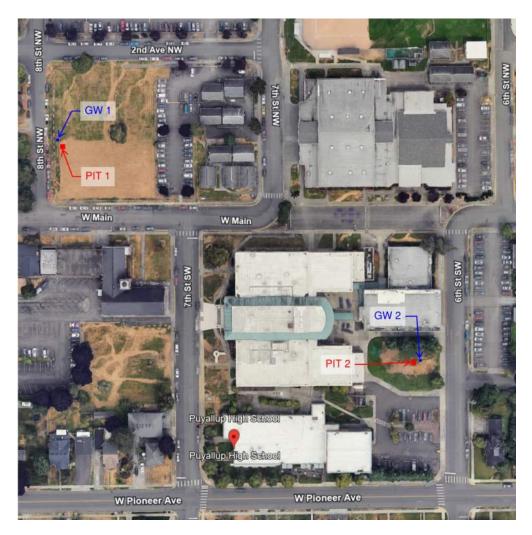
SUMMARY

This report details the results of infiltration testing for use in the stormwater system design of Puyallup High School Portables located within Puyallup, WA. Two (2) Small-Scale Pilot Infiltration Tests (PIT) were conducted on site to determine the onsite stormwater infiltration rate. The test holes were excavated and backfilled by a licensed contractor and the PIT was completed in accordance with the Department of Ecology (ECY) Stormwater Management Manual for Western Washington (Stormwater Manual).

The PIT process evaluates the infiltration within a 12 SF area by first measuring the rate of water required to maintain a constant water elevation of approximately 12-inches in the test pit, and second by measuring the drawdown rate of the water within the test pit. The drawdown is done using a data logger.

The field data is then analyzed, and a factor of safety is applied to determine the stormwater design infiltration rate. Below is a summary of the results.

Test Pit and Ground Water Monitoring Location



Summary of Results

Per the PIT, the site soil is suitable for stormwater infiltration. Soil evaluations were not taken as the designed stormwater BMP is not intended to treat pollution generating surfaces.

Testing	Test PIT	Results	ECY Threshold		
	Pit Depth	4.0-feet	N/A		
Ground Water	Test Hole 1 Groundwater Level	Ground Water Observed at 4.0'	N/A		
Ground Water	Test Hole 2 Groundwater Level	Ground Water Observed at 3.5' Depth	N/A		
	Infiltration Rate Factor of Safety	0.45	N/A		
		Uncorrected: 1.43 inches per hour			
Infiltration Rate	Test Hole 1 Infiltration Rates	Design: 0.64 Inches per hour	≥ 0.3 inches per hour		
		Uncorrected: 4.42 inches per hour			
	Test Hole 2 Infiltration Rates	est Hole 2 Infiltration Rates Design: 1.99 inches per hour			
	Test Hole 1 Lab Analysis	CEC Value: N/A	≥ 5.0 milliequivalents CEC/100g		
		Organic Content: N/A	≥ 1.0%		
Water Quality	Test Hole 2 Lab Analysis	CEC Value: N/A	≥ 5.0 milliequivalents CEC/100g		
		Organic Content: N/A	≥ 1.0%		

INFILTRATION TEST PROCEDURES

Below is the process taken for the Small-Scale PIT:

- □ Identify PIT locations based on the site survey of existing buildings and utilities as well as the potential locations of infiltration facilities based on the preliminary site plan.
- Obtain public and private utility locates. Prior to the PIT utility locates will be called to ensure there are no utilities present in the PIT locations.
- Excavation of PIT holes (approximately 3-feet x 4-feet x 2-feet deep). A 3-feet x 4-feet x 2-feet tall wood box is inserted into the test hole to ensure that the bottom surface area is exactly 12 SF. The box is backfilled to the top edge to ensure stability and infiltration only through the bottom of the test hole for the duration of the PIT.
- A soil sample is collected from the bottom of the hole to test treatment capability. A lab tests the cation exchange rate and organic matter content of soils. Lab results confirm if the soil is suitable for treatment based on Stormwater Manual criteria.
- □ A float system with a water hose connection is set into the center of the test hole. The float system is equipped with a leveling plate, a measuring ruler for visual inspection of water levels and a perforated pipe housing for the data collector.
- Using water transfer tanks or hose spigot as available, the test hole is filled to a 12-inch water depth that is maintained. The presoak period ensures that the soil has been fully saturated before conducting the PIT. A 1-hour stabilization test is performed after the presoak period to confirm soil stabilization. If the test yields 4 constant gallon per minute (GPM) readings that are conducted every 15-minutes, the stabilization of the soil is confirmed.
- A 1-hour GPM test is conducted per the Stormwater Manual. Using a water meter accurate to the nearest tenth of a gallon, a GPM flow rate is recorded every 15-minutes while the water level is maintained at a 12-inch depth. An infiltration rate (in/hr) can be determined using the GPM flow rate and the 12 SF bottom surface area of the hole.
- A drawdown test is performed per Stormwater Manual to determine the drawdown infiltration capability of the soil. A CRS451V (Pressure Transducer) is placed into the test hole and set to take pressure (PSI) readings every 10-minutes. The water source is shut off, and the pressure transducer will measure water drawdown for a 2-hour period. At the end of the period the sensors are removed from the test hole, the data is collected using a PC interface module and the HydroSci program to communicate with the sensor to retrieve the data.
- □ The wood box and the float system are removed from the test hole.
- □ The test hole is then over excavated to confirm there is no ground water mounding.
- □ The test pit then gets backfilled and restored to prior state of excavation.

