Puyallup School District Sparks Stadium Parking Lot Expansion

Preliminary Stormwater Site Plan

Prepared for:

Puyallup School District 323 12th St NW Puyallup, WA 98371

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October 2024

Job Number 19,474



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Plan Preparation

"I hereby state that this Stormwater Site Plan for Sparks Stadium Parking Lot Expansion has been prepared by me or under my supervision and meets the standard of care and expertise which is usual and customary in this community for professional engineers. I understand that the City of Puyallup does not and will not assume liability for the sufficiency, suitability, or performance of the stormwater system prepared by me."



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1 **Project Overview and Conditions Summary**

1.1 Purpose

The purpose of this report is to comply with stormwater requirements detailed in the Washington State Department of Ecology Stormwater Management Manual for Western Washington (herein after referred to as the Manual), in accordance with the City of Puyallup Phase II Municipal Stormwater Permit (NPDES), the City of Puyallup Municipal Code (herein after referred to as PMC) Section 21.10.040, and the City of Puyallup Development Engineering Design Guidelines, Section 200 Documents.

1.2 **Project Overview**

The Puyallup School District (herein after referred to as PSD) proposes to expand the existing parking lot facilities located at District's Sparks Stadium site. Sparks Stadium is located at 601 7th Ave SW, Puyallup, WA 9837, or parcel 0420284126. See the vicinity map included in Appendix A.

The parcel contains the existing Sparks Stadium, two (2) grandstand seating stands, two (2) ticket booths, a storage building and 158 parking stalls. No building improvements are proposed. The project proposes to provide a net increase of 51 stalls so that there will be a total of 209 stalls when the project is complete. To accomplish this, the following stall work is proposed:

158 existing stalls

64 new stalls will be added

11 existing stalls will be removed

5 existing stalls will be converted/removed to 3 ADA stalls added 209 stalls

Of the 64 new stalls, 2 stalls will be electric vehicle (EV) stalls and another 2 will be EV ready. The ADA code requires 7 ADA stalls for the site; the project is providing 8 ADA stalls within the 209 stalls. See site plan included in Appendix B.

The majority of the improvements will occur in the Southwest corner of the site. The two (2) portable buildings that were present at the time of topographic survey work and have since been removed. Parking lot lighting is also proposed. Project landscaping will conform with City of Puyallup Vegetation Management Standards (VMS). The project zoning and comprehensive mapping is PF-Public Facilities.

The project anticipates the following permits: City of Puyallup Conditional Use Permit (CUP,) PLCUP20240081 SEPA City of Puyallup Site Development Permit, TBD Potentially a DOE Construction Stormwater Permit (CSWGP).

1.3 Existing Conditions

The existing project site topography is flat and generally slopes in the southwesterly direction. The surfacing generally consists of grass/landscaping with 2 portable buildings that have been relocated and some existing impervious parking lot pavement.

The existing soils are Puyallup Fine Sandy Loam, according to the National Resource Conservation Service (herein after referred to NRCS) Soil Survey. See Appendix C. These soils are consistent with the silty sand soils found in the Geotechnical Engineer Report, see Appendix D Geotechnical Report. Groundwater monitoring data shows a seasonally high groundwater table within 3' of the surface.

The project site is located in the following Critical Area Zones per City of Puyallup (see Appendix E):

- Aquifer Recharge Area
- Wellhead Protection Area
- Volcanic Hazard Area/Zone
- Seismic Liquefaction Zone.

The site is not located within Flood, Landslide or Wetland critical areas.

1.4 **Proposed Conditions**

The parking lot addition project proposes removal of existing vegetation, including 8 trees and installation of a 64 stall surface parking facility that will increase the net parking lot capacity by 51 stalls. The project proposes pervious pavement surfacing, storm drainage treatment and flow control via pervious pavement. The project proposes to provide electrical lighting, landscaping improvements and offsite alley and driveway improvements.

SPARKS STADIUM PARKING EXP	ANSION				
9/27/2024					
R. HAND					
PRE-DEVELOP MENT AND PROPO	DSED DEVELOPN	IENT AREAS			
		ON	SITE		
	PRE-DEVE		PROPOSED DEVELOPMENT		
DESCRIPTION		AREA (AC)	AREA (SF)	AREA (AC)	
LANDSCAPE/GRASS		0.65	11772		
IMPERVIOUS AC				0.00	
Remove & Replace AC		0.00		0.06	
New AC		0.00			
IMPERVIOUS BUILDING		0.08	-	0.00	
PERVIOUS PAVEMENT		0.00	19429	0.45	
IMPERVIOUS CONCRETE	0	0.00	1410	0.03	
TOTALS	35718	0.82	35718	0.82	
			SITE		
GRAVEL ALLEY	1230	0.03	0	0.00	
CONCRETE DRIVEWAYS,					
WALKS AND AC RESTORATION			2355		
LANDSCAPING/GRASS		0.04	0	0.00	
PERVIOUS PAVEMENT	0	0.00	3000	0.07	
	FORE	0.40	FOFF	0.40	
TOTALS	5355	0.12	5355	0.12	
	44,072		44070		
PROJECT TOTALS	41073	0.94	41073	0.94	

The project surfacing details are summarized below:

2 Discussion of Minimum Requirements

According to the City of Puyallup's adopted DOE Stormwater Manual Flow charts (see Appendix F), all Minimum Requirements, minimum requirements 1-9 are applicable. The minimum requirements apply to the new and replaced hard surfaces and converted vegetation areas. Below is a discussion of the minimum requirements.

2.1 Minimum Requirement #1 – Prepare a Stormwater Site Plan

This Report and accompanying drawings are prepared in accordance with the Manual, Volume 1, Chapter 3, Section 3.4.1

2.2 Minimum Requirement #2 – Construction Stormwater Pollution Prevention

A Construction Stormwater Pollution Prevention Plan (CSWPPP) will be prepared in accordance with DOE Stormwater manual requirements. All elements will be discussed and addressed in a separate report document and submitted at the site development submittal time.

2.3 Minimum Requirement #3 – Source Control for Pollution

The project does not introduce any new source control BMPs. Source Control BMPs that apply to this project shall continue to be practiced in conformance with the Manual Volume II, Chapter 3. Construction BMPs are included in the CSWPPP.

2.4 Minimum Requirement #4 – Preservation of Natural Drainage System and Outfalls

The project proposes to dispose of stormwater through the permeable pavement into the underlying soils and aquifer, whereby preserving the natural drainage system and outfall location.

2.5 Minimum Requirement #5 – On-site Stormwater Management

The project proposal is not flow control exempt. According to the City's adopted DOE Stormwater Manual, the project will comply with MR#5 through list 2 requirements: provide soil amendments in accordance with BMP T5.13 for the landscape areas and the other hard surface areas, such as, removed and replaced imperious asphaltic concrete, new asphaltic concrete, new impervious concrete walks and pervious pavements will be handled with permeable pavement structure. (See Appendix G).

2.6 Minimum Requirement #6 – Runoff Treatment

Runoff treatment will be provided in the compost amended soils located at the permeable pavement subgrade. The Western Washington Hydrology Model (WWHM) will determine if the facility passes or not. The project will comply with MR#6 requirements.

2.7 Minimum Requirement #7 – Flow Control

Flow Control will be provided in the permeable pavement structure through the voids in the underlying base rock materials. The Western Washington Hydrology Model (WWHM) will determine if the facility passes or not. The project complies with WWHM modeling requirements.

2.8 Minimum Requirement #8 – Wetland Protection

There are no wetlands located on or near the project site.

2.9 Minimum Requirement #9 – Operations and Maintenance

An Operations & Maintenance (O&M) Manual will be prepared for the project at the site development permit submittal time.

2.10 Optional Guidance #1 – Financial Liability

The School District is not required to bond the project by state laws.

2.11 Optional Guidance #2 – Off-site Analysis and Mitigation

The project proposes to provide similar pervious pavement for adjacent alley way improvements and impervious concrete and asphalt improvements at the two (2) driveways. The impervious concrete driveway and walkway improvements are essentially replacement of existing impervious facilities.

3 Offsite Analysis Report

The project proposes to provide similar pervious pavement for adjacent alley way improvements and provide impervious concrete and asphalt improvements at the two (2) driveways. A offsite analysis will be provided with the full Stormwater Site Plan Report. For the preliminary Stormwater Site Plan Report, it can be seen without calculation that the pervious pavement concept will work and comply with all Minimum Requirements since the onsite areas comply.

The impervious concrete driveway and walkway improvements are essentially replacement of existing impervious facilities.

4 Permanent Stormwater Control Plan

The project proposes permeable pavement for its permanent stormwater controls. Pervious pavement may be accomplished with traditional pervious concrete pavement or with permeable pavers. Permeable pavement is typically underlain by a small aggregate top course over a larger aggregate base course. The aggregate has void spaces within the rock. The void spaces within the rock provides the flow control. Flow control is determined by WWHM modeling. The proposed facility passes (see Appendix H).

Stormwater treatment is provided by compost amended subgrade or the permeable pavement.

With permeable pavers, the block or pavers are not permeable, but the slits or slots between the blocks is filled with small aggregate. This type of permeable pavement provides maintenance advantages.

The site has a seasonally high groundwater table, to within 3' of the ground surface. The site soils are a silty sand or group B soils. The soils have infiltrations opportunities. In order to create the most feasible option stormwater disposal BMP, permeable pavement is the only option available. Permeable pavement provides opportunities to comply with MR#4 -7. Infiltration ponds, trenches or bioretention facilities are not feasible.

5 Special Reports and Studies

A geotechnical Report is provided in Appendix D.

6 Other Permits

The project anticipates the following permits will be required: City of Puyallup Conditional Use Permit (CUP,) PLCUP20240081 SEPA City of Puyallup Site Development Permit, TBD Potentially a DOE Construction Stormwater Permit (CSWGP).

7 Operations and Maintenance Manual

An O&M Manual will be provided under separate cover. We anticipate that the O&M Manual will include the O&M for the pervious pavement.

8 Declarations of Covenant for Privately Maintained Flow Control and Runoff Treatment BMPs

The School District will provide a facility stormwater maintenance covenant at either the project completion or at permit approval.

9 Declaration of Covenant for Privately Maintained LID BMPs

The School District will provide a facility LID covenant at either the project completion or at permit approval.

Appendices

Appendix A Vicinity Map



Appendix B Site Plan







VICINITY MAP



GENERAL NOTES FOR LIGHTING FIXTURE SCHEDULE 1. PROVIDE BALLASTS TO ACCOMMODATE DUAL LEVEL SWITCHING FOR ALL 3 AND 4 LAMP FIXTURES.

2. SEE DRAWINGS FOR EMERGENCY LIGHTING FIXTURES.

3. FOR LIGHTING CONTROLS WHICH INCLUDE DAYLIGHT, OCCUPANCY SENSORS AND TIME CLOCK CONTROLS, THE ELECTRICAL CONTRACTOR SHALL PROVIDE TESTING OF THE CONTROL DEVICES, COMPONENTS, EQUIPMENT AND SYSTEMS TO MAKE SURE THEY ARE CALIBRATED, ADJUSTED AND OPERATE IN ACCORDANCE WITH DRAWINGS AND SPECIFICATIONS, SEQUENCES OF OPERATION SHALL BE FUNCTIONALLY TESTED IN THE PRESENCE OF THE ENGINEER. A COMPLETE REPORT OF TEST PROCEDURES AND RESULTS SHALL BE PREPARED AND FILED WITH THE OWNER.

LIGHTING FIXTURE SCHEDULE						
SYMBOL	FIXTURE DESCRIPTION	MANUFACTURER/MODEL #	LUMENS	v	w	MOUNTING & REMARKS
AL1	SITE AREA LIGHTING LED WITH HOUSE SIDE SHIELD	MCGRAW-EDISON# GALN-SA1C-840-U-SL4-XX-HSS MCGRAW-EDISON# RSS4A20SXX1X	4922	120/ 277	57	STANDARD FINISH BY ARCHITECT. PROVIDE WITH INTEGRAL SENSOR FOR CONTROL. SEE POLE BASE DETAIL FOR REQUIREMENTS.
AL2	SITE AREA LIGHTING LED	MCGRAW-EDISON# GALN-SA1C-840-U-SL4-XX MCGRAW-EDISON# RSS4A20SXX1X	5856	120/277	57	STANDARD FINISH BY ARCHITECT. PROVIDE WITH INTEGRAL SENSOR FOR CONTROL. SEE POLE BASE DETAIL FOR REQUIREMENTS.
AL3	DUAL HEAD SITE AREA LIGHTING LED	MCGRAW-EDISON# GALN-SA1C-840-U-5WQ-XX-MA1037-XX MCGRAW-EDISON# RSS4A20SXX1X	12522	120/277	114	STANDARD FINISH BY ARCHITECT. PROVIDE WITH INTEGRAL SENSOR FOR CONTROL. SEE POLE BASE DETAIL FOR REQUIREMENTS.



