

# Stormwater Site Plan/Report

### **PUYALLUP MEDICAL OFFICES**

1617 S Merdian

Puyallup, WA 98371 - City of Puyallup

Permit #:

Parcel #7790000140

For: Dr. Fadi Alhafez

Courtesy of: PFHC Puyallup, LLC

**April 24, 2023** 

Revised: 6/11/2024

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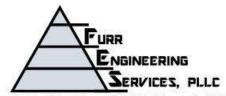
FES Project #23062

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### 1.0 PROJECT OVERVIEW

This project proposes the construction of a new five-story medical building on a 30,513 sf (0.780 ac) parcel (no. 7790000140) located at 1617 S Meridian, Puyallup, WA 98371. This parcel is located in City of Puyallup Zone CG – General Commercial; the development standards for this zone may be found in Puyallup Municipal Code (PMC) 20.30.030. The site is bordered to the east and south by commercial properties; to the north, by 17<sup>th</sup> Ave SE; and to the west by S Meridian. Currently, the site is undeveloped, with a gravel driveway entrance along 17<sup>th</sup> Ave SE. The topography generally slopes down from southeast to northwest, at rates of approximately 8%.

Per the US Natural Resources Conservation Services (NRCS) Web Soil Survey, the site is generally underlain by Kapowsin gravelly ashy loam and Kitsap silt loam. The water table may be expected to lie approximately 16 – 23 inches below the surface. Therefore, infiltration is not considered feasible on this project. Vegetation generally consists of a mixture of hardwood and deciduous trees, shrubs, and groundcover.

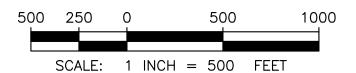
Currently, stormwater runoff sheet-flows northwest towards S Meridian and enters into the City of Puyallup municipal storm system through a catch basin. Flows are conveyed north and discharged to a vegetated slope across S Meridian, eventually flowing into Meeker Creek. Under the developed condition, site stormwater runoff will be collected into a vault and discharged via pump station through a StormFilter manhole into the municipal storm system, following the existing pattern.

Onsite Stormwater Management BMPs/LIDs will be evaluated and used to the maximum extent feasible. Proposed stormwater mitigation will comply with Puyallup Municipal Code (PMC) and the 2019 Department of Ecology (DOE) Stormwater Management Manual for Western Washington (SWMMWW), which has been adopted as the governing manual within the City.



# **VICINITY MAP**







### 2.0 CONDITIONS AND REQUIREMENTS SUMMARY

This project is considered New Development, as the existing impervious area is less than 35% of the total parcel area; see Table 1, below.

Eviating Conditions	Ar	Area		
Existing Conditions	SF	AC		
Parcel area	30,513	0.780		
Hard surface coverage	29	0.001	0.1%	
Pervious (LS)	34,500	34,500		

Table 1: Existing hard surface coverage.

Therefore, the flowchart for New Development (below) will be used to determine the applicability of the Minimum Requirements to this project.



**Start Here** See Redevelopment Project Yes Does the Site have 35% Thresholds and the Figure "Flow or more of existing hard Chart for Determining surface coverage? Requirements for Redevelopment". No Does the Project convert 3/4 acres or more of vegetation to Does the Project result in lawn or landscaped areas, or 5,000 square feet, or convert 2.5 acres or more of No greater, of new plus replaced hard surface native vegetation to pasture? No Yes Yes Does the Project result in 2,000 square feet, or greater, of new plus replaced hard surface area? **All Minimum Requirements** apply to the new and replaced hard surfaces and converted Yes No vegetation areas. Does the Project have land disturbing activities of 7,000 Minimum Requirements #1 square feet or greater? through #5 apply to the new Yes and replaced hard surfaces and the land disturbed. No Minimum Requirement #2 applies. Flow Chart for Determining Requirements for **New Development** DEPARTMENT OF ECOLOGY Please see http://www.ecy.wa.gov/copyright.html for copyright notice including permissions, limitation of liability, and disclaimer.

Figure I-3.1: Flow Chart for Determining Requirements for New Development

Therefore, all Minimum Requirements apply to all new and replaced hard surfaces and vegetation areas, as this project will result in 5,000 sf or greater of new and replaced hard surface area. See Section 4.2: Developed Site Hydrology.

### 2.1 ANALYSIS OF THE MINIMUM REQUIREMENTS

### 2.1.1 MR #1: Preparation of Stormwater Site Plans

This report will serve as the Stormwater Site Plan, prepared per Puyallup Municipal Code and the SWMMWW.



### 2.1.2 MR #2: Construction Stormwater Pollution Prevention

Construction Stormwater Pollution Prevention Plans are prepared per 2019 SWMMWW and City of Puyallup Stormwater Management Standards to address the 13 elements. A SWPPP will be provided as a separate document for approval.

### 2.1.3 MR #3: Source Control of Pollution

Per SWMMWW Volume II, Section 3.2, the following Construction Source Control BMPs will be used as necessary:

BMP C103	High-Visibility Fence
BMP C105	Stabilized Construction Access
BMP C120	Temporary and Permanent Seeding
BMP C121	Mulching
BMP C122	Nets and Blankets
BMP C123	Plastic Covering
BMP C125	Topsoiling/Composting
BMP C140	Dust Control
BMP C150	Materials on Hand
BMP C151	Concrete Handling
BMP C152	Sawcutting and Surfacing Pollution Prevention
BMP C153	Material Delivery, Storage, and Containment
BMP C154	Concrete Washout Area
BMP C160	Certified Erosion and Sediment Control Lead
BMP C162	Scheduling

### 2.1.4 MR #4: Preservation of Natural Drainage Systems and Outfalls

This project comprises a single threshold discharge area (TDA) within the State Highway Drainage Basin, which currently drains to the NW corner and discharges into the municipal storm system in S Meridian. Under the developed condition, stormwater will be conveyed north and into the municipal storm system. Therefore, the existing drainage pattern will be maintained.

### 2.1.5 MR #5: On-site Stormwater Management

Table I-2.5.1 from the SWMMWW (Figure 1, below) was used to determine the onsite stormwater management requirements for this project. Because this project is considered new development, and is situated on a parcel within the urban growth area (UGA), List #2 will be evaluated for feasibility.



Table I-2.5.1 On-Site Stormwater Management Requirements for Projects Triggering Minimum Requirements #1 - #9

Projects Triggering willimital Requirements #1-#9  Project Type and Location Requirement					
Project Type and Location					
New development on any parcel inside	Low Impact Development Performance				
the UGA, or new development outside the	Standard and BMP T5.13: Post-Construction				
UGA on a parcel less than 5 acres	Soil Quality and Depth (p.911); or List #2				
OGA off a parcer less than 5 acres	(applicant option).				
New development outside the UGA on a	Low Impact Development Performance				
	Standard and BMP T5.13: Post-Construction				
parcel of 5 acres or larger	Soil Quality and Depth (p.911).				
Redevelopment on any parcel inside the	Low Impact Development Performance				
UGA, or redevelopment outside the UGA	Standard and BMP T5.13: Post-Construction				
on a parcel less than 5 acres	Soil Quality and Depth (p.911); or List #2				
on a parcer less than 5 acres	(applicant option).				
Redevelopment outside the UGA on a par-	Low Impact Development Performance				
cel of 5 acres or larger	Standard and BMP T5.13: Post-Construction				
cer of 5 acres of larger	Soil Quality and Depth (p.911).				
Note: This table refers to the Urban Growth Area (UGA) as designated under the					
Growth Management Act (GMA) (Chapter 36.70A RCW) of the State of Washington. If					
the Permittee is located in a county that is not subject to planning under the GMA, the					
city limits shall be used.					

Figure 1: Table I-2.5.1 from the SWMMWW

# 2.1.5(a) List #2: Onsite Stormwater Management BMPs for Projects Triggering Minimum Requirements #1 through #9

For each surface consider the BMPs in the order listed for that type of surface. Use the first BMP that is considered feasible. No other onsite stormwater management BMP is necessary for that surface. Feasibility shall be determined by evaluation against:

- Design criteria, limitations, and infeasibility criteria identified for each BMP in the SWMMWW; and
- Competing Needs Criteria listed in Chapter V-5 of the SWMMWW.

### Lawn and landscaped areas:

 Post-Construction Soil Quality and Depth in accordance with BMP T5.13: Post-Construction Soil Quality and Depth

This BMP will be implemented to the maximum extent feasible.

### Roofs:

1. Full Dispersion in accordance with BMP T5.30: Full Dispersion; or

This project does not meet the 65% minimum requirement for native growth protection area (NGPA) for full dispersion.

Downspout Full Infiltration Systems in accordance with BMP T5.10A: Downspout Full Infiltration.

Infiltration BMPs are not proposed due to the high water table.



2. Bioretention (BMP T5.30: Bioretention Cells, Swales, and Planter Boxes) facilities that have a minimum horizontally projected surface area below the overflow which is at least 5% of the total surface area draining to it.

The area and setback requirements of this BMP cannot be met.

3. Downspout Dispersion Systems in accordance with BMP T5.10: Downspout Dispersion Systems.

The minimum required flowpath for this BMP cannot be met.

4. Perforated Stub-out Connections in accordance with BMP T5.10C: Perforated Stub-out Connections.

Perforated connections will not be used due to the high water table.

### **Other Hard Surfaces:**

- Full Dispersion in accordance with BMP T.30: Full Dispersion
   This project does not meet the 65% minimum requirement for native growth protection area (NGPA) for full dispersion.
- 2. Permeable Pavement in accordance with BMP T5.15: Permeable Pavements This BMP will not be used due to the high water table.
- 3. Sheet Flow Dispersion in accordance with BMP T5.12: Sheet Flow Dispersion; or Concentrated Flow Dispersion in accordance with BMP T5.11: Concentrated Flow Dispersion

The minimum required vegetated flow path for dispersion BMPs cannot be met.

### 2.1.6 MR #6: Runoff Treatment

Runoff treatment is required, as this project exceeds the requirements for the construction of stormwater facilities, as shown in Table 2, below:

Criteria	Threshold	Project
Pollution-generating hard surface	≥5,000 sf	11,637 sf
Pollution-generating pervious surface (not including permeable pavements) from which there will be a surface discharge in a natural or man-made conveyance from the site	≥0.75 ac	0 ac

Table 2: Analysis of thresholds requiring runoff treatment.

Water quality treatment shall be provided by a detention/wetvault and a StormFilter Manhole; see Section 4.2.2: Water Quality Treatment.



### 2.1.7 MR #7: Flow control

Flow control is required, as this project does exceed any of the thresholds requiring achievement of the standard flow control requirement for western Washington, summarized in Table 3, below:

Criteria	Threshold	Project
Total effective impervious surface in a threshold discharge	≥10,000 sf	28,794 sf
area	210,000 51	20,7 94 51
Vegetation converted to lawn or landscape	≥0.75 ac	0.119 ac
Native vegetation converted to pasture in a threshold		
discharge area, from which there is a surface discharge in	≥2.5 ac	0 ac
a natural or manmade conveyance system from the site		
Increase in 100-year flow frequency from threshold		
discharge area, resulting from a combination of effective	≥0.15 cfs	0.54 cfs
hard surfaces and converted vegetation area*		
*Modelled in WWHM using 15-minute timesteps; see Section 4.2: Developed	d Site Hydrology.	

Table 3: Analysis of thresholds requiring runoff treatment.

The required level of flow control shall be provided by a combined detention/wetvault; see Section 4.2.1: Flow Control.



### 2.1.8 MR #8: Wetlands Protection

This project discharges to a Cat. II wetland west of the site. The flow control and water quality provided by the vault and StormFilter manhole will be sufficient to ensure protection of this wetland. Wetland hydroperiod modeled in WWHM2012, see section 4.3

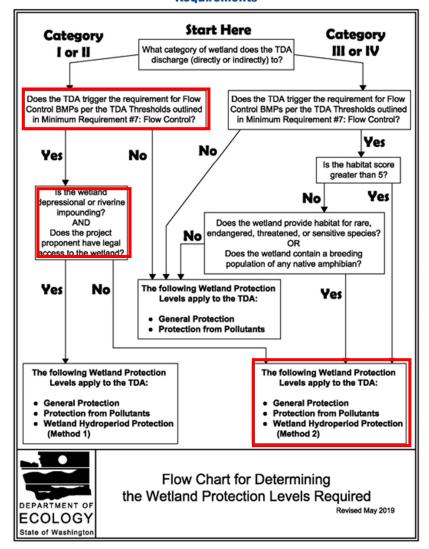


Figure I-3.5: Flow Chart for Determining Wetland Protection Level Requirements



## 2.1.9 MR #9: Operation and Maintenance

Operation and Maintenance guidelines from the SWMMWW will be included in Section 9.0 of this report.

### 2.2 Financial Liability

A bond quantities worksheet for construction and landscaping will be provided, if required.

### 2.3 Conditions of Approval

Reserved.



### 3.0 OFF-SITE ANALYSIS

### 3.1 UPSTREAM TRIBUTARY AREA

This site may receive run-on from upstream properties to the east that is not captured by those properties storm management systems; these amounts are unlikely to contribute significantly to site runoff.

### 3.2 DOWNSTREAM ANALYSIS

In the existing condition, stormwater from the site generally sheet-flows northwest into a catch basin on S Meridian and enters the municipal storm system. Flows are conveyed north, then west across S Meridian, discharging onto a vegetated slope and eventually entering into Meeker Creek and its associated wetland. Under the developed condition, stormwater will generally follow this same pattern.

Review of City of Puyallup GIS assets shows that the municipal storm system to which this site drains discharges to a wetland approximately 400 ft. downstream; see Appendix B: Critical Areas Maps.



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# STORM ANALYSIS PUYALLUP MEDICAL OFFICES DEVELOPED CONDITIONS

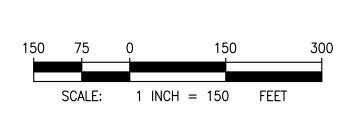
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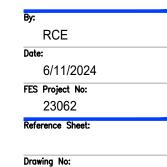
STORM STRUCTURE



STORM PIPE









### 4.0 FLOW CONTROL AND WATER QUALITY FACILITY ANALYSIS AND DESIGN

The City of Puyallup has adopted the 2019 SWMMWW as the governing document for stormwater management within the city. Drainage review requires preparation of engineering site improvement plans, a Technical Information Report, and Erosion/Sedimentation Controls and related information.

Review of NRCS Web Soil Survey (See Appendix A) suggests a shallow water table, generally 11 to 24 inches below the surface; therefore, infiltration is not considered feasible on this site. Onsite stormwater management shall be provided by a combination detention/wetvault.

### 4.1 Existing Site Hydrology

Currently, the site is undeveloped, with vegetation consisting of evergreen and deciduous trees, shrubs, grasses, and groundcover. The topography generally slopes down from southeast to northwest at rates of approximately 8%. Offsite improvements will be included as a part of this project in order to provide sidewalk improvements along S Meridian and 17<sup>th</sup> Ave SE.

Table 4, below, shows a breakdown of the existing site area:

<b>EXISTING CONDITIONS</b>	sf	ac	
PARCEL AREA	30,513	0.700	
DISTURBED AREA	33,994	0.780	
ON-SITE	30,513	0.700	
OFF-SITE	3,481	0.080	
ON-SITE	sf	ac	
IMPERVIOUS	29	0.001	
GRAVEL	29	0.001	
PERVIOUS (LS)	30,484	0.700	
OFF-SITE	sf	ac	
IMPERVIOUS	880	0.020	
GRAVEL	880	0.020	
CONCRETE SIDEWALK	184	0.004	
PERVIOUS (LS)	2,601	0.060	

Table 4: Existing conditions area breakdown.

See the Existing Conditions Exhibit at the end of this section.



### 4.2 Developed Site Hydrology

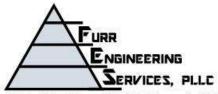
This project proposes the construction of a medical building and associated parking, driveways, walkways, utilities, etc.; Table 5, below, shows a breakdown of the developed areas.

	PROPOSED ON-SITE DEVELOPED		sf	ac
	PARCEL AREA		30,513	0.700
	DI	STURBED AREA	30,513	0.700
	IIV	1PERVIOUS	26,470	0.608
Include a bypass basin for the		10,392	0.239	
frontage improvements along 17th		BUILDING ROOF	12,481	0.287
Ave SE. [drainage report, pg 17]		WALKWAYS	3,596	0.083
		ASPHALT DRIVEWAY	471	0.011
	ASPHALT PARKING (PGHS)		9,921	0.228
\	PERVIOUS (LS)			
	PE	:RVIOUS (LS)	4,044	0.093
		ROP. OFF-SITE DEVELOPMENT	<b>4,044</b> sf	<b>0.093</b> ac
	PF	, ,	,	
	PF DI	ROP. OFF-SITE DEVELOPMENT	sf	ac
	PF DI IN	ROP. OFF-SITE DEVELOPMENT STURBED AREA	sf 3,481	ac 0.080
	PF DI IN	ROP. OFF-SITE DEVELOPMENT STURBED AREA IPERVIOUS	sf 3,481 <b>2,088</b>	ac 0.080 <b>0.048</b>
	PF DI IN	ROP. OFF-SITE DEVELOPMENT STURBED AREA MPERVIOUS DTAL PGHS	sf 3,481 <b>2,088</b> <b>1,008</b>	ac 0.080 <b>0.048</b> <b>0.023</b>
	PF DI IN	ROP. OFF-SITE DEVELOPMENT STURBED AREA IPERVIOUS OTAL PGHS SPHALT ROADWAY/GUTTER (PGHS)	sf 3,481 <b>2,088</b> <b>1,008</b> 708	ac 0.080 <b>0.048</b> <b>0.023</b> 0.016
	PF DI IN TC	ROP. OFF-SITE DEVELOPMENT STURBED AREA MPERVIOUS OTAL PGHS SPHALT ROADWAY/GUTTER (PGHS) CONCRETE SIDEWALK	sf 3,481 <b>2,088</b> <b>1,008</b> 708 1,080	ac 0.080 <b>0.048</b> <b>0.023</b> 0.016 0.025

The post-developed conditions for the map on page 17 state the pervious area is 0.262 acres. Revise accordingly. [drainage report, pg 17]

Stormwater runoff shall be conveyed into a combined detention/wetvault onsite and discharged through a StormFilter manhole into the municipal storm system via pump station, following the same pattern as under the existing condition. An equivalent area from the crown of 17<sup>th</sup> Ave to the property line will be collected by a catch basin on 17<sup>th</sup> Ave Se and directed to the detention/wetvault to mitigate offsite improvements.

The site was modelled in WWHM using the inputs in Table 6, below. The predeveloped condition was modelled as "forest," and hydrologic soil group "C" was used.



WWHM INPUTS - MITIGATED	ac
PREDEVELOPED	0.780
C, FOREST, MOD	0.780
DEVELOPED	0.780
C PASTURE, FLAT	0.1248
ROOF TOPS/FLAT	0.2865
SIDEWALKS/MOD	0.0248
SIDEWALKS/FLAT	0.0826
DRIVEWAY/FLAT	0.0177
ROADS/MOD	0.0162
PARKING/FLAT	0.2278

Table 6: WWHM inputs.

The following flow rates were calculated:

	Flow (cfs)			
Flow Frequency	0501 Predeveloped	0701 Developed, Unmitigated	0801 Developed, Mitigated	
2-year	0.0166	0.2223	0.0081	
5-year	0.0260	0.3112	0.0141	
10-year	0.0311	0.3702	0.0203	
25-year	0.0363	0.4497	0.0315	
50-year	0.0394	0.5135	0.0431	
100-year	0.0419	0.5814	0.0585	
	ΔQ <sub>100</sub> =	0.53	95	

Table 7: Calculated flow rates.

### 4.2.2 Flow Control

Flow control will be provided by a combined detention/wetvault. WWHM modelling was used to verify determine that 16,128 cf of live storage vault with the dimensions of 96'x24'x7' will be adequate; see section 4.4.1.

### 4.2.3 Water Quality

Water quality will be provided by a combined detention/wetvault and by a StormFilter manhole. The auto-vault feature was used in WWHM to determine that 3,197 cf of dead storage with a depth of 4 feet will be required; see Appendix C: StormFilter detail.



### 4.2.4 Pump System

Due to the topography of the site and the location of the proposed detention system beneath the lowest parking level, a pump system will be required to discharge runoff from the vault up to a catch basin and into the municipal storm system.

The proposed pump system shall consist of a Goulds WE05HH pumps and be housed within a 60" manhole. Pump sizing was performed based upon the performance curve supplied by the manufacturer; see Appendix D: WE Series Model 3885 Brochure.

Peak averaging was used to determine average flow rates through the pump system. Table 8, below, summarizes the peak averaging calculations:

Storm Event	(a) Restricted Flowrate	(b) Pump Drawdown Flowrate	(c) Pump Drawdown Time	(d) Wet well Fill Time	(e) Cycle Time	(f) Avg. Flow Rate at Discharge Point Over Cycle Time	
	gpm	gpm	min	min	min	gpm	
2 year	3.64	49.36	4.46	60.60	109.97	2.00	
5 year	6.33	46.67	4.72	34.81	81.49	2.70	
10 year	9.11	43.89	5.02	24.18	68.07	3.24	
25 year	14.14	38.86	5.67	15.58	54.45	4.05	
50 year	19.34	33.66	6.55	11.39	45.04	4.89	
100 year	26.26	26.74	8.24	8.39	35.13	6.27	
(g) Pump Flowrate (gpm)				53.0			
		(h) Wet Well	220.3				

Table 8: Peak averaging design calculations.