FINDINGS AND RECOMMENDATIONS

Groundwater Conditions

The Stormwater Manual specifies minimum separations between the seasonal high groundwater elevation and the bottom of the infiltration facility based on different best management practices (BMP):

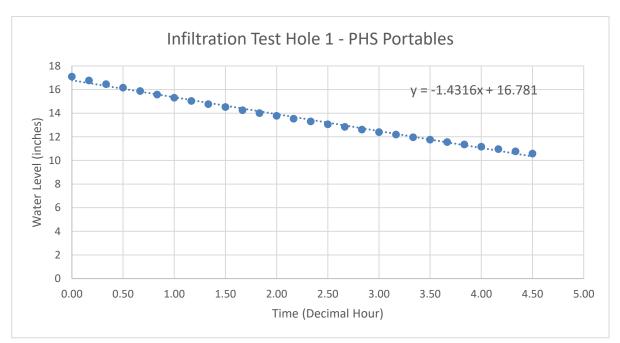
- Downspout Infiltration: 1-foot
- Permeable Pavement: 1-foot
- Infiltration Gallery: 1-foot
- Bioretention: 3-foot

Groundwater was monitored throughout the wet season. The average groundwater depth for Test Hole-1 was determined to be 4.0' below existing grade. The average groundwater depth for Test Hole-2 was determined to be 3.55' below existing grade. With known groundwater conditions for each test hole, there is adequate spacing between groundwater and BMPs. An overflow should be installed with BMP in case of large storm events.

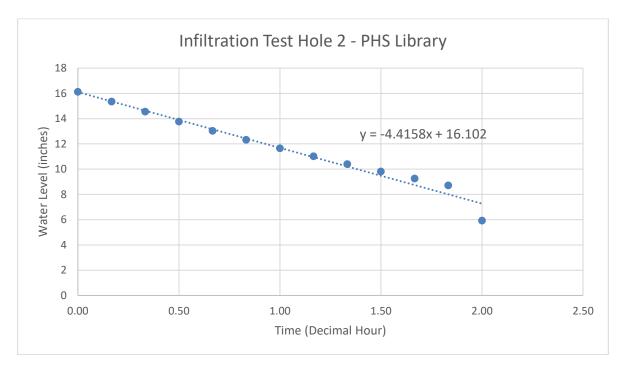
Field Measured Infiltration Rate

The infiltration rate was collected using two methods during the PIT. The first method is to measure the gallons per minute flow rate required to maintain a constant water level in the test pit. The average of the flow rate measurements taken over an hour timeframe.

The second method is to measure the drawdown rate of the test pit. Measurements were taken both visually and with a data logger. The average of the drawdown measurements resulted in the following infiltration rates:



- Test Hole 1: 1.43 inches per hour
- Test Hole 2: 4.42 inches per hour



Design Infiltration Rate

Per the Stormwater Manual a minimum design infiltration rate of 0.3 inches per hour is required for onsite infiltration. The design infiltration rate takes the field measured infiltration rate and applies a factor of safety based on three correction factors. The three corrections are based on site variability, test method, and degree of influent control (See Appendix D).

Issue	Partial Correction Factor			
Site variability and number of locations tested	CF _V = 0.33 to 1.0			
Test Method				
Large-scale PIT	∞ CF _t = 0.75			
Small-scale PIT	■ = 0.50			
Other small-scale (e.g. Double ring, falling head)	∞ = 0.40			
Grain Size Method	[∞] = 0.40			
Degree of influent control to prevent siltation and bio-buildup	CF _m = 0.9			

Total Correction Factor, $CF_T = CF_V \times CF_t \times CF_m$

Per the Stormwater Manual, a site variability correction of 1 is used. A correction of 0.5 for the small-scale PIT and 0.9 for the degree of influent are also used. A total correction factor of 0.45 is applied to the measured infiltration rate yielding a recommended design infiltration rates as follows:

- Test Hole 1: 0.64 inches per hour
- Test Hole 2: 1.99 inches per hour

Treatment Suitability

Per the Stormwater Manual the soils that stormwater is infiltrated into may be used for treatment of pollution generating surfaces if the soil meets specific requirements. Otherwise, a treatment layer is required to treat pollution generating surfaces. The treatment threshold of the infiltrated soil per the Stormwater Manual is a Cation Exchange Capacity greater than or equal to 5 milliequivalents CEC/100g and a minimum of 1.0% organic content.

This project does not propose to manage pollution generating hard surfaces runoff through an infiltration facility; therefore, soil treatment suitability was not evaluated.

TEST PIT PHOTO DOCUMENTATION – TEST HOLE 1











1-Hour GPM Test



Completed Drawdown





Overexcavate to Verify Groundwater Mounding

Backfill and Install Groundwater Monitoring

TEST PIT PHOTO DOCUMENTATION – TEST HOLE 2



3-feet x 4-feet x 2-feet PIT and Pre-Soak



1-Hour GPM Test



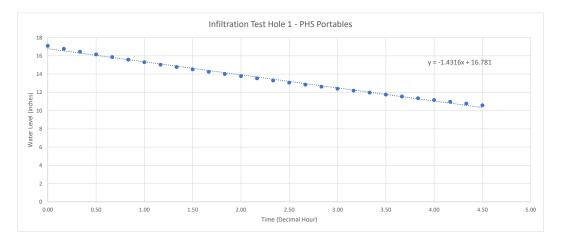
Overexcavate to Verify Groundwater Mounding