EVENT PARKING LAYOUT DESIGN OPTION 6 - ELECTRICAL



Appendix C NRCS Soils Survey



USDA United States Department of Agriculture

> Natural Resources Conservation Service

A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for Pierce County Area, Washington

Sparks Stadium Parking Lot Addition



November 19, 2021

Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/? cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

Custom Soil Resource Report

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

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identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



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Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
31A	Puyallup fine sandy loam	39.8	100.0%
Totals for Area of Interest		39.8	100.0%

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

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An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An association is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

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Pierce County Area, Washington

31A—Puyallup fine sandy loam

Map Unit Setting

National map unit symbol: 2hq9 Elevation: 0 to 390 feet Mean annual precipitation: 35 to 60 inches Mean annual air temperature: 50 degrees F Frost-free period: 170 to 200 days Farmland classification: Prime farmland if irrigated

Map Unit Composition

Puyallup and similar soils: 85 percent Minor components: 2 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Puyallup

Setting

Landform: Terraces, flood plains Parent material: Alluvium

Typical profile

H1 - 0 to 13 inches: ashy fine sandy loam H2 - 13 to 29 inches: loamy fine sand H3 - 29 to 60 inches: fine sand

Properties and qualities

Slope: 0 to 3 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Capacity of the most limiting layer to transmit water (Ksat): High (1.98 to 5.95 in/hr)
Depth to water table: About 48 to 79 inches
Frequency of flooding: OccasionalNone
Frequency of ponding: None
Available water supply, 0 to 60 inches: Moderate (about 6.6 inches)

Interpretive groups

Land capability classification (irrigated): 3w Land capability classification (nonirrigated): 3w Hydrologic Soil Group: A Ecological site: F002XA008WA - Puget Lowlands Riparian Forest Forage suitability group: Droughty Soils (G002XN402WA) Other vegetative classification: Droughty Soils (G002XN402WA) Hydric soil rating: No

Minor Components

Briscot, undrained

Percent of map unit: 2 percent Landform: Depressions Other vegetative classification: Seasonally Wet Soils (G002XN202WA) Hydric soil rating: Yes

Custom Soil Resource Report

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Appendix D Geotechnical Report



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FAX

February 15, 2022

Sitts & Hill Engineers, Inc. 4815 Center Street Tacoma, WA 98409

Attention: Richard C. Hand, P.E.

Subject: **Geotechnical Engineering Report** Sparks Stadium Parking Lot Expansion 615 7th Ave SW Puyallup, Washington 98371 Parcel No. 0420284126

MGI Project Z0194

Dear Mr. Hand:

Migizi Group, Inc. (MGI) is pleased to submit this report describing the results of our geotechnical evaluation for the proposed Sparks Stadium parking lot expansion at Puyallup High School. We previously prepared an infiltration letter for the Sparks Stadium Grass Practice Field dated December 14, 2016.

This report has been prepared for the exclusive use of Sitts & Hill Engineers, Inc., and their consultants, for specific application to this project, in accordance with generally accepted geotechnical engineering practice.

SITE AND PROJECT DESCRIPTION 1.0

The main campus of the Puyallup High School is located northeast of the intersection of 7th St SW and W Pioneer Ave in downtown Puyallup, Washington, as shown on the enclosed Topographic and Location Map (Figure 1). Adjacent properties to the north and northwest also service the high school, containing a gymnasium, pool, softball/baseball field, portables, and staff and student parking. Sparks Stadium is located south of the high school main campus and serves as the venue for football, soccer and track and field sporting events.

Improvement plans call for the construction of supplemental parking immediately west of the existing stadium parking lot on the south side of the main structure. The proposed improvement area has been under ownership by the Puyallup School District and is occupied by grass fields and

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portable structures. The new parking lot will join the existing parking lot at grade and will also include one or more entrance improvements. If feasible, the supplemental parking area will be constructed utilizing pervious pavement materials.

2.0 EXPLORATORY METHODS

We explored surface and subsurface conditions at the project site on January 4-5, 2022. Our exploration and evaluation program comprised the following elements:

- Surface reconnaissance of the site,
- Two test pit explorations (designated TP-1 & TP-2), advanced on January 5, 2022,
- One auger boring exploration (designated MW-1) with a 20-foot groundwater monitoring well installed, advanced on January 4, 2022,
- One Small-Scale Pilot Infiltration Test (PIT) (designated INF-1), conducted on January 5, 2022,
- Four groundwater monitoring site visits conducted between January 18, 2022 and February 7, 2022, and
- A review of published geologic and seismologic maps and literature.

Table 1 (page 3) summarizes the approximate functional locations and termination depths of our subsurface explorations, and Figure 2 depicts their approximate relative locations. The following sections describe the procedures used for excavation of the test pits and auger borings.

TABLE 1 APPROXIMATE LOCATIONS AND DEPTHS OF EXPLORATIONS			
Exploration	Functional Location	Termination Depth (feet)	
TP-1	West-central portion of the site	10	
TP-2	South-central portion of the site	9.5	
MW-1	North-central portion of the site	21.5	

The specific number and locations of our explorations were selected in relation to the existing site features, under the constraints of surface access, underground utility conflicts, and budget considerations.

It should be realized that the explorations performed and utilized for this evaluation reveal subsurface conditions only at discrete locations across the project site and that actual conditions in other areas could vary. Furthermore, the nature and extent of any such variations would not become evident until additional explorations are performed or until construction activities have begun. If significant variations are observed at that time, we may need to modify our conclusions and recommendations contained in this report to reflect the actual site conditions.

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2.1 Test Pit Procedures

Our exploratory test pits were excavated with a rubber-tracked, mini-excavator operated by an excavation contractor under subcontract to MGI. An engineering geologist from our firm observed the test pit excavations, collected soil samples, and logged the subsurface conditions.

The enclosed test pit logs indicate the vertical sequence of soils and materials encountered in our test pits, based on our field classifications. Where a soil contact was observed to be gradational or undulating, our logs indicate the average contact depth. We estimated the relative density and consistency of the in-situ soils by means of the excavation characteristics and the stability of the test pit sidewalls. Our logs also indicate the approximate depths of any sidewall caving or groundwater seepage observed in the test pits. The soils were classified visually in general accordance with the system described in Figure A-1, which includes a key to the exploration log. Summary logs of our explorations are included as Figures A-2 and A-3.

2.2 Auger Boring Procedures

Our exploratory boring was advanced through the soil with a hollow-stem auger, using a truckmounted drill rig, operated by an independent drilling firm working under subcontract to MGI. An engineering geologist from our firm continuously observed the boring, logged the subsurface conditions, and collected representative soil samples. All samples were stored in watertight containers and later transported to a laboratory for further visual examination and testing. After the borings were completed, the boreholes were backfilled in accordance with state requirements.

Throughout the drilling operation, soil samples were obtained at 2½ to 5-foot depth intervals by means of the Standard Penetration Test (SPT) per American Society for Testing and Materials (ASTM:D-1586), or using a large split-spoon sampler. This testing and sampling procedure consists of driving a standard 2-inch-outside-diameter steel split-spoon sampler 18 inches into the soil with a 140-pound hammer free-falling 30 inches. The number of blows struck during the final 12 inches is recorded on the boring logs. If a total of 50 blows are struck within any 6-inch interval, the driving is stopped, and the blow count is recorded as 50 blows for the actual penetration distance. The resulting blow count values indicate the relative density of granular soils and the relative consistency of cohesive soils.

The enclosed boring log describes the vertical sequence of soils and materials encountered in the boring, based primarily on our field classifications and supported by our subsequent laboratory examination and testing. Where a soil contact was observed to be gradational, our logs indicate the average contact depth. Where a soil type changed between sample intervals, we inferred the contact depth. Our log also graphically indicates the blow count, sample type, sample number, and approximate depth of each soil sample obtained from the borings, as well as any laboratory tests performed on these soil samples. If any groundwater was encountered in a borehole, the approximate groundwater depth is depicted on the boring logs. Groundwater depth estimates are typically based on the moisture content of soil samples, the wetted height on the drilling rods, and the water level measured in the borehole after the auger has been extracted. The soils were classified visually in general accordance with the system described in Figure A-1, which includes a key to our exploration logs. A summary log of our exploration is included as Figure A-4.

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2.3 Infiltration Test Procedures

In-situ field infiltration testing was performed for determination of a Design Infiltration Rate in general accordance with the Small-Scale PIT procedures, as described in V-5.4 of the 2019 Washington State Department of Ecology Stormwater Management Manual for Western Washington, as adopted by the City of Puyallup. The first step of this test procedure was to identify a suitable soil stratum for stormwater retention, and once completed, perform an excavation within this soil group with a minimum surface area of 12 square feet (sf). Once the excavation was completed, a vertical measuring rod marked in half-inch increments was installed towards the center of the test area. Water was then introduced into the test area, being conveyed through a 4-inch corrugated pipe to a splash block at the bottom of the excavation. Once 12 inches of water was developed at the bottom of the excavation, the test surface was saturated prior to testing. After the saturation period was completed, a steady state flow rate was developed in order to maintain 12 inches of head at the bottom of the test surface. This steady state rate was maintained for one hour. After completion of the existing water was allowed. We recorded the falling head rate for one hour, for comparison with the steady state rate.

3.0 SITE CONDITIONS

The following sections present our observations, measurements, findings, and interpretations regarding surface, soil, groundwater, infiltration and seismic conditions, and liquefaction potential.

3.1 Surface Conditions

As previously indicated, the main campus of the Puyallup High School is located northeast of the intersection of 7th St SW and W Pioneer Ave in downtown Puyallup, Washington. Adjacent properties to the north and northwest also service the high school, containing a gymnasium, pool, softball/baseball field, portables, and staff and student parking. Sparks Stadium is located south of the high school main campus and serves as the venue for football, soccer and track and field sporting events. The proposed supplemental parking area is located immediately west of the existing stadium parking lot on the south side of the main structure. This property has been under ownership by the Puyallup School District and is occupied by grass fields and portable structures. The proposed improvement area is elongated lengthwise from east to west, spanning approximately 200 feet along this orientation, and extends upwards of 150 feet from north to south.

Topographically, the project area is relatively level, with minimal grade change being observed over its extent. Vegetation onsite is largely limited to lawn grasses, though a mature growth of cedar and fir trees line the north margin of the improvement area.

No hydrologic features were observed on site, such as seeps, springs, ponds and streams.

3.2 Soil Conditions

We observed subsurface conditions through the advancement of two test pit explorations and one auger boring exploration adjacent to proposed improvements. Soil conditions were relatively consistent, generally comprised of a surface mantle of sod and topsoil, underlain by fine-grained alluvial soils associated with the flood plains of the Puyallup River. Alluvial soils, as encountered

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onsite, ranged in composition from a fine sand with silt to mottled sandy silt. In general, the more fine-grained sandy silt horizon was observed in close proximity to existing grade, extending through a depth of approximately 3 feet. Beneath this depth, alluvial soils were primarily comprised of fine silty sand of intermittent lenses of fine sand with silt. Alluvial soils were encountered in a very loose to medium dense in situ condition, with silty sand alluvial soils being observed through the termination of all of our subsurface explorations; a maximum depth of 21 ½ feet.

In the *Geologic Map of the Tacoma* 1:100,000-scale Quadrangle, Washington, as prepared by the Washington State Department of Natural Resources Division of Geology and Earth Resources (WSDNR) (2015), the entire project area is mapped as containing Qa, or Holocene alluvium, which is described as loose, stratified to massively bedded fluvial silt, sand, and gravel; typically, well rounded and moderately to well sorted; locally includes sandy to silty estuarine deposits. The National Cooperative Soil Survey (NCSS) for Pierce County, classifies all soils onsite as 31A – Puyallup fine sandy loam, which reportedly forms from alluvium and produces landforms such as flood plains and terraces. Our field observations generally correspond with the site classification performed by the WSDNR and the NCSS.