Values in the table were calculated as follows:

- a. Restricted flow rate: mitigated (801) flowrates calculated using WWHM in gpm.
- **b.** Pump drawdown flow rate: (g)-(a)
- c. Pump drawdown time: (h)/(b)
- d. Wet well fill time: (h)/(a)
- **e. Cycle time**: (c) + (d)
- f. Avg. flow rate at discharge point over cycle time:  $[(b)^*(c)]/(e)$
- g. Pump flow rate: derived from manufacturer's performance curve based upon calculated head; see Appendix D: WE Series Model 3885 Brochure and Appendix D: Pump Calculations.
- **h. Wet well volume:** see Appendix D: Pump calculations.

Since I've been here with the city, no project has been able to use continuous simulation modeling to pump from the outlet of a stormwater control structure to the downstream drainage system and meet the flow control standard. The WWHM modeling will need to show the developed discharge matches the pre-developed conditions for the actual flows, not an average. To pass, the pump must be the mechanism modeled in WWHM. Revise accordingly. [site plan, pg 19]



### 4.3 Wetland Hydroperiods

The proposed development's impact on the downstream wetland was modeled in WWHM 2012. A basin draining into the category 2 wetland around Meeker Creek was estimated using USGS Topographic Map of Puyallup Quadrangle 7.5-Minute Series; see Figure 2 below. This basin encompasses 557.26 ac. An average slope across the basin was estimated by taking the elevation distance between the high point at the south eastern corner, 460', and the low point in the north western corner, 50', and dividing that by the linear distance between them, 5500', resulting in an average slope of 7.5%. This slope was considered when developing WWHM inputs.

Using the City of Puyallup's zoning map, it was determined that the basin is comprised of roughly 6% RS-6 SFR zone, 27% RS-10 SFR zone, 26% RM-20 MFR zone, 6% MED zone, 7% GC zone, and 28% road. Assuming max allowable coverage for each zone, and 100% coverage for roadways, an average of 64% impervious area within the basin was determined as the predeveloped condition. Impervious area was modeled as ROADS/MOD.

For the developed condition, the inputs from Table 6 were subtracted from the pervious surface total and added as additional impervious surface.

WWHM INPUTS - BASIN	ac
PREDEVELOPED	557.260
C, PASTURE, MOD	200.610
ROADS/MOD	356.650
DEVELOPED	557.260
C PASTURE, MOD	199.94
ROOF TOPS/FLAT	0.29
SIDEWALKS/MOD	0.11
DRIVEWAY/FLAT	0.01
ROADS/MOD	356.67
PARKING/FLAT	0.24

**Table 9: Basin WWHM Inputs** 

### Zoning

- ARO Agriculture, Recreation and Open
- CB Community Business
- CBD Central Business District
- CBD-CORE Central Business District Core
- CCX Community Commercial Mixed Use
- CG General Commercial
- CL Limited Commercial
- CMX Shaw-Pioneer Community Mixed Use
- FAIR Fair
- LMX Limited Mixed Use
- MED Medical
  - ML Limited Manufacturing
- MP Business Park
  - OP Professional Office
- PF Public Facilities

- RM-10 Medium Density Multiple-Family Residential
- RM-20 High Density Multiple-Family Residential
- RM-CORE Regional Growth Center Oriented Multi-Family Residential
- RMX River Road Mixed Use
- RS-04 High Urban Density Single-Family Residential
- RS-06 Urban Density Single-Family Residential
- RS-08 Medium Density Single-Family Residential
- RS-10 Low Urban Density Single-Family Residential
- RS-35 Very Low Density Single-Family Residential
- UCX Urban Center Mixed Use

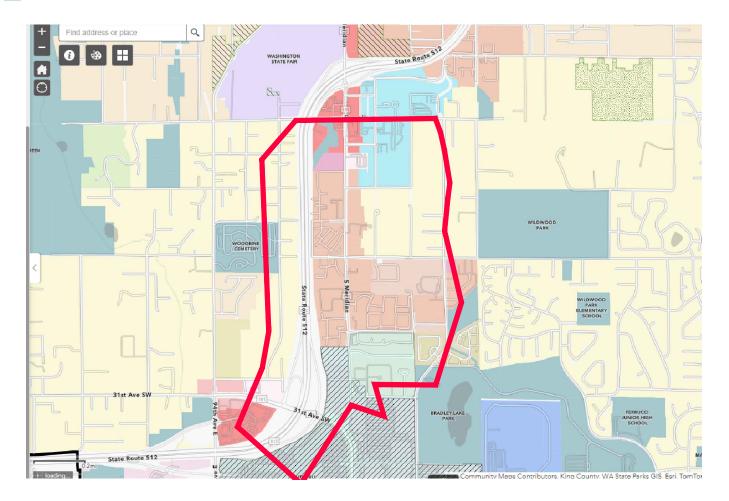
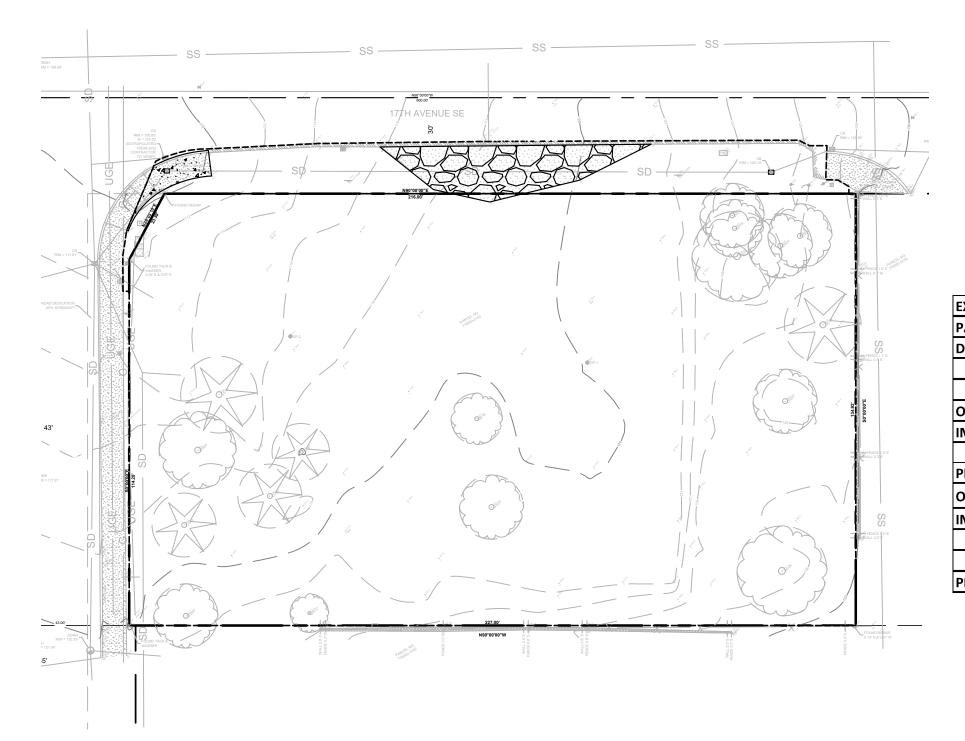


Figure 3 Zoning Map





### **EXISTING CONDITIONS** sf ac PARCEL AREA 30,513 0.700 **DISTURBED AREA** 33,994 0.780 30,513 **ON-SITE** 0.700 OFF-SITE 3,481 0.080 ON-SITE sf ac **IMPERVIOUS** 29 0.001 GRAVEL 29 0.001 PERVIOUS (LS) 30,484 0.700 OFF-SITE sf ac **IMPERVIOUS** 880 0.020 GRAVE 880 0.020 CONCRETE SIDEWALK 184 0.004 PERVIOUS (LS) 2,601 0.060

# STORM ANALYSIS PUYALLUP MEDICAL OFFICES EXISTING CONDITIONS

## **LEGEND - EXISTING**



CONCRETE (OFFSITE)

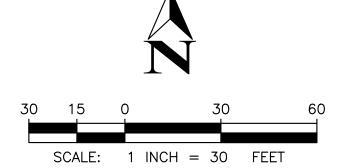


GRAVEL (OFFSITE)

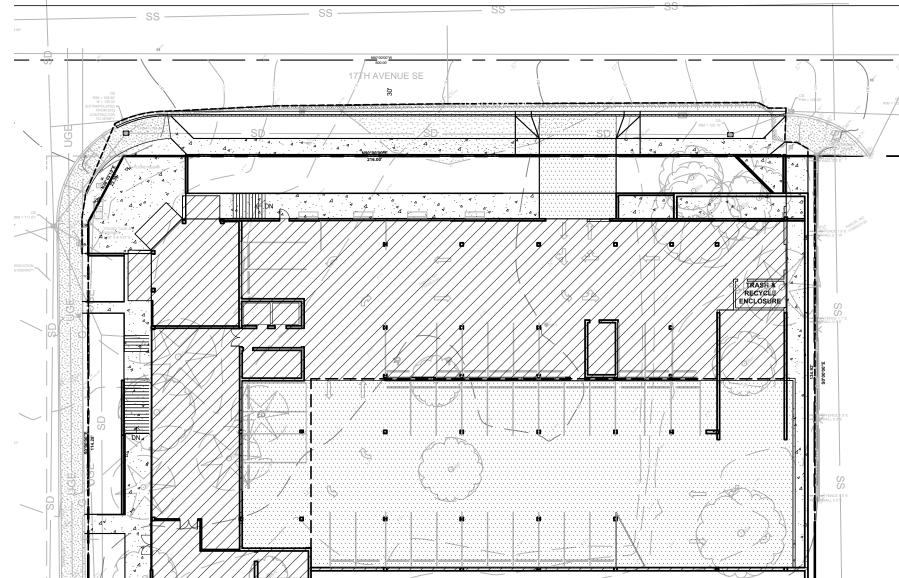


DISTURBED AREA





JV	
Date:	
6/11/2024	
FES Project No:	
23062	
Reference Sheet:	





# STORM ANALYSIS PUYALLUP MEDICAL OFFICES DEVELOPED CONDITIONS

### PROPOSED ON-SITE DEVELOPED sf ac PARCEL AREA 30,513 0.700 **DISTURBED AREA** 30,513 0.700 **IMPERVIOUS** 26,470 0.608 **TOTAL PGHS** 10,392 0.239 **BUILDING ROOF** 12,481 0.287 WALKWAYS 3,596 0.083 **ASPHALT DRIVEWAY** 471 0.011 **ASPHALT PARKING (PGHS)** 9,921 0.228 PERVIOUS (LS) 4,044 0.093 PROP. OFF-SITE DEVELOPMENT sf ac DISTURBED AREA 3,481 0.080 **IMPERVIOUS** 2,088 0.048 TOTAL PGHS 1,008 0.023 ASPHALT ROADWAY/GUTTER (PGHS) 708 0.016 CONCRETE SIDEWALK 1,080 0.025 **ASPHALT DRIVEWAY (PGHS)** 300 0.007 PERVIOUS (LS) 1,393 0.032

## LEGEND - DEVELOPED

DISTURBED AREA

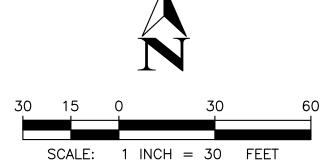
ROOF CONCRETE (OFFSITE)

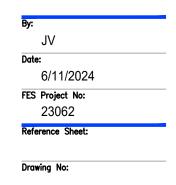
CONCRETE (ONSITE)

ASPHALT (ONSITE)

CONCRETE (OFFSITE)









### 4.4 WWHM Reports

### 4.4.1 Vault Modeling

WWHM2012 PROJECT REPORT

Project Name: 23062 - vault

Site Name: Puyallup Medical Center
Site Address: 1617 S Meridian
City : Puyallup, WA 98371

Report Date: 5/29/2024
Gage : 38 IN CENTRAL
Data Start : 10/01/1901
Data End : 09/30/2059
Precip Scale: 1.00

**Version Date:** 2021/08/18

**Version** : 4.2.18

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Low Flow Threshold for POC 1 : 50 Percent of the 2 Year

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High Flow Threshold for POC 1: 50 year

\_\_\_\_\_

PREDEVELOPED LAND USE

Name : Basin 1

 $\textbf{Bypass:} \ \texttt{No}$ 

GroundWater: No

Pervious Land Use acre
C, Forest, Mod .78

Pervious Total 0.78

Impervious Land Use acre

Impervious Total 0

Basin Total 0.78

\_\_\_\_\_\_

Element Flows To:

FES Project 23062

Surface Interflow Groundwater

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### MITIGATED LAND USE

Name : Basin 1

Bypass: No

GroundWater: No

Pervious Land Use	acre
C, Pasture, Flat	.124

Pervious Total 0.124

Impervious Land Use	e acre
ROADS MOD	0.016
ROOF TOPS FLAT	0.286
DRIVEWAYS FLAT	0.018
SIDEWALKS FLAT	0.083
SIDEWALKS MOD	0.025
PARKING FLAT	0.228

Impervious Total 0.656

Basin Total 0.78

Element Flows To:

Surface Interflow Groundwater

Vault 1 Vault 1

Name : Vault 1
Width : 24 ft.
Length : 96 ft.
Depth: 8 ft.

Discharge Structure
Riser Height: 7 ft.
Riser Diameter: 18 in.
Notch Type: Rectangular
Notch Width: 0.010 ft.
Notch Height: 1.105 ft.

Orifice 1 Diameter: 0.375 in. Elevation: 0 ft.

Element Flows To:

Page 26



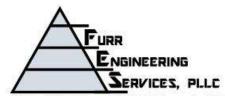
Outlet 1

Outlet 2

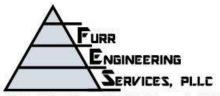
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Vault Hydraulic Table	Vault	Hvdraulic	Table
-----------------------	-------	-----------	-------

Stage(feet)	Area(ac.)	Volume(ac-ft.)	Discharge(cfs)	Infilt(cfs)
0.0000	0.052	0.000	0.000	0.000
0.0889	0.052	0.004	0.001	0.000
0.1778	0.052	0.009	0.001	0.000
0.2667	0.052	0.014	0.002	0.000
0.3556	0.052	0.018	0.002	0.000
0.4444	0.052	0.023	0.002	0.000
0.5333	0.052	0.028	0.002	0.000
0.6222	0.052	0.032	0.003	0.000
0.7111	0.052	0.037	0.003	0.000
0.8000	0.052	0.042	0.003	0.000
0.8889	0.052	0.047	0.003	0.000
0.9778	0.052	0.051	0.003	0.000
1.0667	0.052	0.056	0.003	0.000
1.1556	0.052	0.061	0.004	0.000
1.2444	0.052	0.065	0.004	0.000
1.3333	0.052	0.070	0.004	0.000
1.4222	0.052	0.075	0.004	0.000
1.5111	0.052	0.079	0.004	0.000
1.6000	0.052	0.084	0.004	0.000
1.6889	0.052	0.089	0.005	0.000
1.7778	0.052	0.094	0.005	0.000
1.8667	0.052	0.098	0.005	0.000
1.9556	0.052	0.103	0.005	0.000
2.0444	0.052	0.108	0.005	0.000
2.1333	0.052	0.112	0.005	0.000
2.2222	0.052	0.117	0.005	0.000
2.3111	0.052	0.122	0.005	0.000
2.4000	0.052	0.126	0.005	0.000
2.4889	0.052	0.131	0.006	0.000
2.5778	0.052	0.136	0.006	0.000
2.6667	0.052	0.141	0.006	0.000
2.7556	0.052	0.145	0.006	0.000
2.8444	0.052	0.150	0.006	0.000
2.9333	0.052	0.155	0.006	0.000
3.0222	0.052	0.159	0.006	0.000
3.1111	0.052	0.164	0.006	0.000
3.2000	0.052	0.169	0.006	0.000
3.2889	0.052	0.174	0.006	0.000
3.3778	0.052	0.178	0.007	0.000
3.4667	0.052	0.183	0.007	0.000
3.5556	0.052	0.188	0.007	0.000
3.6444	0.052	0.192	0.007	0.000
3.7333	0.052	0.197	0.007	0.000



0.400000440000				
3.8222	0.052	0.202	0.007	0.000
3.9111	0.052	0.206	0.007	0.000
4.0000	0.052	0.211	0.007	0.000
4.0889	0.052	0.216	0.007	0.000
4.1778	0.052	0.221	0.007	0.000
4.2667	0.052	0.225	0.007	0.000
4.3556	0.052	0.230	0.008	0.000
4.4444	0.052	0.235	0.008	0.000
4.5333	0.052	0.239	0.008	0.000
4.6222	0.052	0.244	0.008	0.000
4.7111	0.052	0.249	0.008	0.000
4.8000	0.052	0.253	0.008	0.000
4.8889	0.052	0.258	0.008	0.000
4.9778	0.052	0.263	0.008	0.000
5.0667	0.052	0.268	0.008	0.000
5.1556	0.052	0.272	0.008	0.000
5.2444	0.052	0.277	0.008	0.000
5.3333	0.052	0.282	0.008	0.000
5.4222	0.052	0.286	0.008	0.000
				0.000
5.5111	0.052	0.291	0.009	
5.6000	0.052	0.296	0.009	0.000
5.6889	0.052	0.300	0.009	0.000
5.7778	0.052	0.305	0.009	0.000
5.8667	0.052	0.310	0.009	0.000
5.9556	0.052	0.315	0.009	0.000
6.0444	0.052	0.319	0.011	0.000
		0.324		
6.1333	0.052		0.013	0.000
6.2222	0.052	0.329	0.015	0.000
6.3111	0.052	0.333	0.017	0.000
6.4000	0.052	0.338	0.020	0.000
6.4889	0.052	0.343	0.023	0.000
6.5778	0.052	0.347	0.026	0.000
6.6667	0.052	0.352	0.029	0.000
6.7556	0.052	0.357	0.023	0.000
6.8444	0.052	0.362	0.035	0.000
6.9333	0.052	0.366	0.038	0.000
7.0222	0.052	0.371	0.093	0.000
7.1111	0.052	0.376	0.628	0.000
7.2000	0.052	0.380	1.445	0.000
7.2889	0.052	0.385	2.416	0.000
7.3778	0.052	0.390	3.427	0.000
7.4667	0.052	0.394	4.367	0.000
7.5556	0.052	0.399	5.138	0.000
7.6444	0.052	0.404	5.690	0.000
7.7333	0.052	0.409	6.055	0.000
7.8222	0.052	0.413	6.467	0.000
7.9111	0.052	0.418	6.806	0.000
8.0000	0.052	0.423	7.128	0.000
8.0889				
	0.052	0.427	7.436	0.000
8.1778	0.000	0.000	7.732	0.000



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### ANALYSIS RESULTS

### Stream Protection Duration

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Predeveloped Landuse Totals for POC #1

Total Pervious Area:0.78 Total Impervious Area:0

Mitigated Landuse Totals for POC #1

Total Pervious Area:0.124
Total Impervious Area:0.656

### Flow Frequency Return Periods for Predeveloped. POC #1

Return Period	Flow(cfs)
2 year	0.016598
5 year	0.025961
10 year	0.031067
25 year	0.036275
50 year	0.039375
100 year	0.041926

### Flow Frequency Return Periods for Mitigated. POC #1

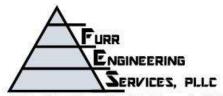
Return Period	Flow(cfs)
2 year	0.00807
5 year	0.014142
10 year	0.020293
25 year	0.031493
50 year	0.043142
100 year	0.058485

\_\_\_\_\_

### Stream Protection Duration

Annual Peaks for Predeveloped and Mitigated. POC #1

Year	Predeveloped	Mitigated
1902	0.012	0.008
1903	0.010	0.006
1904	0.019	0.007
1905	0.008	0.008
1906	0.004	0.005
1907	0.025	0.007
1908	0.019	0.007
1909	0.018	0.008



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1910	0.025	0.007
1911	0.017	0.007
1912	0.063	0.008
1913	0.026	0.009
1914	0.006	0.005
1915	0.011	0.009
1916	0.016	0.007
1917	0.005	0.006
1918	0.018	0.021
1919	0.013	0.007
1920	0.017	0.007
1921	0.019	0.008
1922	0.019	0.007
1923	0.015	0.009
1924	0.007	0.007
1925	0.009	0.006
1926	0.016	0.007
1927	0.010	0.007
1928	0.013	0.008
1929	0.027	0.009
1930	0.017	0.007
1931	0.016	0.008
1932	0.012	0.008
1933	0.012	0.008
1934	0.034	0.135
1935	0.016	0.014
1936	0.014	0.008
1937	0.023	0.007
1938	0.014	0.007
1939	0.001	0.006
1940	0.015	0.008
1941	0.007	0.005
1942	0.023	0.032
1943	0.012	0.008
1944	0.023	0.009
1945	0.019	0.008
1946	0.011	0.006
1947	0.006	0.006
1948	0.035	0.008
1949	0.030	0.009
1950	0.009	0.007
1951	0.011	0.006
1952	0.047	0.009
1953	0.042	0.026
1954	0.015	0.008
1955	0.012	0.006
1956	0.006	0.006
1957	0.021	0.009
1958	0.044	0.086
1959	0.027	0.064