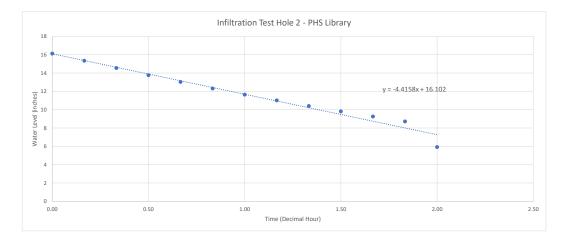
Backfill and Install Groundwater Monitoring

APPENDIX A

Date of test: Number of test:	-								
Instrumentation Norm		PHS Portables			3506 Initial Meter Reading				
Preson: 120PM Start Pre toal Price all 20PM Start Pre toal <td>Date of Test:</td> <td></td> <td>2/10/2024</td> <td>Test start</td> <td></td> <td></td> <td></td> <td></td> <td>I</td>	Date of Test:		2/10/2024	Test start					I
Preson: 120PM Start Pre toal Price all 20PM Start Pre toal <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>1</td>									1
Mather Conditions Clear JC I Inclusion Inclusion <th< td=""><td>Test Pit Dimensions:</td><td></td><td>Width (feet)</td><td>3</td><td>Length (feet)</td><td>4</td><td>Depth (inches)</td><td>24</td><td>[</td></th<>	Test Pit Dimensions:		Width (feet)	3	Length (feet)	4	Depth (inches)	24	[
Mather Conditions Clear JC I Inclusion Inclusion <th< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<>									
Mather Conditions Clear JC I Inclusion Inclusion <th< td=""><td>Presoak:</td><td>12:00PM Start Pre soak</td><td>4hrs at 12-inch water column</td><td></td><td></td><td></td><td></td><td></td><td></td></th<>	Presoak:	12:00PM Start Pre soak	4hrs at 12-inch water column						
Influence Internation (Section Maintained (Inc)): 12 Internation (Section Maintained (Inc)): Internaternation (Section Maintained (Inc)): Internatio									
Infrastator Fast Internation (Second Maintained (Inc)) 12 Internation (Second Maintained (Inc)) 12 Internation (Second Maintained (Inc)) 12 Internation (Second Maintained (Inc)) Internaternation (Second Maintained (Inc)) <th< td=""><td>Weather Conditions:</td><td>Clear</td><td>50° F</td><td></td><td></td><td></td><td></td><td></td><td></td></th<>	Weather Conditions:	Clear	50° F						
Image: space of the s	Weather conditions.	cical	30 1						1
Image: space of the s	Indikantina Tanta				-				
Image Callon: Per Incl: 7.48 Form at Callon:	Inflitration Test:								l
Image in the second of the second o									l
Image Transport Young (galors) Transport Gen (galors) Transport Gen (galors) Transport Gen (galors) Transport Gen (galors) Gen			Gallons Per Inch:	7.48					
Image: Control of the start Meter Start Start O Q<									Infiltration
405 PM Start 358.1 0.2 0.2 0.2 15 3384.7 358.4 0.358.7 0.358.2 0.3 0.1 20 45 3397.0 358.2 0.3 0.3 0.3 20 45 3394.0 359.2 0.3 0.4 0.3 0.3 0.4 20 455 3394.2 3594.8 0.66 3594.2 3594.8 0.66 12.9 Drawdow Tett (Sensor):			Time(Minutes)	Volume (gallons)				(Gallons)	Rate (in/hr)
Image: state in the s						Meter End			
Image: state in the s	4:05 PM Start								1
Image: state of the s			15		3584.7	3584.9	0.3	3.1	1
Image: state of the s			30		3587.9	3588.2	0.3	6.3	
Image: constraint of the second sec									
Drawdown Text (Senor): IMID (CR5451) Senors from Campbell Scients) Image Campbell Scients) Image Campbell Scients I									1.7
Senor Name: IMU 01 (CR5451V Sensor from Campbell Scientk) Resord Messurement Interval Time Stamp Record # Reading (PS) Level (n) Imu (PS)					000112	225 110	0.0		
Senor Name: IMU 01 (CR5451V Sensor from Campbell Scientk) Resord Messurement Interval Time Stamp Record # Reading (PS) Level (n) Imu (PS)	Drawdown Test (Sensor)								
Sensor Name: Compbell Scientik) Image of the sense o	Stawdown rest (Sensor).		IMI 01 (CBS451V Sensors from		1				
Time (Decimal Hours) Record Measurement Intrad Time Stamp Record # Reading (PS) Level (n) Image (N) 0.0000 0 4.05 PM 0 0.61668 17.0943696 1 0.1667 10 4.15 PM 1 0.005066 16.7724752 1 0.3333 20 4.25 PM 2 0.93788 16.6990336 1 0.5000 30 4.35 PM 3 0.582971 16.15995612 1 0.6667 40 4.45 PM 4 0.572547 15.8700284 1 0.6867 70 5.15 PM 7 0.552265 15.5899858 1 1.1667 70 5.15 PM 7 0.542279 15.03197388 1 1.5000 90 5.25 PM 8 0.532373 14.51796538 1 1.6667 100 5.45 PM 10 0.51474 14.25290328 1 2.0000 120 6.05 PM 12 0.497058 13.06068 1	Concor Nomo					1		I	ł
0.000 0 4.05 PM 0 0.5158 17.0943966 1 0.333 20 4.15 PM 1 0.60566 16.7724252 1 0.333 20 4.25 PM 2 0.533786 16.45980336 1 0.5000 30 4.35 PM 3 0.582971 16.15995612 1 0.6667 40 4.45 PM 4 0.572471 15.8100284 1 0.65667 40 4.45 PM 5 0.562265 15.5859858 1 1.10000 60 5.05 PM 6 0.53274 15.31190728 1 1.1667 70 5.15 PM 7 0.542279 15.01307388 1 1.1667 100 5.45 PM 10 0.514174 14.5279022 1 1 1.8333 110 5.55 PM 11 0.505433 14.008.10796 1 2.0000 120 6.05 PM 12 0.49738 13.7763336 1 2.3333	Sensor Name:								
0.000 0 4.05 PM 0 0.5168 17.094366 1 0.333 20 4.15 PM 1 0.60566 16.772452 1 0.3333 20 4.25 PM 2 0.53788 16.45980336 1 0.5000 30 4.35 PM 3 0.582971 16.15995612 1 0.6667 40 4.45 PM 4 0.572471 15.87100284 1 0.6667 40 4.45 PM 5 0.562265 15.589985 1 1.1000 60 5.05 PM 6 0.553274 15.3119728 1 1.1667 70 5.15 PM 7 0.542279 15.03197388 1 1.3333 80 5.25 PM 8 0.532924 14.7726522 1 1.1667 100 545 PM 10 0.514174 14.2529022 1 1.8333 110 555 PM 11 0.505343 14.00810796 1 2.0000 120 6	T (D) (1)	B							l