Excerpt from the Geologic Map of the Tacoma 1:100,000-scale Quadrangle, Washington (WSDNR)(2015)

The enclosed exploration logs (Appendix A) provide a detailed description of the soil strata encountered in our subsurface explorations.

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3.3 Groundwater Conditions

We encountered groundwater at a depth of 5½ to 8½ feet at the time of our subsurface explorations between January 4-5, 2022. Subsequent groundwater monitoring of the well was conducted between January 18th through February 7th of 2022; with four measurements being taken. Seasonally high groundwater rose within 2.75 feet below the rim of the well during our January 18th site visit; with subsequent measurements showing groundwater levels gradually descending. Our groundwater measuring regime will continue along a weekly basis through April of 2022, as dictated in governing stormwater design manuals. Seasonally perched groundwater may also be encountered during an extended period of precipitation due to the poor permeability of site soils and as evidenced by soil mottling.

3.4 Infiltration Conditions

As indicated in the *Soil Conditions* section of this report, the project area is underlain by fine-grained alluvial soils associated with the flood plains of the Puyallup River. This material ranged in composition from fine sand with silt to sandy silt and was typically observed in a very loose to medium dense in situ condition; generally becoming more consolidated with depth. Given the high seasonal water table, as outlined in the previous section, large-scale infiltration facilities, such as trenches, dry wells or ponds, are not feasible for this project. However, we believe that existing hydrogeologic conditions can support pervious pavements, as proposed for this project.

On January 5, 2022, an engineering geologist from MGI performed field infiltration testing using the procedures noted at the onset of this report. The field test (INF-1) was performed towards the southwest corner of the site, between test pit explorations TP-1 and TP-2, as indicated in the attached Figure 2. As described in the *Infiltration Test Procedures* section of this report, there are two complementary portions of the Small PIT procedure used to determine a field infiltration rate: the steady-state period and the falling head period. In our experience, the falling head period is generally more conservative and provides a more accurate evaluation of infiltration conditions. The result of the falling head portion of our Small PIT procedure is recorded in Table 2 (below).

TABLE 2						
FALLING HEAD PERIOD TEST RESULTS						
Test Pit Exploration	Depth of Test Surface	Field Infiltration Rate				
Test Fit Exploration	(feet)	(in/hr)				
INF-1	3	1.5				

A design infiltration rate is determined by applying an appropriate correction factor to the measured infiltration rate. As described in the SWMMWW, this total correction factor (CF_T) should be equal to:

$CF_T = CF_v \times CF_t \times CF_m$

Where CF_v accounts for site variability and number of locations tested, CF_t accounts for uncertainty with the test method, and CF_m accounts for siltation and biofouling. The SWMMWW recommends using a value between 0.33 and 1 for CF_v , a value of 0.5 for CF_t , and a value of 0.9 for CF_m . For this evaluation we used a value of 0.75 for CF_v , giving us a $CF_T = 0.3375$. Applying this value to our

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measured infiltration rate, we recommend using a design infiltration rate of **0.5 inches per hour** for pervious pavements constructed using the silty sand alluvial deposits that underlie the project area as the primary infiltrative medium.

3.5 Seismic Conditions

The site is in the Puget Sound basin which has experienced several earthquakes. A detailed description of the regional seismicity is beyond the scope of this report; however, previous regional earthquakes can be split into two general categories: 1.) large earthquakes with a moment magnitude greater than 8.0 (Mw > 8.0), and 2.) modest size earthquakes with a moment magnitude generally less than 7.25 (Mw < 7.25). In all cases, the thickness of the soil between the bedrock and the ground surface can change (usually amplify) the seismically induced ground motions and therefore the inertial loads acting on surface structures.

"Site Class" is a classification system used by the IBC and ASCE 7 to provide some insight to the potential for ground motion amplification. The site class is based on the properties of the upper 100 feet of the soil and rock materials at the site. MGI used a combination of onsite explorations and our review of the geologic mapping of the site to derive a site class for the site. Based on evaluation and the definitions of Site Class as provided in Table 20.3-1 of ASCE 7-16 (as required by the 2018 International Building Code), the soil conditions on this site satisfy the definition of Site Class D. Our evaluation assumes the soil conditions encountered in the bottom of our explorations, and those from nearby properties, is similar to or increasing in density/consistency down to 100 feet below ground surface.

The 2018 IBC considers earthquake shaking having a 2 percent probability of exceedance in 50 years (i.e. a 2475-year return period), as the code-based design requirement. Using the third-party graphical user interface tools made available by the USGS at https://seismicmaps.org, MGI derived the design ground motions to be used for design of the structures. Our evaluation used ASCE 7-16 as the code reference, Risk Category I/II/III, and Site Class D (Default). The results of our evaluation are provided in Table 2 (page 7):

	TABLE 3 SEISMIC DESIGN PARAMETERS					
Parameter	Value	Basis				
Site Class	D	Table 20.3-1 of ASCE 7-16				
Ss	1.274	seismicmaps.org				
Fa	1.2	seismicmaps.org				
Sms	1.528	= F _a · S ₅ , 2018 IBC Eqn. 16-36				
Sds	1.019	= ² / ₃ S _{MS} , 2018 IBC Eqn. 16-38				
S1	0.439	seismicmaps.org				
Fv	1.86 ^{B, C}	2018 IBC				
S _{M1}	0.817 ^{B, C}	= Fv · S1, 2018 IBC Eqn. 16-37				
Parameter	Value	Basis				

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	SD1	0.544 ^{в, с}	= 2/3 S _{M1} , 2018 IBC Eqn. 16-39				
	PGA	0.5g	seismicmaps.org				
	PGAM	0.6g	seismicmaps.org				
	T ₀	c	Not applicable				
	Ts	C	Not applicable				
	TL	6 sec.	seismicmaps.org				
	 Notes: A. Use the value provided unless the simplified design procedure of ASCE 7 Section 12.14 is used. If this occurs, please contact our office for more information. B. Based on Table 1613.2.3(2) of the 2018 IBC – An ASCE 7-16 Chapter 21 analysis has not been 						
C.	performed. More detailed seismic design criteria are available upon request. Please contact MGI's office for more information.						

3.6 Liquefaction Potential

Liquefaction is a sudden increase in pore water pressure and a sudden loss of soil shear strength caused by shear strains, as could result from an earthquake. Research has shown that saturated, loose, fine to medium sands with a fines (silt and clay) content less than about 20 percent are most susceptible to liquefaction. As with all properties situated within the Puyallup River Valley, site soils exhibit a moderate to high risk to liquefy during a large-scale seismic event. Some degree of post construction settlement should be anticipated in the aftermath of a large-scale seismic event.

4.0 CONCLUSIONS AND RECOMMENDATIONS

Improvement plans call for the construction of supplemental parking immediately west of the existing stadium parking lot on the south side of the main structure. The proposed improvement area has been under ownership by the Puyallup School District and is occupied by grass fields and portable structures. The new parking lot will join the existing parking lot at grade and will also include one or more entrance improvements. If feasible, the supplemental parking area will be constructed utilizing pervious pavement materials. We offer these recommendations:

- <u>Feasibility</u>: Based on our field explorations, research and analyses, the proposed parking lot expansion and onsite stormwater retention appears feasible from a geotechnical standpoint.
- <u>Infiltration Conditions</u>: We recommend using a design infiltration rate of 0.5 inches per hour for pervious pavements constructed using the silty sand alluvial deposits which underly the site as the primary infiltrative medium. This material was relatively consistent and continuous through the termination of our explorations, a maximum depth of 21½ feet.

The following sections of this report present our specific geotechnical conclusions and recommendations concerning site preparation, asphalt pavement, pervious pavement, and structural fill. The Washington State Department of Transportation (WSDOT) Standard Specifications and Standard Plans cited herein refer to WSDOT publications M41-10, *Standard Specifications for Road, Bridge, and Municipal Construction,* and M21-01, *Standard Plans for Road, Bridge, and Municipal Construction,* and M21-01, *Standard Plans for Road, Bridge, and Municipal Construction,* and M21-01, *Standard Plans for Road, Bridge, and Municipal Construction,* and M21-01, *Standard Plans for Road, Bridge, and Municipal Construction,* respectively.

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4.1 Site Preparation

Preparation of the project site should involve erosion control, temporary drainage, clearing, stripping, excavations, cutting, subgrade compaction, and filling.

Erosion Control: Before new construction begins, an appropriate erosion control system should be installed. This system should collect and filter all surface water runoff through silt fencing. We anticipate a system of berms and drainage ditches around construction areas will provide an adequate collection system. Silt fencing fabric should meet the requirements of WSDOT Standard Specification 9-33.2 Table 6. In addition, silt fencing should embed a minimum of 6 inches below existing grade. An erosion control system requires occasional observation and maintenance. Specifically, holes in the filter and areas where the filter has shifted above ground surface should be replaced or repaired as soon as they are identified.

<u>Temporary Drainage</u>: We recommend intercepting and diverting any potential sources of surface or near-surface water within the construction zones before stripping begins. Because the selection of an appropriate drainage system will depend on the water quantity, season, weather conditions, construction sequence, and contractor's methods, final decisions regarding drainage systems are best made in the field at the time of construction. Based on our current understanding of the construction plans, surface and subsurface conditions, we anticipate that curbs, berms, or ditches placed around the work areas will adequately intercept surface water runoff.

<u>Clearing and Stripping</u>: After surface and near-surface water sources have been controlled, sod, topsoil, and root-rich soil should be stripped from the site. Our subsurface explorations indicate that the organic horizon can reach thicknesses of up to 4 to 5 inches. Stripping is best performed during a period of dry weather.

<u>Site Excavations</u>: Based on our explorations, we expect that the vast majority of project excavations will encounter loose to medium dense alluvial sand and silt, which can be readily excavated utilizing standard excavation equipment.

<u>Dewatering</u>: Our explorations and groundwater monitoring regime indicates that seasonally high groundwater levels can rise within 3 feet of existing grade. If groundwater is encountered in shallow excavations above the water table, we anticipate that an internal system of ditches, sump holes, and pumps will be adequate to temporarily dewater excavations. For deeper excavations below the water table, expensive dewater equipment, such as well points, will be necessary in order to temporary dewater excavations.

<u>Temporary Cut Slopes</u>: At this time, final designs and construction sequencing have not been completed. To facilitate project planning we provide the following general comments regarding temporary slopes:

 All temporary soil slopes associated with site cutting or excavations should be adequately inclined to prevent sloughing and collapse,

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- Temporary cut slopes in site soils should be no steeper than 1½H:1V, and
- Temporary slopes should conform to Washington Industrial Safety and Health Act (WISHA) regulations.

These general guidelines are necessarily somewhat conservative (steeper temporary slopes may be possible). As the project progresses, temporary grading plans are developed, final site features are better defined, and a contractor is engaged, MGI may modify these general guidelines to allow steeper slopes.

<u>Subgrade Compaction</u>: Exposed subgrades for the foundation of the proposed residences should be compacted to a firm, unyielding state before new concrete or fill soils are placed. Any localized zones of looser granular soils observed within a subgrade should be compacted to a density commensurate with the surrounding soils. In contrast, any organic, soft, or pumping soils observed within a subgrade should be overexcavated and replaced with a suitable structural fill material.

<u>Site Filling</u>: Our conclusions regarding the reuse of onsite soils and our comments regarding wetweather filling are presented subsequently. Regardless of soil type, all fill should be placed and compacted according to our recommendations presented in the *Structural Fill* section of this report. Specifically, building pad fill soil should be compacted to a uniform density of at least 95 percent (based on ASTM:D-1557).

<u>Onsite Soils</u>: We offer the following evaluation of these onsite soils in relation to potential use as structural fill:

- <u>Surficial Organic Soil</u>: Where encountered, surficial organic soils like duff, topsoil, root-rich soil, and organic-rich fill soils are *not* suitable for use as structural fill under any circumstances, due to high organic content. Consequently, this material can be used only for non-structural purposes, such as in landscaping areas.
- <u>Alluvial Soils</u>: This soil unit appears directly below the organic-rich topsoil encountered across the project area. Due to fines contents occasionally exceeding 50 percent, these soils are extremely moisture sensitive and will be difficult, if not impossible, to reuse during wet weather conditions. Reuse is not recommended, and this material should only be used for non-structural purposes, such as in landscaping areas.