1960	0.007	0.005
1961	0.028	0.027
1962	0.015	0.008
1963	0.007	0.006
1964	0.008	0.006
1965	0.031	0.070
1966	0.009	0.007
1967	0.014	0.006
1968	0.014	0.008
1969	0.014	0.007
1970	0.021	0.008
1971	0.033	0.018
1972	0.022	0.008
1973	0.028	0.009
1974	0.016	0.007
1975	0.035	0.044
1976	0.019	0.008
1977	0.006	0.005
1978	0.031	0.030
1979	0.009	0.007
1980	0.018	0.007
	0.018	
1981		0.008
1982	0.007	0.006
1983	0.028	0.008
1984	0.011	0.007
1985	0.018	0.007
1986	0.016	0.008
1987	0.032	0.021
1988	0.020	0.009
1989	0.018	0.007
1990	0.020	0.007
1991	0.016	0.008
1992	0.023	0.026
1993	0.022	0.007
1994	0.033	0.008
1995	0.006	0.007
1996	0.037	0.034
1997	0.014	0.006
1998	0.016	0.007
1999	0.001	0.007
2000	0.013	0.008
2001	0.006	0.005
	0.026	
2002 2003		0.007
	0.020	0.008
2004	0.019	0.008
2005	0.039	0.008
2006	0.010	0.007
2007	0.010	0.008
2008	0.017	0.007
2009	0.012	0.007



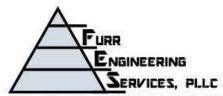
	, 00	
2010	0.010	0.008
2011	0.008	0.007
2012	0.012	0.007
2013	0.009	0.005
2014	0.007	0.006
2015	0.013	0.007
2016	0.005	0.007
2017	0.025	0.009
2018	0.047	0.074
2019	0.045	0.038
	0.014	0.007
2020		
2021	0.023	0.009
2022	0.009	0.006
2023	0.019	0.008
2024	0.046	0.007
2025	0.017	0.008
2026	0.028	0.009
2027	0.010	0.007
2028	0.009	0.006
2029	0.019	0.009
2030	0.035	0.009
2030	0.011	0.006
2032	0.006	0.006
2033	0.010	0.006
2034	0.010	0.007
2035	0.039	0.062
2036	0.021	0.008
2037	0.005	0.006
2038	0.017	0.009
2039	0.002	0.005
2040	0.009	0.007
2041	0.012	0.006
2042	0.039	0.028
2042	0.018	0.009
	0.025	
2044		0.009
2045	0.017	0.009
2046	0.020	0.035
2047	0.015	0.008
2048	0.019	0.007
2049	0.017	0.008
2050	0.012	0.007
2051	0.018	0.008
2052	0.010	0.008
2053	0.018	0.029
2054	0.023	0.009
2055	0.023	0.006
2056	0.008	0.006
2057	0.012	0.008
2058	0.016	0.009
2059	0.028	0.009



### Stream Protection Duration

Ranked	Annual	Peaks	for	Predeveloped	and	Mitigated.	POC	#1
		LCURD	-0-	rrcacveropea	ana	miciga cca.	-00	" -

1       0.0627       0.1346         2       0.0466       0.0740         4       0.0460       0.0695         5       0.0449       0.0639         6       0.0444       0.0620         7       0.0416       0.0438         8       0.0393       0.0380         9       0.0392       0.0352         10       0.0386       0.0341         11       0.0368       0.0319         12       0.0353       0.0298         13       0.0349       0.0293         14       0.0348       0.0225         15       0.0344       0.0274         16       0.0333       0.0255         17       0.0330       0.0257         18       0.0319       0.0215         19       0.0312       0.0210         20       0.0309       0.0183         21       0.0303       0.0143         22       0.0276       0.0091         23       0.0276       0.0091         24       0.0276       0.0091         25       0.0276       0.0091         26       0.0275       0.0091 <t< th=""><th>Rank</th><th>Predeveloped</th><th>Mitigated</th></t<>	Rank	Predeveloped	Mitigated
2       0.0467       0.0856         3       0.0466       0.0740         4       0.0460       0.0639         5       0.0449       0.0620         7       0.0416       0.0438         8       0.0393       0.0380         9       0.0392       0.0352         10       0.0386       0.0341         11       0.0368       0.0319         12       0.0353       0.0298         13       0.0349       0.0293         14       0.0349       0.0293         15       0.0344       0.0274         16       0.0333       0.0265         17       0.0330       0.0257         18       0.0319       0.0215         19       0.0312       0.0210         20       0.0309       0.0183         21       0.0303       0.0143         22       0.0278       0.0094         23       0.0276       0.0091         25       0.0276       0.0091         26       0.0276       0.0091         27       0.0275       0.0091         28       0.0262       0.0099         <			
3       0.0466       0.0740         4       0.0460       0.0695         5       0.0449       0.0620         7       0.0416       0.0438         8       0.0393       0.0380         9       0.0392       0.0352         10       0.0386       0.0341         11       0.0368       0.0319         12       0.0353       0.0298         13       0.0349       0.0293         14       0.0348       0.0285         15       0.0344       0.0274         16       0.0333       0.0265         17       0.0330       0.0257         18       0.0319       0.0215         19       0.0312       0.0210         20       0.0309       0.0183         21       0.0303       0.0143         22       0.0278       0.0094         23       0.0276       0.0091         24       0.0276       0.0091         25       0.0276       0.0091         26       0.0276       0.0091         27       0.0275       0.0089         30       0.0259       0.0089			
4       0.0460       0.0695         5       0.0449       0.0639         6       0.0416       0.0438         8       0.0393       0.0380         9       0.0392       0.0352         10       0.0386       0.0341         11       0.0368       0.0319         12       0.0353       0.0298         13       0.0349       0.0293         14       0.0348       0.0285         15       0.0344       0.0274         16       0.0333       0.0265         17       0.0330       0.0257         18       0.0319       0.0215         19       0.0312       0.0210         20       0.0309       0.0183         21       0.0333       0.0143         22       0.0278       0.0094         23       0.0276       0.0091         24       0.0276       0.0091         25       0.0276       0.0091         26       0.0276       0.0091         28       0.0267       0.0090         29       0.0262       0.0089         31       0.0259       0.0089			
5       0.0449       0.0620         7       0.0416       0.0438         8       0.0393       0.0380         9       0.0392       0.0352         10       0.0366       0.0341         11       0.0368       0.0319         12       0.0353       0.0298         13       0.0349       0.0293         14       0.0348       0.0285         15       0.0344       0.0274         16       0.0333       0.0265         17       0.0330       0.0257         18       0.0319       0.0215         19       0.0312       0.0210         20       0.309       0.0183         21       0.0303       0.0143         22       0.0278       0.0094         23       0.0276       0.0092         24       0.0276       0.0091         25       0.0276       0.0091         26       0.0276       0.0091         27       0.0275       0.0091         28       0.0262       0.0090         30       0.0259       0.0089         31       0.0254       0.0089			
6       0.0444       0.0620         7       0.0416       0.0438         8       0.0393       0.0380         9       0.0392       0.0352         10       0.0386       0.0341         11       0.0368       0.0319         12       0.0353       0.0298         13       0.0349       0.0293         14       0.0348       0.0285         15       0.0344       0.0274         16       0.0333       0.0257         18       0.0319       0.0215         19       0.0312       0.0210         20       0.0309       0.0183         21       0.0303       0.0143         22       0.0278       0.0094         23       0.0276       0.0092         24       0.0276       0.0091         25       0.0276       0.0091         26       0.0276       0.0091         27       0.0275       0.0091         28       0.0267       0.0090         29       0.0262       0.0089         31       0.0254       0.0089         32       0.0253       0.0087			
7       0.0416       0.0438         8       0.0393       0.0380         9       0.0392       0.0352         10       0.0386       0.0341         11       0.0368       0.0319         12       0.0353       0.0298         13       0.0349       0.0293         14       0.0348       0.0285         15       0.0344       0.0274         16       0.0333       0.0265         17       0.0330       0.0257         18       0.0319       0.0210         20       0.0312       0.0210         20       0.0309       0.0183         21       0.0303       0.0143         22       0.0278       0.0094         23       0.0276       0.0091         24       0.0276       0.0091         25       0.0276       0.0091         26       0.0276       0.0091         27       0.0275       0.0091         28       0.0267       0.0090         29       0.0262       0.0090         30       0.0259       0.0089         31       0.0254       0.0089			
8       0.0393       0.0352         10       0.0386       0.0341         11       0.0368       0.0319         12       0.0353       0.0298         13       0.0349       0.0293         14       0.0348       0.0285         15       0.0344       0.0274         16       0.0333       0.0265         17       0.0330       0.0257         18       0.0319       0.0215         19       0.0312       0.0210         20       0.0309       0.0183         21       0.0303       0.0143         22       0.0278       0.0094         23       0.0276       0.0091         24       0.0276       0.0091         25       0.0276       0.0091         26       0.0276       0.0091         27       0.0275       0.0091         28       0.0267       0.0090         30       0.0259       0.0089         31       0.0254       0.0089         32       0.0253       0.0089         33       0.0252       0.0088         34       0.0230       0.0087			
9       0.0392       0.0352         10       0.0386       0.0341         11       0.0368       0.0319         12       0.0353       0.0298         13       0.0349       0.0293         14       0.0348       0.0285         15       0.0344       0.0274         16       0.0333       0.0265         17       0.0330       0.0257         18       0.0319       0.0215         19       0.0312       0.0210         20       0.0309       0.0183         21       0.0303       0.0143         22       0.0278       0.0094         23       0.0276       0.0092         24       0.0276       0.0091         25       0.0276       0.0091         26       0.0276       0.0091         27       0.0275       0.0091         28       0.0262       0.0090         30       0.0259       0.0089         31       0.0254       0.0089         32       0.0253       0.0089         33       0.0252       0.0088         34       0.0248       0.0087			
10       0.0386       0.0319         11       0.0368       0.0319         12       0.0353       0.0298         13       0.0349       0.0293         14       0.0348       0.0285         15       0.0344       0.0274         16       0.0333       0.0265         17       0.0330       0.0257         18       0.0319       0.0215         19       0.0312       0.0210         20       0.0309       0.0183         21       0.0303       0.0143         22       0.0278       0.0094         23       0.0276       0.0091         24       0.0276       0.0091         25       0.0276       0.0091         26       0.0276       0.0091         27       0.0275       0.0091         28       0.0267       0.0090         29       0.0262       0.0090         30       0.0259       0.089         31       0.0254       0.0089         32       0.0253       0.0089         33       0.0252       0.0088         34       0.0230       0.0087			
11       0.0368       0.0319         12       0.0353       0.0298         13       0.0349       0.0293         14       0.0348       0.0274         15       0.0344       0.0274         16       0.0333       0.0265         17       0.0330       0.0257         18       0.0319       0.0215         19       0.0312       0.0210         20       0.0309       0.0183         21       0.0303       0.0143         22       0.0278       0.0094         23       0.0276       0.0091         24       0.0276       0.0091         25       0.0276       0.0091         26       0.0276       0.0091         27       0.0275       0.0091         28       0.0262       0.0090         30       0.0259       0.0089         31       0.0254       0.0089         32       0.0253       0.0089         33       0.0252       0.0088         34       0.0248       0.0087         38       0.0227       0.0087         39       0.0226       0.0087	9	0.0392	0.0352
12       0.0353       0.0298         13       0.0349       0.0293         14       0.0348       0.0285         15       0.0344       0.0274         16       0.0333       0.0265         17       0.0330       0.0257         18       0.0319       0.0215         19       0.0312       0.0210         20       0.0309       0.0183         21       0.0303       0.0143         22       0.0278       0.0094         23       0.0276       0.0091         24       0.0276       0.0091         25       0.0276       0.0091         26       0.0276       0.0091         27       0.0275       0.0091         28       0.0267       0.0090         29       0.0262       0.0090         30       0.0259       0.089         31       0.0254       0.0089         32       0.0253       0.0089         33       0.0252       0.0088         34       0.0248       0.0087         38       0.0220       0.0087         40       0.0225       0.0087	10	0.0386	0.0341
13       0.0349       0.0293         14       0.0348       0.0285         15       0.0344       0.0274         16       0.0333       0.0265         17       0.0330       0.0257         18       0.0319       0.0215         19       0.0312       0.0210         20       0.0309       0.0183         21       0.0303       0.0143         22       0.0278       0.0094         23       0.0276       0.0091         24       0.0276       0.0091         25       0.0276       0.0091         26       0.0276       0.0091         27       0.0275       0.0091         28       0.0262       0.0090         30       0.0259       0.0089         31       0.0254       0.0089         32       0.0253       0.0089         33       0.0252       0.0088         34       0.0248       0.0087         38       0.0220       0.0087         39       0.0226       0.0087         39       0.0226       0.0087         40       0.0225       0.0087	11	0.0368	0.0319
14       0.0348       0.0274         16       0.0333       0.0265         17       0.0330       0.0257         18       0.0319       0.0215         19       0.0312       0.0210         20       0.0309       0.0183         21       0.0303       0.0143         22       0.0278       0.0094         23       0.0276       0.0091         24       0.0276       0.0091         25       0.0276       0.0091         26       0.0276       0.0091         27       0.0275       0.0091         28       0.0267       0.0090         30       0.0259       0.0089         31       0.0254       0.0089         32       0.0253       0.0089         33       0.0252       0.0089         34       0.0248       0.0088         35       0.0230       0.0087         36       0.0230       0.0087         38       0.0227       0.0087         39       0.0226       0.0087         40       0.0225       0.0087         41       0.0220       0.0086	12	0.0353	0.0298
15       0.0344       0.0274         16       0.0333       0.0265         17       0.0330       0.0257         18       0.0319       0.0215         19       0.0312       0.0210         20       0.0309       0.0183         21       0.0303       0.0143         22       0.0278       0.0094         23       0.0276       0.0091         24       0.0276       0.0091         25       0.0276       0.0091         26       0.0276       0.0091         27       0.0275       0.0091         28       0.0267       0.0090         30       0.0259       0.0089         31       0.0259       0.0089         32       0.0253       0.0089         33       0.0252       0.0088         34       0.0248       0.0088         35       0.0230       0.0087         36       0.0230       0.0087         37       0.0228       0.0087         38       0.0227       0.0087         40       0.0225       0.0087         41       0.0220       0.0086	13	0.0349	0.0293
15       0.0344       0.0274         16       0.0333       0.0265         17       0.0330       0.0257         18       0.0319       0.0215         19       0.0312       0.0210         20       0.0309       0.0183         21       0.0303       0.0143         22       0.0278       0.0094         23       0.0276       0.0091         24       0.0276       0.0091         25       0.0276       0.0091         26       0.0276       0.0091         27       0.0275       0.0091         28       0.0267       0.0090         30       0.0259       0.0089         31       0.0259       0.0089         32       0.0253       0.0089         33       0.0252       0.0088         34       0.0248       0.0088         35       0.0230       0.0087         36       0.0230       0.0087         37       0.0228       0.0087         38       0.0227       0.0087         40       0.0225       0.0087         41       0.0220       0.0086	14	0.0348	0.0285
16       0.0333       0.0265         17       0.0330       0.0257         18       0.0319       0.0215         19       0.0312       0.0210         20       0.0309       0.0183         21       0.0303       0.0143         22       0.0278       0.0094         23       0.0276       0.0091         24       0.0276       0.0091         25       0.0276       0.0091         26       0.0276       0.0091         27       0.0275       0.0091         28       0.0267       0.0090         29       0.0262       0.0090         30       0.0259       0.0089         31       0.0254       0.0089         32       0.0253       0.0089         33       0.0252       0.0088         34       0.0248       0.0088         35       0.0230       0.0087         36       0.0230       0.0087         37       0.0228       0.0087         38       0.0227       0.0087         40       0.0225       0.0087         41       0.0220       0.0086	15	0.0344	0.0274
17       0.0330       0.0257         18       0.0319       0.0215         19       0.0312       0.0210         20       0.0309       0.0183         21       0.0303       0.0143         22       0.0278       0.0094         23       0.0276       0.0092         24       0.0276       0.0091         25       0.0276       0.0091         26       0.0276       0.0091         27       0.0275       0.0091         28       0.0267       0.0090         30       0.0259       0.0089         31       0.0254       0.0089         32       0.0253       0.0089         33       0.0252       0.0088         34       0.0248       0.0088         35       0.0230       0.0087         36       0.0230       0.0087         38       0.0227       0.0087         39       0.0226       0.0087         40       0.0225       0.0087         41       0.0220       0.0086         42       0.0216       0.0085         43       0.0212       0.0085 <td></td> <td></td> <td></td>			
18       0.0319       0.0215         19       0.0312       0.0210         20       0.0309       0.0183         21       0.0303       0.0143         22       0.0278       0.0094         23       0.0276       0.0092         24       0.0276       0.0091         25       0.0276       0.0091         27       0.0275       0.0091         28       0.0267       0.0090         29       0.0262       0.0090         30       0.0259       0.0089         31       0.0254       0.0089         32       0.0253       0.0089         33       0.0252       0.0088         34       0.0248       0.0088         35       0.0230       0.0087         36       0.0230       0.0087         38       0.0227       0.0087         39       0.0226       0.0087         40       0.0225       0.0087         41       0.0220       0.0086         42       0.0216       0.0085         43       0.0212       0.0085			
19       0.0312       0.0210         20       0.0309       0.0183         21       0.0303       0.0143         22       0.0278       0.0094         23       0.0276       0.0092         24       0.0276       0.0091         25       0.0276       0.0091         26       0.0276       0.0091         27       0.0275       0.0091         28       0.0267       0.0090         29       0.0262       0.0090         30       0.0259       0.0089         31       0.0254       0.0089         32       0.0253       0.0089         33       0.0252       0.0088         34       0.0248       0.0088         35       0.0230       0.0087         36       0.0230       0.0087         38       0.0227       0.0087         39       0.0226       0.0087         40       0.0225       0.0087         41       0.0220       0.0086         42       0.0216       0.0085         43       0.0213       0.0085         44       0.0212       0.0085 <td></td> <td></td> <td></td>			
20       0.0309       0.0183         21       0.0303       0.0143         22       0.0278       0.0094         23       0.0276       0.0092         24       0.0276       0.0091         25       0.0276       0.0091         26       0.0275       0.0091         27       0.0275       0.0090         28       0.0267       0.0090         29       0.0262       0.0090         30       0.0259       0.0089         31       0.0254       0.0089         32       0.0253       0.0089         33       0.0252       0.0088         34       0.0248       0.0088         35       0.0230       0.0087         36       0.0230       0.0087         37       0.0228       0.0087         38       0.0227       0.0087         40       0.0225       0.0087         41       0.0220       0.0086         42       0.0216       0.0085         43       0.0213       0.0085         44       0.0212       0.0085			
21       0.0303       0.0143         22       0.0278       0.0094         23       0.0276       0.0092         24       0.0276       0.0091         25       0.0276       0.0091         26       0.0275       0.0091         27       0.0275       0.0091         28       0.0267       0.0090         30       0.0259       0.0089         31       0.0254       0.0089         32       0.0253       0.0089         33       0.0252       0.0088         34       0.0248       0.0088         35       0.0230       0.0087         36       0.0230       0.0087         37       0.0228       0.0087         38       0.0227       0.0087         40       0.0225       0.0087         41       0.0220       0.0086         42       0.0216       0.0085         43       0.0213       0.0085			
22       0.0278       0.0094         23       0.0276       0.0092         24       0.0276       0.0091         25       0.0276       0.0091         26       0.0275       0.0091         27       0.0267       0.0090         29       0.0262       0.0090         30       0.0259       0.0089         31       0.0254       0.0089         32       0.0253       0.0089         33       0.0252       0.0088         34       0.0248       0.0088         35       0.0230       0.0087         36       0.0230       0.0087         38       0.0227       0.0087         39       0.0226       0.0087         40       0.0225       0.0087         41       0.0220       0.0086         42       0.0216       0.0085         43       0.0213       0.0085			
23       0.0276       0.0092         24       0.0276       0.0091         25       0.0276       0.0091         26       0.0275       0.0091         27       0.0275       0.0090         28       0.0267       0.0090         30       0.0259       0.0089         31       0.0254       0.0089         32       0.0253       0.0089         33       0.0252       0.0088         34       0.0248       0.0088         35       0.0230       0.0087         36       0.0230       0.0087         37       0.0228       0.0087         38       0.0227       0.0087         40       0.0225       0.0087         41       0.0220       0.0086         42       0.0216       0.0085         43       0.0213       0.0085			
24       0.0276       0.0091         25       0.0276       0.0091         26       0.0275       0.0091         27       0.0275       0.0090         28       0.0267       0.0090         29       0.0262       0.0090         30       0.0259       0.0089         31       0.0254       0.0089         32       0.0253       0.0089         33       0.0252       0.0088         34       0.0248       0.0088         35       0.0230       0.0087         36       0.0230       0.0087         38       0.0227       0.0087         39       0.0226       0.0087         40       0.0225       0.0087         41       0.0220       0.0086         42       0.0216       0.0085         43       0.0213       0.0085         44       0.0212       0.0085			
25       0.0276       0.0091         26       0.0275       0.0091         27       0.0275       0.0090         28       0.0267       0.0090         29       0.0262       0.0090         30       0.0259       0.0089         31       0.0254       0.0089         32       0.0253       0.0089         33       0.0252       0.0088         34       0.0248       0.0088         35       0.0230       0.0087         36       0.0230       0.0087         37       0.0228       0.0087         39       0.0226       0.0087         40       0.0225       0.0087         41       0.0220       0.0086         42       0.0216       0.0085         43       0.0213       0.0085			
26       0.0276       0.0091         27       0.0275       0.0090         28       0.0267       0.0090         29       0.0262       0.0090         30       0.0259       0.0089         31       0.0254       0.0089         32       0.0253       0.0089         33       0.0252       0.0088         34       0.0248       0.0087         35       0.0230       0.0087         36       0.0230       0.0087         37       0.0228       0.0087         39       0.0226       0.0087         40       0.0225       0.0087         41       0.0220       0.0086         42       0.0216       0.0085         43       0.0213       0.0085         44       0.0212       0.0085			
27       0.0275       0.0091         28       0.0267       0.0090         29       0.0262       0.0090         30       0.0259       0.0089         31       0.0254       0.0089         32       0.0253       0.0089         33       0.0252       0.0088         34       0.0248       0.0087         35       0.0230       0.0087         36       0.0230       0.0087         37       0.0228       0.0087         38       0.0227       0.0087         40       0.0225       0.0087         41       0.0220       0.0086         42       0.0216       0.0085         43       0.0213       0.0085         44       0.0212       0.0085			
28       0.0267       0.0090         29       0.0262       0.0090         30       0.0259       0.0089         31       0.0254       0.0089         32       0.0253       0.0089         33       0.0252       0.0088         34       0.0248       0.0087         35       0.0230       0.0087         37       0.0228       0.0087         38       0.0227       0.0087         39       0.0226       0.0087         40       0.0225       0.0087         41       0.0220       0.0086         42       0.0216       0.0085         43       0.0213       0.0085         44       0.0212       0.0085			
29       0.0262       0.0090         30       0.0259       0.0089         31       0.0254       0.0089         32       0.0253       0.0089         33       0.0252       0.0088         34       0.0248       0.0087         35       0.0230       0.0087         37       0.0228       0.0087         38       0.0227       0.0087         39       0.0226       0.0087         40       0.0225       0.0087         41       0.0220       0.0086         42       0.0216       0.0085         43       0.0213       0.0085         44       0.0212       0.0085			
30       0.0259       0.0089         31       0.0254       0.0089         32       0.0253       0.0089         33       0.0252       0.0088         34       0.0248       0.0087         35       0.0230       0.0087         37       0.0228       0.0087         38       0.0227       0.0087         39       0.0226       0.0087         40       0.0225       0.0087         41       0.0220       0.0086         42       0.0216       0.0085         43       0.0213       0.0085         44       0.0212       0.0085			
31       0.0254       0.0089         32       0.0253       0.0089         33       0.0252       0.0088         34       0.0248       0.0087         35       0.0230       0.0087         36       0.0230       0.0087         37       0.0228       0.0087         38       0.0227       0.0087         39       0.0226       0.0087         40       0.0225       0.0087         41       0.0220       0.0086         42       0.0216       0.0085         43       0.0213       0.0085         44       0.0212       0.0085			
32       0.0253       0.0089         33       0.0252       0.0088         34       0.0248       0.0087         35       0.0230       0.0087         36       0.0230       0.0087         37       0.0228       0.0087         38       0.0227       0.0087         39       0.0226       0.0087         40       0.0225       0.0087         41       0.0220       0.0086         42       0.0216       0.0085         43       0.0213       0.0085         44       0.0212       0.0085			
33       0.0252       0.0088         34       0.0248       0.0087         35       0.0230       0.0087         36       0.0230       0.0087         37       0.0228       0.0087         38       0.0227       0.0087         39       0.0226       0.0087         40       0.0225       0.0087         41       0.0220       0.0086         42       0.0216       0.0085         43       0.0213       0.0085         44       0.0212       0.0085			
34       0.0248       0.0088         35       0.0230       0.0087         36       0.0230       0.0087         37       0.0228       0.0087         38       0.0227       0.0087         39       0.0226       0.0087         40       0.0225       0.0087         41       0.0220       0.0086         42       0.0216       0.0085         43       0.0213       0.0085         44       0.0212       0.0085		0.0253	0.0089
35       0.0230       0.0087         36       0.0230       0.0087         37       0.0228       0.0087         38       0.0227       0.0087         39       0.0226       0.0087         40       0.0225       0.0087         41       0.0220       0.0086         42       0.0216       0.0085         43       0.0213       0.0085         44       0.0212       0.0085	33	0.0252	
36       0.0230       0.0087         37       0.0228       0.0087         38       0.0227       0.0087         39       0.0226       0.0087         40       0.0225       0.0087         41       0.0220       0.0086         42       0.0216       0.0085         43       0.0213       0.0085         44       0.0212       0.0085			0.0088
37       0.0228       0.0087         38       0.0227       0.0087         39       0.0226       0.0087         40       0.0225       0.0087         41       0.0220       0.0086         42       0.0216       0.0085         43       0.0213       0.0085         44       0.0212       0.0085	35	0.0230	0.0087
38       0.0227       0.0087         39       0.0226       0.0087         40       0.0225       0.0087         41       0.0220       0.0086         42       0.0216       0.0085         43       0.0213       0.0085         44       0.0212       0.0085	36	0.0230	0.0087
39       0.0226       0.0087         40       0.0225       0.0087         41       0.0220       0.0086         42       0.0216       0.0085         43       0.0213       0.0085         44       0.0212       0.0085	37	0.0228	0.0087
39       0.0226       0.0087         40       0.0225       0.0087         41       0.0220       0.0086         42       0.0216       0.0085         43       0.0213       0.0085         44       0.0212       0.0085	38	0.0227	0.0087
40       0.0225       0.0087         41       0.0220       0.0086         42       0.0216       0.0085         43       0.0213       0.0085         44       0.0212       0.0085			
41       0.0220       0.0086         42       0.0216       0.0085         43       0.0213       0.0085         44       0.0212       0.0085			
42       0.0216       0.0085         43       0.0213       0.0085         44       0.0212       0.0085			
43       0.0213       0.0085         44       0.0212       0.0085			
0.0212 0.0085			
45 0.0207 0.0085			