0.1667 10 4:15 PM 1 0.605066 16.7724252 0.3333 20 4:25 PM 2 0.533788 16.4599036 0.5000 30 4:35 PM 3 0.58278 16.15995612 0.6667 40 4:45 PM 4 0.572547 15.8710024 0.6667 40 4:45 PM 5 0.552561 15.559585 1.0000 60 5:05 PM 6 0.552374 15.3180728 1.1667 70 5:15 PM 7 0.542729 15.0319738 1.5000 90 5:35 PM 9 0.52373 14.517956 1.6667 100 5:45 PM 10 0.51474 14.2520328 1.833 110 5:55 PM 11 0.4537081 13.4507366 2.0000 120 6:35 PM<									l
0.333 20 4.25 PM 2 0.93788 16.458036 0.6667 40 4.45 PM 3 0.82971 16.1599612 0.833 90 4.55 PM 5 0.562265 15.589888 1.0000 60 505 PM 6 0.52374 15.3180728 1.1667 70 5.15 PM 7 0.542279 15.3180728 1.1333 80 5.25 PM 8 0.52373 14.517956 1.5000 90 5.35 PM 9 0.52373 14.517956 1.6667 100 5.45 PM 10 0.514174 14.2229038 2.0000 120 6.05 PM 12 0.497388 13.7078336 2.333 1.40 6.25 PM 14 0.479748 13.29661456 2.333 1.40 6.35 PM 16 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>l</td>									l
0.500 30 4:35 PM 3 0.582971 16:1599612 0.6667 40 4:45 PM 4 0.572547 15:87100284 0.8333 50 4:35 PM 5 0.52265 15:58988 1.000 60 5:05 PM 6 0.52274 15:31190728 1.1667 70 5:15 PM 7 0.542279 15:31190728 1.333 80 5:25 PM 8 0.532924 14:7765328 1.667 100 5:45 PM 9 0.53273 14:0510796 1.833 110 5:55 PM 11 0.505343 14:06810796 2.0000 120 6:05 PM 12 0.49738 13:778936 2.333 140 6:15 PM 13 0.46378 12:4483816 2.3000 150 6:35 PM 15 0.				1					1
0.6667 40 4.45 PM 4 0.57247 18.8710028 Image: constraint of the state of th						16.45980336			1
0.833 50 4-55 PM 5 0.562265 15.585988 1.0000 60 5.05 PM 6 0.552374 15.31180728 1.1667 70 5.15 PM 7 0.542279 15.0319738 1.1333 80 5.25 PM 8 0.532374 14.5177956 1.16667 100 5.45 PM 9 0.53437 14.07265328 1.1833 110 5.55 PM 10 0.514174 14.25290328 1.1833 110 5.55 PM 11 0.50543 14.4001796 2.0667 130 6.15 PM 13 0.488469 13.54036068 2.333 140 6.25 PM 14 0.479748 13.29861456 2.3667 160 6.45 PM 16 0.463378 12.84483816 2.6667 160	0.5000	30	4:35 PM	3	0.582971	16.15995612			1
10000 60 5:05 PM 6 0.552274 15.31180728 Image: constraint of the state of t	0.6667	40	4:45 PM	4	0.572547	15.87100284			
10000 60 5:05 PM 6 0.552274 15.31180728 Image: constraint of the state of t	0.8333	50	4:55 PM	5	0.562265	15.5859858			
1.1667 70 5:15 PM 7 0.542279 15.03197388 Image: constraint of the state of									
1.333 80 5:25 PM 8 0.532924 14.726328 1.5000 90 5:35 PM 9 0.52373 14.517956 1.6667 100 5:45 PM 10 0.51474 14.5290328 1.8333 110 5:55 PM 11 0.505343 14.00810796 2.0000 120 6:05 PM 12 0.497038 13.7789336 2.1667 130 6:15 PM 13 0.488469 13.54036068 2.3333 140 6:25 PM 14 0.479748 13.29861456 2.5000 150 6:35 PM 15 0.471365 13.066278 2.8333 170 6:55 PM 17 0.455239 12.6192508 3.0000 180 7:05 PM 19 0.431804 11.96960688 3.3333 200									
1.5000 90 5:35 PM 9 0.52373 14.517956 1.6667 100 5:45 PM 10 0.514174 14.25290328 1.833 110 5:55 PM 11 0.505343 14.00810796 2.0000 120 6:05 PM 12 0.497038 13.77789336 2.1667 130 6:15 PM 13 0.488469 13.54036068 2.333 140 6:25 PM 14 0.479748 13.29661456 2.5000 150 6:35 PM 15 0.471365 13.0662378 2.8333 170 6:35 PM 17 0.453239 12.6192508 3.0000 180 7:05 PM 18 0.447283 12.3986476 3.3333 200 7:25 PM 20 0.431804 19.9696688 3.4667 220 7:45 PM									
1.6667 100 5.45 PM 10 0.514174 14.25290328 1.8333 110 5.55 PM 11 0.50543 14.00810796 2.0000 120 6.05 PM 12 0.497038 13.77789336 2.1667 130 6.15 PM 13 0.488469 13.54036068 2.333 140 6.25 PM 14 0.479748 13.29861456 2.5000 150 6.35 PM 15 0.471865 13.0662378 2.6667 160 6.45 PM 16 0.463378 12.84483816 3.0000 180 7.05 PM 18 0.447283 12.3986476 3.1667 190 7.15 PM 19 0.438966 12.18837312 3.333 200 7.25 PM 20 0.431804 11.96960688 3.8333 230 7									
1.8333 110 5:55 PM 11 0.505343 14.00810796 Image: constraint of the state o									
2.0000 120 6:05 PM 12 0.497038 13.77789336 2.1667 130 6:15 PM 13 0.488469 13.5403608 2.3333 140 6:25 PM 14 0.47748 13.29861456 2.5000 150 6:35 PM 15 0.471365 13.0662378 2.6667 160 6:45 PM 16 0.463378 12.84483816 2.8333 170 6:55 PM 17 0.455239 12.61922508 3.0000 180 7:05 PM 18 0.447283 12.39868476 3.1667 190 7:15 PM 19 0.439696 12.18837312 3.3333 200 7:25 PM 20 0.416743 11.55211596 3.4333 230 7:55 PM 23 0.409753 11.35835316 4.0000 24									l
2.1667 130 6:15 PM 13 0.488469 13.54036068 2.3333 140 6:25 PM 14 0.479748 13.29861456 2.5000 150 6:35 PM 15 0.471365 13.0662378 2.6667 160 6:45 PM 16 0.463378 12.84483816 2.8333 170 6:55 PM 17 0.455239 12.6192508 3.0000 180 7:05 PM 18 0.447283 12.39868476 3.3333 200 7:25 PM 19 0.439696 12.18837312 3.3333 200 7:25 PM 20 0.447484 11.9696088 3.3000 210 7:35 PM 21 0.424222 11.75943844 3.8333 230 7:55 PM 22 0.416743 11.55241596 4.0000 240 8:05 PM 25 0.395456 10.96204032									l