<u>Permanent Slopes</u>: All permanent cut slopes and fill slopes should be adequately inclined to reduce long-term raveling, sloughing, and erosion. We generally recommend that no permanent slopes be steeper than 2H:1V. For all soil types, the use of flatter slopes (such as 2½H:1V) would further reduce long-term erosion and facilitate revegetation.

<u>Slope Protection</u>: We recommend that a permanent berm, swale, or curb be constructed along the top edge of all permanent slopes to intercept surface flow. Also, a hardy vegetative groundcover should be established as soon as feasible, to further protect the slopes from runoff water erosion. Alternatively, permanent slopes could be armored with quarry spalls or a geosynthetic erosion mat.

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4.2 Asphalt Pavement

Since asphalt pavements could potentially be used in the new parking areas and entryways, we offer the following comments and recommendations for pavement design and construction.

<u>Subgrade Preparation</u>: All soil subgrades should be thoroughly compacted, then proof-rolled with a loaded dump truck or heavy compactor. Any localized zones of yielding subgrade disclosed during this proof-rolling operation should be over excavated to a maximum depth of 12 inches and replaced with a suitable structural fill material. All structural fill should be compacted according to our recommendations given in the *Structural Fill* section. Specifically, the upper 2 feet of soils underlying pavement section should be compacted to at least 95 percent (based on ASTM D-1557), and all soils below 2 feet should be compacted to at least 90 percent.

<u>Pavement Materials</u>: For the base course, we recommend using imported washed crushed rock, such as "Crushed Surfacing Base Course" per WSDOT Standard Specification 9-03.9(3) but with a fines content of less than 5 percent passing the No. 200 Sieve. Although our explorations do not indicate a need for a pavement subbase, if a subbase course is needed, we recommend using imported, clean, well-graded sand and gravel such as "Ballast" or "Gravel Borrow" per WSDOT Standard Specifications 9-03.9(1) and 9-03.14, respectively.

<u>Conventional Asphalt Sections</u>: A conventional pavement section typically comprises an asphalt concrete pavement over a crushed rock base course. We recommend using the following conventional pavement sections:

Minimum Thickness							
Pavement Course	Automobile Parking Areas	Areas Subject to Truck Loads	High Traffic Driveways				
Asphalt Concrete Pavement	2 inches	3 inches	4 inches				
Crushed Rock Base	4 inches	6 inches	8 inches				
Granular Fill Subbase (if needed)	6 inches	9 inches	12 inches				

<u>Compaction and Observation</u>: All subbase and base course material should be compacted to at least 95 percent of the Modified Proctor maximum dry density (ASTM D-1557), and all asphalt concrete should be compacted to at least 92 percent of the Rice value (ASTM D-2041). We recommend that an MGI representative be retained to observe the compaction of each course before any overlying layer is placed. For the subbase and pavement course, compaction is best observed by means of frequent density testing. For the base course, methodology observations and hand-probing are more appropriate than density testing.

<u>Pavement Life and Maintenance</u>: No asphalt pavement is maintenance-free. The above-described pavement sections present our minimum recommendations for an average level of performance during a 20-year design life; therefore, an average level of maintenance will likely be required.

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Furthermore, a 20-year pavement life typically assumes that an overlay will be placed after about 10 years. Thicker asphalt and/or thicker base and subbase courses would offer better long-term performance but would cost more initially; thinner courses would be more susceptible to "alligator" cracking and other failure modes. As such, pavement design can be considered a compromise between a high initial cost and low maintenance costs versus a low initial cost and higher maintenance costs.

4.3 Pervious Pavement

We understand that pervious pavements will likely be used be used in the new parking areas and entryways. We offer the following comments and recommendations for pavement construction.

<u>Subgrade Preparation</u>: The existing subgrade under all pervious pavements must remain in an uncompacted condition to facilitate water infiltration. Traffic from construction equipment and vehicles should be limited to the extent practical prior to placement of the pavement section.

Any concentrated areas of fines accumulation due to ponding may be removed to a maximum depth of 6 inches. If desired, these areas may be re-leveled using clean sand. Materials meeting the requirements for "Sand Drainage Blanket" in Section 9-03.13(1) of the WSDOT Standard Specifications may be used for this purpose.

We recommend placement of a nonwoven filter fabric such as Mirafi 160N or equal over the prepared subgrade prior to construction of the pervious pavement section.

<u>Construction Observation</u>: We recommend that an MGI representative be retained to observe and document the placement of each course before any overlying layer is placed.

4.4 Structural Fill

The term "structural fill" refers to any material placed under foundations, retaining walls, slab-ongrade floors, sidewalks, pavements, and other structures. Our comments, conclusions, and recommendations concerning structural fill are presented in the following paragraphs.

<u>Materials</u>: Typical structural fill materials include clean sand, gravel, pea gravel, washed rock, crushed rock, well-graded mixtures of sand and gravel (commonly called "gravel borrow" or "pitrun"), and miscellaneous mixtures of silt, sand, and gravel. Recycled asphalt, concrete, and glass, which are derived from pulverizing the parent materials, are also potentially useful as structural fill in certain applications. Soils used for structural fill should not contain any organic matter or debris, nor any individual particles greater than about 6 inches in diameter.

<u>Fill Placement</u>: Clean sand, gravel, crushed rock, soil mixtures, and recycled materials should be placed in horizontal lifts not exceeding 8 inches in loose thickness, and each lift should be thoroughly compacted with a mechanical compactor.

Migizi Group, Inc.

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Sitts & Hill Engineers – Sparks Stadium Parking Lot Expansion, 615 7th Ave SW, Puyallup, WA February 15, 2022 Geotechnical Engineering Report Z0194

<u>Compaction Criteria</u>: Using the Modified Proctor test (ASTM:D-1557) as a standard, we recommend that structural fill used for various onsite applications be compacted to the following minimum densities:

Fill Application	Minimum Compaction
Asphalt pavement base	95 percent
Asphalt pavement subgrade (upper 2 feet)	95 percent
Asphalt pavement subgrade (below 2 feet)	90 percent

<u>Subgrade Observation and Compaction Testing</u>: Regardless of material or location, all structural fill should be placed over firm, unyielding subgrades prepared in accordance with the *Site Preparation* section of this report. The condition of all subgrades should be observed by geotechnical personnel before filling or construction begins. Also, fill soil compaction should be verified by means of in-place density tests performed during fill placement so that adequacy of soil compaction efforts may be evaluated as earthwork progresses.

Soil Moisture Considerations: The suitability of soils used for structural fill depends primarily on their grain-size distribution and moisture content when they are placed. As the "fines" content (that soil fraction passing the U.S. No. 200 Sieve) increases, soils become more sensitive to small changes in moisture content. Soils containing more than about 5 percent fines (by weight) cannot be consistently compacted to a firm, unyielding condition when the moisture content is more than 2 percentage points above or below optimum. For fill placement during wet-weather site work, we recommend using "clean" fill, which refers to soils that have a fines content of 5 percent or less (by weight) based on the soil fraction passing the U.S. No. 4 Sieve.

5.0 RECOMMENDED ADDITIONAL SERVICES

Because the future performance and integrity of the structural elements will depend largely on proper site preparation, drainage, fill placement, and construction procedures, monitoring and testing by experienced geotechnical personnel should be considered an integral part of the construction process. Subsequently, we recommend that MGI be retained to provide the following post-report services:

- Review all construction plans and specifications to verify that our design criteria presented in this report have been properly integrated into the design,
- · Prepare a letter summarizing all review comments (if required),
- Check all completed subgrades for footings and slab-on-grade floors before concrete is poured, in order to verify their bearing capacity, and
- Prepare a post-construction letter summarizing all field observations, inspections, and test
 results (if required).

Migizi Group, Inc.

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6.0 CLOSURE

The conclusions and recommendations presented in this report are based, in part, on the explorations that we observed for this study; therefore, if variations in the subgrade conditions are observed at a later time, we may need to modify this report to reflect those changes. Also, because the future performance and integrity of the project elements depend largely on proper initial site preparation, drainage, and construction procedures, monitoring and testing by experienced geotechnical personnel should be considered an integral part of the construction process. MGI is available to provide geotechnical monitoring of soils throughout construction.

We appreciate the opportunity to be of service on this project. If you have any questions regarding this report or any aspects of the project, please feel free to contact our office.

Respectfully submitted,

MIGIZI GROUP, INC. Wash Br Zachafy I ach L. Logan, L.G. Project Geologist



James E. Brigham, P.E. Senior Principal Engineer

Page 14 of 14







APPENDIX A SOIL CLASSIFICATION CHART AND KEY TO TEST DATA

LOG OF TEST PITS AND AUGER BORINGS

	GRAVELS	CLEAN GRAVELS WITH LITTLE OR	GW	WELL GRADED GRAVELS, GRAVEL-SAND MIXTURES		
	MORE THAN HALF	NO FINES	GP	POORLY GRADED GRAVELS, GRAVEL-SAND MIXTURES		
SOILS) sieve	COARSE FRACTION IS LARGER THAN NO. 4 SIEVE	GRAVELS WITH	GM	SILTY GRAVELS, POORLY GRADED GRAVEL-SAND-SILT MIXTURES		
COARSE GRAINED SOILS More than Half > #200 sieve	NO. 4 SIEVE	OVER 15% FINES	GC	CLAYEY GRAVELS, POORLY GRADED GRAVEL-SAND-CLAY MIXTURES		
than Hal	SANDS	CLEAN SANDS WITH LITTLE	sw	WELL GRADED SANDS, GRAVELLY SANDS		
COAR More t	MORE THAN HALF	OR NO FINES	SP	POORLY GRADED SANDS, GRAVELLY SANDS		
	COARSE FRACTION IS SMALLER THAN NO. 4 SIEVE	SANDS WITH	SM	SILTY SANDS, POORLY GRADED SAND-SILT MIXTURES		
	NO. 4 SIEVE	OVER 15% FINES	sc	CLAYEY SANDS, POORLY GRADED SAND-CLAY MIXTURES		
		ID CLAYS	ML	INORGANIC SILTS AND VERY FINE SANDS, ROCK FLOUR, SILTY OR CLAYEY FINE SANDS, OR CLAYEY SILTS WITH SLIGHT PLASTICITY		
0ILS 0 sieve		LESS THAN 50	CL	INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY, GRAVELLY CLAYS, SANDY CLAYS, SILTY CLAYS, LEAN CLAYS		
NED SC f < #200			OL	ORGANIC CLAYS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY		
FINE GRAINED SOILS More than Half < #200 sieve			MH	INORGANIC SILTS, MICACEOUS OR DIATOMACIOUS FINE SANDY OR SILTY SOILS, ELASTIC SILTS		
More		ID CLAYS REATER THAN 50	сн	INORGANIC CLAYS OF HIGH PLASTICITY, FAT CLAYS		
			ОН	ORGANIC CLAYS OF MEDIUM TO HIGH PLASTICITY, ORGANIC SILTS		
	HIGHLY ORGAI	NIC SOILS	Pt <u>v vv</u>	PEAT AND OTHER HIGHLY ORGANIC SOILS		
×	Modified California		RV	R-Value		
\boxtimes	Split Spoon		SA	Sieve Analysis		
	Pushed Shelby Tube		SW	Swell Test		
	Auger Cuttings		TC	Cyclic Triaxial		
B	Grab Sample		TX	Unconsolidated Undrained Triaxial		
	Sample Attempt with N	lo Recovery	TV	Torvane Shear		
CA	Chemical Analysis		UC	Unconfined Compression		
CN	Consolidation		(1.2)	(Shear Strength, ksf)		
CP	Compaction		WA	Wash Analysis		
DS	Direct Shear		(20)	(with % Passing No. 200 Sieve)		
PM	Permeability		Ā	Water Level at Time of Drilling		
PP	Pocket Penetrometer		Ŧ	Water Level after Drilling(with date measured)		
SOI	L CLASSIFICATI	ON CHART AND) KEY TO	TEST DATA		