46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68	0.0202 0.0199 0.0199 0.0198 0.0193 0.0192 0.0189 0.0187 0.0187 0.0187 0.0187 0.0185 0.0185 0.0185 0.0183 0.0181 0.0179 0.0177	0.0084 0.0084 0.0084 0.0083 0.0083 0.0082 0.0082 0.0082 0.0081 0.0081 0.0081 0.0081 0.0081 0.0081 0.0089 0.0079 0.0079 0.0079 0.0079 0.0079 0.0079
69 70	0.0174 0.0169	0.0078
71 72	0.0169 0.0169	0.0077
73	0.0169	0.0077
74 75	0.0168 0.0167	0.0076 0.0076
76 77	0.0166 0.0165	0.0076 0.0076
78	0.0164	0.0076
79	0.0164	0.0076
80 81	0.0163 0.0161	0.0076 0.0075
82	0.0160	0.0075
83 84	0.0158 0.0157	0.0075 0.0075
85	0.0157	0.0073
86	0.0151	0.0074
87 88	0.0150 0.0150	0.0074
89	0.0148	0.0074
90 91	0.0146 0.0140	0.0074
92	0.0140	0.0074
93	0.0138	0.0073
94 95	0.0136 0.0136	0.0073 0.0073



140       0.0071       0.0060         141       0.0071       0.0060	96 97 98 99 100 101 102 103 104 105 106 107 108 109 110 111 112 113 114 115 116 117 118 119 120 121 122 123 124 125 126 127 128 129 130 131 132 133 134 135 136 137 138 139 139 130 131 132 133 134 135 136 137 138 139 130 131 131 131 131 131 131 131	0.0135 0.0133 0.0130 0.0127 0.0125 0.0124 0.0123 0.0122 0.0121 0.0121 0.0121 0.0120 0.0119 0.0117 0.0116 0.0115 0.0115 0.0115 0.0106 0.0106 0.0102 0.0102 0.0102 0.0102 0.0102 0.0101 0.0101 0.0101 0.0101 0.0101 0.0101 0.0101 0.0101 0.0101 0.0101 0.0109 0.0099 0.0099 0.0099 0.0099 0.0098 0.0086 0.0086 0.0086 0.0086 0.0085 0.0082 0.0073 0.0073 0.0073	0.0073 0.0072 0.0072 0.0072 0.0072 0.0071 0.0071 0.0071 0.0071 0.0071 0.0070 0.0070 0.0069 0.0069 0.0069 0.0069 0.0069 0.0066 0.0065
142 0.0069 0.0060	136 137 138 139 140 141	0.0079 0.0078 0.0073 0.0071 0.0071	0.0062 0.0062 0.0061 0.0061 0.0060



146	0.0064	0.0057
147	0.0064	0.0057
148	0.0063	0.0056
149	0.0062	0.0055
150	0.0062	0.0055
151	0.0060	0.0054
152	0.0055	0.0054
153	0.0053	0.0054
154	0.0049	0.0053
155	0.0035	0.0053
156	0.0016	0.0053
157	0.0013	0.0053
158	0.0008	0.0048

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Stream Protection Duration POC #1

The Facility PASSED

The Facility PASSED.

Flow(cfs)	Predev	Mit Pero	centage	Pass/Fail
0.0083	53118	51229	96	Pass
0.0086	49091	32315	65	Pass
0.0089	45489	19224	42	Pass
0.0092	42265	10155	24	Pass
0.0096	39246	8953	22	Pass
0.0099	36470	8055	22	Pass
0.0102	33972	7679	22	Pass
0.0105	31639	7318	23	Pass
0.0108	29379	6992	23	Pass
0.0111	27396	6681	24	Pass
0.0114	25628	6415	25	Pass
0.0118	24005	6183	25	Pass
0.0121	22570	5956	26	Pass
0.0124	21230	5762	27	Pass
0.0127	19922	5518	27	Pass
0.0130	18736	5296	28	Pass
0.0133	17623	5079	28	Pass
0.0136	16554	4905	29	Pass
0.0139	15468	4748	30	Pass
0.0143	14537	4580	31	Pass
0.0146	13673	4415	32	Pass
0.0149	12881	4266	33	Pass
0.0152	12099	4125	34	Pass
0.0155	11401	3987	34	Pass
0.0158	10692	3866	36	Pass
0.0161	10066	3736	37	Pass
0.0165	9451	3612	38	Pass
0.0168	8914	3487	39	Pass



0.0171 0.0174 0.0177	8388 7889 7485	3371 3258 3154	40 41 42	Pass Pass Pass
0.0177	7053	3045	43	Pass
0.0183	6615	2944	44	Pass
0.0187	6271	2877	45	Pass
0.0190	5961	2794	46	Pass
0.0193	5695	2711	47	Pass
0.0196	5418	2633	48	Pass
0.0199	5174	2545	49	Pass
0.0202	4906	2464	50	Pass
0.0205	4668	2389	51	Pass
0.0209	4481	2306	51	Pass
0.0212	4303	2233	51	Pass
0.0215	4118	2158	52	Pass
0.0218	3913	2083	53	Pass
0.0221	3710	2015	54	Pass
0.0224	3528	1936	54	Pass
0.0227	3371	1884	55	Pass
0.0231	3210	1829	56	Pass
0.0234	3094	1768	57	Pass
0.0237	2982	1709	57	Pass
0.0240	2878	1648	57	Pass
0.0243	2757	1573	57 57	Pass
0.0246	2614 2503	1510 1450	57 57	Pass
0.0249	2303	1387	57	Pass Pass
0.0256	2302	1329	57	Pass
0.0259	2197	1264	57	Pass
0.0262	2074	1211	58	Pass
0.0265	1995	1156	57	Pass
0.0268	1898	1100	57	Pass
0.0271	1808	1047	57	Pass
0.0274	1718	996	57	Pass
0.0278	1637	945	57	Pass
0.0281	1585	894	56	Pass
0.0284	1502	851	56	Pass
0.0287	1428	800	56	Pass
0.0290	1359	745	54	Pass
0.0293	1285	691	53	Pass
0.0296	1229	662	53	Pass
0.0300	1175	636	54	Pass
0.0303	1112	613	55	Pass
0.0306	1066	589	55	Pass
0.0309	1018	565	55	Pass
0.0312	973	537	55	Pass
0.0315	929	513	55	Pass
0.0318	877	471	53	Pass
0.0322	819	452	55 E E	Pass
0.0325	780	432	55	Pass



0.0328 0.0331 0.0334 0.0337 0.0340 0.0344	736 691 635 597 553 509 471	410 394 374 354 331 307 291	55 57 58 59 59 60 61	Pass Pass Pass Pass Pass Pass
0.0350	423	270	63	Pass
0.0353	392	253	64	Pass
0.0356	361	242	67	Pass
0.0359	337	227	67	Pass
0.0362	312	213	68	Pass
0.0365	297	198	66	Pass
0.0369	274	182	66	Pass
0.0372	254	169	66	Pass
0.0375	240	153	63	Pass
0.0378	221	135	61	Pass
0.0381	207	120	57	Pass
	194	119	61	Pass
0.0387	176	116	65	Pass
	156	115	73	Pass
0.0394	142	112	78	Pass

Water Quality BMP Flow and Volume for POC #1 On-line facility volume: 0.0734 acre-feet On-line facility target flow: 0.0969 cfs.

Adjusted for 15 min: 0.0969 cfs.

Off-line facility target flow: 0.0557 cfs.

Adjusted for 15 min: 0.0557 cfs.

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#### LID Report

LID Technique Water Ouality Percent	Used for I	otal Volume	Volume	Infiltration	Cumulative	Percent
water Quality Percent	Treatment?	Needs	Through	Volume	Volume	Volume
Water Ouality	ii ca chicire.	Necab	IIIIOugii	VOIGING	VOIGING	VOIAME
~ 1		Treatment	Facil	ity (ac-ft.)	Infi	ltration
Infiltrated	Treated					
		(ac-ft)	(ac-ft)		Credit	
Vault 1 POC	N	252.02			N	0.00
Total Volume Infiltrated		252.02	0.00	0.00		0.00
0.00 0%	No Treat. Ci	redit				
Compliance	with	LID		Standa	rd	8
Duration Analysis Result =	· Passed					

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#### Perlnd and Implnd Changes

No changes have been made.



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#### 4.4.2 Wetlands Modeling

#### WWHM2012 PROJECT REPORT

Project Name: 23062 - wetlands

Site Name:

Site Address: 1617 S. Meridian

: Puyallup **Report Date:** 6/4/2024 : 38 IN CENTRAL Gage Data Start : 10/01/1901 Data End: 09/30/2059 Precip Scale: 1.00

**Version Date:** 2021/08/18

**Version** : 4.2.18

Low Flow Threshold for POC 1: 50 Percent of the 2 Year

High Flow Threshold for POC 1: 50 year

PREDEVELOPED LAND USE

Name : Basin 1

Bypass: No

GroundWater: No

Pervious Land Use C, Pasture, Mod 200.61

Pervious Total 200.61

Impervious Land Use acre

ROADS MOD 356.65



Impervious Total 356.65

Basin Total 557.26

Element Flows To:

Surface Interflow Groundwater

MITIGATED LAND USE

Name : Basin 1

Bypass: No

GroundWater: No

Pervious Land Use acre

C, Pasture, Mod 200.013

Pervious Total 200.013

Impervious Land Use acre

ROADS MOD 356.662
ROOF TOPS FLAT 0.301
SIDEWALKS MOD 0.156
PARKING MOD 0.128

Impervious Total 357.247

Basin Total 557.26

Element Flows To:

Surface Interflow Groundwater

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ANALYSIS RESULTS

Stream Protection Duration



Predeveloped Landuse Totals for POC #1

Total Pervious Area:200.61 Total Impervious Area:356.65

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Mitigated Landuse Totals for POC #1

Total Pervious Area:200.013
Total Impervious Area:357.247

#### Flow Frequency Return Periods for Predeveloped. POC #1

Return Period	Flow(cfs)
2 year	141.737865
5 year	194.267147
10 year	233.866522
25 year	289.696614
50 year	335.710024
100 year	385.700953

#### Flow Frequency Return Periods for Mitigated. POC #1

Return Period	Flow(cfs)
2 year	141.946328
5 year	194.548924
10 year	234.202942
25 year	290.109351
50 year	336.185131
100 year	386.243359

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#### Stream Protection Duration

Annual Peaks for Predeveloped and Mitigated. POC #1

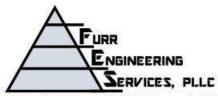
Aiiiiuai	reaks	TOT Predevero	ped and Mitig
Year		Predeveloped	Mitigated
1902		159.645	159.902
1903		174.824	175.107
1904		209.829	210.118
1905		96.153	96.300
1906		108.799	108.968
1907		134.189	134.378
1908		109.392	109.559
1909		134.685	134.894
1910		137.936	138.117
1911		146.997	147.224
1912		284.893	285.212
1913		132.978	133.163
1914		512.016	512.732
1915		90.245	90.383
1916		177.910	178.174