2.333 140 6:25 PM 14 0.479748 13.29861456 Image: constraint of the system of									
2.5000 150 6:35 PM 15 0.471365 13.0662378 1 1 2.6667 160 6:45 PM 16 0.463378 12.8443336 1 2.8333 170 6:55 PM 17 0.455239 12.6192508 1 3.0000 180 7:05 PM 18 0.47233 12.3986476 1 3.1667 190 7:15 PM 19 0.439696 12.18837312 1 3.333 200 7:25 PM 20 0.431804 11.96960688 1 3.5000 210 7:35 PM 21 0.424222 11.75943384 1 1 3.6667 220 7:45 PM 22 0.416743 11.55211596 1 1 3.8333 230 7:55 PM 23 0.400753 11.35835316 1 1 4.0607 250 8:15 PM 25 0.389456 10.96204032 1 1 4.1667 250 8:35 PM 27 0.381685 10.5803082 1 1 4.3333 260 8:25 PM <									i
2.6667 160 6:45 PM 16 0.46378 12.8443816 2.8333 170 6:55 PM 17 0.455239 12.6192508 3.0000 180 7:05 PM 18 0.447283 12.3986476 3.1667 190 7:15 PM 19 0.439696 12.1887312 3.3333 200 7:25 PM 20 0.431804 11.99960688 3.5000 210 7:35 PM 21 0.424222 11.75943384 3.6667 220 7:45 PM 22 0.416743 11.552156 3.8333 230 7:55 PM 23 0.409753 11.35835316 4.0000 240 8:05 PM 24 0.4027 11.15244 4.333 260 8:15 PM 25 0.395456 10.9624032 4.3333 260									l
2.8333 170 6:55 PM 17 0.455239 12.61922508 3.0000 180 7:05 PM 18 0.447283 12.3966476 3.1667 190 7:15 PM 19 0.439696 12.18873712 3.3333 200 7:25 PM 20 0.431804 11.96960688 3.5000 210 7:35 PM 21 0.424222 11.75943384 3.6667 220 7:45 PM 22 0.416743 11.5211596 3.8333 230 7:55 PM 23 0.409753 11.35835316 4.0000 240 8:05 PM 24 0.4027 11.162844 4.3333 260 8:15 PM 25 0.395456 10.96204032 4.5000 270 8:35 PM 27 0.381685 10.580382									I
2.8333 170 6:55 PM 17 0.455299 12.61922508 3.0000 180 7:05 PM 18 0.447283 12.3966476 3.1667 190 7:15 PM 19 0.439696 12.18873712 3.3333 200 7:25 PM 20 0.431804 11.96960688 3.5000 210 7:35 PM 21 0.424222 11.75943384 3.6667 220 7:45 PM 22 0.416743 11.5211596 3.8333 230 7:55 PM 23 0.409753 11.35835316 4.0000 240 8:05 PM 24 0.4027 11.162844 4.3333 260 8:15 PM 25 0.395456 10.96204032	2.6667	160	6:45 PM	16	0.463378	12.84483816			
3.0000 180 7.05 PM 18 0.447283 12.39868476 Image: constraint of the system of		170	6:55 PM		0.455239	12.61922508			
3.1667 190 7:15 PM 19 0.439696 12.18837312 3.3333 200 7:25 PM 20 0.431804 11.96960688 3.5000 210 7:35 PM 21 0.424222 11.75943384 3.6667 220 7:45 PM 22 0.416743 11.551156 3.8333 230 7:55 PM 23 0.409753 11.35835316 4.0000 240 8:05 PM 24 0.4027 11.162844 4.1667 250 8:15 PM 25 0.395456 10.96204032 4.3333 260 8:25 PM 26 0.388569 10.7113268 4.5000 270 8:35 PM 27 0.381685 10.5803082 4.5000 270 8:35 PM 27 0.381685 10.5803082	3.0000	180	7:05 PM	18	0.447283	12.39868476			
3.333 200 7:25 PM 20 0.431804 11.9696688 3.5000 210 7:35 PM 21 0.424222 11.75943384 3.6667 220 7:45 PM 22 0.416743 11.5521596 3.8333 230 7:55 PM 23 0.409753 11.35835316 4.0000 240 8:05 PM 24 0.4027 11.162844 4.1667 250 8:15 PM 25 0.395456 10.96204032 4.3333 260 8:25 PM 26 0.388569 10.7513268 4.5000 270 8:35 PM 27 0.381685 10.580382									
3.5000 210 7:35 PM 21 0.424222 11.75943384 3.6667 220 7:45 PM 22 0.416743 11.55211596 3.8333 230 7:55 PM 23 0.409753 11.35835316 4.0000 240 8:05 PM 24 0.4027 11.15284 4.1667 250 8:15 PM 25 0.395456 10.96204032 4.3333 260 8:25 PM 26 0.388569 10.77113268									[
3.6667 220 7:45 PM 22 0.416743 11.55211596 3.8333 230 7:55 PM 23 0.409753 11.35833316 4.0000 240 8:05 PM 24 0.4027 11.152843 4.1667 250 8:15 PM 25 0.395456 10.96204032 4.3333 260 8:25 PM 26 0.388569 10.77113268 4.5000 270 8:35 PM 27 0.381685 10.5803082 4.5000 270 8:35 PM 27 0.381685 10.5803082							1	1	
3.8333 230 7:55 PM 23 0.409753 11.35835316 Image: constraint of the system of									
4.0000 240 8:05 PM 24 0.4027 11.162844 4.1667 250 8:15 PM 25 0.395456 10.96204032 4.3333 260 8:25 PM 26 0.388569 10.77113268 4.5000 270 8:35 PM 27 0.381685 10.5803082 1 1 1 1 1 1 <t< td=""><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td><td> </td><td> </td></t<>			-						
4.1667 250 8:15 PM 25 0.395456 10.96204032 4.3333 260 8:25 PM 26 0.388569 10.77113268 4.5000 270 8:35 PM 27 0.381685 10.5803082									
4.3333 260 8:25 PM 26 0.388569 10.77113268 4.5000 270 8:35 PM 27 0.381685 10.5803082 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td> </td>									
4.5000 270 8:35 PM 27 0.381685 10.5803082 Image: Constraint of the second sec									
Image: second								L	
Image: Second	4.5000	270	8:35 PM	27	0.381685	10.5803082			i
Image: Second			ļ		ļ				l
Factor of Safety: 0.45									<u> </u>
							Average Infiltration Rate:	1.43	
									i
					1		Factor of Safety:	0.45	
			1		1	1			
Design Infiltration Rate: 0.64					1	1	Design Infiltration Rate:	0.64	