LGD A NNNN02 GINT US LAB.GPJ 11/4/05

100	GIZI	B G	OUP (PO Tac	zi Group, li Box 44840 oma, WA 9 phone: 25	8448	-940	0		BORING NUMBER MW-1 PAGE 1 OF 1 Figure A-4
CLI	IEN'	т_5	Sitts	& Hill I	Engineers,	Inc.				PROJECT NAME Sparks Stadium Parking Lot Expansion
					Z0194					PROJECT LOCATION _615 7th Ave SW, Puyallup, WA 98371
DA	TE	STA	RTE	D _1/4	1/22		со	MF	PLETED 1/4/22	GROUND ELEVATION HOLE SIZE _4.25" HSA
										GROUND WATER LEVELS:
DR	ILLI	NG	мет	HOD	D50 Track	Rig				Z AT TIME OF DRILLING 8.50 ft
LO	GGI	ED E	BY _	ZLL			СН	EC	KED BY JEB	AT END OF DRILLING
NO										AFTER DRILLING
o DEPTH		SAMPLE TYPE	NUMBER	RECOVERY (in) (RQD)	BLOW COUNTS (N VALUE)	U.S.C.S.	GRAPHIC 1 OG			MATERIAL DESCRIPTION
							<u></u>	-		
3 LOG.GPJ	-	_				sм				silty sand (loose, moist)
BORIN			SS S-1	12	7-4-3 (7)			T	3.0 (SP-SM) Gray/brown f	fine sand with silt (loose, wet)
Z0194	ť	N	_			SP- SM				
Z0194/		M	SS		0-0-3				5.5	
- ND-	1	<u>N</u>	S-2	6	(3)				(SM) Gray/brown fine	silty sand (very loose, wet)
ORINGS	-					SM				
AND B	1	X	SS 3-3	12	4-5-4 (9)	<u> </u>			8.0 Ţ (SM) Gray fine silty sa	and (loose, wet)
T PITS	ť	<u> </u>	_		.,					
≝10										
ESKT0			SS S-4	12	3-3-4 (7)					
	-		SS 5-5	12	4-4-6 (10)	SM			Grades to medium de	nse
H/TPL		V.	SS S-6	12	3-5-8				21.0	
SLB.	1	/\\`	J-0		(13)	SP-	Ш			fine sand with silt (medium dense, wet)
ENER						0.01	'			Bottom of borehole at 21.5 feet.
OPY OF G										

MIGIZI		PŐ Tac	Box coma	roup, I 44840 , WA 9 ne: 25)	TEST PIT NUMBER TP-1 PAGE 1 OF 1 Figure A-2
CLIER	VT Sitts	& Hill	Engi	neers,	Inc.	PROJECT NAME Sparks Stadium Parking Lot Expansion
						PROJECT LOCATION 615 7th Ave SW, Puyallup, WA 98371
						22 GROUND ELEVATION TEST PIT SIZE
					Paulman	
					er Tracked Mini Excavator	
LOGO	GED BY	ZLL			CHECKED BY _JEE	AT END OF EXCAVATION
NOTE	s					AFTER EXCAVATION
O DEPTH	SAMPLE TYPE NUMBER	U.S.C.S.	GRAPHIC			MATERIAL DESCRIPTION
			<u></u>	0.4	Sod and topsoil	
F -	1	SM	\otimes	1.0	(SM) Brown silty sand w	ith gravel (medium dense, moist) (Fill)
L		/	M	×1.0	(SP-SM) Grav fine sand	with silt (loose, wet) (Alluvium)
4 TEST PITS.0		SP- SM		2.5		
0194/2019		ML		3.5	(ML) Gray/brown mottle	d sandy silt (soft, wet) (Alluvium)
21			H1	3.5	(SM) Gray fine silty san	d (loose, wet) (Alluvium)
		SM				
1/22					Severe caving observed	
- 2/1					rtapiu groundwater seep	bage observed at 6.5 feet
NERAL BH / TP LOGS - FIGURE.GDT -					The depths on the test p considered accurate to (oit logs are based on an average of measurements across the test pit and should be 0.5 foot. Bottom of test pit at 10.0 feet.
COPY OF GEI						

200	GIZI GROU	PO Tac	Box coma	roup, l 44840 , WA 9 ne: 25)	TEST PIT NUMBER TP-2 PAGE 1 OF 1 Figure A-3
CLI	IENT Sit	ts & Hill	Engi	neers,	Inc.	PROJECT NAME Sparks Stadium Parking Lot Expansion
	OJECT N					PROJECT LOCATION 615 7th Ave SW, Puyallup, WA 98371
DA	TE STAR	TED 1/	5/22		COMPLETED 1/5/22	GROUND ELEVATION TEST PIT SIZE
					Paulman	
				_	er Tracked Mini Excavator	
		ZLL			CHECKED BY JEB	
NO	TES		_			AFTER EXCAVATION
O DEPTH	O (ff) SAMPLE TYPE NUMBER	U.S.C.S.	GRAPHIC			MATERIAL DESCRIPTION
			\overline{m}	<u>°</u> 0.3	Sod and topsoil	
F	+	SM		8	(SM) Brown silty sand (loose, m	noist) (Alluvium)
-	-			1.0	(ML) Gray/brown mottled sandy	sit (act wet) (Allwing)
S.GP					(ML) Gray/brown mottled sandy	siit (soft, wet) (Alluvium)
Z0194 TEST PIT	5	ML		3.0		
0194	1		İΠ		(SM) Gray fine silty sand (loose	, wet) (Alluvium)
COPY OF GENERAL BH / TP LOGS - FIGURE.GDT - 2/11/22 1544 - C.USERSUESSICABIZAKOFESK OPTEST PTS AND BORINGS - GINTZ0194/Z0194 Z674 PTS GPU	-	SM		9.5	∑ Source point abage of from 2	to 10 feet
15:46					Severe caving observed from 3 Rapid groundwater seepage ob	
11/22						are based on an average of measurements across the test pit and should be
- 2					considered accurate to 0.5 foot	
GDT						Bottom of test pit at 9.5 feet.
:0PY OF GENERAL BH / TP LOGS - FIGURE						

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17921 Bothell Everett Hwy, Ste 102, Bothell, WA 98012

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PROJECT NAME		PF	ROJECT NO.	FIELD REPORT NO.
Sparks Stadium Parking Lot Expansion			Z0194	1
ADDRESS 615 7 th Ave SW		DA	1/18/22	PAGE 1OF1
CITY OR COUNTY Puyallup	PERM	IT NO. AF	RIVAL TIME	DEPARTURE TIME
CLIENT Sitts & Hill Engineers		PROJECT MANAGER / nes Brigham 2)
GENERAL CONTRACTOR	MIGIZI	FIELD REPRESENTATI	VE / PHONE NO.	
SUBCONTRACTOR	WEATH O'CO			
TYPE OF WORK PERFORMED Monitoring Well Measurements				
EQUIPMENT USED				
	COMMENTS			
Rep onsite to perform monitoring well measure	ment at MW-1. At 10:2	5 am, water le	evels were 2.	76 feet below
rim of well.				
		and the second		
The sector is filled field as a discussed with the sector is a sector of the sector is a s		m		
The contents of this field report were discussed with the contractor		An		
	MG	IZI Gloop, Inc., Field Rep	presentative	
7	7	ha	1	
A preliminary copy of this field report was left on site. All rec nerein are subject to change pending review by the Migizi project		121 Group, Inc., Project M	lanager	
resent are subject to change pending review by the wigizi project				
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PROJECT NAME	and the second se			
Sparks Stadium Parking Lot Expansion		PROJECT NO. Z0194	FIELD REPORT NO.	
ADDRESS 615 7 th Ave SW			DATE 01/25/22	PAGE 1 OF 1
CITY OR COUNTY Puyallup		PERMIT NO.	ARRIVAL TIME 9:30 am	DEPARTURE TIME
CLIENT Sitts & Hill Engineers			NAGER / PHONE NO. 10 am 253-537-9400	
GENERAL CONTRACTOR		MIGIZI FIELD REPRESENTATIVE / PHONE NO. Zach Logan 360-689-5810		
SUBCONTRACTOR		weather O'cast		
TYPE OF WORK PERFORMED Monitoring Well Measurements				
EQUIPMENT USED				
	COMMENTS			
Rep onsite to perform monitoring well meas	urement at MW-1. At 9	30 am, wat	er levels were 2.74	feet below
rim of well.				
		_		
				9.475
The contents of this field report were discussed with the cont	ractor's on-site representative.	22	n	
		MrGIZ/Groop, Inc.,	Field Representative	
A preliminary copy of this field report was left on site. A herein are subject to change pending review by the Migizi pro	Il recommendations contained oject manager.	MIGIZI Greep, Inc.,	Project Manager	

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Sparks Stadium Parking Lot Expansion		PROJECT NO. Z0194	FIELD REPORT NO.	
address 615 7 th Ave SW			DATE 02/01/22	PAGE 1 OF 1
CITY OR COUNTY Puyallup		PERMIT NO.	ARRIVAL TIME 9:45 am	DEPARTURE TIME
CLIENT Sitts & Hill Engineers		MIGIZI PROJECT MANAGER / PHONE NO. James Brigham 253-537-9400		
GENERAL CONTRACTOR		MIGIZI FIELD REPRESENTATIVE / PHONE NO. Zach Logan 360-689-5810		
SUBCONTRACTOR		WEATHER O'cast		
TYPE OF WORK PERFORMED Monitoring Well Measurements				
EQUIPMENT USED				
Rep onsite to perform monitoring well mea	COMMENTS	0:45 am wat	or lovele were 2.6	P faat balaw
rim of well.	asciellent at WW-1. At	9.45 am, wat	er levels were 3.00	b leet below
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		MiGIZI Groop, Inc.,	Field Representative	
A preliminary copy of this field report was left on site. herein are subject to change pending review by the Migizi p	All recommendations contained project manager.	MIGIZI Group, Inc.,	Project Manager	
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(425) 398-2300 office • (425) 398-2333 fax

PROJECT NAME			PROJECT NO.	FIELD REPORT NO.
Sparks Stadium Parking Lot Expansion		Z0194	4	
ADDRESS 615 7 th Ave SW			DATE 02/07/22	PAGE 1 OF 1
сіту ок социту Puyallup		PERMIT NO.	ARRIVAL TIME 10:25 am	DEPARTURE TIME
CLIENT Sitts & Hill Engineers		MIGIZI PROJECT MANAGER / PHONE NO. James Brigham 253-537-9400		1
GENERAL CONTRACTOR		MIGIZI FIELD REPRESENTATIVE / PHONE NO. Zach Logan 360-689-5810		
SUBCONTRACTOR	WEATHER O'cast			
TYPE OF WORK PERFORMED Monitoring Well Measurements				
EQUIPMENT USED				
	COMMENTS			
Rep onsite to perform monitoring well meas	surement at MW-1. At	10:25 am, w	ater levels were 4.	27 feet below
rim of well.				
The contents of this field report were discussed with the con	tractor's on-site representative.			
The contents of this field report were discussed with the con	tractor's on-site representative		, Field Representative	
_		MIGIZI Group, Inc	, Field Representative	
The contents of this field report were discussed with the con A preliminary copy of this field report was left on site. A	Il recommendations contained	MIGIZI Group, Inc	n	

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PROJECT NAME Sparks Stadium Parking Lot Expansion		PROJECT NO. Z0194	FIELD REPORT NO.
ADDRESS 615 7 th Ave SW		DATE 02/21/22	PAGE
	PERMIT NO.	ARRIVAL TIME	1 OF 1 DEPARTURE TIME
Puyallup			
CLIENT Sitts & Hill Engineers	MIGIZI PROJECT MANAG	m 253-537-9400	
GENERAL CONTRACTOR	MIGIZI FIELD REPRESEN	TATIVE / PHONE NO.	
	Zach Logan 360-689-5810		
SUBCONTRACTOR	WEATHER O'cast		
TYPE OF WORK PERFORMED Monitoring Well Measurements			
EQUIPMENT USED			
COMMENT			
Rep onsite to perform monitoring well measurement at MW-1	1. At 10:15 am, wate	er levels were 4.7	'3 feet below
rim of well.			
-End-			
		24	
The contents of this field report were discussed with the contractor's on-site represe			
A preliminary copy of this field report was left on site. All recommendations co	MiGizi Group, Inc., Fi	Jon E. J	1
herein are subject to change pending review by the Migizi project manager.	MIGIZI Group, Inc., Pr	roject Manager	
	V		

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Sparks Stadium Parking Lot Expansion		PROJECT NO. Z0194	FIELD REPORT NO.
ADDRESS		DATE	PAGE
615 7 th Ave SW		03/21/22	1 OF 1
CITY OR COUNTY Puyallup	PERMIT NO.	ARRIVAL TIME	DEPARTURE TIME
CLIENT Sitts & Hill Engineers	MIGIZI PROJECT MAN	ager / PHONE NO. am 253-537-9400	•
GENERAL CONTRACTOR	MIGIZI FIELD REPRESENTATIVE / PHONE NO. Zach Logan 360-689-5810		
SUBCONTRACTOR	WEATHER O'cast		
TYPE OF WORK PERFORMED Monitoring Well Measurements			
EQUIPMENT USED			
COMMEN	NTS		
Rep onsite to perform monitoring well measurement at MW-	-1. At 1:30 pm, wat	er levels were 4.6	2 feet below
rim of well.			
-End-	-		
The contents of this field report were discussed with the contractor's on-site repres	sentative.	n	
	\mathcal{C}	Field Representative	n
A preliminary copy of this field report was left on site. All recommendations of herein are subject to change pending review by the Migizi project manager.	MIGIZI Group, Ing	, Project Manager	

Appendix E City of Puyallup Critical Areas 1.