1917       77.365       77.475         1918       134.249       134.467         1919       89.092       89.221         1920       127.513       127.693         1921       97.720       97.855         1922       159.995       160.218         1923       105.130       105.279         1924       191.072       191.358         1925       82.836       82.961         1926       153.084       153.327         1927       139.896       140.092         1928       94.517       94.655         1929       187.985       188.291         1930       208.016       208.336         1931       102.872       103.026         1932       113.623       113.788         1931       102.872       103.026         1932       113.623       113.788         1933       107.788       107.939         1934       169.867       170.108         1935       88.799       88.927         1937       196.320       196.629         1938       98.445       98.576         1939       112.512       112.687			
1919       89.092       89.221         1920       127.513       127.693         1921       97.720       97.855         1922       159.995       160.218         1923       105.130       105.279         1924       191.072       191.358         1925       82.836       82.961         1926       153.084       153.327         1927       139.896       140.092         1928       94.517       94.655         1929       187.985       188.291         1930       208.016       208.336         1931       102.872       103.026         1932       113.623       113.788         1933       107.788       107.939         1934       169.867       170.108         1935       88.799       88.927         1936       129.522       129.721         1937       196.320       196.629         1938       98.445       98.576         1939       112.512       112.687         1940       226.664       227.002         1941       226.116       226.454         1942       151.121       151.343 <t< td=""><td>1917</td><td>77.365</td><td>77.475</td></t<>	1917	77.365	77.475
1919       89.092       89.221         1920       127.513       127.693         1921       97.720       97.855         1922       159.995       160.218         1923       105.130       105.279         1924       191.072       191.358         1925       82.836       82.961         1926       153.084       153.327         1927       139.896       140.092         1928       94.517       94.655         1929       187.985       188.291         1930       208.016       208.336         1931       102.872       103.026         1932       113.623       113.788         1933       107.788       107.939         1934       169.867       170.108         1935       88.799       88.927         1936       129.522       129.721         1937       196.320       196.629         1938       98.445       98.576         1939       112.512       112.687         1940       226.664       227.002         1941       226.116       226.454         1942       151.121       151.343 <t< td=""><td>1918</td><td>134.249</td><td>134.467</td></t<>	1918	134.249	134.467
1920       127.513       127.693         1921       97.720       97.855         1922       159.995       160.218         1923       105.130       105.279         1924       191.072       191.358         1925       82.836       82.961         1926       153.084       153.327         1927       139.896       140.092         1928       94.517       94.655         1929       187.985       188.291         1930       208.016       208.336         1931       102.872       103.026         1932       113.623       113.788         1931       102.872       103.026         1932       113.623       113.788         1932       113.623       113.788         1933       107.788       107.939         1934       169.867       170.108         1935       88.799       88.927         1937       196.320       196.629         1938       98.445       98.576         1939       112.512       112.687         1940       226.664       227.002         1941       226.116       226.454			
1921       97.720       97.855         1922       159.995       160.218         1923       105.130       105.279         1924       191.072       191.358         1925       82.836       82.961         1926       153.084       153.327         1927       139.896       140.092         1928       94.517       94.655         1929       187.985       188.291         1930       208.016       208.336         1931       102.872       103.026         1932       113.623       113.788         1933       107.788       107.939         1934       169.867       170.108         1935       88.799       88.927         1936       129.522       129.721         1937       196.320       196.629         1938       98.445       98.576         1939       112.512       112.687         1940       226.664       227.002         1941       226.116       226.454         1942       151.121       151.343         1943       142.680       142.909         1944       217.246       217.562			
1922       159.995       160.218         1923       105.130       105.279         1924       191.072       191.358         1925       82.836       82.961         1926       153.084       153.327         1927       139.896       140.092         1928       94.517       94.655         1929       187.985       188.291         1930       208.016       208.336         1931       102.872       103.026         1932       113.623       113.788         1933       107.788       107.939         1934       169.867       170.108         1935       88.799       88.927         1936       129.522       129.721         1937       196.320       196.629         1938       98.445       98.576         1939       112.512       112.687         1940       226.664       227.002         1941       226.166       227.002         1941       226.166       226.454         1942       151.121       151.343         1943       142.680       142.909         1944       217.246       217.562			
1923       105.130       105.279         1924       191.072       191.358         1925       82.836       82.961         1926       153.084       153.327         1927       139.896       140.092         1928       94.517       94.655         1929       187.985       188.291         1930       208.016       208.336         1931       102.872       103.026         1932       113.623       113.788         1933       107.788       107.939         1934       169.867       170.108         1935       88.799       88.927         1936       129.522       129.721         1937       196.320       196.629         1938       98.445       98.576         1939       112.512       112.687         1940       226.664       227.002         1941       226.116       226.454         1942       151.121       151.343         1943       142.680       142.909         1944       217.246       217.562         1945       153.143       153.397         1946       143.257       143.446			
1924       191.072       191.358         1925       82.836       82.961         1926       153.084       153.327         1927       139.896       140.092         1928       94.517       94.655         1929       187.985       188.291         1930       208.016       208.336         1931       102.872       103.026         1932       113.623       113.788         1933       107.788       107.939         1934       169.867       170.108         1935       88.799       88.927         1936       129.522       129.721         1937       196.320       196.629         1938       98.445       98.576         1939       112.512       112.687         1940       226.664       227.002         1941       226.116       226.454         1942       151.121       151.343         1943       142.680       142.909         1944       217.246       217.562         1945       153.143       153.397         1946       143.257       143.446         1947       96.012       96.162	1922	159.995	
1925       82.836       82.961         1926       153.084       153.327         1927       139.896       140.092         1928       94.517       94.655         1929       187.985       188.291         1930       208.016       208.336         1931       102.872       103.026         1932       113.623       113.788         1933       107.788       107.939         1934       169.867       170.108         1935       88.799       88.927         1936       129.522       129.721         1937       196.320       196.629         1938       98.445       98.576         1939       112.512       112.687         1940       226.664       227.002         1941       226.116       226.454         1942       151.121       151.343         1943       142.680       142.909         1944       217.246       217.562         1945       153.143       153.397         1946       143.257       143.446         1947       96.012       96.162         1948       130.980       131.193	1923	105.130	105.279
1925       82.836       82.961         1926       153.084       153.327         1927       139.896       140.092         1928       94.517       94.655         1929       187.985       188.291         1930       208.016       208.336         1931       102.872       103.026         1932       113.623       113.788         1933       107.788       107.939         1934       169.867       170.108         1935       88.799       88.927         1936       129.522       129.721         1937       196.320       196.629         1938       98.445       98.576         1939       112.512       112.687         1940       226.664       227.002         1941       226.116       226.454         1942       151.121       151.343         1943       142.680       142.909         1944       217.246       217.562         1945       153.143       153.397         1946       143.257       143.446         1947       96.012       96.162         1948       130.980       131.193	1924	191.072	191.358
1926       153.084       153.327         1927       139.896       140.092         1928       94.517       94.655         1929       187.985       188.291         1930       208.016       208.336         1931       102.872       103.026         1932       113.623       113.788         1933       107.788       107.939         1934       169.867       170.108         1935       88.799       88.927         1936       129.522       129.721         1937       196.320       196.629         1938       98.445       98.576         1939       112.512       112.687         1940       226.664       227.002         1941       226.116       226.454         1942       151.121       151.343         1943       142.680       142.909         1944       217.246       217.562         1945       153.143       153.397         1946       143.257       143.446         1947       96.012       96.162         1948       130.980       131.193         1950       132.931       133.133	1925		
1927       139.896       140.092         1928       94.517       94.655         1929       187.985       188.291         1930       208.016       208.336         1931       102.872       103.026         1932       113.623       113.788         1933       107.788       107.939         1934       169.867       170.108         1935       88.799       88.927         1936       129.522       129.721         1937       196.320       196.629         1938       98.445       98.576         1939       112.512       112.687         1940       226.664       227.002         1941       226.116       226.454         1942       151.121       151.343         1943       142.680       142.909         1944       217.246       217.562         1945       153.143       153.397         1946       143.257       143.446         1947       96.012       96.162         1948       130.980       131.193         1950       132.931       133.133         1951       236.884       237.220			
1928       94.517       94.655         1929       187.985       188.291         1930       208.016       208.336         1931       102.872       103.026         1932       113.623       113.788         1933       107.788       107.939         1934       169.867       170.108         1935       88.799       88.927         1936       129.522       129.721         1937       196.320       196.629         1938       98.445       98.576         1939       112.512       112.687         1940       226.664       227.002         1941       226.116       226.454         1942       151.121       151.343         1943       142.680       142.909         1944       217.246       217.562         1945       153.143       153.397         1946       143.257       143.446         1947       96.012       96.162         1948       130.980       131.193         1950       132.931       133.133         1951       236.884       237.220         1952       225.857       226.141			
1929       187.985       188.291         1930       208.016       208.336         1931       102.872       103.026         1932       113.623       113.788         1933       107.788       107.939         1934       169.867       170.108         1935       88.799       88.927         1936       129.522       129.721         1937       196.320       196.629         1938       98.445       98.576         1939       112.512       112.687         1940       226.664       227.002         1941       226.116       226.454         1942       151.121       151.343         1943       142.680       142.909         1944       217.246       217.562         1945       153.143       153.397         1946       143.257       143.446         1947       96.012       96.162         1948       130.980       131.193         1949       200.387       200.716         1950       132.931       133.133         1951       236.884       237.220         1955       137.689       137.869			
1930       208.016       208.336         1931       102.872       103.026         1932       113.623       113.788         1933       107.788       107.939         1934       169.867       170.108         1935       88.799       88.927         1936       129.522       129.721         1937       196.320       196.629         1938       98.445       98.576         1939       112.512       112.687         1940       226.664       227.002         1941       226.116       226.454         1942       151.121       151.343         1943       142.680       142.909         1944       217.246       217.562         1945       153.143       153.397         1946       143.257       143.446         1947       96.012       96.162         1948       130.980       131.193         1949       200.387       200.716         1950       132.931       133.133         1951       236.884       237.220         1953       187.364       187.616         1955       137.689       137.869			
1931       102.872       103.026         1932       113.623       113.788         1933       107.788       107.939         1934       169.867       170.108         1935       88.799       88.927         1936       129.522       129.721         1937       196.320       196.629         1938       98.445       98.576         1939       112.512       112.687         1940       226.664       227.002         1941       226.116       226.454         1942       151.121       151.343         1943       142.680       142.909         1944       217.246       217.562         1945       153.143       153.397         1946       143.257       143.446         1947       96.012       96.162         1948       130.980       131.193         1950       132.931       133.133         1951       236.884       237.220         1952       225.857       226.141         1953       187.364       187.616         1954       109.450       109.615         1955       137.689       137.869			
1932       113.623       113.788         1933       107.788       107.939         1934       169.867       170.108         1935       88.799       88.927         1936       129.522       129.721         1937       196.320       196.629         1938       98.445       98.576         1939       112.512       112.687         1940       226.664       227.002         1941       226.116       226.454         1942       151.121       151.343         1943       142.680       142.909         1944       217.246       217.562         1945       153.143       153.397         1946       143.257       143.446         1947       96.012       96.162         1948       130.980       131.193         1949       200.387       200.716         1950       132.931       133.133         1951       236.884       237.220         1952       225.857       226.141         1953       187.364       187.616         1954       109.450       109.615         1955       137.689       137.869	1930		
1933       107.788       107.939         1934       169.867       170.108         1935       88.799       88.927         1936       129.522       129.721         1937       196.320       196.629         1938       98.445       98.576         1939       112.512       112.687         1940       226.664       227.002         1941       226.116       226.454         1942       151.121       151.343         1943       142.680       142.909         1944       217.246       217.562         1945       153.143       153.397         1946       143.257       143.446         1947       96.012       96.162         1948       130.980       131.193         1949       200.387       200.716         1950       132.931       133.133         1951       236.884       237.220         1952       225.857       226.141         1953       187.364       187.616         1954       109.450       109.615         1955       137.689       137.869         1958       160.793       161.002	1931	102.872	103.026
1934       169.867       170.108         1935       88.799       88.927         1936       129.522       129.721         1937       196.320       196.629         1938       98.445       98.576         1939       112.512       112.687         1940       226.664       227.002         1941       226.116       226.454         1942       151.121       151.343         1943       142.680       142.909         1944       217.246       217.562         1945       153.143       153.397         1946       143.257       143.446         1947       96.012       96.162         1948       130.980       131.193         1949       200.387       200.716         1950       132.931       133.133         1951       236.884       237.220         1952       225.857       226.141         1953       187.364       187.616         1954       109.450       109.615         1955       137.689       137.869         1957       108.064       108.216         1958       160.793       161.002	1932	113.623	113.788
1934       169.867       170.108         1935       88.799       88.927         1936       129.522       129.721         1937       196.320       196.629         1938       98.445       98.576         1939       112.512       112.687         1940       226.664       227.002         1941       226.116       226.454         1942       151.121       151.343         1943       142.680       142.909         1944       217.246       217.562         1945       153.143       153.397         1946       143.257       143.446         1947       96.012       96.162         1948       130.980       131.193         1949       200.387       200.716         1950       132.931       133.133         1951       236.884       237.220         1952       225.857       226.141         1953       187.364       187.616         1954       109.450       109.615         1955       137.689       137.869         1957       108.064       108.216         1958       160.793       161.002	1933	107.788	107.939
1935       88.799       88.927         1936       129.522       129.721         1937       196.320       196.629         1938       98.445       98.576         1939       112.512       112.687         1940       226.6664       227.002         1941       226.116       226.454         1942       151.121       151.343         1943       142.680       142.909         1944       217.246       217.562         1945       153.143       153.397         1946       143.257       143.446         1947       96.012       96.162         1948       130.980       131.193         1949       200.387       200.716         1950       132.931       133.133         1951       236.884       237.220         1952       225.857       226.141         1953       187.364       187.616         1954       109.450       109.615         1955       137.689       137.869         1956       117.102       117.276         1957       108.064       108.216         1958       160.793       161.002			
1936       129.522       129.721         1937       196.320       196.629         1938       98.445       98.576         1939       112.512       112.687         1940       226.664       227.002         1941       226.116       226.454         1942       151.121       151.343         1943       142.680       142.909         1944       217.246       217.562         1945       153.143       153.397         1946       143.257       143.446         1947       96.012       96.162         1948       130.980       131.193         1949       200.387       200.716         1950       132.931       133.133         1951       236.884       237.220         1952       225.857       226.141         1953       187.364       187.616         1954       109.450       109.615         1955       137.689       137.869         1957       108.064       108.216         1958       160.793       161.002         1959       160.706       160.909         1960       116.884       117.064 <td></td> <td></td> <td></td>			
1937       196.320       196.629         1938       98.445       98.576         1939       112.512       112.687         1940       226.664       227.002         1941       226.116       226.454         1942       151.121       151.343         1943       142.680       142.909         1944       217.246       217.562         1945       153.143       153.397         1946       143.257       143.446         1947       96.012       96.162         1948       130.980       131.193         1949       200.387       200.716         1950       132.931       133.133         1951       236.884       237.220         1952       225.857       226.141         1953       187.364       187.616         1954       109.450       109.615         1955       137.689       137.869         1957       108.064       108.216         1958       160.793       161.002         1959       160.706       160.909         1960       116.884       117.064         1961       329.802       330.313 <td></td> <td></td> <td></td>			
1938       98.445       98.576         1939       112.512       112.687         1940       226.664       227.002         1941       226.116       226.454         1942       151.121       151.343         1943       142.680       142.909         1944       217.246       217.562         1945       153.143       153.397         1946       143.257       143.446         1947       96.012       96.162         1948       130.980       131.193         1949       200.387       200.716         1950       132.931       133.133         1951       236.884       237.220         1952       225.857       226.141         1953       187.364       187.616         1954       109.450       109.615         1955       137.689       137.869         1956       117.102       117.276         1957       108.064       108.216         1958       160.793       161.002         1959       160.706       160.909         1960       116.884       117.064         1961       329.802       330.313 <td></td> <td></td> <td></td>			
1939       112.512       112.687         1940       226.664       227.002         1941       226.116       226.454         1942       151.121       151.343         1943       142.680       142.909         1944       217.246       217.562         1945       153.143       153.397         1946       143.257       143.446         1947       96.012       96.162         1948       130.980       131.193         1949       200.387       200.716         1950       132.931       133.133         1951       236.884       237.220         1952       225.857       226.141         1953       187.364       187.616         1954       109.450       109.615         1955       137.689       137.869         1956       117.102       117.276         1957       108.064       108.216         1958       160.793       161.002         1959       160.706       160.909         1960       116.884       117.064         1961       329.802       330.313         1962       141.405       141.620 </td <td></td> <td></td> <td></td>			
1940       226.664       227.002         1941       226.116       226.454         1942       151.121       151.343         1943       142.680       142.909         1944       217.246       217.562         1945       153.143       153.397         1946       143.257       143.446         1947       96.012       96.162         1948       130.980       131.193         1949       200.387       200.716         1950       132.931       133.133         1951       236.884       237.220         1952       225.857       226.141         1953       187.364       187.616         1954       109.450       109.615         1955       137.689       137.869         1956       117.102       117.276         1957       108.064       108.216         1958       160.793       161.002         1959       160.706       160.909         1960       116.884       117.064         1961       329.802       330.313         1962       141.405       141.620         1963       95.895       96.051 <td></td> <td></td> <td></td>			
1941       226.116       226.454         1942       151.121       151.343         1943       142.680       142.909         1944       217.246       217.562         1945       153.143       153.397         1946       143.257       143.446         1947       96.012       96.162         1948       130.980       131.193         1949       200.387       200.716         1950       132.931       133.133         1951       236.884       237.220         1952       225.857       226.141         1953       187.364       187.616         1954       109.450       109.615         1955       137.689       137.869         1956       117.102       117.276         1957       108.064       108.216         1958       160.793       161.002         1959       160.706       160.909         1960       116.884       117.064         1961       329.802       330.313         1962       141.405       141.620         1963       95.895       96.051         1964       357.819       358.330 <td></td> <td></td> <td></td>			
1942       151.121       151.343         1943       142.680       142.909         1944       217.246       217.562         1945       153.143       153.397         1946       143.257       143.446         1947       96.012       96.162         1948       130.980       131.193         1949       200.387       200.716         1950       132.931       133.133         1951       236.884       237.220         1952       225.857       226.141         1953       187.364       187.616         1954       109.450       109.615         1955       137.689       137.869         1957       108.064       108.216         1958       160.793       161.002         1959       160.706       160.909         1960       116.884       117.064         1961       329.802       330.313         1962       141.405       141.620         1963       95.895       96.051         1964       357.819       358.330         1965       151.135       151.343	1940		
1943       142.680       142.909         1944       217.246       217.562         1945       153.143       153.397         1946       143.257       143.446         1947       96.012       96.162         1948       130.980       131.193         1949       200.387       200.716         1950       132.931       133.133         1951       236.884       237.220         1952       225.857       226.141         1953       187.364       187.616         1954       109.450       109.615         1955       137.689       137.869         1956       117.102       117.276         1957       108.064       108.216         1958       160.793       161.002         1959       160.706       160.909         1960       116.884       117.064         1961       329.802       330.313         1962       141.405       141.620         1963       95.895       96.051         1964       357.819       358.330         1965       151.135       151.343	1941	226.116	226.454
1944       217.246       217.562         1945       153.143       153.397         1946       143.257       143.446         1947       96.012       96.162         1948       130.980       131.193         1949       200.387       200.716         1950       132.931       133.133         1951       236.884       237.220         1952       225.857       226.141         1953       187.364       187.616         1954       109.450       109.615         1955       137.689       137.869         1956       117.102       117.276         1957       108.064       108.216         1958       160.793       161.002         1959       160.706       160.909         1960       116.884       117.064         1961       329.802       330.313         1962       141.405       141.620         1963       95.895       96.051         1964       357.819       358.330         1965       151.135       151.343	1942	151.121	151.343
1945       153.143       153.397         1946       143.257       143.446         1947       96.012       96.162         1948       130.980       131.193         1949       200.387       200.716         1950       132.931       133.133         1951       236.884       237.220         1952       225.857       226.141         1953       187.364       187.616         1954       109.450       109.615         1955       137.689       137.869         1956       117.102       117.276         1957       108.064       108.216         1958       160.793       161.002         1959       160.706       160.909         1960       116.884       117.064         1961       329.802       330.313         1962       141.405       141.620         1963       95.895       96.051         1964       357.819       358.330         1965       151.135       151.343	1943	142.680	142.909
1945       153.143       153.397         1946       143.257       143.446         1947       96.012       96.162         1948       130.980       131.193         1949       200.387       200.716         1950       132.931       133.133         1951       236.884       237.220         1952       225.857       226.141         1953       187.364       187.616         1954       109.450       109.615         1955       137.689       137.869         1956       117.102       117.276         1957       108.064       108.216         1958       160.793       161.002         1959       160.706       160.909         1960       116.884       117.064         1961       329.802       330.313         1962       141.405       141.620         1963       95.895       96.051         1964       357.819       358.330         1965       151.135       151.343	1944	217.246	217.562
1946       143.257       143.446         1947       96.012       96.162         1948       130.980       131.193         1949       200.387       200.716         1950       132.931       133.133         1951       236.884       237.220         1952       225.857       226.141         1953       187.364       187.616         1954       109.450       109.615         1955       137.689       137.869         1956       117.102       117.276         1957       108.064       108.216         1958       160.793       161.002         1959       160.706       160.909         1960       116.884       117.064         1961       329.802       330.313         1962       141.405       141.620         1963       95.895       96.051         1964       357.819       358.330         1965       151.135       151.343	1945		
1947       96.012       96.162         1948       130.980       131.193         1949       200.387       200.716         1950       132.931       133.133         1951       236.884       237.220         1952       225.857       226.141         1953       187.364       187.616         1954       109.450       109.615         1955       137.689       137.869         1956       117.102       117.276         1957       108.064       108.216         1958       160.793       161.002         1959       160.706       160.909         1960       116.884       117.064         1961       329.802       330.313         1962       141.405       141.620         1963       95.895       96.051         1964       357.819       358.330         1965       151.135       151.343			
1948       130.980       131.193         1949       200.387       200.716         1950       132.931       133.133         1951       236.884       237.220         1952       225.857       226.141         1953       187.364       187.616         1954       109.450       109.615         1955       137.689       137.869         1956       117.102       117.276         1957       108.064       108.216         1958       160.793       161.002         1959       160.706       160.909         1960       116.884       117.064         1961       329.802       330.313         1962       141.405       141.620         1963       95.895       96.051         1964       357.819       358.330         1965       151.135       151.343			
1949       200.387       200.716         1950       132.931       133.133         1951       236.884       237.220         1952       225.857       226.141         1953       187.364       187.616         1954       109.450       109.615         1955       137.689       137.869         1956       117.102       117.276         1957       108.064       108.216         1958       160.793       161.002         1959       160.706       160.909         1960       116.884       117.064         1961       329.802       330.313         1962       141.405       141.620         1963       95.895       96.051         1964       357.819       358.330         1965       151.135       151.343			
1950       132.931       133.133         1951       236.884       237.220         1952       225.857       226.141         1953       187.364       187.616         1954       109.450       109.615         1955       137.689       137.869         1956       117.102       117.276         1957       108.064       108.216         1958       160.793       161.002         1959       160.706       160.909         1960       116.884       117.064         1961       329.802       330.313         1962       141.405       141.620         1963       95.895       96.051         1964       357.819       358.330         1965       151.135       151.343			
1951       236.884       237.220         1952       225.857       226.141         1953       187.364       187.616         1954       109.450       109.615         1955       137.689       137.869         1956       117.102       117.276         1957       108.064       108.216         1958       160.793       161.002         1959       160.706       160.909         1960       116.884       117.064         1961       329.802       330.313         1962       141.405       141.620         1963       95.895       96.051         1964       357.819       358.330         1965       151.135       151.343			
1952       225.857       226.141         1953       187.364       187.616         1954       109.450       109.615         1955       137.689       137.869         1956       117.102       117.276         1957       108.064       108.216         1958       160.793       161.002         1959       160.706       160.909         1960       116.884       117.064         1961       329.802       330.313         1962       141.405       141.620         1963       95.895       96.051         1964       357.819       358.330         1965       151.135       151.343			
1953       187.364       187.616         1954       109.450       109.615         1955       137.689       137.869         1956       117.102       117.276         1957       108.064       108.216         1958       160.793       161.002         1959       160.706       160.909         1960       116.884       117.064         1961       329.802       330.313         1962       141.405       141.620         1963       95.895       96.051         1964       357.819       358.330         1965       151.135       151.343			
1954       109.450       109.615         1955       137.689       137.869         1956       117.102       117.276         1957       108.064       108.216         1958       160.793       161.002         1959       160.706       160.909         1960       116.884       117.064         1961       329.802       330.313         1962       141.405       141.620         1963       95.895       96.051         1964       357.819       358.330         1965       151.135       151.343	1952		226.141
1955       137.689       137.869         1956       117.102       117.276         1957       108.064       108.216         1958       160.793       161.002         1959       160.706       160.909         1960       116.884       117.064         1961       329.802       330.313         1962       141.405       141.620         1963       95.895       96.051         1964       357.819       358.330         1965       151.135       151.343	1953	187.364	187.616
1956     117.102     117.276       1957     108.064     108.216       1958     160.793     161.002       1959     160.706     160.909       1960     116.884     117.064       1961     329.802     330.313       1962     141.405     141.620       1963     95.895     96.051       1964     357.819     358.330       1965     151.135     151.343	1954	109.450	109.615
1957       108.064       108.216         1958       160.793       161.002         1959       160.706       160.909         1960       116.884       117.064         1961       329.802       330.313         1962       141.405       141.620         1963       95.895       96.051         1964       357.819       358.330         1965       151.135       151.343	1955	137.689	137.869
1957       108.064       108.216         1958       160.793       161.002         1959       160.706       160.909         1960       116.884       117.064         1961       329.802       330.313         1962       141.405       141.620         1963       95.895       96.051         1964       357.819       358.330         1965       151.135       151.343	1956	117.102	117.276
1958       160.793       161.002         1959       160.706       160.909         1960       116.884       117.064         1961       329.802       330.313         1962       141.405       141.620         1963       95.895       96.051         1964       357.819       358.330         1965       151.135       151.343			
1959     160.706     160.909       1960     116.884     117.064       1961     329.802     330.313       1962     141.405     141.620       1963     95.895     96.051       1964     357.819     358.330       1965     151.135     151.343			
1960       116.884       117.064         1961       329.802       330.313         1962       141.405       141.620         1963       95.895       96.051         1964       357.819       358.330         1965       151.135       151.343			
1961       329.802       330.313         1962       141.405       141.620         1963       95.895       96.051         1964       357.819       358.330         1965       151.135       151.343			
1962       141.405       141.620         1963       95.895       96.051         1964       357.819       358.330         1965       151.135       151.343			
1963       95.895       96.051         1964       357.819       358.330         1965       151.135       151.343			
1964       357.819       358.330         1965       151.135       151.343			
1965 151.135 151.343			
	1964		
1966 103.384 103.546	1965		
	1966	103.384	103.546