				1	1			
Project Location:	PHS Library			4502 Initial Meter Reading				1
Date of Test:		2/10/2024	Test start					l
								1
Test Pit Dimensions:		Width (feet)	3	Length (feet)	4	Depth (inches)	24	1
Presoak:	12:00PM Start Pre soak	4hrs at 12-inch water column						
Weather Conditions:	Clear	50° F						
weather conditions.	cical	50 1						1
Infiltration Test:			-	1				
innitration rest.			12					
		Water Column Maintained (inches):	12					l
		Gallons Per Inch:	7.48					
							Flow	Infiltration
		Time(Minutes)	Volume (gallons)		low Rate (GPN		(Gallons)	Rate (in/hr)
				Meter Start	Meter End	Flow (Gallons)		1
4:15 PM Start		0		4702.0	4702.8	0.8	0.8	1
		15		4711.5	4712.2	0.7	10.2	
		30		4721.7	4722.4	0.7	20.4	[
		45	-	4732.2	4732.9		30.9	
	1	43		4732.2	4732.3	0.8	41.6	5.6
	<u> </u>	60		4/42.9	4/43./	0.8	41.0	5.0
Descudence Test (Car								
Drawdown Test (Sensor):					<u> </u>			l
		JMJ 02 (CRS451V Sensors from						ł
Sensor Name:		Campbell Scientic)						i
Time (Decimal Hours)	Record Measurement Interval	Time Stamp	Record #	Reading (PSI)	Level (in)			l
0.0000	0	4:05 PM	0	0.5816216	16.12255075			1
0.1667	10	4:15 PM	1	0.5537774	15.35070953			
0.3333	20	4:25 PM	2	0.5248642	14.54923562			
0.5000	30	4:35 PM	3	0.4966844	13.76809157			
0.6667	40	4:45 PM	4	0.4701035	13.03126902			
0.8333	50	4:55 PM	5	0.4443737	12.31803896			
1.0000	60	5:05 PM	6	0.4201141	11.64556285			
								l
1.1667	70	5:15 PM	7	0.3973055	11.01330846			l
1.3333	80	5:25 PM	8	0.3752191	10.40107345			l
1.5000	90	5:35 PM	9	0.3541772	9.817791984			1
1.6667	100	5:45 PM	10	0.334096	9.26114112			1
1.8333	110	5:55 PM	11	0.3144749	8.717244228			1
2.0000	120	6:05 PM	12	0.2135902	5.920720344			
					l			[
				1	1			1
				1	1			
	ł			+				
					<u> </u>			
				-				
	<u> </u>							I
								I
					1			
				1	1			
								I
						Average Infiltration Rate:	4.42	
								I
						Factor of Safety:	0.45	1
								l
					1	Design Infiltration Rate:	1.99	[
l								