2. Wellhead Protection

Drinking Water



Flood FEMA map 3.

National Flood Hazard Layer FIRMette **FEMA** Legend SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT SPARKS STADIUM SITE 01 **7TH AVENUE SW** ARCEL: 0420284126 CONALARD AR OF MINIMAL 20N R4E

Ø 3C0341F 3/7/2017 A4E S33 1:6,000 0 250 500 1,000 1,500 2,000

Basemap Imagery Source: USGS National Map 2023

Without Base Flood Elevation (BFE) With BFE or Depth Zone AE, AO, AH, VE, AR SPECIAL FLOOD HAZARD AREAS Regulatory Floodway 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile *Zone X* Future Conditions 1% Annual Chance Flood Hazard Zone X Area with Reduced Flood Risk due to Levee. See Notes. Zone X OTHER AREAS OF FLOOD HAZARD Area with Flood Risk due to Levee Zone D NO SCREEN Area of Minimal Flood Hazard Zone X Effective LOMRs OTHER AREAS Area of Undetermined Flood Hazard Zone D GENERAL ----- Channel, Culvert, or Storr STRUCTURES IIIII Levee, Dike, or Floodwall - - - - Channel, Culvert, or Storm Sewer B 20.2 Cross Sections with 1% Annual Chance 17.5 Water Surface Elevation East all Transect
 Hards Journal State
 Coastal Transect
 Base Flood Elevation Line (BFE)
 Limit of Study
 Jurisdiction Boundary Gastal Transect Baseline
 Profile Baseline
 Hydrographic Feature -----OTHER FEATURES Digital Data Available No Digital Data Available MAP PANELS Unmapped 0 The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

accuracy saminaria The flood hazardia directly from the authoritative NFHL web services provided by FEMA. This map was exported on \$1/10244 at 61.0PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

4. Lakes, Streams and Wetlands

NATURAL ENVIRONMENT









PUYALLUP COMPREHENSIVE PLAN

PAGE 2.15

5. Landslide Hazards

NATURAL ENVIRONMENT







PUYALLUP COMPREHENSIVE PLAN

PAGE 2.9

6. Seismic Hazards

NATURAL ENVIRONMENT



Map 2-2: Seismic Hazards Areas



PUYALLUP COMPREHENSIVE PLAN

PAGE 2.8

7. Volcanic Hazard Areas



63

Zoning Map 8.

TRANSPORTATION ELEMENT



Map 7-1: Zoning Map IZZNA AV R (16) an 48Th St ź Valley Valley Ave Main St 5 anc Stewart Ave AL Pionee E P PROJECT SITE 601 7th Ave SW 84Th S in 23Rd 96Th St 512 Rd 104Th St 112Th St 112 (162) **OP** - Professional Office RM-10 - Medium Density Multiple-Family Residential CB - Community Business RM-20 - High Density Multiple-Family Residential CBD - Central Business District RM-CORE - Downtown-Oriented High Density Multiple-Family Residential CBD-CORE - Central Business District Core KS-04 - High Urban Density Single-Family Residential RS-06 - Urban Density Single-Family CG - General Commercial **Zoning Map** CL - Limited Commercial RS-08 - Medium Density Single-Family RMX - River Road Mixed Use RS-10 - Low Urban Density Single-Family Residential RS-35 - Very Low Density Single-Family Residential CMX - Shaw-Pioneer Community Mixed Use ML - Limited Manufacturing MP - Business Park MED - Medical PDC - Planned Comm unity Development FAIR - Fair PuyallupMOVES PDR - Planned Residential Development ARO - Agriculture, Recreation and Open Space City Limits () PUYALLUP COMPREHENSIVE PLAN

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Appendix F Flow Charts for Determining Minimum Requirements



Figure I-3.1: Flow Chart for Determining Requirements for New Development

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Figure I-3.2: Flow Chart for Determining Requirements for Redevelopment

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Appendix G MR#5 Flow Charts

Options		
Use the LID BMPs from List #2 for all sur- faces within each type of surface in List #2; or		
Use any Flow Control BMPs desired to achieve the LID Performance Standard, and apply <u>BMP T5.13: Post-Construction</u> <u>Soil Quality and Depth.</u>		
r Use any Flow Control BMPs desired to achieve the LID Performance Standard, and apply <u>BMP</u> <u>T5.13: Post-Construction Soil Quality and Depth</u> .		

Flow Control Exempt Projects

Projects qualifying as Flow Control exempt in accordance with the <u>TDA Exemption</u> in <u>I-3.4.7</u> <u>MR7: Flow Control</u> shall either:

• Use the LID BMPs from List #3 for all surfaces within each type of surface in List #3;

or

 Use any Flow Control BMP(s) desired to achieve the LID Performance Standard, and apply BMP T5.13: Post-Construction Soil Quality and Depth.

If the project has multiple TDAs, all TDAs must be Flow Control exempt per the <u>TDA Exemption</u> in <u>I-3.4.7 MR7: Flow Control</u> for the project to use the options listed here.



The text in this box originates from one or more of the following Permits: Appendix 1 of the Phase I / Phase II Municipal Stormwater Permits Construction Stormwater General Permit

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Figure I-3.3: Flow Chart for Determining MR #5 Requirements

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Compliance Methods

LID Performance Standard

The LID Performance Standard compliance method for Minimum Requirement #5 requires modeling the proposed Flow Control BMPs to demonstrate the flow reduction as described below. Note that in order to meet the LID Performance Standard, the chosen Flow Control BMPs will most likely need to include infiltration.

Stormwater discharges shall match developed discharge durations to pre-developed durations for the range of pre-developed discharge rates from 8% of the 2-year peak flow to 50% of the 2-year peak flow. Refer to the <u>Flow Control Performance Standard</u> section in <u>I-3.4.7 MR7: Flow</u> <u>Control for information about the assignment of the pre-developed condition. Project sites that</u> must also meet <u>I-3.4.7 MR7: Flow Control</u> must match flow durations between 8% of the 2-year flow through the full 50-year flow.

Designers selecting this option cannot use <u>BMP T5.14</u>: <u>Rain Gardens</u> to achieve the LID Performance Standard. They may choose to use <u>BMP T7.30</u>: <u>Bioretention</u> to achieve the LID Performance Standard.



The text in this box originates from one or more of the following Permits: Appendix 1 of the Phase I / Phase II Municipal Stormwater Permits Construction Stormwater General Permit

The List Approach

The List Approach compliance method for Minimum Requirement #5 requires evaluating the BMPs in Table I-3.2: The List Approach for MR5 Compliance.

For each surface, evaluate the feasibility of the BMPs in the order listed, and use the first BMP that is considered feasible. The designer must document the site conditions and infeasibility criteria used to deem BMPs infeasible. Once a BMP is deemed feasible and used for a surface, no other BMP from the list is necessary for that surface.

If all BMPs in the list are infeasible, then the designer must document the site conditions and infeasibility criteria used to deem each BMP infeasible. This documentation will demonstrate compliance with Minimum Requirement #5.

Feasibility shall be determined by evaluation against:

- Design criteria, limitations, and infeasibility criteria identified for each BMP in this manual; and
- · Competing Needs Criteria as listed below.



The text in this box originates from one or more of the following Permits: Appendix 1 of the Phase I / Phase II Municipal Stormwater Permits Construction Stormwater General Permit

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Table I-3.2: The List Approach for MR5 Compliance				
List #1	List #2	List #3		
(For MR #1 - #5 Projects That Are Not Flow Control Exempt)	(For MR #1 - #9 Projects That Are Not Flow Control Exempt)	(For Flow Control Exempt Pro- jects)		
Surfa	Surface Type: Lawn and Landscaped Areas			
BMP T5.13: Post-Construction	BMP T5.13: Post-Construction	BMP T5.13: Post-Construction		
Soil Quality and Depth	Soil Quality and Depth	Soil Quality and Depth		
	Surface Type: Roofs			
1. <u>BMP T5.30: Full Dis-</u> persion or <u>BMP T5.10A: Downspout</u> Full Infiltration	1. <u>BMP T5.30: Full Dispersion</u> or <u>BMP T5.10A: Downspout</u> Full Infiltration	1. <u>BMP T5.10A: Downspout</u> <u>Full Infiltration</u>		
2. <u>BMP T5.14: Rain Gardens</u> or <u>BMP T7.30: Bioretention</u>	2. BMP TT.30. Bioretention	2. <u>BMP T5.10B: Downspout</u> <u>Dispersion Systems</u>		
3. <u>BMP T5.10B: Downspout</u> <u>Dispersion Systems</u>	3. BMP T5.10B: Downspout Dispersion Systems	3. <u>BMP T5.10C: Perforated</u> Stub-out Connections		
4. <u>BMP T5.10C: Perforated</u> <u>Stub-out Connections</u>	4. <u>BMP T5.10C: Perforated</u> <u>Stub-out Connections</u>	Stub-out Connections		
:	Surface Type: Other Hard Surface	s		
1. BMP T5.30: Full Dis- persion	1. BMP T5.30: Full Dis- persion			
 2. <u>BMP T5.15: Permeable</u> <u>Pavements</u> or <u>BMP T5.14: Rain Gardens</u> or <u>BMP T7.30: Bioretention</u> 3. <u>BMP T5.12: Sheet Flow</u> <u>Dispersion</u> or <u>BMP T5.11: Concentrated</u> <u>Flow Dispersion</u> 	2. <u>BMP T5.15: Permeable</u> <u>Pavements</u> 3. <u>BMP T7.30: Bioretention</u> 4. <u>BMP T5.12: Sheet Flow</u> <u>Dispersion</u> or <u>BMP T5.11: Concentrated</u> <u>Flow Dispersion</u>	BMP T5.12: Sheet Flow Dis- persion or BMP T5.11: Concentrated Flow Dispersion		
Notes for using the List Approach:		1		

1. Size <u>BMP T5.14: Rain Gardens</u> and <u>BMP T7.30: Bioretention</u> used in the List Approach to have a minimum horizontal projected surface area below the overflow which is at least 5% of the area drain-

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Table I-3.2: The List	Approach for MR5 Con	npliance (continued)

	List #1	List #2	List #3	
	r MR #1 - #5 Projects That Not Flow Control Exempt)	(For MR #1 - #9 Projects That Are Not Flow Control Exempt)	(For Flow Control Exempt Pro- jects)	
	ing to it.			
2	 When the designer encounters <u>BMP T5.15: Permeable Pavements</u> in the List Approach, it is not a requirement to pave these surfaces. Where pavement is proposed, it must be permeable to the extent feasible unless <u>BMP T5.30: Full Dispersion</u> is employed. 			

Objective

The objective of On-Site Stormwater Management is to use practices distributed across a development that reduce the amount of disruption of the natural hydrologic characteristics of the site.

Competing Needs Criteria

LID BMPs can be superseded or restricted where they are in conflict with:

- Requirements of the following federal or state laws, rules, and standards:
 - Historic Preservation Laws and Archaeology Laws as listed at <u>https://dah-p.wa.gov/project-review/preservation-laws</u>,
 - Federal Superfund or Washington State Model Toxics Control Act,
 - · Federal Aviation Administration requirements for airports,
 - Americans with Disabilities Act.
- When an LID requirement has been found to be in conflict with special zoning district design criteria adopted and being implemented pursuant to a community planning process. The existing local codes may supersede or reduce the LID requirement.
- Public health and safety standards (e.g. active zone of a skate park, bike park, or sport court where permeable pavement violates safety standards).
- Transportation regulations to maintain the option for future expansion or multi-modal use of public rights-of-way.
- A local Critical Area Ordinance that provides protection of tree species.
- A local code or rule adopted as part of a Wellhead Protection Program established under the Federal Safe Drinking Water Act; or adopted to protect a Critical Aquifer Recharge Area established under the State Growth Management Act.