1967 1968	156.196 136.221	156.395 136.428
1969	110.362	110.530
1970	133.020	133.214
1971	126.365	126.537
1972 1973	466.724 242.243	467.393 242.631
1974	169.466	169.734
1975	178.906	179.149
1976	191.471	191.750
1977	88.383	88.516
1978	147.011	147.209
1979	142.430	142.661
1980	161.097	161.324
1981	152.083	152.299
1982	114.656	114.835
1983	150.028	150.237
1984	145.520	145.742
1985	193.551	193.799
1986	94.421	94.550
1987	156.026	156.273
1988	88.914	89.041
1989	98.796	98.924
1990	119.350 205.196	119.516
1991 1992	208.554	205.482 208.847
1993	167.170	167.446
1994	123.838	124.018
1995	94.416	94.560
1996	134.481	134.669
1997	118.824	118.991
1998	136.344	136.539
1999	174.132	174.387
2000	124.338	124.525
2001	130.956	131.141
2002	194.382	194.632
2003	144.075	144.257
2004	165.124	165.379
2005	403.628	404.205
2006	146.453	146.688
2007	166.662	166.924
2008	136.289	136.496
2009	105.210 134.165	105.355
2010 2011	144.315	134.375 144.515
2012	123.435	123.627
2012	129.256	129.451
2013	133.065	133.266
2015	209.670	209.964
2016	150.166	150.365



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2017	186.553	186.863
2018	153.317	153.483
2019 2020	193.376 141.376	193.606 141.587
2020	119.758	119.932
2022	199.439	199.765
2023	269.426	269.808
2024	323.401	323.790
2025	150.709	150.914
2026	231.457	231.762
2027	166.543	166.808
2028 2029	59.767 101.526	59.866 101.676
2030	212.339	212.632
2031	65.246	65.346
2032	124.029	124.200
2033	140.653	140.879
2034	104.364	104.536
2035	138.327	138.507
2036 2037	113.942 182.448	114.106 182.714
2037	140.233	140.432
2039	307.855	308.296
2040	114.165	114.333
2041	134.687	134.906
2042	158.031	158.287
2043	175.623 122.467	175.907 122.658
2044 2045	95.295	95.442
2046	115.837	116.012
2047	126.830	127.041
2048	108.750	108.922
2049	160.837	161.099
2050	124.648	124.825
2051 2052	170.323 154.837	170.572 155.065
2052	112.205	112.386
2054	232.554	232.897
2055	142.368	142.568
2056	192.976	193.253
2057	86.530	86.666
2058 2059	205.773 226.723	206.073 227.073
2000	220.125	221.013

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#### Stream Protection Duration

FES Project 23062

Ranked Annual Peaks for Predeveloped and Mitigated. POC #1

Rank	Predeveloped	Mitigated
1	512.0160	512.7320
2	466.7240	467.3930



3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	403.6280 357.8190 329.8020 323.4010 307.8550 284.8930 269.4260 242.2430 236.8840 232.5540 231.4570 226.7230 226.6640 225.8570 217.2460 212.3390 209.8290 209.6700 208.5540 208.0160 205.7730 205.1960 200.3870 199.4390 196.3200 194.3820 193.5510	404.2050 358.3300 330.3130 323.7900 308.2960 285.2120 269.8080 242.6310 237.2200 232.8970 231.7620 227.0730 227.0020 226.4540 226.4410 217.5620 212.6320 210.1180 209.9640 208.8470 208.8470 208.3360 206.0730 205.4820 200.7160 199.7650 196.6290 194.6320 193.7990
31 32	193.3760 192.9760	193.6060 193.2530
33 34	191.4710 191.0720	191.7500 191.3580
35	187.9850	188.2910
36	187.3640	187.6160
37 38	186.5530 182.4480	186.8630 182.7140
39	178.9060	179.1490
40	177.9100	178.1740
41	175.6230	175.9070
42	174.8240	175.1070
43 44	174.1320 170.3230	174.3870 170.5720
45	169.8670	170.3720
46	169.4660	169.7340
47	167.1700	167.4460
48	166.6620	166.9240
49	166.5430	166.8080
50 51	165.1240 161.0970	165.3790 161.3240
52	160.8370	161.3240



53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 94 95 96 96 97 97 97 97 97 97 97 97 97 97 97 97 97	160.7930 160.7060 159.9950 159.6450 158.0310 156.1960 156.0260 154.8370 153.3170 153.1430 153.0840 152.0830 151.1210 150.7090 150.1660 150.0280 147.0110 146.9970 146.4530 145.5200 144.3150 144.0750 143.2570 142.6800 142.4300 142.4300 142.3680 141.4050 141.3760 140.6530 140.6530 140.2330 139.8960 138.3270 137.9360 137.6890 136.2210 134.6870 134.6870 134.6850 134.6850 134.4810 134.2490 134.1890	161.0020 160.9090 160.2180 159.9020 158.2870 156.3950 156.2730 155.0650 153.4830 153.3970 153.3270 152.2990 151.3430 150.9140 150.3650 150.2370 147.2240 147.2240 147.2240 147.2240 147.2240 147.2240 147.2240 147.22570 143.4460 142.5680 144.5150 144.5150 144.5570 143.4460 142.9090 142.6610 142.5680 141.6200 141.5870 140.8790 140.8790 140.8790 140.8790 140.8790 140.920 138.5070 138.1170 137.8690 136.4960 134.8940 134.6690 134.8940 134.6690 134.8940 134.6690 134.3780
92 93 94 95 96 97 98 99	134.6850 134.4810 134.2490 134.1890 134.1650 133.0650 133.0200 132.9780 132.9310	134.8940 134.6690 134.4670 134.3780 134.3750 133.2660 133.2140 133.1630 133.1330
101 102	130.9800 130.9560	131.1930 131.1410



103 104 105 106 107 108 109 110 111 112 113 114 115 116 117	129.5220 129.2560 127.5130 126.8300 126.3650 124.6480 124.3380 124.0290 123.8380 123.4350 122.4670 119.7580 119.3500 118.8240 117.1020 116.8840	129.7210 129.4510 127.6930 127.0410 126.5370 124.8250 124.5250 124.2000 124.0180 123.6270 122.6580 119.9320 119.5160 118.9910 117.2760 117.0640
119	115.8370	116.0120
120 121	114.6560 114.1650	114.8350 114.3330
122	113.9420	114.1060
123	113.6230	113.7880
124	112.5120	112.6870
125	112.2050	112.3860
126	110.3620	110.5300
127	109.4500	109.6150
128 129	109.3920	109.5590 108.9680
130	108.7990 108.7500	108.9220
131	108.0640	108.9220
132	107.7880	107.9390
133	105.2100	105.3550
134	105.1300	105.2790
135	104.3640	104.5360
136	103.3840	103.5460
137	102.8720	103.0260
138	101.5260	101.6760
139	98.7962	98.9235
140	98.4452	98.5755
141 142	97.7195 96.1529	97.8553 96.2998
143	96.0121	96.1618
144	95.8949	96.0509
145	95.2953	95.4423
146	94.5165	94.6551
147	94.4205	94.5599
148	94.4162	94.5496
149	90.2451	90.3834
150	89.0918	89.2213
151	88.9140	89.0413
152	88.7985	88.9270



153	88.3833	88.5164
154	86.5300	86.6662
155	82.8363	82.9611
156	77.3652	77.4751
157	65.2463	65.3459
158	59.7669	59.8660

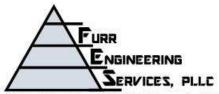
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Stream Protection Duration POC #1

The Facility FAILED

Facility FAILED duration standard for 1+ flows.

Flow(cfs)	Predev	Mit Perce	entage	Pass/Fail
70.8689	3965	3985	100	Pass
73.5441	3394	3414	100	Pass
76.2193	2938	2960	100	Pass
78.8944	2637	2641	100	Pass
81.5696	2346	2359	100	Pass
84.2447	2087	2100	100	Pass
86.9199	1881	1893	100	Pass
89.5951	1686	1697	100	Pass
92.2702	1505	1509	100	Pass
94.9454	1323	1331	100	Pass
97.6206	1175	1183	100	Pass
100.2957	1070	1077	100	Pass
102.9709	986	993	100	Pass
105.6460	882	886	100	Pass
108.3212	809	812	100	Pass
110.9964	724	729	100	Pass
113.6715	655	660	100	Pass
116.3467	594	598	100	Pass
119.0219	547	550	100	Pass
121.6970	498	504	101	Fail
124.3722	445	447	100	Pass
127.0473	401	403	100	Pass
129.7225	366	368	100	Pass
132.3977	330	331	100	Pass
135.0728	297	299	100	Pass
137.7480	269	270	100	Pass
140.4232	241	243	100	Pass
143.0983	216	218	100	Pass
145.7735	204	207	101	Pass
148.4486	192	193	100	Pass
151.1238	181	181	100	Pass
153.7990	161	161	100	Pass
156.4741	151	151	100	Pass
159.1493	143	143	100	Pass
161.8245	128	128	100	Pass



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1000 mm - 1000	000			
164.4996	124	124	100	Pass
167.1748	113	113	100	Pass
169.8499	103	103	100	Pass
172.5251	99	99	100	Pass
175.2003	96	96	100	Pass
177.8754	92	93	101	Pass
180.5506	88	88	100	Pass
183.2258	79	79	100	Pass
185.9009	76	76	100	Pass
188.5761	70	70	100	
191.2512	70 67	68	101	Pass
				Pass
193.9264	62	62	100	Pass
196.6016	57	59	103	Pass
199.2767	53	54	101	Pass
201.9519	49	49	100	Pass
204.6271	49	49	100	Pass
207.3022	43	43	100	Pass
209.9774	37	39	105	Pass
212.6525	35	36	102	Pass
215.3277	35	35	100	Pass
218.0029	32	32	100	Pass
220.6780	32	32	100	Pass
223.3532	32	32	100	Pass
226.0284	30	31	103	Pass
228.7035	25	27	108	Pass
231.3787	24	24	100	Pass
234.0538	22	22	100	Pass
236.7290	22	22	100	Pass
239.4042	20	20	100	Pass
242.0793	19	19	100	Pass
244.7545	18	18	100	Pass
247.4297	18	18	100	Pass
250.1048	16	16	100	Pass
252.7800	16	16	100	Pass
255.4551	16	16	100	Pass
258.1303	16	16	100	Pass
260.8055	16	16	100	
				Pass
263.4806	16	16	100	Pass
266.1558	16	16	100	Pass
268.8310	14	15	107	Pass
271.5061	12	12	100	Pass
274.1813	12	12	100	Pass
276.8564	11	11	100	Pass
279.5316	11	11	100	Pass
282.2068	11	11	100	Pass
284.8819	11	11	100	Pass
287.5571	10	10	100	Pass
290.2323	10	10	100	Pass
292.9074	10	10	100	Pass
295.5826	10	10	100	Pass



298.2577	10	10	100	Pass
300.9329	10	10	100	Pass
303.6081	10	10	100	Pass
306.2832	10	10	100	Pass
308.9584	9	9	100	Pass
311.6336	9	9	100	Pass
314.3087	9	9	100	Pass
316.9839	9	9	100	Pass
319.6590	9	9	100	Pass
322.3342	9	9	100	Pass
325.0094	8	8	100	Pass
327.6845	8	8	100	Pass
330.3597	6	8	133	Fail
333.0349	6	6	100	Pass
335.7100	6	6	100	Pass

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The development has an increase in flow durations from 1/2 Predeveloped 2 year flow to the 2 year flow or more than a 10% increase from the 2 year to the 50 year flow.

Water Quality BMP Flow and Volume for POC #1

On-line facility volume: 0 acre-feet On-line facility target flow: 0 cfs.

Adjusted for 15 min: 0 cfs.

Off-line facility target flow: 0 cfs.

Adjusted for 15 min: 0 cfs.

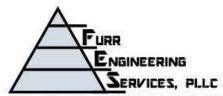
#### LID Report

LID Technique Water Ouality B	Percent	Used for Comment	Total Volume	Volume	Infiltration	Cumulative	Percent
water guarrey i	CICCIIC	Treatment?	Needs	Through	Volume	Volume	Volume
Water Quality		11000	1,0000	1111000911	V0140		10140
			Treatment	Facil	ity (ac-ft.)	Inf	iltration
Infiltrated		Treated					
			(ac-ft)	(ac-ft)	1	Credit	
Total Volume Inf	filtrated		0.00	0.00	0.00		0.00
0.00	<b>)</b> %	No Treat. C	Credit				
Compliance		with	LID		Standa	rd	8
Duration Analysi	is Result =	Failed					

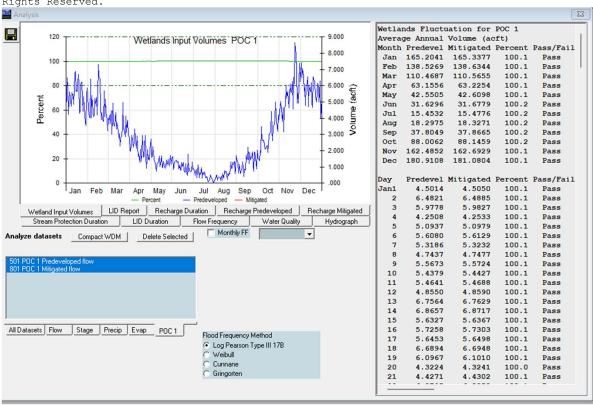
#### Perlnd and Implnd Changes

No changes have been made.

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### 5.0 SPECIAL REPORTS AND STUDIES

Geotechnical Report: Proposed Medical Building 11504 NE 21<sup>st</sup> St. Bellevue WA, by PanGeo Inc., dated September 9, 2020, File No. 20-294



### 6.0 OTHER PERMITS

**Grading Permit** 

**Building Permit** 



#### 7.0 ESC ANALYSIS AND DESIGN

SWPPP is submitted under separate cover.

Design of the ESC plan was completed in conformance with Core Requirement per the 2019 SMMWW. Compliance with the 13 minimum requirements is summarized below.

- 1. Clearing Limits: Clearing limits have been delineated BMP C233 on sheets of the civil plans.
- 2. Construction Access: An armored construction entrance BMP C105 is shown on the plan.
- 3. Control Flow Rates: Silt Fence will be used to reduce the flow.
- 4. Install Sediment Controls: A construction entrance will be installed at the entrance to the project site. See TESC plan for location of construction entrance and detail.
- 5. Stabilize Soils: The proposed sediment ponds will be used for sediment retention. Sediment retention will be designed per the stormwater manual.
- 6. Protect Slopes: Not Required for this project.
- 7. Protect Drain Inlets: Inlets are sufficiently far away from the construction and don't need protection.
- 8. Stabilize Channels and Outlets: There are no channels or outlets.
- 9. Control Pollutants: Flow Control: BMP C151, BMP C152, BMP C153 and BMP C154.
- 10. Control Dewatering: Dewatering is not expected for this project
- 11. Maintain BMP's: CESCL
- 12. Manage the Project: CESCL
- 13. Protect LID BMP's: Silt Fence will be placed around the infiltration areas to protect them from compaction.

During the wet season (October 1 to April 30) any site with exposed soils shall be subject to the "Wet Season Requirements" contained in the ESC Standards. In addition to the ESC cover measures, these provisions include covering any newly-seeded areas with mulch and seeding as much disturbed area as possible during the first week of October to provide grass cover for the wet season.

Prior to obtaining final construction approval, the site shall be stabilized, structural ESC measures (such as silt fences and sediment traps) shall be removed, and drainage facilities shall be cleaned as specified in the ESC Standards.



# 8.0 BOND QUANTITIES

To be provided at final approval if required



### 9.0 OPERATIONS AND MAINTENANCE MANUAL

# **Table V-A.2: Maintenance Standards - Infiltration (continued)**

Maintenance Component	Defect	Conditions When Maintenance Is Needed	Results Expected When Maintenance Is Per- formed
		(A percolation test pit or test of facility indicates facility is only working at 90% of its designed capabilities. Test every 2 to 5 years. If two inches or more sediment is present, remove).	
Filter Bags (if applicable)	Filled with Sediment and Debris	Sediment and debris fill bag more than 1/2 full.	Filter bag is replaced or system is redesigned.
Rock Filters	Sediment and Debris	By visual inspection, little or no water flows through filter during heavy rain storms.	Gravel in rock filter is replaced.
Side Slopes of Pond	Erosion	See Table V-A.1: Maintenance Standards - Detention Ponds	See <u>Table V-A.1</u> : Maintenance Standards - Detention Ponds
Emergency Overflow Spillway	Tree Growth	See Table V-A.1: Maintenance Standards - Detention Ponds	See <u>Table V-A.1: Maintenance Standards - Detention Ponds</u>
and Berms over 4 feet in height.	Piping	See <u>Table V-A.1: Maintenance Standards - Detention Ponds</u>	See Table V-A.1: Maintenance Standards - Detention Ponds
Emergency Overflow Spillway	Rock Missing	See <u>Table V-A.1: Maintenance Standards - Detention Ponds</u>	See Table V-A.1: Maintenance Standards - Detention Ponds
Enlergency Overnow Spiliway	Erosion	See Table V-A.1: Maintenance Standards - Detention Ponds	See Table V-A.1: Maintenance Standards - Detention Ponds
Pre-settling Ponds and Vaults	Facility or sump filled with Sediment and/or debris	6" or designed sediment trap depth of sediment.	Sediment is removed.

# Table V-A.3: Maintenance Standards - Closed Detention Systems (Tanks/Vaults)

Maintenance Component	Defect	Results Expected When Maintenance is Performed		
	Plugged Air Vents	One-half of the cross section of a vent is blocked at any point or the vent is damaged.	Vents open and functioning.	
	Debris and Sediment	Accumulated sediment depth exceeds 10% of the diameter of the storage area for 1/2 length of storage vault or any point depth exceeds 15% of diameter.	All sediment and debris removed from storage	
Storage Area	Debris and Sediment	(Example: 72-inch storage tank would require cleaning when sediment reaches depth of 7 inches for more than 1/2 length of tank.)	area.	
	Lainta Datusaan Tarih/Dina Caatian	Any openings or voids allowing material to be transported into facility.	All joint between tank/pipe sections are sealed.	
	Joints Between Tank/Pipe Section	(Will require engineering analysis to determine structural stability).	All joint between tank/pipe sections are sealed.	
	Tank Pipe Bent Out of Shape	Any part of tank/pipe is bent out of shape more than 10% of its design shape. (Review required by engineer to determine structural stability).	Tank/pipe repaired or replaced to design.	
	Vault Structure Includes Cracks in Wall, Bottom,	Cracks wider than 1/2-inch and any evidence of soil particles entering the structure through the cracks, or maintenance/inspection personnel determines that the vault is not structurally sound.	Vault replaced or repaired to design specifications and is structurally sound.	
	Damage to Frame and/or Top Slab	Cracks wider than 1/2-inch at the joint of any inlet/outlet pipe or any evidence of soil particles entering the vault through the walls.	No cracks more than 1/4-inch wide at the joint of the inlet/outlet pipe.	