APPENDIX B



Stainless-Steel Vented Stand-Alone Pressure Transducer



Pressure Transducer Combined with a Recorder

R 😪 🕄 68

PRODUCT

High resolution and accuracy

Overview

The CRS451V consists of a submersible water-level and watertemperature sensor with its own time clock and memory to store the collected data—in a compact stainless-steel case. This data logging capability frees users to place the sensor in remote sites and let it collect data for long periods. HydroSci software is included and elegantly supports test setup, data retrieval, and data display. Long battery life and rugged construction mean you can trust the CRS451V to collect important data. Low cost and ease of use make it a good choice in a variety of applications. The CRS456V is the same as this, but with a titanium case.

Benefits and Features

- > Sensors and data-collection features in one instrument case
- > Rugged stainless-steel case protects piezoresistive sensor
- Quality construction ensures product reliability
- > Fully temperature-compensated

> Fast scan rate

-) Large data-storage capacity
- > Long battery life
- Easy-to-use software

Detailed Description

The CRS451V has several pressure range options.

HydroSci software is available for download. This software simplifies the process of configuring the CRS451V. Users can

configure the CRS451V to monitor surface water, ground water, or a standard pump test.

HydroSci software will display the data in tabular or graphical formats.

Specifications

Venting

Vented

Measurement Time

< 1.0 s

APPENDIX C

INFILTRATION TEST

The Washington State Department of Ecology Stormwater Manual provides testing procedures and best practices, which are described below.

- Testing should occur between December 1 and April 1.
- The horizontal and vertical locations of the PIT shall be surveyed by a licensed land surveyor and accurately shown on the design drawings.
- Excavate the test pit to the estimated elevation of the proposed infiltration into the native soil. Note that for some proposed BMPs, such as and <u>BMP T5.15: Per-meable Pavements</u>, this will be below the proposed finished grade. If the native soils will have to meet a minimum subgrade compaction requirement (for example, the road subgrade if using <u>BMP T5.15: Permeable Pavements</u>), compact the native soil to that requirement prior to testing. Lay back the slopes sufficiently to avoid caving and erosion during the test. Altern- atively, consider shoring the sides of the test pit.
- The horizontal surface area of the bottom of the test pit should be approximately 100 square feet. Document the size and geometry of the test pit.
- Install a vertical measuring rod (long enough to measure the ponded water depth, minimum 5- ft. long) marked in half-inch increments in the center of the pit bottom.
- Use a rigid 6-inch diameter pipe with a splash plate on the bottom to convey water to the test pit and reduce side-wall erosion or excessive disturbance of the test pit bottom. Excessive erosion and bottom disturbance will result in clogging of the infiltration receptor and yield lower than actual infiltration rates.
- Add water to the pit at a rate that will maintain a water level between 6 and 12 inches above the bottom of the pit. A rotameter can be used to measure the flow rate into the pit.

The depth should not exceed the proposed maximum depth of water expected in the completed BMP. For infiltration BMPs serving large drainage areas, designs with multiple feet of standing water can have infiltration tests with greater than 1 foot of standing water.

- Every 15-30 min, record the cumulative volume and instantaneous flow rate in gallons per minute necessary to maintain the water level at the same point on the measuring rod.
- Keep adding water to the pit until one hour after the flow rate into the pit has stabilized (constant flow rate; a goal of 5% or less variation in the total flow) while maintaining the same pond water level. The total of the pre-soak time plus one hour after the flow rate has stabilized should be no less than 6 hours.
- After the flow rate has stabilized for at least one hour, turn off the water and record the rate of infiltration (the drop rate of the standing water) in inches per hour from the measuring rod data, until the pit is empty. Consider running this falling head phase of the test several times to estimate the dependency of the infiltration rate with head.
- At the conclusion of testing, over-excavate the pit to see if the test water is mounded on shallow restrictive layers or if it has continued to flow deep into the subsurface. The depth of excavation varies depending on soil type and depth to the hydraulic restricting layer, and is determined by the

engineer or certified soils professional. Mounding is an indication that a mounding analysis is necessary.

DATA ANALYSIS

Calculate and record the initial K_{sat} rate in inches per hour in 30 minutes or one-hour increments until one hour after the flow has stabilized.

Use statistical/trend analysis to obtain the hourly flow rate when the flow stabilizes. This would be the lowest hourly flow rate. *Example:*

The area of the bottom of the test pit is 8.5-ft. by 11.5-ft. (97.75 sq. ft.).