Supplemental Guidelines

In order to meet the LID Performance Standard, designers may use any Flow Control BMP in the SWMMWW. There are no specific Flow Control BMPs that must be used to meet the LID Performance Standard.

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Appendix H Permanent Stormwater Control Calculations



General Model Information

WWHM2012 Project Name: prelim calcs				
Site Name:	Sparks Stadium			
Site Address:	601 7th ave sw			
City:	Puyallup			
Report Date:	10/2/2024			
Gage:	42 IN EAST			
Data Start:	10/01/1901			
Data End:	09/30/2059			
Timestep:	15 Minute			
Precip Scale:	1.000			
Version Date:	2024/06/28			
Version:	4.3.1			

POC Thresholds

Low Flow Threshold for POC1: High Flow Threshold for POC1: 50 Percent of the 2 Year

50 Year

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Landuse Basin Data Predeveloped Land Use

Basin 1 Bypass:	No	
GroundWater:	No	
Pervious Land Use C, Lawn, Flat	acre 0.65	
Pervious Total	0.65	
Impervious Land Use ROADS FLAT ROOF TOPS FLAT	acre 0.08 0.08	
Impervious Total	0.16	
Basin Total	0.81	~
Element Flow Componants Surface Inter Componant Flows To: POC 1 POC	flow	Groundwater

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Mitigated Land Use

Basin 1 Landscape Bypass:	No
GroundWater:	No
Pervious Land Use C, Lawn, Flat	acre 0.27
Pervious Total	0.27
Impervious Land Use	acre
Impervious Total	0
Basin Total	0.27

Element Flow Componants: Surface Interflow Groundwater Componant Flows To: Gravel Trench Bed 1 Gravel Trench Bed 1

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Impervious walk

Bypass: No Impervious Land Use acre SIDEWALKS FLAT 0.03 Element Flow Componant: Surface Componant Flows To: Permeable Pavement 2

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Remove & New AC

Bypass: No Impervious Land Use ROADS FLAT 0.07 Element Flow Componant: Surface Componant Flows To: Permeable Pavement 2 POC 1

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Pervious Pavemnent Bypass:

GroundWater: No Pervious Land Use acre C, Pasture, Flat .45 Element Flow Componants: Surface Interflow Groundwater Componant Flows To: Permeable Pavement 2

No

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> Routing Elements Predeveloped Routing

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Mitigated Routing

Permeable Pavement 2 Pavement Area:0.4435 acre.Pavement Length Pavement Width:	139.00 ft.
Pavement thickness: Pour Space of Pavement: Material thickness of second layer: Pour Space of material for second layer: Material thickness of third layer: Pour Space of material for third layer: Infiltration On	Pavement slope 1:0.02 To 1 0.67 0.4 0.33 0.4 0.5 0.4
Infiltration rate: Infiltration safety factor: Total Volume Infiltrated (ac-ft.): Total Volume Through Riser (ac-ft.): Total Volume Through Facility (ac-ft.): Percent Infiltrated: Total Precip Applied to Facility: Total Evap From Facility: Discharge Structure Riser Height: 2.5 ft. Riser Diameter: 1668 in. Notch Type: Rectangular Notch Width: 13.900 ft. Element Outlets: Outlet 1 Outlet 2	0.5 1 281.58 0 281.58 100 0 22.904

Permeable Pavement Hydraulic Table

Stage(feet) 0.0000	Area(ac.) 0.443	Volume(ac-ft.) 0.000	Discharge(cfs) 0.000	Infilt(cfs) 0.000
0.0278	0.443	0.004	0.000	0.223
0.0556	0.443	0.004	0.000	0.223
0.0833	0.443	0.014	0.000	0.223
0.0000	0.443	0.019	0.000	0.223
0.1389	0.443	0.024	0.000	0.223
				• •
0.1667	0.443	0.029	0.000	0.223
0.1944	0.443	0.034	0.000	0.223
0.2222	0.443	0.039	0.000	0.223
0.2500	0.443	0.044	0.000	0.223
0.2778	0.443	0.049	0.000	0.223
0.3056	0.443	0.054	0.000	0.223
0.3333	0.443	0.059	0.000	0.223
0.3611	0.443	0.064	0.000	0.223
0.3889	0.443	0.069	0.000	0.223
0.4167	0.443	0.073	0.000	0.223
0.4444	0.443	0.078	0.000	0.223
0.4722	0.443	0.083	0.000	0.223
0.5000	0.443	0.088	0.000	0.223
				* *
0.3611 0.3889 0.4167 0.4444	0.443 0.443 0.443 0.443	0.064 0.069 0.073 0.078	0.000 0.000 0.000 0.000	0.223 0.223 0.223 0.223

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2.2222	0.443	0.586	28.41	0.223
2.2500	0.443	0.599	30.06	0.223
2.2778	0.443	0.611	31.75	0.223
2.3056	0.443	0.623	33.46	0.223
2.3333	0.443	0.636	35.21	0.223
2.3611	0.443	0.648	36.98	0.223
2.3889	0.443	0.660	38.79	0.223
2.4167	0.443	0.673	40.62	0.223
2.4444	0.443	0.685	42.48	0.223
2.4722	0.443	0.697	44.37	0.223
2.5000	0.443	0.710	46.28	0.223

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Gravel Trench Bed 1 Bottom Length: Bottom Width: Trench bottom slope 1: Trench Left side slope 0: Trench right side slope 2: Material thickness of first layer: Pour Space of material for first layer: Material thickness of second layer: Pour Space of material for second layer: Material thickness of third layer: Pour Space of material for third layer: Infiltration On	108.00 ft. 108.00 ft. 0.001 To 1 0.001 To 1 0.001 To 1 0.67 0.4 0 0 0 0
Infiltration rate:	0.5
Infiltration safety factor:	1
Total Volume Infiltrated (ac-ft.):	198.415
Total Volume Through Riser (ac-ft.): Total Volume Through Facility (ac-ft.):	0 198.415
Percent Infiltrated:	100
Total Precip Applied to Facility:	142.722
Total Evap From Facility:	0
Discharge Structure	•
Riser Height: 0 ft.	
Riser Diameter: 0 in.	>
Element Outlets:	-
Outlet 1 Outlet 2	
Outlet Flows To:	
$\langle \rangle \rangle \langle \rangle$	

Gravel Trench Bed Hydraulic Table

Stage(feet) 0.0000 0.0186 0.0371 0.0557 0.0742 0.0928 0.1113 0.1299 0.1484 0.1670 0.1856 0.2041 0.2227 0.2412 0.2598 0.2783 0.2969 0.3154 0.3340 0.3526 0.3711 0.2027	Area(ac.) 0.267	Volume(ac-ft.) 0.000 0.002 0.004 0.006 0.007 0.009 0.011 0.013 0.015 0.017 0.019 0.021 0.023 0.025 0.027 0.029 0.031 0.033 0.035 0.037 0.039 0.031	0.000 0.000	0.000 0.135 0.
0.3526	0.267	0.037	0.000	0.135

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0.4639 0.4824 0.5010 0.5196 0.5381 0.5567 0.5752 0.5938 0.6123 0.6309 0.6494 0.6680 0.6680 0.6680 0.7051 0.7237 0.7422 0.7608 0.7793 0.7979 0.8164 0.8350 0.8536 0.8721 0.8907 0.9092 0.9278	0.267 0.267	0.049 0.051 0.053 0.055 0.057 0.059 0.061 0.063 0.065 0.067 0.069 0.071 0.076 0.081 0.091 0.091 0.096 0.101 0.096 0.101 0.106 0.111 0.116 0.121 0.126 0.131 0.136 0.141	0.000 0.000	0.135 0
0.9463	0.267	0.146	0.000	0.135
0.9649	0.267	0.151	0.000	0.135
0.9834	0.267	0.156	0.000	0.135
1.0020 1.0206	0.267	0.161 0.166	0.000 0.000 0.000	0.135 0.135
1.0391 1.0577	0.267	0.170 0.175	0.000 0.000	0.135
1.0762	0.267	0.180	0.000	0.135
1.0948	0.267	0.185	0.000	0.135
1.1133	0.267	0.190	0.000	0.135
1.1319	0.267	0.195	0.000	0.135
1.1504	0.267	0.200	0.000	0.135
1.1690	0.267	0.205	0.000	
1.1876	0.267	0.210	0.000	0.135
1.2061	0.267	0.215	0.000	0.135
1.2247	0.267	0.220	0.000	0.135
1.2432	0.267	0.225	0.000	0.135
1.2618	0.267	0.230	0.000	0.135
1.2803	0.267	0.235	0.000	0.135
1.2989	0.267	0.240	0.000	0.135
1.3174	0.267	0.245	0.000	0.135
1.3360	0.267	0.250	0.000	0.135
1.3546	0.267	0.255	0.000	0.135
1.3731	0.267	0.260	0.000	0.135
1.3917	0.267	0.265	0.000	0.135
1.4102	0.267	0.270	0.000	0.135
	0.267	0.275	0.000	0.135
1.4473 1.4659	0.267	0.280 0.285	0.000 0.000	0.135
1.4844	0.267 0.267	0.290	0.000	0.135
1.5030	0.267	0.295	0.000	0.135
1.5216	0.267	0.300	0.000	0.135

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1.5401	0.267	0.305	0.000	0.135
1.5587	0.267	0.310	0.000	0.135
1.5772	0.267	0.315	0.000	0.135
1.5958	0.267	0.320	0.000	0.135
1.6143	0.267	0.325	0.000	0.135
1.6329	0.267	0.329	0.000	0.135
1.6514	0.267	0.334	0.000	0.135

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Ranked Annual	Peaks for Predeve
Rank	Predeveloped M

	папк	Predeveloped	miligaled
	1	0.4139	0.0000
1	2	0.3926	0.0000
;	3	0.3648	0.0000
	4	0.3457	0.0000
	5	0.2805	0.0000
	6	0.2702	0.0000
	7	0.2697	0.0000
1	8	0.2658	0.0000
1	9	0.2452	0.0000
	10	0.2368	0.0000

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11 23 45 67 89 0 12 3 45 67 89 0 12 34 56 7 89 0 12 34 56 7 89 0 12 34 56 7 89 0 12 34 56 7 89 0 12 34 56 7 89 0 12 34 56 7 89 0 12 34 56 7 89 0 12 34 56 7 89 0 12 34 56 7 89 0 12 34 55 55 55 55 55 55 55 55 55 55 55 55 55	0.2331 0.2311 0.2311 0.2311 0.2311 0.2311 0.2311 0.2311 0.2311 0.2311 0.2075 0.1905 0.1880 0.1822 0.1757 0.1728 0.1728 0.1712 0.1610 0.1562 0.1492 0.1435 0.1432 0.1435 0.1432 0.1435 0.1435 0.14336 0.1336 0.1336 0.1336 0.1336 0.1336 0.1336 0.1336 0.1336 0.1336 0.1336 0.1279 0.1274 0.1251 0.1251 0.1251 0.1251 0.1251 0.1251 0.1251 0.1200 0.1175 0.1174 0.1173 0.1132 0.1134 0.1097 0.1097 0.1091 0.1021	0.0000 0.0000
62	0.1071	0.0000
63	0.1031	0.0000

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LID Duration Flows The Facility PASSED

Flow(cfs) 0.0073 0.0077 0.0081 0.0085 0.0089 0.0093 0.0097 0.0100 0.0104 0.0108 0.0112 0.0116 0.0120 0.0124 0.0128 0.0132 0.0135 0.0139 0.0143 0.0147 0.0151 0.0155 0.0159 0.0166 0.0170 0.0174 0.0178 0.0182 0.0182 0.0186 0.0170 0.0174 0.0178 0.0182 0.0186 0.0190 0.0174 0.0194 0.0205 0.0209 0.0213 0.0217 0.0225 0.0229 0.0232 0.0236 0.0244 0.0252 0.0256 0.0260 0.0261 0.0261 0.0261 0.0271	Predev 404037 379051 355728 334066 314232 295729 278610 262654 24752 233957 221326 209027 197669 187088 177171 167698 159055 1508566 143155 135953 129139 122823 116840 111189 105871 100774 91356 87090 82990 79112 75400 71799 68531 65262 62270 59445 56675 53999 51451 49074 46830 44592 36600 34016 32481 310630	Mit 000000000000000000000000000000000000	Percentage 0 0 0 0 0 0 0 0 0 0 0 0 0	Pass/Fail Pass Pass Pass Pass Pass Pass Pass Pas
0.0271	29700	0	0	Pass
0.0275	28493		0	Pass