# Table V-A.3: Maintenance Standards - Closed Detention Systems (Tanks/Vaults) (continued)

Maintenance Component	Defect	Conditions When Maintenance is Needed	Results Expected When Maintenance is Performed
	Cover Not in Place Cover is missing or only partially in place. Any open manhole requires maintenance.		Manhole is closed.
Manhole  Locking Mechanism Not Working  Mechanism cannot be opened by one maintenance person with proper tools. Bolts into frame have less than 1/2 inch of thread (may not apply to self-locking lids).		Mechanism opens with proper tools.	
	Cover Difficult to Remove	One maintenance person cannot remove lid after applying normal lifting pressure. Intent is to keep cover from sealing off access to maintenance.	
	Ladder is unsafe due to missing rungs, misalignment, not securely attached to structure wall, rust, or cracks.		Ladder meets design standards. Allows maintenance person safe access.
Catch Basins	See Table V-A.5: Maintenance Standards - Catch Basins	See <u>Table V-A.5: Maintenance Standards - Catch Basins</u>	See Table V-A.5: Maintenance Standards - Catch Basins

### **Table V-A.4: Maintenance Standards - Control Structure/Flow Restrictor**

Maintenance Com- ponent	Defect	Condition When Maintenance is Needed	Results Expected When Maintenance is Performed
	Trash and Debris (Includes Sediment)	Material exceeds 25% of sump depth or 1 foot below orifice plate.	Control structure orifice is not blocked. All trash and debris removed.
General	Structure is not securely attached to mannole wall.  Structure is not in upright position (allow up to 10% from plumb).  Connections to outlet pipe are not watertight and show signs of rust.  Any holes - other than designed holes - in the structure		Structure securely attached to wall and outlet pipe.  Structure in correct position.  Connections to outlet pipe are water tight; structure repaired or replaced and works as designed.  Structure has no holes other than designed holes.
Cleanout Gate	Damaged or Missing	Cleanout gate is not watertight or is missing.  Gate cannot be moved up and down by one maintenance person.  Chain/rod leading to gate is missing or damaged.  Gate is rusted over 50% of its surface area.	Gate is watertight and works as designed. Gate moves up and down easily and is watertight. Chain is in place and works as designed. Gate is repaired or replaced to meet design standards.
Orifice Plate	Damaged or Missing	Control device is not working properly due to missing, out of place, or bent orifice plate.	Plate is in place and works as designed.
	Obstructions	Any trash, debris, sediment, or vegetation blocking the plate.	Plate is free of all obstructions and works as designed.
Overflow Pipe	Obstructions	Any trash or debris blocking (or having the potential of blocking) the overflow pipe.	Pipe is free of all obstructions and works as designed.
Manhole	See Table V-A.3: Maintenance Standards - Closed Detention Systems (Tanks/Vaults)	See Table V-A.3: Maintenance Standards - Closed Detention Systems (Tanks/Vaults)	See Table V-A.3: Maintenance Standards - Closed Detention Systems (Tank-s/Vaults)
Catch Basin	See Table V-A.5: Maintenance Standards - Catch Basins	See Table V-A.5: Maintenance Standards - Catch Basins	See Table V-A.5: Maintenance Standards - Catch Basins

# **Table V-A.5: Maintenance Standards - Catch Basins**

Maintenance Component	Defect	Conditions When Maintenance is Needed	Results Expected When Maintenance is per- formed
	Trash & Debris	Trash or debris which is located immediately in front of the catch basin opening or is blocking inletting capacity of the basin by more than 10%.  Trash or debris (in the basin) that exceeds 60 percent of the sump depth as measured from the bottom of basin to invert of the lowest pipe into or out of the basin, but in no case less than a minimum of six inches clearance from the debris surface to the invert of the lowest pipe.  Trash or debris in any inlet or outlet pipe blocking more than 1/3 of its height.  Dead animals or vegetation that could generate odors that could cause complaints or dangerous gases (e.g., methane).	No Trash or debris located immediately in front of catch basin or on grate opening.  No trash or debris in the catch basin.  Inlet and outlet pipes free of trash or debris.  No dead animals or vegetation present within the catch basin.
	Sediment	Sediment (in the basin) that exceeds 60 percent of the sump depth as measured from the bottom of basin to invert of the lowest pipe into or out of the basin, but in no case less than a minimum of 6 inches clearance from the sediment surface to the invert of the lowest pipe.	No sediment in the catch basin
General	Structure Damage to Frame and/or Top Slab	Top slab has holes larger than 2 square inches or cracks wider than 1/4 inch. (Intent is to make sure no material is running into basin).  Frame not sitting flush on top slab, i.e., separation of more than 3/4 inch of the frame from the top slab. Frame not securely attached	Top slab is free of holes and cracks.  Frame is sitting flush on the riser rings or top slab and firmly attached.
	Fractures or Cracks in Basin Walls/ Bottom	Maintenance person judges that structure is unsound.  Grout fillet has separated or cracked wider than 1/2 inch and longer than 1 foot at the joint of any inlet/outlet pipe or any evidence of soil particles entering catch basin through cracks.	Basin replaced or repaired to design standards.  Pipe is regrouted and secure at basin wall.
	Settlement/ Mis- alignment	If failure of basin has created a safety, function, or design problem.	Basin replaced or repaired to design standards.
	Vegetation	Vegetation growing across and blocking more than 10% of the basin opening.  Vegetation growing in inlet/outlet pipe joints that is more than six inches tall and less than six inches apart.	No vegetation blocking opening to basin.  No vegetation or root growth present.
	Contamination and Pollution	See <u>Table V-A.1: Maintenance Standards - Detention Ponds</u>	No pollution present.
	Cover Not in Place	Cover is missing or only partially in place. Any open catch basin requires maintenance.	Cover/grate is in place, meets design standards, and is secured
Catch Basin Cover	Locking Mechanism Not Working	Mechanism cannot be opened by one maintenance person with proper tools. Bolts into frame have less than 1/2 inch of thread.	Mechanism opens with proper tools.
	Cover Difficult to Remove	One maintenance person cannot remove lid after applying normal lifting pressure.  (Intent is keep cover from sealing off access to maintenance.)	Cover can be removed by one maintenance person.
Ladder	Ladder Rungs Unsafe Ladder is unsafe due to missing rungs, not securely attached to basin wall, misalignment, rust, cracks, or sharp edges.		Ladder meets design standards and allows maintenance person safe access.
	Grate opening Unsafe	Grate with opening wider than 7/8 inch.	Grate opening meets design standards.
Metal Grates	Trash and Debris	Trash and debris that is blocking more than 20% of grate surface inletting capacity.	Grate free of trash and debris.
(If Applicable)	Damaged or Missing.	Grate missing or broken member(s) of the grate.	Grate is in place, meets the design standards, and is installed and aligned with the flow path.

# **Table V-A.12: Maintenance Standards - Wetvaults (continued)**

Maintenance Component	Defect	Condition When Maintenance is Needed	Results Expected When Maintenance is Performed
		and non-floatables).	
	Sediment Accumulation in Vault	Sediment accumulation in vault bottom exceeds the depth of the sediment zone plus 6-inches.	Remove sediment from vault.
	Damaged Pipes	Inlet/outlet piping damaged or broken and in need of repair.	Pipe repaired and/or replaced.
	Access Cover Damaged/Not Working	Cover cannot be opened or removed, especially by one person.	Cover repaired or replaced to proper working specifications.
	Ventilation	Ventilation area blocked or plugged.	Blocking material removed or cleared from ventilation area. A specified % of the vault surface area must provide ventilation to the vault interior (see design specifications).
	Vault Structure Damage - Includes Cracks	Maintenance/inspection personnel determine that the vault is not structurally sound.	Vault replaced or repairs made so that vault meets design specifications and is structurally sound.
	in Walls Bottom, Damage to Frame and/or Top Slab	Cracks wider than 1/2-inch at the joint of any inlet/outlet pipe or evidence of soil particles entering through the cracks.	Vault repaired so that no cracks exist wider than 1/4-inch at the joint of the inlet/outlet pipe.
	Baffles	Baffles corroding, cracking, warping and/or showing signs of failure as determined by maintenance/inspection staff.	Baffles repaired or replaced to specifications.
	Access Ladder Damage	Ladder is corroded or deteriorated, not functioning properly, not attached to structure wall, missing rungs, has cracks and/or misaligned. Confined space warning sign missing.	Ladder replaced or repaired to specifications, and is safe to use as determined by inspection personnel. Replace sign warning of confined space entry requirements. Ladder and entry notification complies with OSHA standards.

# Table V-A.13: Maintenance Standards - Sand Filters (Above Ground/Open)

Maintenance Component	Defect	Condition When Maintenance is Needed	Results Expected When Maintenance is Performed
	Sediment Accu- mulation on top layer	Sediment depth exceeds 1/2-inch.	No sediment deposit on grass layer of sand filter that would impede permeability of the filter section.
	Trash and Debris Accumulations	Trash and debris accumulated on sand filter bed.	Trash and debris removed from sand filter bed.
	Sediment/ Debris in Clean-Outs	When the clean-outs become full or partially plugged with sediment and/or debris.	Sediment removed from clean-outs.
Above Ground (open sand fil-	Sand Filter Media	Drawdown of water through the sand filter media takes longer than 24-hours, and/or flow through the overflow pipes occurs frequently.	Top several inches of sand are scraped. May require replacement of entire sand filter depth depending on extent of plugging (a sieve analysis is helpful to determine if the lower sand has too high a proportion of fine material).
ter)	Prolonged Flows	Sand is saturated for prolonged periods of time (several weeks) and does not dry out between storms due to continuous base flow or prolonged flows from detention facilities.	Low, continuous flows are limited to a small portion of the facility by using a low wooden divider or slightly depressed sand surface.
	Short Circuiting	When flows become concentrated over one section of the sand filter rather than dispersed.	Flow and percolation of water through sand filter is uniform and dispersed across the entire filter area.
	Erosion Damage to Slopes	Erosion over 2-inches deep where cause of damage is prevalent or potential for continued erosion is evident.	Slopes stabilized using proper erosion control measures.
	Rock Pad Miss- ing or Out of Place	Soil beneath the rock is visible.	Rock pad replaced or rebuilt to design specifications.

# Table V-A.13: Maintenance Standards - Sand Filters (Above Ground/Open) (continued)

Maintenance Component	Defect	Condition When Maintenance is Needed	Results Expected When Maintenance is Performed
	Flow Spreader	Flow spreader uneven or clogged so that flows are not uniformly distributed across sand filter.	Spreader leveled and cleaned so that flows are spread evenly over sand filter.
	Damaged Pipes	Any part of the piping that is crushed or deformed more than 20% or any other failure to the piping.	Pipe repaired or replaced.

# **Table V-A.14: Maintenance Standards - Sand Filters (Below Ground/Enclosed)**

Maintenance Component	Defect	Condition When Maintenance is Needed	Results Expected When Maintenance is Performed	
	Sediment Accumulation on Sand Media Section	Sediment depth exceeds 1/2-inch.	No sediment deposits on sand filter section that which would impede permeability of the filter section.	
	Sediment Accumulation in Pre-Settling Portion of Vault	Sediment accumulation in vault bottom exceeds the depth of the sediment zone plus 6-inches.	No sediment deposits in first chamber of vault.	
	Trash/Debris Accumulation	Trash and debris accumulated in vault, or pipe inlet/outlet, floatables and non-floatables.	Trash and debris removed from vault and inlet/outlet piping.	
	Sediment in Drain Pipes/Cleanouts	When drain pipes, cleanouts become full with sediment and/or debris.	Sediment and debris removed.	
	Short Circuiting	When seepage/flow occurs along the vault walls and corners. Sand eroding near inflow area.	Sand filter media section re-laid and compacted along perimeter of vault to form a sem seal. Erosion protection added to dissipate force of incoming flow and curtail erosion.	
	Damaged Pipes	Inlet or outlet piping damaged or broken and in need of repair.	Pipe repaired and/or replaced.	
Below Ground	Access Cover Damaged/Not Working	Cover cannot be opened, corrosion/deformation of cover.	Cover repaired to proper working specifications or replaced.	
Vault.	Access Cover Damagea/Not Working	Maintenance person cannot remove cover using normal lifting pressure.		
	Ventilation	Ventilation area blocked or plugged	Blocking material removed or cleared from ventilation area. A specified % of the vault surface area must provide ventilation to the vault interior (see design specifications).	
	Vault Structure Damaged; Includes Cracks in Walls, Bottom, Damage to Frame and/or Top	Cracks wider than 1/2-inch or evidence of soil particles entering the structure through the cracks, or maintenance/inspection personnel determine that the vault is not structurally sound.	Vault replaced or repairs made so that vault meets design specifications and is structurally sound.	
	Slab.	Cracks wider than 1/2-inch at the joint of any inlet/outlet pipe or evidence of soil particles entering through the cracks.	Vault repaired so that no cracks exist wider than 1/4-inch at the joint of the inlet/outlet pipe.	
	Baffles/Internal walls  Baffles or walls corroding, cracking, warping and/or showing signs of failure as determined by maintenance/inspection person.		Baffles repaired or replaced to specifications.	
	Access Ladder Damaged	Ladder is corroded or deteriorated, not functioning properly, not securely attached to structure wall, missing rungs, cracks, and misaligned.	Ladder replaced or repaired to specifications, and is safe to use as determined by inspection personnel.	

# **Table V-A.15: Maintenance Standards - Manufactured Media Filters**

Maintenance Component	Defect	Condition When Maintenance is Needed	Results Expected When Maintenance is Performed
Below Ground	Sediment Accumulation on Media.	Sediment depth exceeds 0.25-inches.	No sediment deposits which would impede permeability of the

# **Table V-A.15: Maintenance Standards - Manufactured Media Filters (continued)**

Maintenance Component	Defect	Condition When Maintenance is Needed	Results Expected When Maintenance is Performed	
			compost media.	
	Sediment Accumulation in Vault	Sediment depth exceeds 6-inches in first chamber.	No sediment deposits in vault bottom of first chamber.	
	Trash/Debris Accumulation	Trash and debris accumulated on compost filter bed.	Trash and debris removed from the compost filter bed.	
	Sediment in Drain Pipes/Clean-Outs	When drain pipes, clean-outs, become full with sediment and/or debris.	Sediment and debris removed.	
	Damaged Pipes	Any part of the pipes that are crushed or damaged due to corrosion and/or settlement.	Pipe repaired and/or replaced.	
Vault	Access Cover Damaged/Not Working	Cover cannot be opened; one person cannot open the cover using normal lifting pressure, corrosion/deformation of cover.	Cover repaired to proper working specifications or replaced.	
	Vault Structure Includes Cracks in Wall, Bottom,	Cracks wider than 1/2-inch or evidence of soil particles entering the structure through the cracks, or maintenance/inspection personnel determine that the vault is not structurally sound.	Vault replaced or repairs made so that vault meets design specifications and is structurally sound.	
	Damage to Frame and/or Top Slab	Cracks wider than 1/2-inch at the joint of any inlet/outlet pipe or evidence of soil particles entering through the cracks.	Vault repaired so that no cracks exist wider than 1/4-inch at the joint of the inlet/outlet pipe.	
	Baffles	Baffles corroding, cracking warping, and/or showing signs of failure as determined by maintenance/inspection person.	Baffles repaired or replaced to specifications.	
	Access Ladder Damaged	Ladder is corroded or deteriorated, not functioning properly, not securely attached to structure wall, missing rungs, cracks, and misaligned.	Ladder replaced or repaired and meets specifications, and is safe to use as determined by inspection personnel.	
Below Ground	Media	Drawdown of water through the media takes longer than 1 hour, and/or overflow occurs frequently.	Media cartridges replaced.	
Cartridge Type	Short Circuiting	Flows do not properly enter filter cartridges.	Filter cartridges replaced.	



**APPENDIX A: NRCS WEB SOIL SURVEY** 

#### MAP LEGEND

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Water Features

Transportation

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Background

Spoil Area

Stony Spot

Wet Spot

Other

Rails

**US Routes** 

Major Roads

Local Roads

Very Stony Spot

Special Line Features

Streams and Canals

Interstate Highways

Aerial Photography

#### Area of Interest (AOI)

Area of Interest (AOI)

#### Soils

Soil Map Unit Polygons



Soil Map Unit Points

#### Special Point Features

(o) Blowout

Borrow Pit

Clay Spot

Closed Depression

Gravel Pit

Gravelly Spot

Landfill

Lava Flow

Marsh or swamp

Mine or Quarry

Miscellaneous Water

Perennial Water

Rock Outcrop

Saline Spot

sandy Spot

Severely Eroded Spot

Sinkhole

Slide or Slip

Sodic Spot

#### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24.000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Pierce County Area, Washington Survey Area Data: Version 18, Sep 8, 2022

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jul 31, 2022—Aug 8, 2022

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

# **Map Unit Legend**

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
13B	Everett very gravelly sandy loam, 0 to 8 percent slopes	27.4	9.5%
13C	Everett very gravelly sandy loam, 8 to 15 percent slopes	23.8	8.3%
13D	Everett very gravelly sandy loam, 15 to 30 percent slopes	14.6	5.1%
19C	Kapowsin gravelly ashy loam, 6 to 15 percent slopes	17.0	5.9%
19D	Kapowsin gravelly ashy loam, 15 to 30 percent slopes	25.9	9.0%
20C	Kitsap silt loam, 8 to 15 percent slopes	70.4	24.5%
20D	Kitsap silt loam, 15 to 30 percent slopes	70.2	24.4%
31A	Puyallup fine sandy loam	17.1	6.0%
37A	Semiahmoo muck	2.1	0.7%
38A	Shalcar muck	19.0	6.6%
Totals for Area of Interest		287.5	100.0%

## Pierce County Area, Washington

### 19D—Kapowsin gravelly ashy loam, 15 to 30 percent slopes

#### **Map Unit Setting**

National map unit symbol: 2t61y Elevation: 50 to 900 feet

Mean annual precipitation: 30 to 50 inches Mean annual air temperature: 48 to 52 degrees F

Frost-free period: 150 to 220 days

Farmland classification: Farmland of statewide importance

#### **Map Unit Composition**

Kapowsin and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of

the mapunit.