Water flow rate was measured and recorded at intervals ranging from 15 to 30 minutes throughout the test. Between 400 minutes and 1,000 minutes the flow rate stabilized between 10 and 12.5 gal- lons per minute or 600 to 750 gallons per hour, or 80.2 to 100 ft³ per hour. Dividing this rate by the surface area gives an initial K_{sat} of 9.8 to 12.3 inches per hour.

K_{sat} Determination Option 2: Small Scale Pilot Infiltration Test (PIT)

A small-scale PIT can be substituted for <u>Ksat Determination Option 1: Large Scale Pilot Infiltration</u> <u>Test (PIT)</u> in any of the following instances:

- The drainage area to the infiltration BMP is less than 1 acre.
- The testing is for <u>BMP T7.30: Bioretention</u> or <u>BMP T5.15: Permeable Pavements</u> that either serve small drainage areas and/or are widely dispersed throughout a project site.
- The site has a high infiltration rate (>4 in/hr), making a large scale PIT difficult, and the site geo- technical investigation suggests uniform subsurface characteristics.

INFILTRATION TEST

Use the same procedures described above in <u>Ksat Determination Option 1: Large Scale Pilot Infiltra-tion Test</u> (<u>PIT</u>), with the following changes:

- The horizontal surface area of the bottom of the test pit should be 12 to 32 square feet. It may be circular or rectangular. Document the size and geometry of the test pit.
- The rigid pipe with a splash plate used to convey water to the pit may be a 3-inch diameter pipe for pits on the smaller end of the recommended surface area, or a 4-inch pipe for pits on the larger end of the recommended surface area.
- Pre-soak period: Add water to the pit so that there is standing water for at least 6 hours. Maintain the pre-soak water level at least 12 inches above the bottom of the pit.
- At the end of the pre-soak period, add water to the pit at a rate that will maintain a 6-12 inch water level above the bottom of the pit over a full hour. The depth should not exceed the pro- posed

maximum depth of water expected in the completed facility.

• Every 15 minutes, record the cumulative volume and instantaneous flow rate in gallons per minute necessary to maintain the water level at the same point (between 6 inches and 1 foot) on the measuring rod. The specific depth should be the same as the maximum designed pond- ing depth (usually 6 – 12 inches).

After one hour, turn off the water and record the rate of infiltration (the drop rate of the standing water) in inches per hour from the measuring rod data, until the pit is empty.

- A self-logging pressure sensor may also be used to determine water depth and drain-down.
- At the conclusion of testing, over-excavate the pit to see if the test water is mounded on shallow restrictive layers or if it has continued to flow deep into the subsurface. The depth of excavation varies depending on soil type and depth to the hydraulic restricting layer, and is determined by the engineer or certified soils professional. The soils professional should judge whether a mounding analysis is necessary.

APPENDIX D

CALCULATED DESIGN INFILTRATION RATE:

Site variability and number of locations tested (CF_v) - The number of locations tested must be capable of producing a picture of the subsurface conditions that fully rep- resents the conditions throughout the proposed location of the infiltration BMP. The partial correction factor used for this issue depends on the level of uncertainty that adverse subsurface conditions may occur. If the range of uncertainty is low - for example, conditions are known to be uniform through previous exploration and site geological factors

- one pilot infiltration test (or grain size analysis location) may be adequate to justify a partial correction factor at the high end of the range.

If the level of uncertainty is high, a partial correction factor near the low end of the range may be appropriate. This might be the case where the site conditions are highly variable due to conditions such as a deposit of ancient landslide debris, or buried stream channels. In these cases, even with many explorations and several pilot infiltration tests (or several grain size test locations), the level of uncertainty may still be high.

A partial correction factor near the low end of the range could be assigned where conditions have a more typical variability, but few explorations and only one pilot infiltration test (or one grain size analysis location) is conducted. That is, the number of explorations and tests conducted do not match the degree of site variability anticipated.

- Uncertainty of test method (CF_t) accounts for uncertainties in the testing methods. For the full scale PIT method, CF_t = 0.75; for the small-scale PIT method, CF_t = 0.50; for smaller-scale infiltration tests such as the double-ring infiltrometer test, CF_t = 0.40; for grain size analysis, CF_t = 0.40. These values are intended to represent the difference in each test's ability to estimate the actual saturated hydraulic conductivity. The assumption is the larger the scale of the test, the more reliable the result.
- Degree of influent control to prevent siltation and bio-buildup (CF_m) Even with a pre-settling basin or a basic treatment BMP for pre-treatment, the soil's initial infiltration rate will gradually decline as more and more stormwater, with some amount of suspended material, passes through the soil profile. The maintenance schedule calls for removing sediment when the BMP is infiltrating at only 90% of its design capacity. Therefore, a correction factor, CF_m, of 0.9 is called for.

Table V-5.1: Correction Factors to be Used With In-Situ Saturated Hydraulic Conductivity Measurements to Estimate Design Rates

Issue	Partial Correction Factor
Site variability and number of locations tested	CF _v = 0.33 to <mark>1.0</mark>
Test Method	
Large-scale PIT	∞ CF _t = 0.75
Small-scale PIT	₂ <mark>= 0.50</mark>
Other small-scale (e.g. Double ring, falling head)	≥ = 0.40
Grain Size Method	▣ = 0.40
Degree of influent control to prevent siltation and bio-buildup	CF _m <mark>= 0.9</mark>

Total Correction Factor, $CF_T = CF_v \times CF_t \times CF_m$

Total Correction Factor, $CF_T = 1.0 \times 0.5 \times 0.9$

CF_T = 0.45