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0.0423 6510 0 0 Pass 0.0427 6260 0 0 Pass 0.0431 6050 0 0 Pass 0.0434 5850 0 0 Pass 0.0438 5629 0 0 Pass 0.0442 5459 0 0 Pass 0.0442 5459 0 0 Pass 0.0446 5262 0 0 Pass 0.0450 5063 0 0 Pass 0.0454 4905 0 0 Pass 0.0458 4737 0 0 Pass
--

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Duration Flows The Facility PASSED

Flow(cfs) 0.0458 0.0484 0.0510 0.0537 0.0563 0.0589 0.0616 0.0642 0.0695 0.0721 0.0747 0.0747 0.0774 0.0800 0.0826 0.0853 0.0932 0.0958 0.0932 0.0958 0.0932 0.0958 0.0984 0.1011 0.1037 0.1063 0.1090 0.1116 0.1142 0.1169 0.1221 0.1248 0.1274 0.1353 0.1379 0.1406 0.1432 0.1458 0.1435 0.1511 0.1537 0.1563 0.1590 0.1616 0.1642 0.1695 0.1721 0.1748 0.1774 0.1774 0.1800 0.1827	Predev 4737 3753 3021 2522 2125 1825 1563 1363 1040 922 828 737 630 565 500 450 450 450 450 450 450 45		Percentage 0 0 0 0 0 0 0 0 0 0 0 0 0	Pass/Fail Pass Pass Pass Pass Pass Pass Pass Pas
0.1827	49	0	0	Pass

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Water Quality

Water QualityWater Quality BMP Flow and Volume for POC #1On-line facility volume:0 acre-feetOn-line facility target flow:0 cfs.Adjusted for 15 min:0 cfs.Off-line facility target flow:0 cfs.Adjusted for 15 min:0 cfs.

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LID Report

LID Technique	Used for Treatment ?	Total Volume Needs Treatment (ac-ft)	Volume Through Facility (ac-ft)	Infiltration Volume (ac-ft)	Cumulative Volume Infiltration Credit	Percent Volume Infiltrated	Water Quality	Percent Water Quality Treated	Comment
Permeable Pavement 2 POC		256.24				100.00			
Gravel Trench Bed 1 POC		180.56				100.00			
Total Volume Infiltrated		436.80	0.00	0.00		100.00	0.00	0%	No Treat. Credit
Compliance with LID Standard 8% of 2-yr to 50% of 2-yr									Duration Analysis Result = Passed

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POC 2

POC #2 was not reported because POC must exist in both scenarios and both scenarios must have been run.

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Model Default Modifications

Total of 0 changes have been made.

PERLND Changes No PERLND changes have been made.

IMPLND Changes No IMPLND changes have been made.

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> Appendix Predeveloped Schematic



prelim calcs

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Mitigated Schematic



prelim calcs

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Predeveloped UCI File

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prelim calcs

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Mitigated UCI File

RUN GLOBAL WWHM4 model simulation START 1901 10 01 RUN INTERP OUTPUT LEVEL 3 END 2059 09 30 0 0 RUN RESUME UNIT SYSTEM 1 1 END GLOBAL FILES <File> <Un#> <-----File Name---->*** <-ID-> * * * WDM 26 prelim calcs.wdm MESSU 25 27 Mitprelim calcs.MES Mitprelim calcs.L61 28 Mitprelim calcs.L62 30 POCprelim calcs1.dat END FILES OPN SEQUENCE INGRP INDELT 00:15 PERLND 16 IMPLND 20 IMPLND 21 PERLND 40 RCHRES 1 IMPLND 19 RCHRES 2 COPY 1 COPY 501 DISPLY 1 END INGRP END OPN SEQUENCE DISPLY DISPLY-INF01 # - #<-----Title-----1 Gravel Trench Bed 1 ----->***TRAN PIVL DIG1 FIL1 PYR DIG2 FIL2 YRND MAX 1 2 30 END DISPLY-INFO1 END DISPLY COPY TIMESERIES # - # NPT NMN *** 1 1 1 501 1 1 END TIMESERIES END COPY GENER OPCODE # # OPCD *** END OPCODE PARM K *** # # END PARM END GENER PERLND GEN-INFO <PLS ><-----Name---->NBLKS Unit-systems Printer *** # - # User t-series Engl Metr *** _r1e: 27 *** in out 16 C, Lawn, Flat 40 C, Pasture, Flat 1 1 1 1 0 1 1 1 1 27 0 END GEN-INFO *** Section PWATER*** ACTIVITY 16 prelim calcs 10/2/2024 4:53:58 PM

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4.0 0 0 1 0 0 0 0 0 0 0 0 0 END ACTIVITY PRINT-INFO
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 END PWAT-PARM1 PWAT-PARM2 PWATER input info: Part 2 *** <PLS > LZSN INFILT # - # ***FOREST LSUR SLSUR KVARY AGWRC 16 0 40 ° 0.03 0.5 4.5 400 0.05 0.996 0 4.5 0.06 400 0.05 0.5 0.996 END PWAT-PARM2 PWAT-PARM3 PWATER input info: Part 3 <PLS > # - # ***PETMAX PETMIN INFEXE INFILD DEEPFR BASETP AGWETP 16 0 0 2 0 0 ゝ 2 2 40 0 0 0 0 END PWAT-PARM3 PWAT-PARM4 PWATER input info Part 4 CEPSC UZSN NSUR 0.1 0.25 0.25 0.15 0.4 0.3 <PLS > * * * IRC LZETP *** # - # INTFW 0.5 16 0.1 6 0.25 0.15 40 0.5 0.4 6 END PWAT-PARM4 PWAT-STATE1 <PLS > *** Initial conditions at start of simulation ran from 1990 to end of 1992 (pat 1-11-95) RUN 21 *** # *** CEPS SURS UZS # IFWS LZS AGWS GWVS 0 16 0 0 0 2.5 0 1 4.0 0 0 0 0 2.5 1 0 END PWAT-STATE1 END PERLND IMPLND GEN-INFO <PLS ><-----> Unit-systems Printer *** User t-series Engl Metr *** # - # *** in out 27 20 SIDEWALKS/FLAT 1 0 1 1 21 1 27 ROADS/FLAT 1 1 0 19 27 Porous Pavement 1 1 1 0 END GEN-INFO *** Section IWATER*** ACTIVITY # - # ATMP SNOW IWAT SLD IWG IQAL *** 0 20 0 21 0 0 19 1 0 0 0 0 END ACTIVITY PRINT-INFO <ILS > ******** Print-flags ******** PIVL PYR # - # ATMP SNOW IWAT SLD IWG IQAL ******* 0 0 0 4 0 0 0 1 9 20 prelim calcs 10/2/2024 4:53:58 PM

21 0 0 4 0 0 0 1 9 19 0 0 4 0 0 0 1 9 END PRINT-INFO TWAT-PARM1 <PLS > IWATER variable monthly parameter value flags *** # - # CSNO RTOP VRS VNN RTLI *** 0 0 20 0 0 0 21 0 0 0 0 0 19 0 0 0 0 0 END IWAT-PARM1 IWAT-PARM2 IWATER input info: Part 2 LSUR SLSUR NSUR <PLS > # - # *** * * * RETSC LSUR 0.01 400 0.1 20 0.1 21 400 0.1 0.1 19 400 0.01 0.1 0.1 END IWAT-PARM2 IWAT-PARM3 <PLS > IWATE # - # ***PETMAX IWATER input info: Part 3 *** PÊTMIN 2.0 0 0 20 21 19 0 0 0 0 END IWAT-PARM3 IWAT-STATE1 # - # *** RETS SURS SURS 20 0 0 21 0 0 19 0 0 END IWAT-STATE1 END IMPLND SCHEMATIC <-Source-> <--Area--> <-Target-> MBLK *** <Name> # Basin 1 Landscape*** PERLND 16 PERLND 16 <Name> <-factor-> Tbl# * * * # 0.27 RCHRES 2 1 0.27 RCHRES 1 3 Impervious walk*** 0.0676 IMPLND IMPLND 20 19 53 Pervious Pavemnent*** PERLND 40 1.0145 IMPLND 19 54 PERLND 40 1.0145 IMPLND 19 55 Remove & New AC*** IMPLND 21 IMPLND 19 0.1578 IMPLND 19 53 0.4435 RCHRES 2 5 *****Routing***** PERLND 16 0.27 COPY 12 1 PERLND 0.27 COPY 16 1 13 0.03 IMPLND 20 COPY 1 15 COPY IMPLND 21 0.07 1 15 PERLND 40 0.45 COPY 12 1 PERLND 40 0.45 COPY 13 1 2 RCHRES 1 COPY 501 17 RCHRES 1 1 COPY 501 17 END SCHEMATIC NETWORK <-Wolume-> <-Grp> <-Member-><--Mult-->Tran <-Target vols> <-Grp> <-Member-> ***
<Name> # <Name> # #<-factor->strg <Name> # # <Name> # # <Name> # # ***
COPY 501 OUTPUT MEAN 1 1 48.4 DISPLY 1 INPUT TIMSER 1

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<-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Target vols> <-Grp> <-Member-> *** <Name> <Name> # # *** # <Name> # #<-factor->strg <Name> # # END NETWORK RCHRES GEN-INFO Name Nexits Unit Systems Printer *** RCHRES #<----> User T-series Engl Metr LKFG * * * in out 1 Gravel Trench Be-012 2 1 2 Permeable Paveme-010 2 1 *** 0 1 1 1 1 28 1 28 0 1 END GEN-INFO *** Section RCHRES*** ACTIVITY # - # HYFG ADFG CNFG HTFG SDFG GQFG OXFG NUFG PKFG PHFG *** 1 0 END ACTIVITY PRINT-INFO
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 2 END HYDR-PARM1 HYDR-PARM2 LEN DELTH STCOR KS DB50 FTABNO *** # - # <-----><-----><-----><-----> * * * 1 1 0.02 0.0 0.0 0.5 0.03 0.0 0.0 0.5 0 0 2 END HYDR-PARM2 HYDR-TYTT 0.0 END HIDK-FARME HYDR-INIT RCHRES Initial conditions for each HYDR section # - # *** VOL Initial value of COLIND Initial value of OUT *** ac-ft for each possible exit for each possible exit ---> *** <---><---> Initial value of OUTDGT
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END EXT SOURCES EXT TARGETS <-Volume-> <-Grp> <-Member-> <mult>Tran <- <name> # <name> # #<-factor->strg <n RCHRES 2 HYDR RO 1 1 1 WD RCHRES 2 HYDR O 2 1 1 WD RCHRES 2 HYDR O 2 1 1 WD RCHRES 2 HYDR STAGE 1 1 WD COPY 1 OUTPUT MEAN 1 1 48.4 WD COPY 501 OUTPUT MEAN 1 1 48.4 WD RCHRES 1 HYDR RO 1 1 1 WD RCHRES 1 HYDR O 1 1 1 WD RCHRES 1 HYDR O 2 1 1 WD RCHRES 1 HYDR O 2 1 1 WD RCHRES 1 HYDR STAGE 1 HYDR ST</n </name></name></mult>	lame> # <name> tem strg strg*** M 1004 FLOW ENGL REPL M 1005 FLOW ENGL REPL M 1006 FLOW ENGL REPL M 1007 STAG ENGL REPL M 701 FLOW ENGL REPL M 801 FLOW ENGL REPL M 1000 FLOW ENGL REPL M 1001 FLOW ENGL REPL M 1002 FLOW ENGL REPL</name>
-	<pre>'arget> <-Grp> <-Member->*** 4 4:53:58 PM Page 39</pre>

<name> MASS-LINK</name>		#<-factor->	<name></name>		<name> # #***</name>
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prelim calcs

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Predeveloped HSPF Message File

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Mitigated HSPF Message File

ORAL

prelim calcs

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www.clearcreeksolutions.com

prelim calcs

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