#### **Description of Kapowsin**

#### Setting

Landform: Moraines

Landform position (two-dimensional): Footslope, backslope

Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Linear

Parent material: Volcanic ash mixed with glacial drift over dense

glaciomarine deposits

#### Typical profile

Ap - 0 to 7 inches: gravelly ashy loam
Bhs - 7 to 11 inches: gravelly ashy loam
Bs1 - 11 to 15 inches: gravelly ashy loam

2Bs2 - 15 to 25 inches: loam 3Bstm - 25 to 29 inches: loam 3Cd - 29 to 59 inches: gravelly loam

#### **Properties and qualities**

Slope: 15 to 30 percent

Depth to restrictive feature: More than 80 inches; More than 80

inches

Drainage class: Moderately well drained

Capacity of the most limiting layer to transmit water (Ksat): Very low

(0.00 to 0.00 in/hr)

Depth to water table: About 11 to 24 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 5.3 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: B

Ecological site: F002XA004WA - Puget Lowlands Forest Forage suitability group: Limited Depth Soils (G002XF303WA)

Other vegetative classification: Limited Depth Soils

(G002XF303WA) *Hydric soil rating:* No

#### **Minor Components**

#### **Alderwood**

Percent of map unit: 10 percent

Landform: Hills, ridges

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Nose slope, side slope, talf

Down-slope shape: Convex, linear Across-slope shape: Convex Hydric soil rating: No

#### **Barneston**

Percent of map unit: 5 percent Landform: Moraines, eskers, kames

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

### **Data Source Information**

Soil Survey Area: Pierce County Area, Washington

Survey Area Data: Version 18, Sep 8, 2022

## Pierce County Area, Washington

#### 20C—Kitsap silt loam, 8 to 15 percent slopes

#### **Map Unit Setting**

National map unit symbol: 2hpv

Elevation: 0 to 590 feet

Mean annual precipitation: 37 inches Mean annual air temperature: 50 degrees F

Frost-free period: 160 to 200 days

Farmland classification: Farmland of statewide importance

#### **Map Unit Composition**

Kitsap and similar soils: 85 percent Minor components: 2 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Kitsap**

#### Setting

Landform: Terraces

Parent material: Glaciolacustrine deposits

#### **Typical profile**

H1 - 0 to 10 inches: ashy silt loam H2 - 10 to 32 inches: silty clay loam

H3 - 32 to 60 inches: stratified silt to silty clay loam

#### **Properties and qualities**

Slope: 8 to 15 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Moderately well drained

Capacity of the most limiting layer to transmit water

(Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)

Depth to water table: About 16 to 23 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: High (about 11.5 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4w

Hydrologic Soil Group: C/D

Ecological site: F002XA004WA - Puget Lowlands Forest Forage suitability group: Soils with Moderate Limitations

(G002XS601WA)

Other vegetative classification: Soils with Moderate Limitations

(G002XS601WA) *Hydric soil rating:* No

### **Minor Components**

#### **Bellingham**

Percent of map unit: 2 percent Landform: Depressions

Other vegetative classification: Wet Soils (G002XN102WA)

Hydric soil rating: Yes

### **Data Source Information**

Soil Survey Area: Pierce County Area, Washington

Survey Area Data: Version 18, Sep 8, 2022

## Pierce County Area, Washington

#### 20D—Kitsap silt loam, 15 to 30 percent slopes

#### **Map Unit Setting**

National map unit symbol: 2hpw

Elevation: 0 to 660 feet

Mean annual precipitation: 37 inches Mean annual air temperature: 50 degrees F

Frost-free period: 160 to 200 days

Farmland classification: Farmland of statewide importance

#### **Map Unit Composition**

Kitsap and similar soils: 85 percent Minor components: 2 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Kitsap**

#### Setting

Landform: Terraces

Parent material: Glaciolacustrine deposits

#### **Typical profile**

H1 - 0 to 10 inches: ashy silt loam H2 - 10 to 32 inches: silty clay loam

H3 - 32 to 60 inches: stratified silt to silty clay loam

#### **Properties and qualities**

Slope: 15 to 30 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Moderately well drained

Capacity of the most limiting layer to transmit water

(Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)

Depth to water table: About 16 to 23 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: High (about 11.5 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: C/D

Ecological site: F002XA004WA - Puget Lowlands Forest

Forage suitability group: Sloping to Steep Soils (G002XN702WA)

Other vegetative classification: Sloping to Steep Soils

(G002XN702WA) Hydric soil rating: No

### **Minor Components**

### **Bow variant**

Percent of map unit: 2 percent
Landform: Depressions
Other vegetative classification: Sloping to Steep Soils
(G002XN702WA)
Hydric soil rating: Yes

## **Data Source Information**

Soil Survey Area: Pierce County Area, Washington

Survey Area Data: Version 18, Sep 8, 2022



## APPENDIX B: CITY OF PUYALLUP CRITICAL AREA MAPS

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# Earthquake Hazard

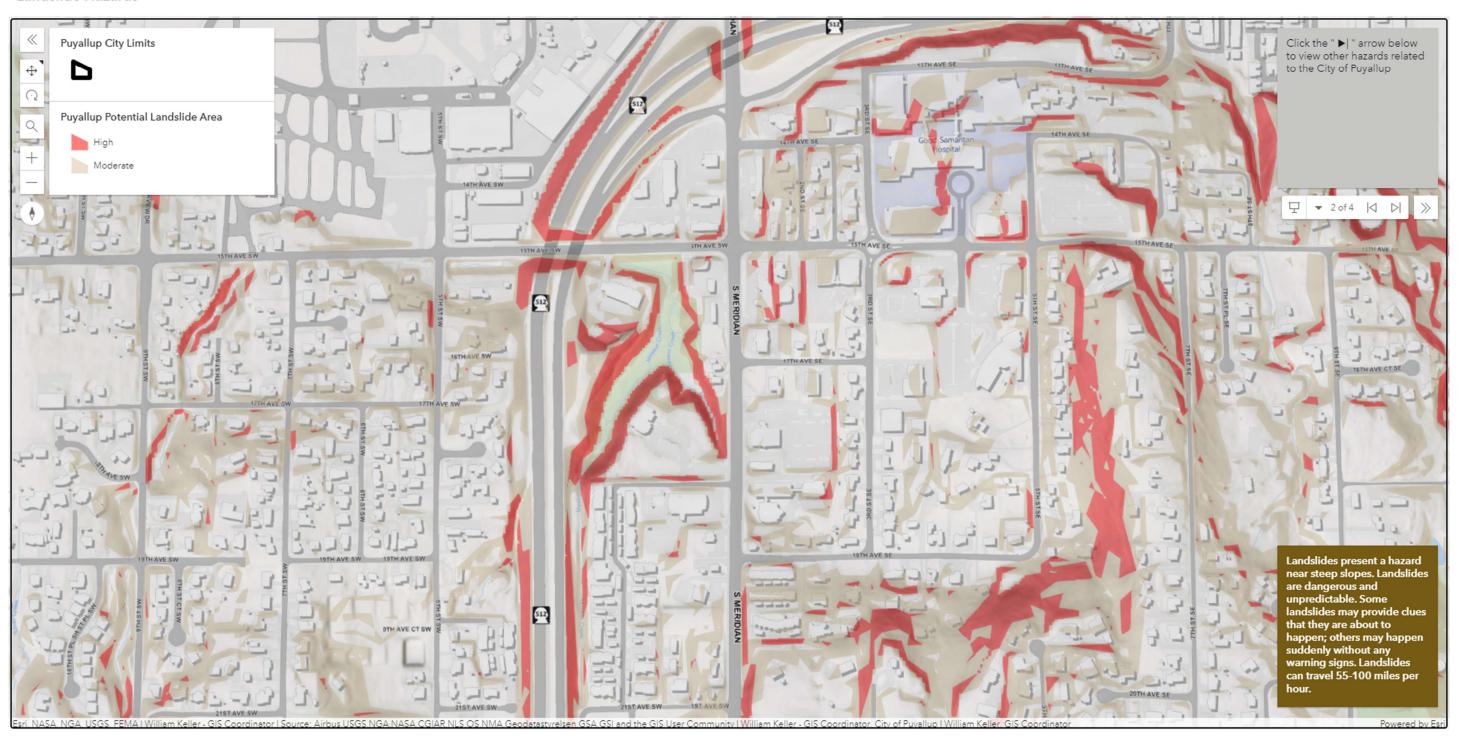


### Lahar Hazards

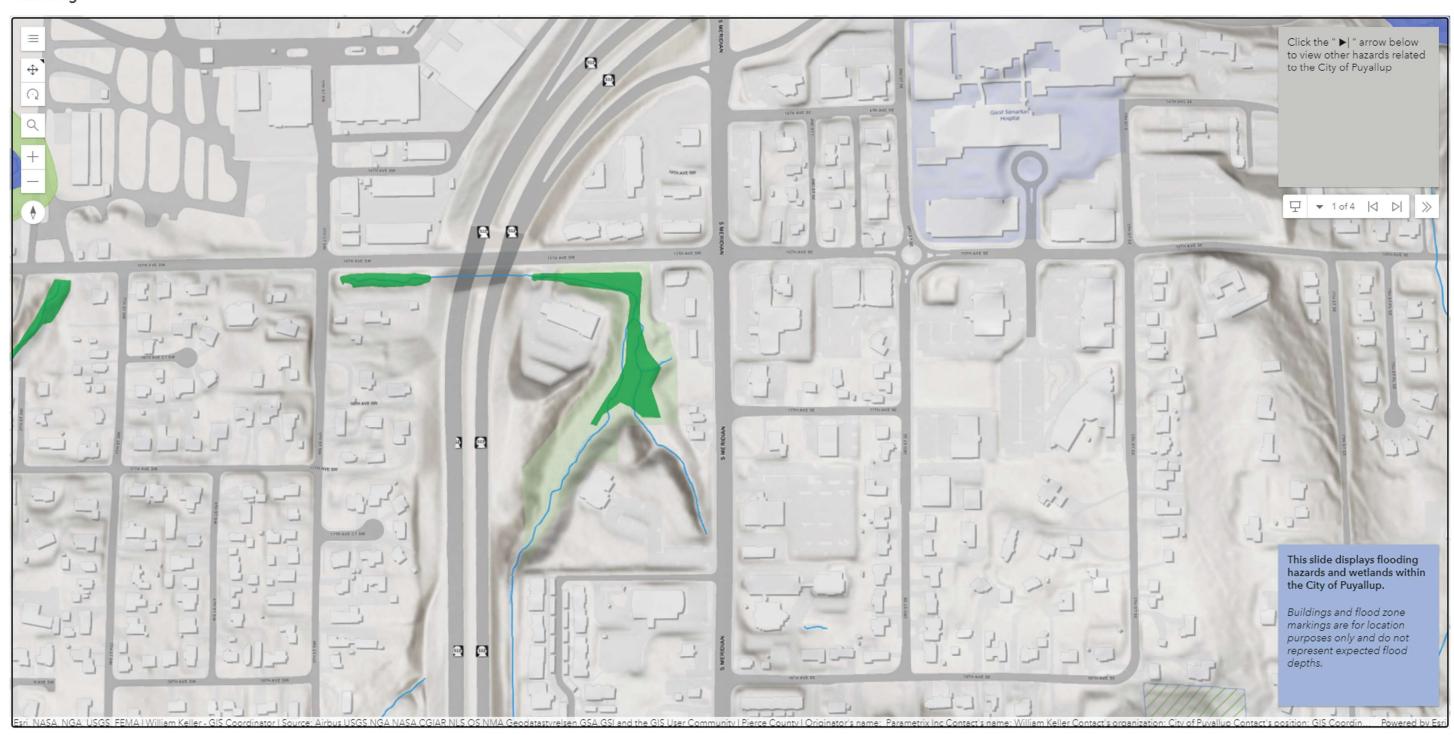




### Landslide Hazards



# Flooding

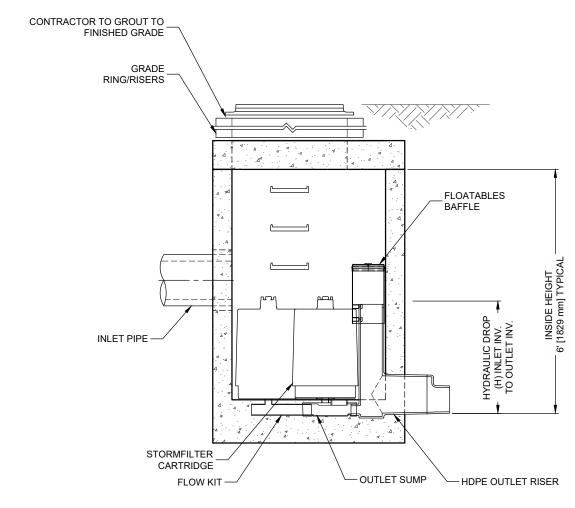




**APPENDIX C: STORMFILTER DETAIL** 

### **PLAN VIEW**

STANDARD OUTLET RISER FLOWKIT: 40A



# **SECTION A-A**



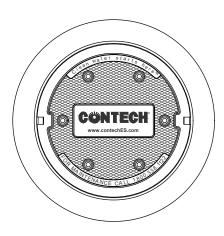
#### STORMFILTER DESIGN NOTES

STORMFILTER TREATMENT CAPACITY IS A FUNCTION OF THE CARTRIDGE SELECTION AND THE NUMBER OF CARTRIDGES. THE STANDARD MANHOLE STYLE IS SHOWN WITH THE MAXIMUM NUMBER OF CARTRIDGES (3). VOLUME SYSTEM IS ALSO AVAILABLE WITH MAXIMUM 3 CARTRIDGES. Ø4 [1219 mm] MANHOLE STORMFILTER PEAK HYDRAULIC CAPACITY IS 1.0 CFS [28.3 L/s]. IF THE SITE CONDITIONS EXCEED 1.0 CFS [28.3 L/s] AN UPSTREAM BYPASS STRUCTURE IS REQUIRED.

#### CARTRIDGE SELECTION

CARTRIDGE HEIGHT	27" [686 mm]			18" [458 mm]			LOW DROP		
RECOMMENDED HYDRAULIC DROP (H)	3.05' [930 mm]			2.3' [700 mm]			1.8' [550 mm]		
SPECIFIC FLOW RATE (gpm/sf) [L/s/m²]	2 [1.30]	1.67* [1.08]	1 [0.65]	2 [1.30]	1.67* [1.08]	1 [0.65]	2 [1.30]	1.67* [1.08]	1 [0.65]
CARTRIDGE FLOW RATE (gpm) [L/s]	22.5 [1.42]	18.79 [1.19]	11.25 [0.71]	15 [0.95]	12.53 [0.79]	7.5 [0.44]	10 [0.63]	8.35 [0.54]	5 [0.32]

<sup>\* 1.67</sup> gpm/sf [1.08 L/s/m²] SPECIFIC FLOW RATE IS APPROVED WITH PHOSPHOSORB® (PSORB) MEDIA ONLY



# FRAME AND COVER

(DIAMETER VARIES) N.T.S.

SITE SPECIFIC DATA REQUIREMENTS					
STRUCTURE ID					*
WATER QUALITY	FLOW RAT	E (	cfs) [L/s]		*
PEAK FLOW RAT	E (cfs) [L/s]				*
RETURN PERIOD	OF PEAK F	LO	W (yrs)		*
CARTRIDGE HEIC	GHT (SEE TA	ABL	E ABOVE)		*
NUMBER OF CAR	TRIDGES F	REC	UIRED		*
CARTRIDGE FLO	W RATE				*
MEDIA TYPE (PE	RLITE, ZPG	, PS	SORB)		*
·					•
PIPE DATA:	I.E.	-	MATERIAL	D	IAMETER
INLET PIPE #1	*		*		*
INLET PIPE #2	*		*		*
OUTLET PIPE	*		*		*
RIM ELEVATION					*
ANTI-FLOTATION	BALLAST		WIDTH		HEIGHT
*					*
NOTES/SPECIAL REQUIREMENTS:					
* PER ENGINEER	OF RECOR	RD			

#### GENERAL NOTES

- CONTECH TO PROVIDE ALL MATERIALS UNLESS NOTED OTHERWISE.
- 2. DIMENSIONS MARKED WITH () ARE REFERENCE DIMENSIONS. ACTUAL DIMENSIONS MAY VARY.
- 3. FOR SITE SPECIFIC DRAWINGS WITH DETAILED VAULT DIMENSIONS AND WEIGHTS, PLEASE CONTACT YOUR CONTECH ENGINEERED SOLUTIONS LLC REPRESENTATIVE. www.ContechES.com
- 4. STORMFILTER WATER QUALITY STRUCTURE SHALL BE IN ACCORDANCE WITH ALL DESIGN DATA AND INFORMATION CONTAINED IN THIS DRAWING.
- 5. STRUCTURE SHALL MEET AASHTO HS-20 LOAD RATING, ASSUMING EARTH COVER OF 0' 5' [1524 mm] AND GROUNDWATER ELEVATION AT, OR BELOW, THE OUTLET PIPE INVERT ELEVATION. ENGINEER OF RECORD TO CONFIRM ACTUAL GROUNDWATER ELEVATION. CASTINGS SHALL MEET AASHTO M306 AND BE CAST WITH THE CONTECH LOGO.
- FILTER CARTRIDGES SHALL BE MEDIA-FILLED, PASSIVE, SIPHON ACTUATED, RADIAL FLOW, AND SELF CLEANING. RADIAL MEDIA DEPTH SHALL BE 7-INCHES [178 mm]. FILTER MEDIA CONTACT TIME SHALL BE AT LEAST 38 SECONDS.
- 7. SPECIFIC FLOW RATE IS EQUAL TO THE FILTER TREATMENT CAPACITY (gpm) [L/s] DIVIDED BY THE FILTER CONTACT SURFACE AREA (sq ft)[m²].
  8. STORMFILTER STRUCTURE SHALL BE PRECAST CONCRETE CONFORMING TO ASTM C-478 AND AASHTO LOAD FACTOR DESIGN METHOD.
- INSTALLATION NOTES
- A. ANY SUB-BASE, BACKFILL DEPTH, AND/OR ANTI-FLOTATION PROVISIONS ARE SITE-SPECIFIC DESIGN CONSIDERATIONS AND SHALL BE SPECIFIED BY ENGINEER OF RECORD.
- B. CONTRACTOR TO PROVIDE EQUIPMENT WITH SUFFICIENT LIFTING AND REACH CAPACITY TO LIFT AND SET THE STORMFILTER STRUCTURE.
- C. CONTRACTOR TO INSTALL JOINT SEALANT BETWEEN ALL STRUCTURE SECTIONS AND ASSEMBLE STRUCTURE.
- D. CONTRACTOR TO PROVIDE, INSTALL, AND GROUT INLET PIPE(S).
- E. CONTRACTOR TO PROVIDE AND INSTALL CONNECTOR TO THE OUTLET RISER STUB. STORMFILTER EQUIPPED WITH A DUAL DIAMETER HDPE OUTLET STUB AND SAND COLLAR. IF OUTLET PIPE IS LARGER THAN 8 INCHES [200 mm], CONTRACTOR TO REMOVE THE 8 INCH [200 mm] OUTLET STUB AT MOLDED-IN CUT LINE. COUPLING BY FERNCO OR EQUAL AND PROVIDED BY CONTRACTOR.
- F. CONTRACTOR TO TAKE APPROPRIATE MEASURES TO PROTECT CARTRIDGES FROM CONSTRUCTION-RELATED EROSION RUNOFF.



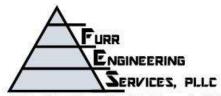
800-338-1122 513-645-7000 513-645-7993 FAX

SFMH48 STORMFILTER STANDARD DETAIL



# **APPENDIX D: PUMP CALCULATIONS**

Pump: Gould's WE Series Model 3885	WE05HH		
Peak Wet Weather Flow (gpm)	53.0		
Force Main size (inches)	0.12		
Peak Wet Weather Flow (cfs)	0.12		between 2 - 8
Peak Velocity (fps)	5.41	okay	fps
receiving MH invert	105.96		
wet well invert	99.73		
static head	6.23		
force main length	87.8		
Minor Losses equivalent length	46.0		
total equivalent length	133.8		
dynamic head	9.100599		
total head	15.3306		
O (400 was at flavorests, 0004) [-f-1	0.0505		
Q <sub>in</sub> (100-year flow rate, 0801) [cfs] T <sub>min</sub> (cycle time between pump starts)	0.0585		
[sec]	390		
n (starts per hour)	8		
c (min. cycle time) [sec]	60		
V <sub>min</sub> (volume of wetwell) [cf]	29.45241		
A (cross-sectional area of wetwell) [sf] 60" type 2	19.63494		
<b>,</b>			
$H_{\text{min}}$ (distance between pumps OFF and lead pump ON) [ft]	3		
$H_{\text{lag}}$ (difference between lag pump ON and lead pump OFF) [ft]	0.5		
$H_{\text{res}}$ (difference between inlet invert elevation and lag pump ON) [ft]	1		



			sum eq
Minor losses	number	eq L ft	L
regular 90 elbow	0	13	0.0
long radius 90 elbow	0	4.6	0.0
regular 45 elbow	1	5.5	5.5
tee, flow through line			
(run)	0	17	0.0
tee, flow through stem	0	21	0.0
180 return bend	0	13	0.0
globe valve	0	110	0.0
gate valve	1	2.5	2.5
angle valve	0	18	0.0
swing check valve	1	38	38.0
coupling or union	0	0.65	0.0
			46.0

pumps off depth (ft) 1.5 pumps off elevation 95.23 lead pump ON elevation 98.23 lag pump ON elevation 98.73 inlet invert elevation 99.73

pump flow rate (gpm)

53.0

wet cell volume 29.45241 cf 220.3193 gal

1 cf = 7.48052



Storm Event	(a) Restricted Flowrate	(b) Pump Drawdown Flowrate	(c) Pump Drawdown Time	(d) Wet well Fill Time	(e) Cycle Time	(f) Avg. Flow Rate at Discharge Point Over Cycle Time
	gpm	gpm	min	min	min	gpm
2 year	3.64	49.36	4.46	60.60	109.97	2.00
5 year	6.33	46.67	4.72	34.81	81.49	2.70
10 year	9.11	43.89	5.02	24.18	68.07	3.24
25 year	14.14	38.86	5.67	15.58	54.45	4.05
50 year	19.34	33.66	6.55	11.39	45.04	4.89
100 year	26.26	26.74	8.24	8.39	35.13	6.27

(g) Pump Flowrate (gpm)	53.0
(h) Wet Well Volume (gal)	220.3

- (a) Restricted Flow Rate: Mitigated (801) flowrates calculated using WWHM converted to gpm
- (b) Pump Drawdown Flow Rate: (g)-(a)
- (c) Pump Drawdown Time: (h)/(b)
- (d) Wet Well Fill Time: (h)/(a)
- (e) Cycle Time: (c)+(d)
- (f) Avg. Flow Rate at Discharge Point Over Cycle Time:  $[(b)^*(c)]/(e)$
- (g) Pump Flow Rate: derived from manufacturer's performance curve based on calculated head
- (h) **Wet Well Volume:**  $V=h\pi r^2 = 29.45 \text{ cf} = 220.32 \text{ gal}$

h= 1.5 ft r= 5ft

flow	flow (cfs)		
frequency (cfs)	501	701	801
2 year	0.0166	0.2323	0.0081
5 year	0.0260	0.3122	0.0141
10 year	0.0311	0.3702	0.0203
25 year	0.0363	0.4497	0.0315
50 year	0.0394	0.5135	0.0431
100 year	0.0419	0.5814	0.0585

1cfs = 448.831175 gpm